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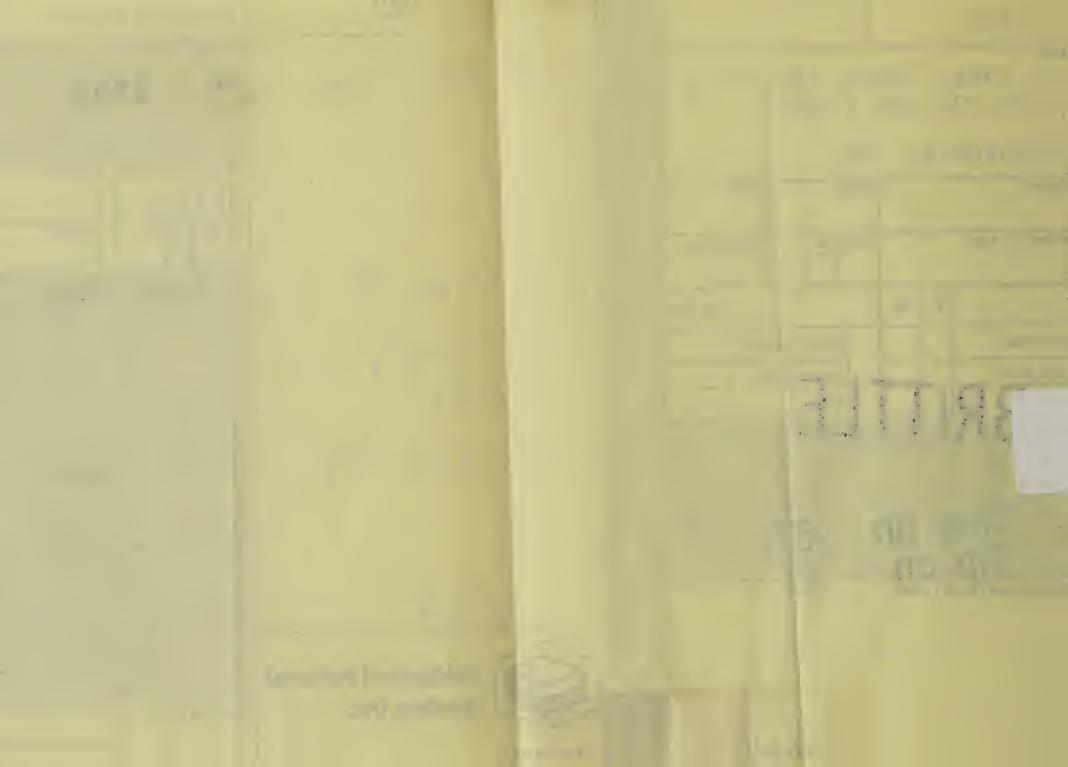




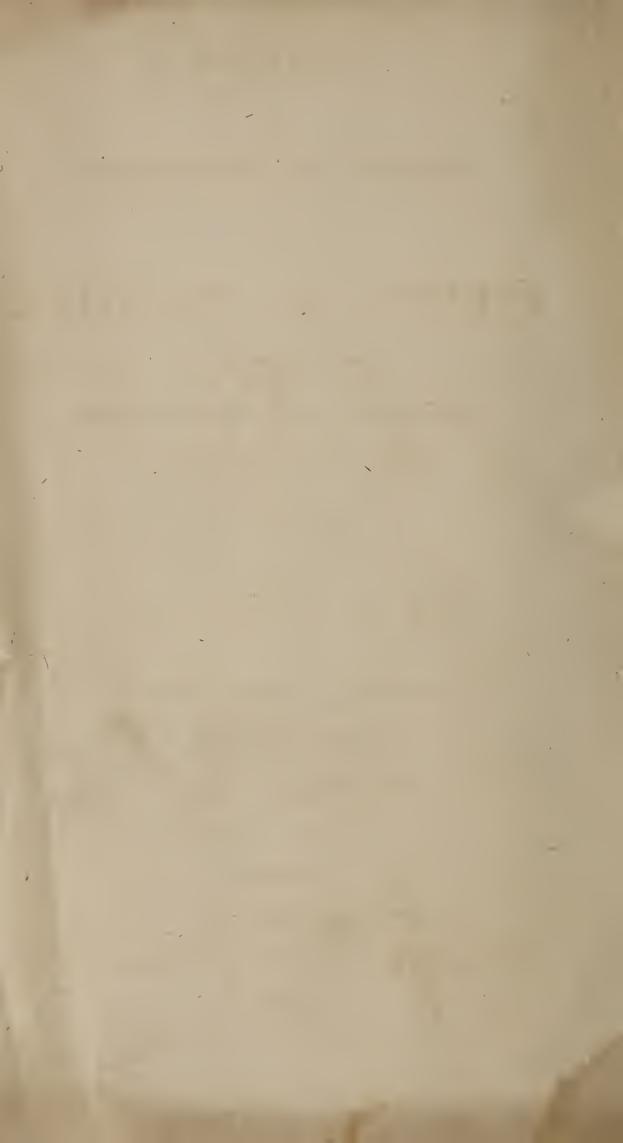




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## GEOMETRY AND TRIGONOMETRY:

WITH A

# TREATISE ON SURVEYING,

IN WHICH THE PRINCIPLES OF

## RECTANGULAR SURVEYING,

WITHOUT PLOTTING,

ARE EXPLAINED.

BY ABEL FLINT, A.M.

STEREOTYPE EDITION, ENLARGED,

WITH ADDITIONAL TABLES.

BY GEORGE GILLET,

SURVEYOR GENERAL OF CONNECTICUT.

HARTFORD:

BELKNAP AND HAMERSLEY.
1839.

Entered,
according to the Act of Congress, in the year 1835, by
Edward P. Cooke,
in the Clerk's Office of the District Court of
Connecticut.

917



THE original compiler of the following work designed, in preparing it, to furnish a plain and concise system of PRACTICAL SURVEYING.

That he did not fail of success, has been proved by the high estimation in which this treatise has been, and is, at the present time, held by Surveyors, and by the continued and increasing demand for it.

In the present edition, practical matter has been added by George Giller, Esq., Surveyor General of the state of Connecticut; and in addition to all the tables of the best treatises extant, it contains the only table of Natural Tangents ever published in this country.

In the table of logarithms, and of logarithmic sines, &c., the decimals are carried to six figures, and a column of differences is added, for the purpose of finding intermediate numbers. The use of these tables is so familiarly explained and illustrated by examples, that no other instruction upon this subject is necessary.

The articles on distributing estates, locating and surveying roads, and on levelling, cannot fail of being highly useful to the practical surveyor.

The work being now used extensively in schools and academies, it has been the chief object of the publishers to render it acceptable as a text book.

The subscribers have examined, in manuscript, the additions to the seventh edition of FLINT'S SURVEYING, by GEORGE GILLET, Esq., Surveyor General of Connecticut, and find them to embrace a system of correct, useful, and practical matter, judiciously arranged, and clearly explained to the understanding of the learner. Having long acted as Surveyors under public authority, we recommend this work, as containing all the elementary science, and requisite tables, necessary or convenient for the learner and the practitioner. The present is a more full and complete system than any former edition.

full and complete system than any former edition.

MOSES WARREN, Dep. Sur. N. London Co.

LEMUEL INGALLS, late Dep. Sur. Windham Co.

DANIEL ST. JOHN, Dep. Sur. Hartford Co.

ASAHEL DEWEY, County Sur., N. London Co.

JONATHAN NICHOLS, Dep. Sur. Windham Co.

Connecticut, August, 1832.

FLINT'S SURVEYING has now been before the public upwards of thirty years. During this period, it has passed through numerous editions, and been enriched, from time to time, by important contributions from the present Surveyor General, George Gillet, Esq. The distinguishing feature of the work, as now published, is its excellent adaptation to the every day wants of the practical surveyor, while it supplies to academies and private students an eminently useful, clear, and well-digested system of elementary instruction, both in the theory and practice of Surveying. I know of no work, in this respect, which equals it.

E. H. BURRITT, Civil Engineer.

New Britain, Con., Nov., 1835.

## GEOMETRY.

GEOMETRY is a science which treats of the properties of magnitude.

### PART I.

### GEOMETRICAL DEFINITIONS.

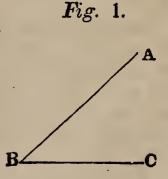
1. A point is a small dot; or, mathematically considered, is that which has no parts, being of itself indivisible.

2. A line has length but no breadth.

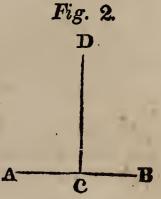
3. A superficies or surface, called also area, has length and breadth, but no thickness.

4. A solid has length, breadth, and thickness.

- 5. A right line is the shortest that can be drawn between two points.
- 6. The inclination of two lines meeting one another, or the opening between them, is called an angle. Thus, at B, Fig. 1, is an angle, formed by the meeting of the lines A B and B C.



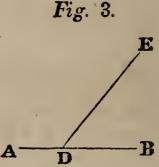
7. If a right line C D, Fig. 2, fall upon another right line A B, so as to incline to neither side, but make the angles on each side equal, then those angles are called right angles; and the line C D is said to be perpendicular to the other line.



8. An obtuse angle is greater than a right angle; as ADE, Fig. 3.

9. An acute angle is less than a right

angle; as EDB, Fig. 3.



Note. When three letters are used to express an angle, the middle letter denotes the angular point.

10. A circle is a round figure bounded by a single line, in every part equally distant from some point, which is called the centre. Fig. 4.

11. The circumference or periphery of a circle is the bounding line; as A DEB,

Fig. 4.

12. The radius of a circle is a line drawn from the centre to the circumference; as CB, Fig. 4. Therefore all radii

of the same circle are equal.

13. The diameter of a circle is a right line drawn from one side of the circumference to the other, passing through the centre; and it divides the circle into two equal parts, called semicircles; as AB or DE, Fig. 5.

14. The circumference of every circle A is supposed to be divided into 360 equal parts, called degrees; and each degree into 60 equal parts, called minutes; and each minute into 60 equal parts, called seconds;

and these into thirds, &c.

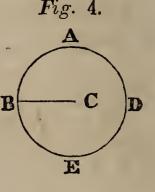
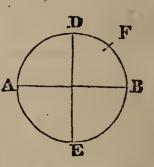


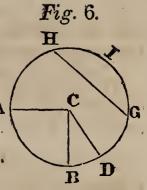
Fig. 5.



Since all circles are divided into the same number of degrees, a degree is not to be accounted a quantity of any determinate length, as so many inches or feet, &c. but is always to be reckoned as being the 360th part of the circumference of any circle, without regarding the size of the circle.

15. An arc of a circle is any part of the circumference; as BF or FD, Fig. 5; and is said to be an arc of as many degrees as it contains 360th parts of the whole circle.

16. A chord is a right line drawn from one end of an arc to another, and is the measure of the arc; as HG is the chord-of A the arc H I G, Fig. 6.



The chord of an arc of 60 degrees is equal in length to the radius of the circle of which the arc is a part.

17. The segment of a circle is a part of a circle cut off by a chord; thus, the space comprehended between the arc HIG and the chord HG is called a segment. Fig. 6.

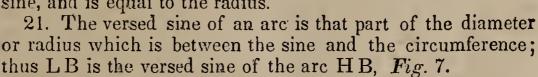
18. A sector of a circle is a space contained between two radii, and an arc less than a semicircle; as BCD, or ACD,

Fig. 6.

19. The sine of an arc is a line drawn from one end of the arc, perpendicular to the radius or diameter drawn through the other end: or, it is half the chord of double the arc; thus, HL is the sine of the arc HB, Fig. 7.

20. The sines on the same diameter increase in length till they come to the cen-A tre, and so become the radius, after which they diminish. Hence it is plain that the sine of 90 degrees is the greatest possible

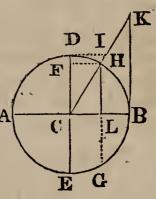
sine, and is equal to the radius.



22. The tangent of an arc is a right line touching the circumference, and drawn perpendicular to the diameter; and is terminated by a line drawn from the centre through the other end of the arc; thus, BK is the tangent of the arc BH, Fig. 7.

The tangent of an arc of 45 degrees is equal in length to the radius of the circle of which the arc is a part.

Fig. 7.



- 23. The secant of an arc is a line drawn from the centre through one end of the arc till it meets the tangent; thus, CK is the secant of the arc BH, Fig. 7.
- 24. The complement of an arc is what the arc wants of 90 degrees, or a quadrant: thus, H D is the complement of the arc B H, Fig. 7.
- 25. The supplement of an arc is what the arc wants of 180 degrees, or a semicircle; thus ADH is the supplement of the arc BH, Fig. 7.
  - Note. It will be seen by reference to Fig. 7, that the sine of any arc is the same as that of its supplement. So, likewise, the tangent and secant of any arc are used also for its supplement.
- 26. The sine, tangent, or secant, of the complement of any arc, is called the co-sine, co-tangent, or co-secant of the arc; thus, F H is the sine, D I the tangent, and C I the secant of the arc D H; or they are the co-sine, co-tangent, and co-secant of the arc B H, Fig. 7.

[The terms sine, tangent, and secant, are abbreviated thus: sin., tan., and sec. So, likewise, co-sine, co-tangent, and co-secant, are written co-sin., co-tan., and co-sec.]

27. The measure of an angle is the arc of a circle contained between the two lines which form the angle, the angular point being the centre; thus, the angle HCB, Fig. 7, is measured by the arc BH; and is said to contain as many degrees as the arc does.

Note. An angle is esteemed greater or less, according to the opening of the lines which form it, or as the arc intercepted by those lines contains more or fewer degrees. Hence it may be observed, that the size of an angle does not depend at all upon the length of the including lines; for all arcs described on the same point, and intercepted by the same right lines, contain exactly the same number of degrees, whether the radius be longer or shorter.

28. The sine, tangent, or secant of an arc, is also the sine, tangent, or secant of the angle whose measure the arc is.

		Fig. 8.	
29. Parallel lines are such as are equal-	A_		_B
ly distant from each other; as AB and CD,			
Fig. 8.	c-		-D

30. A triangle is a figure bounded by

three lines; as A B C, Fig. 9.

31. An equilateral triangle has its three sides equal in length to each other. Fig. 9.

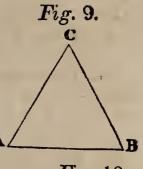


Fig. 10.

32. An isosceles triangle has two of its sides equal. Fig. 10.



Fig. 11.

33. A scalene triangle has three unequal sides. Fig. 11.



Fig. 12.

34. A right angled triangle has one right angle. Fig. 12.

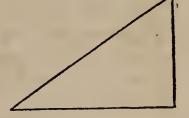
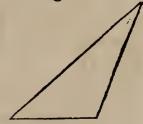


Fig. 13.

35. An obtuse angled triangle has one obtuse angle. Fig. 13.



36. An acute angled triangle has all its angles acute.

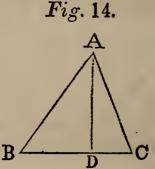
Fig. 9, or 10.

37. Acute and obtuse angled triangles, are called oblique angled triangles, or simply oblique triangles; in which the lower side is generally called the base, and the other two, legs.

38. In a right angled triangle, the longest side is called the hypothenuse, and the other two, legs, or base, and perpen-

dicular.

- Note. The three angles of every triangle being added together will, amount to 180 degrees; consequently the two acute angles of a right angled triangle amount to 90 degrees, the right angle being also 90.
- 39. The perpendicular height of a triangle is a line drawn from one of the angles perpendicular to its opposite side; thus, the dotted line A D, Fig. 14, is the perpendicular height of the triangle A B C.



Note. This perpendicular may be drawn from either of the angles; and whether it falls within the triangle, or on one of the lines continued beyond the triangle, is immaterial.

Fig. 15.

40. A square is a figure bounded by four equal sides, and containing four right angles. Fig. 15.



Fig. 16.

41. A parallelogram, or oblong square, is a figure bounded by four sides, the opposite ones being equal, and the angles right.\* Fig. 16.

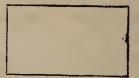
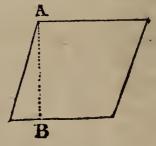


Fig. 17.

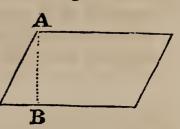
42. A rhombus is a figure bounded by four equal sides, but has its angles oblique. Fig. 17.



\* Any four sided figure, having its opposite sides parallel, is a parallelogram; but, in this book, the *term* is understood as it is here explained. Sometimes this figure is called a rectangle.

Fig. 18.

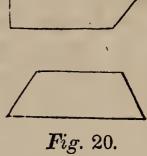
43. A rhomboid is a figure bounded by four sides, the opposite ones being equal, but the angles oblique. Fig. 18.



44. The perpendicular height of a rhombus or rhomboides, is a line drawn from one of the angles to its opposite side; thus, the dotted lines A B, Figs. 17 and 18, represent the perpendicular heights of those figures.

Fig. 19.

45. A trapezoid is a figure bounded by four sides, two of which are parallel, though of unequal lengths. Fig. 19 and Fig. 20.



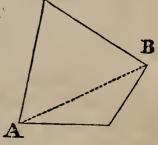
Note. Fig. 19 is sometimes called a right angled trapezium.

Fig. 21.

46. A trapezium is a figure bounded by

four unequal sides. Fig. 21.

47. A diagonal is a line drawn between two opposite angles; as the line A B, Fig. 21.



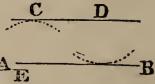
48. Figures which consist of more than four sides are called polygons; if the sides are equal to each other, they are called regular polygons, and are sometimes named from the number of their sides, as pentagon, or hexagon, a figure of five or six sides, &c.; if the sides are unequal, they are called irregular polygons.

### PART II.

#### GEOMETRICAL PROBLEMS.

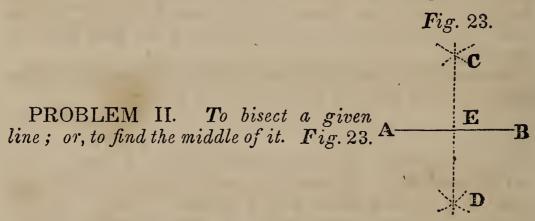
Fig. 22.

PROBLEM I. To draw a line parallel to another line at any given distance; as at the point D, to make a line parallel A to the line A B. Fig. 22.



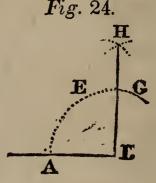
With the dividers take the nearest distance between the point D and the given line A B; with that distance set one foot of the dividers any where on the line A B, as at E, and draw the arc C; through the point D draw a line so as just to touch the top of the arc C.

A more convenient way to draw parallel lines is with a parallel rule. [The parallel rules, however, found in cases of mathematical instruments, are often inaccurate.]



Open the dividers to any convenient distance, more than half the given line A B, and with one foot in A, describe an arc above and below the line, as at C and D; with the same distance, and one foot in B, describe arcs to cross the former; lay a rule from C to D, and where the rule crosses the line, as at E, will be the middle.

PROBLEM III. To erect a perpendisular from the end, or any part of a given line. Fig. 24.



Open the dividers to any convenient distance, as from D to A, and with one foot on the point D, from which the perpendicular is to be erected, describe an arc, as A E G; set off the same distance A D, from A to E, and from E to G; upon E and G describe two arcs to intersect each other at H; draw a line from H to D, and one line will be perpendicular to the other.

Note. There are other methods of erecting a perpendicular, but this is the most simple.

PROBLEM IV. From a given point, as at C, to drop a perpendicular A B on a given line AB, Fig. 25.

With one foot of the dividers in C, describe an arc to cut the given line in two places, as at F and G; upon F and G describe two arcs to intersect each other below the line, as at D; lay a rule from C to D, and draw a line from C to the given line.

Perpendiculars may be more readily raised and let fall, by

a small square made of brass, ivory, or wood.

PROBLEM V. To make an angle at E, A requal to a given angle ABC, Fig. 26.

B

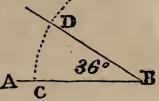
H

E

Open the dividers to any convenient distance, and with one foot in B, describe the arc FG; with the same distance, and one foot in E, describe an arc from H; measure the arc FG, and lay off the same distance on the arc from H to I; draw a line through I to E, and the angles will be equal.

Fig. 27.

PROBLEM VI. To make an acute angle equal to a given number of degrees, suppose 36. Fig. 27.



Draw the line A B of any convenient length; from a scale of chords take 60 degrees with the dividers, and with one foot in B, describe an arc from the line A B; from the same scale take the given number of degrees, 36, and lay it on the arc from C to D; draw a line from B through D, and the angle at B will be an angle of 36 degrees.

Fig. 28.

PROBLEM VII. To make an obtuse E C angle, suppose of 110 degrees. Fig. 28.

Take a chord of 60 degrees as before, and describe an arc greater than a quadrant; set off 90 degrees from B to C, and from C to E set off the excess above 90, which is 20; draw a line from G through E, and the angle will contain 110 degrees.

[It is best, however, in making obtuse angles, to take from the scale the chord of half the angle, and set it off twice.

This will save taking two separate chords.]

Note. In a similar manner angles may be measured; that is, with a chord of 60 degrees describe an arc on the angular point, and on a scale of chords measure the arc intercepted by the lines forming the angle.

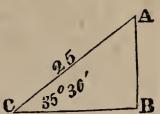
A more convenient method of making and measuring angles, is to use a protractor instead of a scale and dividers.

PROBLEM VIII. To make a triangle L of three given lines, as BO, BL, LO, Fig. 29, any two of which are greater than the third.

Draw the line B L from B to L; from B, with the length of the line B O, describe an arc as at O; from L, with the length of the line L O, describe another arc, to intersect the former; from O draw the lines OB and OL, and BOL will be the triangle required.

Fig. 30.

PROBLEM IX. To make a right angled triangle, the hypothenuse and angles being given. Fig. 30.



Suppose the hypothenuse CA 25 rods or chains, the angle at C 35° 30′, and consequently the angle at A 54° 30′. See note after the 38th Geometrical Definition.

Note. When degrees and minutes are expressed, they are distinguished from each other by a small cipher at the right hand of the degrees, and a dash at the right hand of the minutes; thus, 35° 30′, is 35 degrees and 30 minutes.

Draw the line C B an indefinite length; at C make an angle 35° 30'; through where that number of degrees cuts the arc, draw the line CA 25 rods, which must be taken from some scale of equal parts; drop a perpendicular from A to B, and

the triangle will be completed.

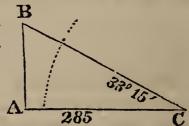
[A scale of equal parts may be found on one side of Gunter's scale, occupying half its length. It will be known by slanting lines which cross it at each end. The length of the scale, not occupied by these oblique lines, is equally divided into several larger divisions, numbered on one side, and likewise twice as many smaller, numbered on the other. In taking distances from the scale, each of these divisions, (either the larger or the smaller, as is most convenient,) must be considered 1, 10, 100, &c. rods, chains, or other dimensions of length. If each division be called 1, it will be easy to take off the required number. But the scale is not usually long enough for this. When each division is called 10, as many divisions must be taken, as there are tens in the given number. For the excess of tens, in this case, the little scale with the oblique lines is used. Each side of this little scale is divided into 10 equal parts, and each of these parts is, of course, 1. Then to take off the hypothenuse, 25, above, we should take in the dividers 2 of the divisions of the large scale, and 5 of those of the small one. There is one of these little scales for the greater, and one for the smaller divisions of the large scale. When each division of the large scale is called 100, each of those of the small one becomes 10, and the units are found by means of the oblique lines. These

are drawn across parallel lines, running the whole length of the scale, from each division on one side, to the next higher on the other. The parallel lines divide the width of the scale into 10 equal parts. Since each oblique line, then, in crossing the scale, passes over one division of length, it is evident that, in passing one tenth across, (that is to the first parallel line,) it will pass over one tenth of a division of length; in passing two tenths across, ( that is, to the second parallel line,) it will pass over two tenths of a division of length, and so on. The parallel lines are numbered at the end of the scale. To take off a distance, containing hundreds, then, as 234, we must place one foot of the dividers on the second division of the larger scale, and on the parallel line marked 4, and extend the other foot to the third oblique line. Decimals may evidently be taken off in a similar manner; the divisions of the larger scale being made units, and those of the smaller, tenths and hundredths.

Note. The length of the two legs may be found by measuring them upon the same scale of equal parts from which the hypothenuse was taken.

Fig. 31.

PROBLEM X. To make a right angled triangle, the angles and one leg being given. Fig. 31.

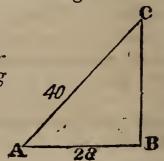


Suppose the angle at C 33° 15′, and the leg A C 285. Draw the leg A C, making it in length 285; at A erect a perpendicular an indefinite length; at C make an angle of 33° 15′; through where that number of degrees cuts the arc, draw a line till it meets the perpendicular at B.

Note. If the given line CA should not be so long as the chord of 60°, it may be continued beyond A, for the purpose of making the angle.

Fig. 32.

PROBLEM XI. To make a right angled triangle, the hypothenuse and one leg being given. Fig. 32.



Suppose the hypothenuse A C 40, and the leg A B 28.

Draw the leg A B in length 28; from B erect a perpendicular an indefinite length; take 40 in the dividers, and setting one foot in A, wherever the other foot strikes the perpendicular will be the point C.

Note. When the triangle is constructed, the angles may be measured by a protractor, or by a scale of chords.

PROBLEM XII. To make a right angled triangle, the two legs being given.

Fig. 33.

C

A

B

Suppose the leg A B 38, and the leg B C 46.

Draw the leg A B in length 38; from B erect a perpendicular to C, in length 46; and draw a line from A to C.

PROBLEM XIII. To make an oblique angled triangle, the angles and one side being given. Fig. 34.

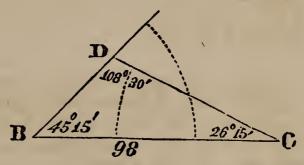


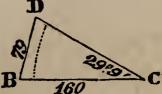
Fig. 34.

Suppose the side B C 98; the angle at B 45° 15′, the angle at D 108° 30′, consequently the other angle 26° 15′.

Draw the side B C in length 98; on the point B make an angle of 45° 15'; on the point C make an angle of 26° 15', and draw the lines B D and C D.

Fig. 35.

PROBLEM XIV. To make an oblique angled triangle, two sides and an angle opposite to one of them being given. Fig. 35.

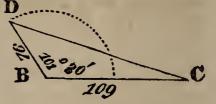


Suppose the side B C 160, the side B D 79, and the angle at C 29° 9'.

Draw the side B C in length 160; at C make an angle of 29° 9', and draw an indefinite line through where the degrees cut the arc; take 79 in the dividers, and with one foot in B lay the other on the line C D; the point D will be the other angle of the triangle.

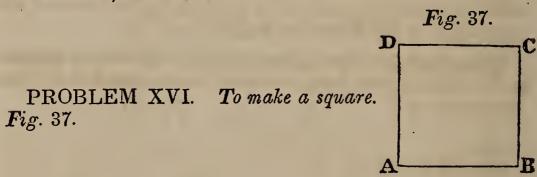
Fig. 36.

PROBLEM XV. To make an Doblique angled triangle, two sides and their contained angle being given. Fig. 36.

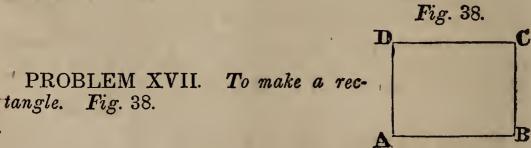


Suppose the side B C 109, the side B D 76, and the angle at B 101° 30′.

Draw the side B C in length 109; at B make an angle of 101° 30′, and draw the side B D in length 76; draw a line from D to C, and it is done.

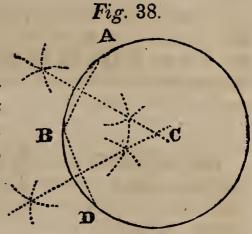


Draw the line A B the length of the proposed square; from B erect a perpendicular to C, and make it of the same length as A B; from A and C, with the same distance in the dividers, describe arcs intersecting each other at D, and draw the lines A D and D C.



Draw the line A B equal to the longest side of the rectangle; on B erect a perpendicular the length of the shortest side to C; from C, with the longest side, and from A, with the shortest side, describe arcs intersecting each other at D, and draw the lines A D and C D.

PROBLEM XVIII. To describe a circle which shall pass through any three given points, not lying in a right line, as A, B, D. Fig. 39.



Draw lines from A to B, and from B to D; bisect those lines by PROBLEM II, and the point where the bisecting lines intersect each other, as at C, will be the centre of the circle.

PROBLEM XIX. To find the centre of a circle.

By the last PROBLEM it is plain, that if three points be any where taken in the given circle's periphery, the centre of the circle may be found as there taught.

Directions for constructing irregular figures of four or more sides, may be found in the following treatise on Surveying.

## TRIGONOMETRY.

TRIGONOMETRY is that part of practical Geometry, by which the sides and angles of triangles are measured; whereby three things being given, either all sides, or sides and angles, a fourth may be found; either by measuring with a scale and dividers, according to the Problems in Geometry, or more accurately by calculation with logarithms, or with natural sines.

TRIGONOMETRY is divided into two parts, rectangular and oblique-angular.

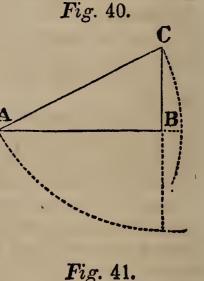
### PART I.

#### RECTANGULAR TRIGONOMETRY.

This is founded on the following methods of applying a circle to a triangle.

PROPOSITION I. In every right angled triangle, as A B C, Fig. 40, it is plain from Fig. 7, compared with the Geometrical definitions to which that Figure refers, that if the hypothenuse A C be made radius, and with it an arc of a circle be described from each end, B C will be the sine of the angle at A, and A B the sine of the angle at C; that is, the legs will be sines of their opposite angles.

PROPOSITION II. If one leg, AB, Fig. 41, be made radius, and with it on the point A an arc be described, then BC, the other leg, will be the tangent, and AC the secant of the angle at A; and if BC be made radius, and an arc be described with it on the point C, then AB will be the tangent, and AC the secant of the angle at C; that is, if one A



C

leg be made radius, the other leg will be a tangent of its opposite angle, and the hypothenuse a secant of the same angle.

Thus, as different sides are made radius, the other sides acquire different names, which are either sines, tangents, or

secants.

As the sides and angles of triangles bear a certain proportion to each other, two sides and one angle, or one side and two angles being given, the other sides or angles may be found by instituting proportions, according to the following rules.

RULE I. To find a side, either of the sides may be made radius, then institute the following proportion:

As THE NAME OF THE SIDE GIVEN, (which will be either

radius, sine, tangent, or secant;)

Is to the length of the side given;

So is the name of the side required, (which also will be either radius, sine, tangent, or secant;)

TO THE LENGTH OF THE SIDE REQUIRED.

RULE II. To find an angle, one of the given sides must be made radius, then institute the following proportion:

As THE LENGTH OF THE GIVEN SIDE MADE RADIUS; Is TO ITS NAME, (that is, radius;)

So is the length of the other given side;

To ITS NAME, (which will be either sine, tangent, or se-

cant.)

Having instituted the proportion, look for the corresponding logarithms, in the logarithms of numbers for the length of the sides; and in the table of artificial sines and tangents, for the logarithmic sine, tangent, or secant.

ADD TOGETHER THE LOGARITHMS OF THE SECOND AND THIRD TERMS, AND FROM THEIR SUM SUBSTRACT THE LOGARITHM OF THE FIRST TERM: THE REMAINDER WILL BE THE LOGARITHM OF THE FOURTH TERM, WHICH SEEK IN THE TABLES, AND FIND ITS CORRESPONDING NUMBER, OR DEGREES AND MINUTES.

See the introduction to the table of logarithms; which should be attentively studied by the learner, before he proceeds any further.

Note. The logarithm for radius is always 10, which is the logarithmic sine of 90°, and the logarithmic tangent of 45.

The preceding PROPOSITIONS and RULES being duly attended to, the solution of the following CASES of Rectangular Trigonometry will be easy:\*

## CASE I.

The angles and hypothenuse given, to find the legs. Fig. 42.

In the triangle ABC, given the hypothenuse AC 25 rods or chains; the angle at A 35° 30': and consequently the angle at C 54° 30': (See Note, Geom. Def. 38.) to find the legs.

Making the hypothenuse radius, the proportions will be:

To find the leg A B.

As radius --- 10.0000000
: hyp. AC, 25 - 1.397940
: sine ACB, 54° 30′ 9.910686

11.308626
10.000000

To find the leg B C.
As radius --- 10.0000000
: hyp. AC, 25 - 1.397940
: sine CAB, 35°30′ 9.763954
11.161894
10.0000000

: leg AB, 20.35 nearly 1.308626 : legBC, 14.52 nearly 1.161894

Note. When the first term is radius, it may be substracted by cancelling the first figure of the sum of the other two terms.

As secants are excluded from the tables, such cases in Trigonometry as are solved by secants are also excluded.

[The learner should exercise himself, in this and the following rules in Trigonometry, in stating all the proportions which can be made, until he is able to do it with facility.]

<sup>•</sup> See Practical Trigonometry in, the Appendix.

#### BY NATURAL SINES.

This case may be solved by natural sines,\* according to

the following proportions:

As unity, or 1, is to the length of the hypothenuse, so is the natural sine of the smallest angle, to the length of the shortest leg. Or, so is the natural sine of the largest angle, to the length of the longest leg.

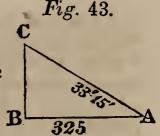
Or, which is the same thing, MULTIPLY THE NATURAL SINES OF THE TWO ANGLES BY THE HYPOTHENUSE; THE PRODUCTS WILL BE THE LENGTH OF THE TWO LEGS.

Nat. s	ine of 350	30′	EXAMPLE. Nat.	sine of 54°	30 <b>′</b>
Нур.	0.58070 25		Нур.	0.81412	
Tryp.			rry p.		
	290350 116140			407060 162824	
	14.51750			20.35300	
Leg B C	14.52		Leg	AB 20.35	

Note. The third decimal figure in the first product being 7, the preceding figure may be called one more than it is, viz. 2. And whenever in any product, &c. there are more places of decimals than you wish to work with, if the one at the right hand of the last which you wish to retain is more than 5, add a unit to the last, because a greater decimal number than 5 is more than half.

## CASE II.

The angles and one leg given, to find the hypothenuse and the other leg. Fig. 43.



<sup>\*</sup> See the Introduction to the Table of Natural Sines.

In the triangle ABC, given the leg AB 325, the angle at A 33° 15′, and the angle at C 56° 45′; to find the hypothenuse and the leg BC.

Making the hypothenuse radius, the proportions will be;

To find the hypothenuse.
As sine of C, 56° 45′ 9.922355; leg A B, 325.
2.511883; Radius
10.0000000
12.511883
9.922355
12.250896
9.922355

: Hyp. 388.6 2.589528: leg. B, C. 2131 2.328541

Note. If the leg B C had been given, instead of the leg AB, the proportions would have been the same, the obvious changes being made.

#### BY NATURAL SINES.

To solve this CASE by natural sines, institute the follow-

ing proportions:

To find the hypothenuse. As the natural sine of the angle opposite the given leg, is to the length of the leg, so is unity, or 1, to the length of the hypothenuse.

Or, which is the same thing, DIVIDE THE GIVEN LEG BY THE NATURAL SINE OF ITS OPPOSITE ANGLE, AND THE QUOTIENT WILL BE THE HYPOTHENUSE.

To find the other leg. As the natural sine of the angle opposite the given leg, is to the length of the given leg, so is the natural sine of the angle opposite the other leg, to the length of the other leg.

#### EXAMPLE.

Given leg 325. Nat. sine of 56° 45′, the angle opposite the given leg, 0.83629. Nat. sine of 33° 15′, the angle opposite the other leg, 0.54829.

As 0.83629: 325::1:388.6.

As 0.83629: 325:: 0.54829: 213.07.

### CASE III.

The hypothenuse and one leg given, to find the angles and the other leg. Fig. 44.

A

40

Fig. 44.

In the triangle A C B, given the hypothenuse A C 50, and the leg A B 40, to find the angles and leg B C.

Making the hypothenuse radius, the proportion to find the angle A C B will be:

As hyp. 50 - : radius : leg A B 40 -	1.698970 10.000000 1.602060
	11.602060 1.698970
: sine A CB, 53° 8'	9.903090

The angle A C B being 53° 8', the other is consequently 36° 52'.

The angles being found, the leg B C may be found by either of the preceding cases. It is 30.

#### BY NATURAL SINES.

The angle opposite the given leg, may be found by the following proportion:

As the hypothenuse is to unity, or 1, so is the given leg to the nat. sine of its opposite angle.

Or, which is the same thing, DIVIDE THE GIVEN LEG BY THE HYPOTHENUSE, AND THE QUOTIENT WILL BE THE NAT. SINE.

#### EXAMPLE.

The leg A B 40, divided by the hypothenuse 50, gives a

quotient 0.80000; which, looking in the table of nat. sines, the nearest corresponding number of degrees and minutes will be found to be 53° 8′, the angle A C B.

#### BY THE SQUARE ROOT.

In this CASE the required leg may be found by the square root, without finding the angles; according to the following PROPOSITION:

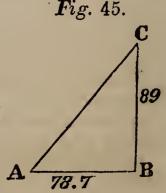
IN EVERY RIGHT ANGLED TRIANGLE, THE SQUARE OF THE HYPOTHENUSE IS EQUAL TO THE SUM OF THE SQUARES OF THE TWO LEGS. Hence,

THE SQUARE OF THE GIVEN LEG BEING SUBSTRACTED FROM THE SQUARE OF THE HYPOTHENUSE, THE REMAINDER WILL BE THE SQUARE OF THE REQUIRED LEG.

As in the preceding EXAMPLE; the square of the leg A B 40 is 1600; this substracted from the square of the hypothenuse 50, which is 2500, leaves 900, the square of the leg B C, the square root of which is 30, the length of leg B C, as found by logarithms.

## CASE IV.

The legs given, to find the angles and hypothenuse. Fig. 45.



In the triangle A B C, given the leg A B 78.7, and the leg B C 89; to find the angles and hypothenuse.

Making the leg A B radius, the proportion to find the angle B A C will be,

As leg A B, 78.7 - 1.895975 : radius - 10.000000 : leg B C, 89 - 1.949390 11.949390 1.895975

: tang. B A C, 48° 31′ 10.053415

'The angle A C B is consequently 41° 29'.

Making the leg B C radius, the proportion to find the angle B C A will be similar, with the obvious differences.

The angles being found, the hypothenuse may be found by

Case II. It is nearest 119.

### BY THE SQUARE ROOT.

In this case, the hypothenuse may be found by the square root, without finding the angles; according to the following **PROPOSITION**.

IN EVERY RIGHT ANGLED TRIANGLE, THE SUM OF THE SQUARES OF THE TWO LEGS IS EQUAL TO THE SQUARE OF THE HYPOTHENUSE.

In the above EXAMPLE, the square of A B 78.7 is 6193.69, the square of B C 89 is 7921; these added make 14114.69, the square root of which is nearest 119.

### BY NATURAL SINES.

The hypothenuse being found by the square root, the angles may be found by nat. sines, according to the preceding CASE.

Hyp. Leg B C. Nat. Sine. 119) 89.00000 (74789 83.3

57 47	-
_	40 33
_	070 952
	1180 1071
	109

The nearest degrees and minutes corresponding to the above nat. sine, are 48° 24′, for the angle B A C. The difference between this and the angle, as found by logarithms, is occasioned by dividing by 119, which is not the exact length of the hypothenuse it being a fraction too much.

#### BY NATURAL TANGENTS.

B. C. Leg A B. Rad. **78.7** : + 1 89.0 89.0 Nat. Tang. 78.7) 89.0 (: 1.13087=48° 31' 787 1030 787 2430 2361 6900 6296 6040 5509

# PART II.

### OBLIQUE TRIGONOMETRY.

The solution of the first two cases of Oblique Trigonom.

etry depends on the following PROPOSITION.

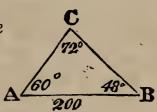
In all plane triangles, the sides are in proportion to each other, as the sines of their opposite angles. That is, as the sine of one angle is to its opposite side, so is the sine of another angle to its opposite side. Or, as one side is to the sine of its opposite angle, so is another side to the sine of its opposite angle, so is another side to the sine of its opposite angle.

Note. When an angle exceeds 90°, make use of its supplement, which is what it wants of 180°. Note, Def. 25. Geom.

# CASE I.

Fig. 46.

The angles and one side given, to find the other sides. Fig. 46.



In the triangle ABC, given the angle at B 48°, the angle at C 72°, consequently the angle at A 60°, and the side AB 200, to find the sides AC and BC.

		To find the side B C.
As sine A CB, 72°	9.978206	As sine A CB, $72^{\circ}$ - $9.978206$
: side AB, 200 -	2.301030	: side AB, 200 - 2.301030
:: sine A B C, 48°	-9.871073	:: sine B A C, 60° - 9.937531
	12.172103	12.328561
	9.978206	9.978206
43 4 4		
: side A C, 156 -	2.193897	: side B C, 182 - 2.260355

### BY NATURAL SINES.

As the nat. Sine of the angle opposite the given side is to the given side, so is the nat. Sine of the angle opposite either of the required sides to that required side.

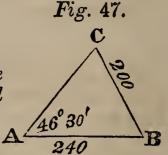
Given side 200; nat. sine of 72°, its opposite angle, 0.95115, nat. sine of ABC 48°, 0.74314; nat. sine of BAC 60°,

0.86617. Thus,

0.95115 : 200 : : 0.74314 : 156. 0.95115 : 200 : : 0.86617 : 182.

### CASE II.

Two sides, and an angle opposite to one of them given, to find the other angles and side. Fig. 47.



In the triangle ABC, given the side AB 240, the side BC 200, and the angle at A 46° 30′; to find the other angles and the side AC.

To find the angle A C B.	
As side B C, 200 - 2.301030	Angle at A 46° 30′
: sine BAC, 46° 30′ 9.860562	C 60 30
:: side AB, 240 - 2.380211	
	107.00
12.240773	
2.301030	Sum of the three angles 1800
	Sum of two 1070
:sineacB,60°30' nearly9.939743	-
	Angle at B 73
The side A C will be found b	

Note. If the given angle be obtuse, the angle sought will be acute; but if the given angle be acute, and opposite a given lesser side, then the angle found by the operation may be either obtuse or acute. It ought therefore to be mentioned which it is, by the conditions of the question.

#### BY NATURAL SINES.

As the side opposite the given angle is to the nat. sine of that angle, so is the other given side to the nat. sine of its opposite angle.

One given side 200, nat. sine of 46° 30′, its opposite angle, 0.72537, the other given side 240.

As 200: 0.72537:: 240: 0.87044=60° 30′.

### CASE III.

Two sides and their contained angle given, to find the other angles and side.

Fig. 48.

C

given, to find the other angles and side.

A

26

A

240

B

The solution of this CASE depends on the following PROP-

IN EVERY PLANE TRIANGLE, AS THE SUM OF ANY TWO SIDES IS TO THEIR DIFFERENCE, SO IS THE TANGENT OF HALF THE SUM OF THE TWO OPPOSITE ANGLES TO THE TANGENT OF HALF THE DIFFERENCE BETWEEN THEM.

ADD THIS HALF DIFFERENCE TO HALF THE SUM OF THE ANGLES, AND YOU WILL HAVE THE GREATER ANGLE, AND SUBSTRACT THE HALF DIFFERENCE FROM THE HALF SUM, AND YOU WILL HAVE THE LESSER ANGLE.

In the triangle ABC, given the side AB 240, the side AC 180, and the angle at A 36° 40′, to find the other angles and side.

Side A B .	240	<b>A</b> B	240
AC -	180	A C -	180
Sum of the two	sides 420	Difference	60

The given angle BAC 36° 40′, substracted from 180°, leaves 143° 20′, the sum of the other two angles, the half of which is 71° 40′.

As the sum of two sides, 420	2.623249 1.778151 10.479695
	12.257846 2.623249
: tangent half difference, 23° 20' nearly	9.634597
The half sum of the two unknown angles, The half difference between them,	71° 40′ 23 20
Add, gives the greater angle A C B	95 00
Substract, gives the lesser angle ABC	48 23

The side B C may be found by CASE I. or II.

# CASE IV.

The three sides given, to find the angles. Fig. 49.

A 105 D B

The solution of this CASE depends on the following PROP-OSITION.

IN EVERY PLANE TRIANGLE, AS THE LONGEST SIDE IS TO THE SUM OF THE OTHER TWO SIDES, SO IS THE DIFFERENCE BETWEEN THOSE TWO SIDES TO THE DIFFERENCE BETWEEN THE SEGMENTS OF THE LONGEST SIDE, MADE BY A PERPEN-DICULAR LET FALL FROM THE ANGLE OPPOSITE THAT SIDE

Half the difference between these segments, added to half the sum of the segments, that is, to half the length of the longest side, will give the greatest segment; and this half difference substracted from the half sum will be the lesser segment. The triangle being thus divided, becomes two right angled triangles, in which the hypothenuse and one leg are given to find the angles. ARC given the side AR 105 the side AC

In the triangle A B C, given		, the side A C
85, and the side B C 50, to fine Side A C - 85	A C	- 85
BC - 50	B C	- 50
	ъО -	
Sum of the two sides 135	Diffe	erence 35
As the longest side AB, 10	5	2.021189
: sum of the other two sides, 1		2.130334
:: difference between those sid		1.544068
		<del>,</del>
		3.674402
		2.021189
3100	4	1 050010
: difference between the segme	ents, 45	1.653213
Walf the aids A D		FOF
Half the side A B Half the difference of the seg	monto	- 52.5 - 22.5
rian the difference of the seg	mems •	- 44.0
Add, gives the greater segmen	nt A D	- 75.0
Substract, gives the lesser seg	ment BD	30.0
Thus the triangle is divide	d into two right	angled trian-
gles, ADC and BDC; in e	ach of which the	hypothenuse
and one leg are given to find	the angles.	
To find the angle DCA.		
As hyp. A C, 85 - 1.929419		
: radius 10.000000		
:: seg. A. D., 75, - 1.875061	:: seg. B D, 30	- 1.477121
11 975061		11 477101
11.875061 1.929419		11.477121 1.698970
1.929413		1.090970
: sine DCA, 61° 56′ 9.945642	: sine DCB, 36°	52' 9.778151
The anala D C A C10 FC		00 1
The angle DCA 61° 56′,	substracted from 90	J, leaves the
angle C A D 28° 4'.		

The angle DCB 36° 52′, substracted from 90°, leaves the

angle CBD 53° 16′.

The angle DCA 61° 56′, added to the angle DCB 36° 52′, gives the angle ACB 98° 48′.

This case may also be solved according to the following

PROPOSITION.

IN EVERY PLANE TRIANGLE, AS THE PRODUCT OF ANY TWO SIDES CONTAINING A REQUIRED ANGLE IS TO THE PRODUCT OF HALF THE SUM OF THE THREE SIDES, AND THE DIFFERENCE BETWEEN THAT HALF SUM AND THE SIDE OPPOSITE THE ANGLE REQUIRED, SO IS THE SQUARE OF RADIUS TO THE SQUARE OF THE CO-SINE OF HALF THE ANGLE REQUIRED.

Those who make themselves well acquainted with TRIGO-NOMETRY, will find its application easy to many useful purposes, particularly to the mensuration of heights and distances. These are here omitted, because as this work is designed principally to teach the art of common FIELD-SURVEYING, it was thought improper to swell its size, and consequently increase its price, by inserting any thing not particularly connected with that art.

It is recommended to those who design to be surveyors, to study TRIGONOMETRY thoroughly; for though a common field may be measured without an acquaintance with that science, yet many cases will occur in practice, where a knowledge of it will be found very beneficial; particularly in dividing land, and ascertaining the boundaries of old surveys. Indeed no one who is ignorant of TRIGONOMETRY, can be an accomplished surveyor.

# SURVEYING.

SURVEYING is the art of measuring, laying out, and dividing land.

# PART I.

#### MEASURING LAND.

The most common measure for land is the acre; which contains 160 square rods, poles, or perches; or 4 square

roods, each containing 40 square rods.

The instrument most in use, for measuring the sides of fields, is Gunter's chain, which is in length 4 rods, or 66 feet; and is divided into 100 equal parts, called links, each containing 7 inches and 92 hundredths. Consequently, 1 square chain contains 16 square rods, and ten square chains make 1 acre.

In small fields, or where the land is uneven, as is the case with a great part of the land in New England, it is better to use a chain of only two rods in length; as the survey can be more accurately taken.\*

# SECTION I.

### PRELIMINARY PROBLEMS.

PROBLEM I. To reduce two rod chains to four roa chains.

RULE. If the number of two rod chains be even, take half the number for four rod chains, and annex the links, if any; thus, 16 two rod chains and 37 links, make 8 four rod chains and 37 links.

But if the number of chains be odd, take half the greatest even number for chains, and for the remaining number add 50 to the link: Thus, 17 two rod chains and 42 links makes 8 four rod chains and 92 links.

PROBLEM II. To reduce two rod chains to rods and decimal parts.

\* As there is no standard of long measure established by the General Government, the standard yard, which is kept in the State Treasurer's office, is adopted as a standard of long measure for Connecticut. Each chain of 2 rods, should be 11, and each of 4 rods, 22 yards, in length.

Rule. Multiply the chains by 2, and the links by 4, which will give hundredths of a rod; thus, 17 two rod chains and 21 links, make 34 rods and 84 hundredths; expressed thus, 34.84 rods.

If the links exceed 25, add one to the number of rods, and multiply the excess by 4: thus, 15 two rod chains and 38 links make 31.52 rods.

PROBLEM III. To reduce four rod chains to rods and

decimal parts.

Rule. Multiply the chains, or chains and links, by 4; the product will be rods and hundredths: thus, 8 chains and 64 links, make 34.56 rods.

The reverse of this rule, that is, dividing by 4, will reduce rods and decimals to chains and links: thus, 105.12 rods, make 26 chains and 28 links.

PROBLEM IV. To reduce square rods to acres.

Rule. Divide the rods by 160, and the remainder by 40, if it exceeds that number, for roods or quarters of an acre: thus 746 square rods make 4 acres, 2 roods, and 26 rods.

PROBLEM V. To reduce square chains to acres.

RULE. Divide by 10; or, which is the same thing, cut off the right hand figure: thus, 1460 square chains make 146 acres; and 846 square chains make 84 acres and 6 tenths.

PROBLEM VI. To reduce square links to acres.
Rule. Divide by 100000; or, which is the same thing, cut off the 5 right hand figures: thus, 3845120 square links make 38 acres and 45120 decimals.

Note. When the area of a field, by which is meant its superficial contents, is expressed in square chains and links, the whole may be considered as square links, and the number of acres contained in the field, found as above. Then multiply the figures cut off by 4, and again cut off 5 figures, and you have the roods; multiply the figures last cut off by 40, and again cut off 5 figures, and you have the rods.

Example. How many acres, roods, and rods, are there in 156 square chains and 3274 square links?

15)63274 square links.

2)53096 40

21)23840

Answer. 15 acres 2 roods and 21 rods.

PROBLEMS for finding the area of right lined figures, and also of circles.

PROBLEM VII. To find the area of a square or rectangle.

RULE. Multiply the length into the breadth; the product

will be the area.

PROBLEM VIII. To find the area of a rhombus or rhomboid.

RULE. Drop a perpendicular from one of the angles to its opposite side, and multiply that side into the perpendicular; the product will be the area.

PROBLEM IX. To find the area of a triangle.

RULE 1. Drop a perpendicular from one of the angles to its opposite side, which may be called the base; then multiply the base by half the perpendicular, or the perpendicular by half the base; the product will be the area. Or, multiply the whole base by the whole perpendicular, and half the product will be the area.

RULE 2. If it be a right angled triangle, multiply one of the legs into half the other; the product will be the area. Or, multiply the two legs into each other, and half the

product will be the area.

RULE 3. When the three sides of a triangle are known,

the area may be found arithmetically, as follows:

Add together the three sides; from half their sum substract each side, noting down the remainders; multiply the half sum by one of those remainders, and that product by another remainder, and that product by the other remainder; the square root of the last product will be the area.\*

Example. Suppose a triangle whose three sides are 24,

20, and 18 chains. Demanded the area.

24+20+18=62, the sum of the three sides, the half of which is 31. From 31 substract 24, 20, and 18; the three remainders will be 7, 11, and 13.

 $31\times7=217$ ;  $217\times11=2387$ ;  $2387\times13=31031$ , the square root of which is 176.1, or 17 acres, 2 roods, and 17 rods.

#### BY LOGARITHMS.

As the addition of logarithms is the same as the multiplication of their corresponding numbers; and as the number answering to one half of a logarithm will be the square root of the number corresponding to that logarithm: it follows, that if the logarithm of the half sum of the three sides, and

\* Better expressed thus. From half the sum of the sides substract each side separately. Multiply the half sum and the several remainders together, and the square root of the product will be the area.—ED.

the logarithms of the three remainders, be added together, the number corresponding to one half the sum of those logarithms will be the area of the triangle.

The half sum, 31	1.491362
The first remainder, 7	0.845098
The second remainder, 11	1.041393
The third remainder, 13	1.113943
ml (.1 01000 000 1	1.101806
The square of the area, 31030.083 nearly	4.491796
Anna 176 aguara chaing 150 aguara linka	2.245898
Area, 176 square chains 150 square links.	2.240090

RULE 4. When two sides of a triangle, and their contained angle, that is, the angle made by those sides, are given, the

area may be found as follows:

Add together the logarithms of the two sides, and the logarithmic sine of the angle; from their sum substract the logarithm of radius, the remainder will be the logarithm of double the area.

EXAMPLE. Suppose a triangle, one of whose sides is 105 rods, and another 85, and the angle contained between them 28° 5′. Demanded the area.

	021189
	929419
Sine angle, 28° 5′ 9.6	572795
13.6	523403
Substract radius 10.0	000000
Double area, 4200 rods nearly 3.6	523403

Answer, 2100 rods.

Note. Radius may be substracted by cancelling the left hand figure of the index, or substracting 10, without the trouble of setting down the ciphers.

#### BY NATURAL SINES.

Multiply the two given sides into each other, and that product by the natural sine of the given angle; the last product will be double the area of the triangle.

Nat. sine of the angle 28° 5′, 0.47076.

 $105\times85=8925$ , and  $8925\times0.47076=4201$ , the double area of the triangle.

PROBLEM X. To find the area of a trapezoid.

RULE. Multiply half the sum of the two parallel sides by the perpendicular distance between them, or the sum of the two parallel sides by half the perpendicular distance, the product will be the area.

PROBLEM XI. To find the area of a trapezium, or ir-

regular four sided figure.

RULE. Draw a diagonal between two opposite angles, which will divide the trapezium into two triangles. Find the area of each triangle, and add them together. Or, multiply the diagonal by half the sum of the two perpendiculars let fall upon it, or the sum of the two perpendiculars by half the diagonal, the product will be the area.

Note. Where the length of the four sides and of the diagonal is known, the area of the two triangles, into which the trapezium is divided, may be calculated arithmetically, according to Prob. IX. Rule 3.

PROBLEM XII. To find the area of a figure containing

more than four sides.

RULE. Divide the figure into triangles, and trapezia, by drawing as many diagonals as are necessary, which diagonals must be so drawn as not to intersect each other; then find the area of each of the several triangles or trapezia, and add them together; the sum will be the area of the whole figure.

Note. A little practice will suggest the most convenient way of drawing the diagonals, but whichever way they are drawn, provided they do not intersect each other, the whole area will be found the same.

PROBLEM XIII. Respecting circles.

RULE 1. If the diameter be given, the circumference may be found by one of the following proportions: as 7 is to 22, or more exactly, as 113 is to 355, or in decimals, as 1 is to 3.14159, so is the diameter to the circumference.

RULE 2. If the circumference be given, the diameter may be found by one of the following proportions: as 22 is to 7, or as 355 is to 113, or as 1 is to 0,31831, so is the circumference to the diameter.

RULE'3. The diameter and circumference being known, multiply half the one into half the other, and the product will be the area.

RULE 4. From the diameter only, to find the area: multiply the square of the diameter by 0.7854, and the product will be the area.

RULE 5. From the circumference only to find the area:

multiply the square of the circumference by 0.07958, and the

product will be the area.

RULE 6. The area being given, to find the diameter: divide the area by 0.7854, and the quotient will be the square of the diameter; from this extract the square root, and you will have the diameter.

RULE 7. The area being given, to find the circumference: divide the area by 0.07958, and the quotient will be the square of the circumference; from this extract the square root, and you will have the circumference.

To find the area of an Ellipse or an Ellipsis

RULE. Multiply the product of the two diameters by 0.7854, and point off from the product as many figures at the right hand as there are decimals in both factors, and those at the left will be the area of the figure.

EXAMPLE. What is the area of an ellipse, of which the longest diameter is 65 rods and 10 links, and the shortest is 45 rods and 10 links.

Longest diameter, 65.4 Shortest diameter, 45.4
2616
3270
2616
2969.16
.7854
1187664
1484580
2375328
2078412
2331.978264 1
160)2332(14
160
732
740
92
A. Q. R.
Answer, 14 2 12

### SECTION II.

The following cases teach the most usual methods of taking the survey of fields; also, how to protract or draw a plot of them, and to calculate their area.

Note. The field book is a register containing the length of the sides of a field, as found by measuring them with a chain; also, the bearings, or courses of the sides, or the quantity of the several angles, as found by a compass or other instrument for that purpose; together with such remarks as the surveyor thinks proper to make in the field.

# CASE I.

### TO SURVEY A TRIANGULAR FIELD.

Measure the sides of a field with a chain, and enter their several lengths in a field-book; protract the field on paper, and then find the area by Prob. IX. Rule 1. Or, without plotting the field, calculate the area by Prob. IX. Rule 3.

,	Fig. 50.
FIELD BOOK. See Fig.	50. <b>C</b>
Chains.	N .
AB 20	
BC 24	D CE
CA 18	S D
To find the area.	2/20/29
Ch. L.	1700 OF.
Base B C 24.00	
Half perp. A D- 7.34	$\mathbf{A}^{\prime}$
1	20 Ch.
0.200	
9600	
7200	
16800	
-	
Acres 17)61600	
4	•
Roods 2)46400	
40	·
Rods 18)56000	
A 70 1 70	1.3.
Acres Roods R	tods

Area 17-2-18.56

5

Note. When there are ciphers at the right hand of the links, they may be rejected; remembering to cut off a proper number of figures according to decimal rules.

Observe, That in measuring with a chain, slant or inclined surfaces, as the sides of hills, should be measured horizontally, and not on the plane or surface of the hill; otherwise, a survey cannot be accurately taken. To effect this, the lower end of the chain must be raised from the ground, so as to have the whole in a horizontal line; and the end thus raised must be directly over the point where the chain begins or ends, according as you are ascending or descending a hill; which point may be ascertained by a plummet and line.

### CASE II.

### TO SURVEY A FIELD IN THE FORM OF A TRAPEZIUM.

Measure the several sides, and a diagonal between two opposite angles; protract the field, and find the area by Problem XI. Or, without protracting the field, calculate the area according to the *note* at the end of that PROBLEM.

			Fig. 51.	
FIELD-BO	OK.	See Fig. 51	1. Di 21	
		Ch. L.	21 50	\ C
AΒ	•	27.50		a
$\mathbf{B}\mathbf{C}$	•	11.70		
CD	•	21.50	×/ \20	13
DA	-	14.70	The state of the s	10
Diag. AC	•	28.	A 07 50	B
			A 27 50	

### TO PROTRACT THIS TRAPEZIUM.

Draw the side AB, the given length; with the diagonal AC 28, and the side BC 11.70, describe cross arcs as at C, from A and B as centres; and the point of intersection will represent that corner of the field: then, with the side CD 21.50, and the side AD 14.70, describe cross arcs as at D, from A and C as centres; and the point of intersection will represent that corner of the field.

### TO FIND THE AREA.

Perpendicular B a	- 11.34
D m	- 11.10
TI-16 diamonal A C	22.44
Half diagonal A C	- 14.00
	897600
	2244
	Acres 31)416
	4
	Rood 1)664
	40
	D 1 00)=00
Acres	Rods 26)560 Rood Rods
	_1_26.56

Note. The perpendiculars need not be actually drawn; their length may be obtained as follows: from the angle opposite the diagonal open the dividers so as when one foot is in the angular point, as at B, the other, being moved backwards and forwards, may just touch the diagonal at A, and neither go the least above or below it; that distance in the dividers being measured on the scale, will give the length of the perpendicular.

# CASE III.

TO SURVEY A FIELD WHICH HAS MORE THAN FOUR SIDES,
BY THE CHAIN ONLY.

Measure the several sides, and from some one of the angles from which the others may be seen, measure diagonals to them; draw a plot of the field, and find the area by Problem XII.

ABCCD DE EFA

FIELD-BOOK. See Fig. 52

D-BOOF	K. S	ee Fig. 52	n.		ig. 52.	
<b>c</b>	20.40	a		E 20	E 13	
		30	60			A.
		Ch. L. 30.60		Diagon		
		20.40		Diagon	- -	Ch. L.
		22.40 A C	_		_	45.
	_	16.20 A D				35.
•				•		24.20
•	•	13.50 AE	•	•	•	24.20
•	•	28.				,

### TO PROTRACT THIS FIELD.

Draw the side AB, making it the given length 30.60; with the diagonal AC 45, and the side BC 20.40, describe cross arcs as at C, from the points A and B as centres, and the point of intersection will represent that corner of the field; draw the side BC, and the dotted diagonal AC; with the diagonal AD 35, and the side CD 22.40, describe cross arcs as at D, from the points A and C, and draw the side CD, and the dotted diagonal AD. Proceed in this manner till all the sides and diagonals are drawn.

#### TO FIND THE AREA.

The field being plotted, may be divided into one trapezium and two triangles; the area of which is calculated as follows:

The trapezium AB Perpend. Ba  Do -	C D. 11.68 17.10	The triangle A I Half perp. E m Diag. A D	
Half diag. A C ;	27.78 22.50		${2450}$ $1470$
	143900 5756 5756	Square chains •	171.50
Square chains - 6	647.5500	-	
The triangle A F Perpend. E n Half side A F -	E. 11.65 14	Trap. ABCD - Triangle ADE - Triangle AFE -	171.50
	4660 1165	Acres	98)215
Square chains	163.10	Roc	ods .860 40
Acres Roods Rods Area 98—0—34.4	1	$\mathbf{Rods}$	34)400

## REMARKS.

As each of the sides of the several triangles, into which the preceding plot of a field is divided, is known from the fieldbook, the area of the field may be calculated arithmetically, by finding the area of each triangle, according to Prob. IX. Rule 3; and then adding the whole together. This method, though it may require more time, is preferable to the other, because more accurate. Indeed it is always better to calculate the area of a field arithmetically than geometrically, for in the former no two persons can differ in their calculations; whereas, according to the latter, which is the common method of casting the contents of a field, it is hardly to be expected that any two persons will perfectly agree. inaccuracy of scales, and the difficulty of determining with precision the length of sides and perpendiculars with a scale and dividers, render it almost if not quite impossible to obtain the exact area of a field, in the method commonly practised, even if the surveyor has measured it accurately in the first place.

Other methods of taking the survey of a field by the chain only, are mentioned in some treatises on this subject, but they are rather curious than useful; and it is much better to ascertain the angles by an accurate compass, or some instrument designed purposely for taking angles.

### CASE IV.

### TO SURVEY A FIELD WITH A CHAIN AND COMPASS.

Measure the length of the sides with a chain, and take their bearing or course with a compass;\* enter these in a field-book; plot the field on paper, and calculate the area by the directions already given.

### TO PROTRACT OR DRAW A MAP OF A FIELD.

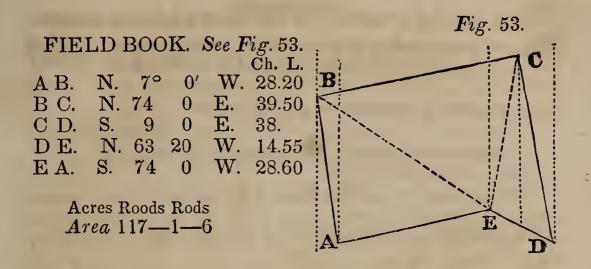
Draw a line to represent a meridian, or north and south line, from which lay off a bearing or course of the first side of the field, with a protractor, or from a line of chords; and from a scale of equal parts, measure the length of the side, and draw a line to represent it.

At the end of this line draw a line parallel to the meridian line, and then lay off the second side of the field as before taught; proceed in the same manner to draw parallel lines, and lay off the several sides till the whole is protracted.

In protracting a field, let the top of the paper be considered as north, the bottom south, the right hand east, and the left hand west; lay the course to the right or left of the meridian line, according as it is east or west, and upwards or downwards, according as it is north or south.

In all protractions, if the end of the last distance falls exactly on the point from which you began, the course also being right, the field work and protractions are truly taken and performed; if not, an error must have been committed in one of them: in such cases, make a second protraction; if this agrees with the former, it is to be presumed the fault is in the field work; a re-survey must then be taken.

\* A compass may be so constructed with two indexes, one moveable and the other fixed, as to ascertain the angles made by two sides, without reference to the bearing of those sides. Such a compass would be particularly useful in surveying land where there are mineral substances which have an influence upon the compass needle, attracting it one way or the other, and thus rendering it impossible to take a course by it with precision.



## REMARKS.

The sides of the several triangles into which the plot of a field is divided may be found by trigonometry; and then the area of each triangle may be calculated according to Prop. IX. Rule 3. The sum of the areas of the several triangles will be the area of the whole field. This method may require more time, but it is perfectly accurate, since no dependence is placed on the uncertain measurement of scale and dividers.

In the preceding EXAMPLE, suppose the field divided into three triangles. See Fig. 53. In the triangle EAB, the sides E A and A B are known from the FIELD BOOK, and their contained angle is known from the bearing of the sides. The other angles and the side EB may be found by OBLIQUE TRIGONOMETRY, CASE III.; and then there will be the three sides to find the area. In the triangle E B C, the side B C is known from the field book, and the side EB is found as above mentioned; the angle EBA is also found as above; this substracted from the angle ABC, which may be found from the bearing of the sides AB and BC, will leave the angle EBC; there will then be the two sides and their contained angle to find the third side; and this being found, there will be the three sides to find the area. In the triangle E D C, the sides D E and D C are known from the FIELD BOOK, and their contained angle is known from the bearing of the sides. The side E C and the area may be found as above.

It is recommended to the learner to make these calcula-

tions, as it will improve him in the knowledge of trigonometry.

Note. Two sides and their contained angle being given, the area

may be found by Prob. IX. Rule 4.

#### ANOTHER METHOD OF PROTRACTING FIELDS. .

Without drawing parallel lines at the end of each side, a field may be protracted by the angles made by the several sides; and the angle made between any two sides may be found by the following RULES.

RULE 1. If the course or bearing of one of the sides is north and the other south, one east and the other west, sub-

stract the less course from the greater.

RULE 2. If one is north and the other south, and both

east or west, add both courses together.

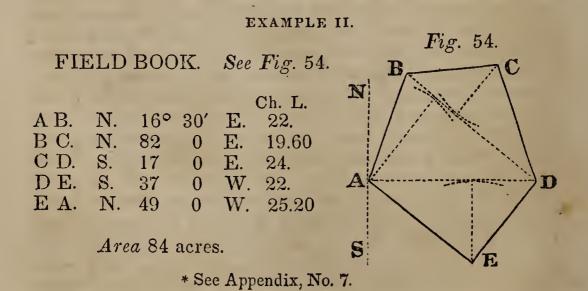
RULE 3. If both are north or south, and one east and the other west, substract their sum from 180°.

RULE 4. If both are north or south, and both east or west, add the less course to the supplement of the greater.

In each case, the result will give the angle contained by

the two sides.

To protract a field according to the preceding rules, is preferable to the method of doing it by parallel lines, though it may not be so easy to the learner at first. It is difficult to draw parallel lines with perfect accuracy, and a small deviation from a true line may make considerable difference in the plot of a field.\*

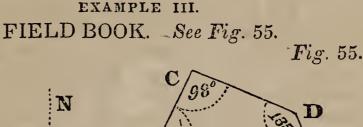


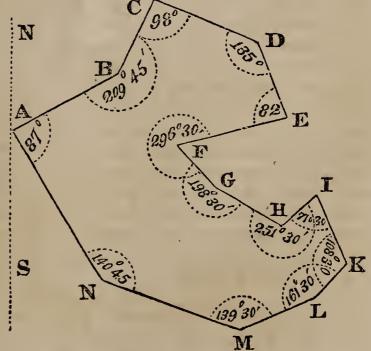
TO DRAW A PLOT OF THIS FIELD, ACCORDING TO THE PRE-CEDING RULES.

Having drawn the side AB, according to the directions before given for laying off the first course and distance, compare the first and second courses together, and they will be found to be both north and both east; consequently, the angle between them is found by Rule 4, as follows: 16° 30' the less course, and 98°, the supplement of the greater, being added, the sum is 114° 30', for the angle at B. Compare the second and third courses, and they will be found to be one north and one south, and both east; consequently, according to Rule 2, 82°, the second course, added to 17°, the third course, the sum 99°, is the angle at C. The third and fourth courses are both south, and one east and the other west. The angle between them at D is 126°; for 17°, the third course added to 37°, the fourth course, is 54°, which substracted from 180°, leaves 126°, according to Rule 3. The fourth and fifth courses are one south and the other north, and both west. According to Rule 2, 27°, the fourth course, added to 49°, the fifth course, the sum 86°, is the angle at E.

A little practice will render this mode of protracting a field familiar and easy, and an attention to the courses will show

in what direction the angle is to be made.





Ch. L. AB. N. 56° E. 21.60 15' BC. N. 26 30 E. 13.44 CD. S. 71 E. 18.96 30 DE. S. 26 30 E. 13.44 EF. S. 71 30 W. 18.96 FG. S. 45 0 E. 8.47 GH. S. 63 30 E. 13.44 HI. N. 45 8.47 E. 0 IK. S. 26 30 E. 13.44 KL. S. 45 W. 8.47 0 LM. S. 63 W. 30 13.44 MN. N. W. 76 0 24.73 NA. N. 36 45 W. 30. Acres Roods Rods Area 167-1-30

The above field may be protracted, and its area calculated according to the directions given in the preceding EXAMPLES.

### SEVERAL FIELD BOOKS TO EXERCISE THE LEARNER IN PLOT-TING FIELDS AND CALCULATING THEIR AREA.

								Ch. L.
	No. I.	Rods	8.	N.	539	15'	W.	11.60
1.	N. 15° 0′ E.	320	9.	N.	36	45	E.	19.20
2.	N. 37 30 E.	160	10.	N.	22	30	E.	14.
3.	East	120	11.	S.	76	45	E.	12.
4.	S. 11 0 E.	200	12.	S.	15	0	W.	10.85
5.	South	216	13.	S.	16	45	W.	10.12
6.	West	160			Acı	res Ro	ods R	ods.
7.	S. 36 30 W.	160		A	rea :	110-	-2-2	3
8.	N. 38 15 W.	136						
	Acres Roods	Rods.			$N_0$	o. III.		Rods
	Area 744-3-	<b>–</b> 28	1.	S.	65°	40'	W.	49.7
	4		2.	S.	67	15	W.	34.5
	No. II.	Ch. L.	3.	S.	54	0	W.	17.9
1.	N. 75° 0′ E.	13.70	4.	S.	20	0	W.	5.8
2.	N. 20 30 E.	10.30	5.	S.	7	30	E.	29.4
3.	East	16.20	6.	N.	83	0	E.	107.4
4.	S. 33 30 W.	35.30	7.	N.	5	50	W.	22.
5.	S. 76 0 W.	16.	8.	N.	18	30	W.	46.
6.	North	9.	41					Rods.
7.	S. 84 0 W.	11.60			$A_i$	rea 3	1—1-	<b>—</b> 19

		N	o. IV		Rods.						Rods.
1.	N.	439		w.	12.44	10.	N.	640	0'	E.	12.5
2.	N.	64	0	W.	8.	11.	N.	49	0	E.	14.
3.	N.	52	0	W.	14.60	12.	N.	26	10	W.	19.3
4.	N.	37	5	W.	51.36	13.	N.	21	0	W.	18.3
5.	N.	15	30	W.	21.76	14.	N.	44	10	w.	18.
<i>5</i> .	N.	20	40	W.	44.60	15.	N.	64		E.	30.5
7.	N.	88	20	E.	167.60	16.	N.		30	W.	39.
8.	S.	34	40	E.	71.20	17.	N.	86	5 5	E.	
	S.	75	0	W.	69.72	11.			oods Roods		26.7
9.	S.	55	0	W.	64.60	A	rea 4				·•
10.			0	W.		,£,£	.,			1~	
11.	S.	25 cres	$\mathbf{R}$ oods		18.12			No	o. VI	T. (	Ch. L.
A			- 2 —		J•	1.	N.	00		W.	
t						2.	Ñ.	19	30	W.	
		N	o. V	•	Rods.	3.	N.	23	0	W.	
1.	S.	110	50'	W.	34.6	4.	N.	41	35	W.	
2.	S.	63	20	E.	93.6	5.	N.	3	0	W.	
3.	N.	4	0	W.	34.9	6.	S.	86	50		13.33
4.	S.	89	55	E.	40.1	7.	N	2	15	W.	17.65
5.	N.	5	20	W.	35.5	8.	N.	85	45	E.	12.56
6.	N.	69	40	W.	60.	9.	S.	2	10	E.	8.
7.	S.	78	0	W.		10.	N.	86	45	E.	7.38
8.	N.	67	20	W.	1.2	11.	S.	3	15	E.	13.20
9.	S	72	30	W.	10.4	12.	N.	87	0	E.	29.92
10.	S.	66	55	W.	15.2	13.	N.	49	20	E.	4.04
	A	cres	Roods	Rod		14.	No	_			2.23
$\dot{A}$	rea 4	41 —	- 1 —	- 34		15.	N.	50	35	E.	6.50
		-		-		16.	S.	22	50	E.	17.94
		N	lo. V	I.	Rods.	17.	S.	34	0	W.	
1.	S.	34°	0'	E.	42.8	18.	S.	41	0	W.	3.
2.	S.	29	0	$\mathbf{E}$ .	69.4	19.	S.	22	50	W.	9.25
3.	S.	64	50	W.	<b>5</b> 3.	20.	S.	3	40	E.	
4.	S.	25	0	$\mathbf{E}$ .	4.	21.	S.	86	0	W.	
5.	S.	66	30	W.	39.	22.	S.	0	25	W.	
6.	N.	25	0	W.	4.	23.	S.	2	0	W.	
7.	S.	64	45	W.	32.2	24.	S.	10	0	E.	
8.	N.	30	30	W.	18.3	25.	S.	86	0		34.60
9.	N.	56	30	E.	34.5				Roods		
						£	1rea ?				
						1					

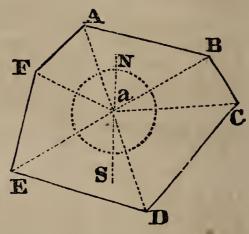
# CASE V.

WITHIN THE FIELD, FROM WHICH THE SEVERAL ANGLES MAY BE SEEN.

Take the bearing of the angles, and measure their distance from the station.

FIELD BOOK. See Fig. 56.

Fig. 56.



200 W. From station to A. N. 8.70 В. N. 60 E. 10. C. N. E. 87 11.40D. S. 15 E. 10.50 E. S. 60 W. 12. F. N. 65 8.78

#### TO PROTRACT THIS FIELD.

Draw a meridian line as N. S. From some point in that line as a centre, lay off the bearing and distance to the several angles, and draw lines from one angle to another, as AB, BC, CD, &c.

#### TO FIND THE AREA.

The area may be calculated according to Prob. XII. by measuring diagonals and perpendiculars; or more accurately according to Prob. IX. Rule 4.

As the bearing and distance of the lines from the station to the several angles are known, two sides and their contained angle are given in each of the triangles into which the plot is divided; the area may, therefore, be readily calculated by the RULE above referred to.

Note. As in the operation, the logarithm of radius is to be substracted from the sum of the other logarithms, it may be done by respecting the left hand figure, without the trouble of putting down the ciphers and substracting.

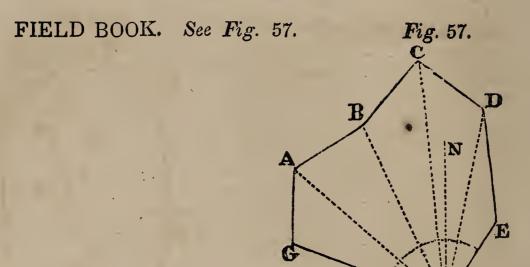
Triangle a A B.	Triangle a DE.
a A, 8.70 0.939519	
a B, 10 1.000000	a E, 12 1.079181
Sine A a B, 80° - 9.993351	Sine Da E, 75° - 9.984944
Doub. area, 85.67 - 1.932870	Doub. area, 121.7 - 2.085314
m: 1 - D C	
Triangle a B C.	$oxed{Triangle a E F.}$
a B, 10 1.000000	a E, 12 1.079181
a C, 11.40 1.056905	a F, 8.78 0.943495
Sine B a C, 27° - 9.657047	a F, 8.78 0.943495 Sine E a F. 55° - 9.913365
Doub. area, 51.75 - 1.713952	Doub. area, 86.31 - 1.936041
	Triangle a F A.
a C, 11.40 1.056905	
a D, 10.50 1 021189	a A, 8.70 0.939519
Sine Ca D, 78° - 9.990404	Sine F a A, 45° - 9.849485
Doub. area, 117 - 2.068498	Doub. area, 54.01 - 1.732499
<del></del>	

riangle a A B	-	85.67	827
аВС	-	51.75	4
a C D	-	117.1	
a D E	-	121.7	3)308
a E F	-	86.31	40
a F A	-	54.01	
			12)320
Double area -	-	516.54	Acres Roods Rods.
		Ar	ea 25 — 3 — 12.32
Area	•	25)827	

# CASE VI.

TO SURVEY A FIELD FROM SOME ONE OF THE ANGLES, FROM WHICH THE OTHERS MAY BE SEEN.

From the stationary angle, take the bearing and distance to each of the other angles, with a compass and chain.



				Ch. L.
FG.	N.	700	W.	14.60
FA.	N.	50	W.	18.20
FB.	N.	30	W.	16.80
FC.	N.	10	W.	21.20
FD.	N.	7	E.	16.95
FE.	N.	-30	E.	8.50

### TO DRAW A PLOT OF THIS FIELD.

Draw a meridian line to pass through the stationary angle as at F. From the point F, lay off the bearing and distance to the several angles, and connect them by lines, as F G, F A, F B. &c.

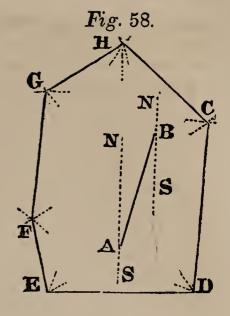
The area may be calculated as taught in the preceding CASE.

# CASE VII.

TO SURVEY A FIELD FROM TWO STATIONS WITHIN THE FIELD, PROVIDED THE SEVERAL ANGLES CAN BE SEEN FROM EACH STATION.

Find the bearing from each station to the respective angles; and also the bearing and distance from one station to the other.

FIELD BOOK. See Fig. 58.



1	First	Stati	on.			S	lecon	d Sta	tion	) <b>.</b>
AC.	N.	380	30'	E.		B C.	S.	82°	$\theta'$	E.
AD.	S.	69	0	E.	/	BD.	S.	17	0	E.
AE.	S.	59	0	W.		BE.	S.	28	0	W.
AF.	N.	63	0	W.		BF.	S.	49	0	W.
AG.	N.	21	0	W.		BG.	N.	76	0	W.
AH.	No	rth.				BH.	N.	24	0	W.

Stationary line A B. N. 14° E. 20 chains.

#### TO PROTRACT THIS FIELD.

At the first station A, draw a meridian line, and lay off the bearings to the respective angles; draw the stationary line AB, according to the bearing and distance; at B draw a meridian line parallel to the other, and lay off the bearings to the angles, as taken from this station; from each station draw lines through the degree which shows the bearing of each angle, as marked by the protractor or line of chords, and the points where those lines intersect each other will be the angles of the field. Connect those angular points together by lines, and those lines will represent the several sides of the field.

# CASE VIII.

### TO SURVEY AN INACCESSIBLE FIELD.

Fix upon two stations at a convenient distance from the

field, from each of which the several angles may be seen; from each station take the bearing of the angles; and take the bearing and distance from one station to the other.\*

FIELD BOOK. See Fig. 59. Fig. 59. 14 B S First Station. Second Station. 90 AE. N. 15'  $\mathbf{E}$ . BE.N. 50° 0' W. AF. N. N. 16 E. BF. 29 15 0 W. AG. B D. N. 14 E. N. 3024 0 W. AD. N. 39 E. BG. 30 0 N. 21 W. AH. N. 40 0 E. BH. N. E. 5 0 AC. E. N. 72 B C. E. 0 N. 20 30 Ch. L.

Stationary distance AB. S. 88° 30' E. 19.20.

44...

The directions given in the last ease for plotting the field, will apply in this case also; and the area in this and the preceding case may be calculated in the manner pointed out in Case IV. by dividing the plot into triangles, and measuring diagonals and perpendiculars. Or the sides may be found by trigonometry, and the area calculated arithmetically, as already taught.

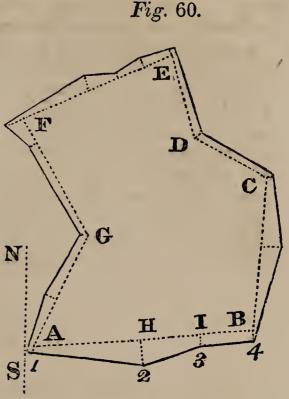
## CASE IX.

### TO SURVEY A FIELD WHERE THE BOUNDARY LINES ARE

\* This method of practice is subject to much error.

VERY IRREGULAR, WITHOUT NOTICING WITH THE COMPASS EVERY SMALL BEND.

Begin near one corner of the field, as at A, Fig. 60, and measure to the next large corner, as B, in a straight line; noticing also the bearing of this line. From the line take offsets to the several bends, at right angles from the line; noticing in the field book at what part of the line they are taken, as at A1, H2, I3, B4. Proceed in the same manner round the field. In the figure, the dotted lines represent the stationary lines, and the black lines the boundaries of S the field.



Bearing and Distance.	Offsets.	Bearing and Distance.	Offsets.
Ch. L.	Ch. L.	Ch. L.	Ch. L.
AB. N. 85° 0' E. 11.20	0.56	EF. S.67° 50′ W. 8.20	0.40
at 5.40	1.40	at 1.04	0.36
8.26	0.36	2.96	0.33
the end	0.36	5.88	1.
BC. N. 7° 20' E. 7.96	0.20	the end	0.12
at 2.36	0.36	FG. S. 27° 40′ E. 7.06	1.20
4.28	0.96	at 2.	0.24
the end	0.30	the end	0.16
CD. N. 62° 0' W. 4.68		G A. S. 25° 20′ W. 6.48	
at 4.34	0.30	at 3.80	0.80
DE. N.11° 10′ W. 4.20	0.30	the end	0.40

#### TO PROTRACT THIS FIELD.

Draw the stationary lines according to the directions in Case IV. From A make an offset of 56 links to I; measure from A to H 540 links, and make the offset, H 2, 140 links; measure from A to I 826 links, and make the offset I 3, 36 links; at B make the offset B 4, 36 links. Proceed in the same manner round the field, and connect the ends of the offsets by links, which will represent the boundaries of the field.

6\*

#### TO FIND THE AREA.

Find the area within the stationary lines as before taught; then of the several small trapezoids, rectangles, and triangles, made by the stationary lines, offsets, and boundary lines, and add the whole together: thus, add 56 links, the offset A 1, to 140 links, the offset H 2, and multiply their sum, 196, by half 540, the length of the line A H, and the product 52920 square links, will be the area of the trapezoid A H 21; again, add 140, the offset H 2, to 36, the offset I 3, and multiply their sum, 176, by half 286, the length of the line H I, and the product, 25168 square links, will be the area of the trapezoid H I 32. Proceed in the same manner to calculate the area of all the trapezoids, triangles, &c.

### CASE X.

TO SURVEY A FIELD BY TAKING OFFSETS BOTH TO THE RIGHT AND LEFT; THAT IS, WITHIN AND WITHOUT THE FIELD, AS OCCASION SHALL REQUIRE, IN CONSEQUENCE OF THE STATIONARY LINES CROSSING THE BOUNDARY LINES; ALSO, BY INTERSECTIONS, THAT IS, TAKING THE BEARING OF AN INACCESSIBLE CORNER FROM TWO STATIONS.

The directions given in the preceding CASE, together with the following FIELD BOOK, will show the learner how to survey a field like the following, and also to protract it when surveyed. FIELD BOOK. See Fig. 61.

Fig. 61.

Fig. 61.

Offsets, to the Left.	Bearing and distance.	Offsets, to the Right.	Remarks.
Ch. L. 1.12 3.40 1.25			A tower bears from A. N. 48° W.
1.45	B C. N. 27° 45′ W. 21.12 at 4.10 10.25 15.	1.20	
	C 1. S. 82° 15′ E. 5.48 1 2 N. 70 0 E. 13.28 2 D. N. 20 0 E. 3.36	5	From C go into the field to 1, on account of some impediment on or near the boundary line. At D, you get into another corner of the field.
-	DF. S. 35° 0′ E. 15.18		E. an inaccessible corner, bears from D. S. 65° 30′ E.
2.20 2.32	FA. S. 15° 15′ E. 15.10 at 1.20 7.45 12.25		E. the inaccessible corner, bears from F. N. 4° W.

Note.—To draw a tree, house, tower, or any other remarkable object, in its proper place, in the plot of a field—from any two stations, while surveying the field, take the bearing of an object, and the intersection of the lines, which represent the bearings, will determine the place of the object, in the same manner that the tower is drawn in the figure.

### TO FIND THE AREA OF THE ABOVE FIELD.

Find the area within the stationary lines, and then of the several small trapezoids, &c. remembering to distinguish those without the stationary lines from those which are within. Substract the area of those within the stationary lines from the area of those without, and add the remainder to the area contained within the stationary lines; the sum will be the whole area of the field.

[Or, add the areas of those without the stationary lines, to the area contained within those lines, and substract from the sum the areas of the several triangles, trapezoids, &c. within the stationary lines.]

### SECTION III.

RECTANGULAR SURVEYING, OR AN ACCURATE METHOD OF CALCULATING THE AREA OF A FIELD ARITHMETICALLY, FROM THE FIELD BOOK, WITHOUT THE NECESSITY OF PROTRACTING IT, AND MEASURING WITH A SCALE AND DIVIDERS, AS, IS COMMONLY PRACTISED.

I. Survey the field in the usual method, with an accurate compass and chain, and from the field book set down, in a traverse table, the course or bearing of the several sides, and their length in chains and links, or rods and decimal parts of a rod; as in the 2nd and 3d columns of the following EX-AMPLE.

	South Areas.		1 1	t 1	7858.1020	9166.7040	1	2119.0959	1	4245.4016 19143.9019
	North Areas.	1600.0910	2085.1276	1	1	1 1	1 1	 	560.1830	4245.4016
ı	2 Dep. Col.	20.74	65.86	120.28	159.88	169.44	129.49	65.79	20.12	
	1 Dep. 2 Dep. Col.	20.74	45.12	75.16	84.72	84.72	44.77	21.02	0.0	
	W.	!			1		40. 0 39.95	23.79	21.05 21.02	84.60 84.84 84.72 84.72
	田田	20.71 20.74	24.35 24.38	30.00	9.54		:		•	84.60
	\overline{\sqrt{a}}	1	15 1		49.08	54.0 $54.10$	1	32.15 32.21		135.70 135.23 84.60 84.84 135.46 135.46 84.72 84.72
	Z.	77.27	31.73			1	!	!	26.70 26.65	135.70 135.46
	ch	08	40	30	20	54	40	0	34	
	Courses.	N. 15° 0′ E.	2 N. 37 30 E.	East	4 S. 11 0 E.	5 South	6 West	7 S. 36 30 W.	8 N. 38 15 W.	
	No.	1	S,	က	4	ಸ	9	1	00	

19143.9019 sum of South Areas. 4245.4016 North do.

2)14898.5003

Acres 744)92501

4

Roods 3)70004

40

Rods 28)00160

Acres Roods Rods
Area 744 — 3 — 28

2. Calculate by RIGHT ANGLED TRIGONOMETRY, CASE I, or find by the table of difference of latitude and departure,\* or by the table of natural sines,† the northing or southing, easting or westing, made on each course, and set them down against their several courses in their proper columns, marked N. S. E. W.

Note. To determine whether the latitude and departure for any particular course and distance are accurately calculated, square each of them; and if they are right, the sum of their squares will equal the square of the distance, for the following reason: the latitude and departure represent the two legs of a right angled triangle, and the distance the hypothenuse; and it is a mathematical truth, that the square of the hypothenuse of any right angled triangle, is equal to the sum of the squares of the two legs.

3. If the survey has been accurately taken, the sum of the northings will equal that of the southings, and the sum of the eastings will equal that of the westings. If, upon adding up the respective columns, these are found to differ very considerably, the field should be again surveyed; as some error must have been committed, either in taking the courses, or measuring the sides. If the difference is small, a judicious, experienced surveyor, will judge from the nature of the ground, or shape of the field surveyed, where the mistake was most probably made, and will correct accordingly. the northings and southings, and the eastings and westings, may be equalled by balancing them, as follows: substract one half the difference from that column which is the largest, and add it to that column which is the smallest; and let the difference, to be added or substracted, be divided among the several courses, according to their length.

In Example I., the upper numbers are the northings, &c., as found by a table of difference of latitude and departure. The several columns being added, the northings are found to exceed the southings 47 links, and the westings to exceed the eastings 24 links; [47 being uneven, drop a link from the northings, and it becomes 46. Let half of this (23) be taken from the northings, and added to the southings;] likewise, take 12 links from the westings, and add it to the eastings. Take from the first course of the northings 12 links, from the second 7, and from the third 5; to the first southing add 7 links, to the second 10, and to the third 6; add to the first easting 3 links, to the second 3, to the third 4, and to the

t See the remarks preceding the table of natural sines.

<sup>\*</sup> For an explanation of this table, and the manner of using it, see the remarks preceding the table.

fourth 2; take from the first westing 5 links, from the second 4, and from the third 3. [These are the proportional corrections belonging to each, as found by calculation.\*] The lower numbers will then represent the northings, &c. as balanced.

4. These columns being balanced, proceed to form a departure column, or a column of meridian distances; which shows how far the end of each side of the field is east or west of the station where the calculation begins. This column is formed by a continual addition of the eastings, and substraction of the westings; or by adding the westings and

substracting the eastings: see Example 1.

The first easting, 20.74, is set for the first number in the departure column; to this add 24.38, the second easting, and it makes 45.12, for the second number; to this add 30.04, the third easting, and it makes 75.16, for the third number; to this add 9.56, the fourth easting, and it makes 84.72, for the fourth number; the fifth course being south, it is evident the meridian distance will remain the same, therefore place against it the same easting as for the preceding course; from this substract 39.95, the first westing, and it leaves 44.77, for the sixth course; from this substract 23.75, the second westing, and it leaves 21.02, for the seventh course; from this substract 21.02, the last westing, and it leaves 0.0 to be set against the last course, which shows that the additions and substractions have been accurately made. For as the eastings and westings equal each other, it is evident that the one being added and the other substracted, there will be in the end no remainder.

5. The next step in the process is to form a second departure column, the numbers in which show the sum of the meridian distances at the end of the first and second, second

and third, third and fourth courses, &c.

The first number in this column will be the first in the other departure column; to which add the second number in that column for the second in this; for the third add the second and third; and for the fourth the third and fourth; and so on, until the column be completed. See Example I.

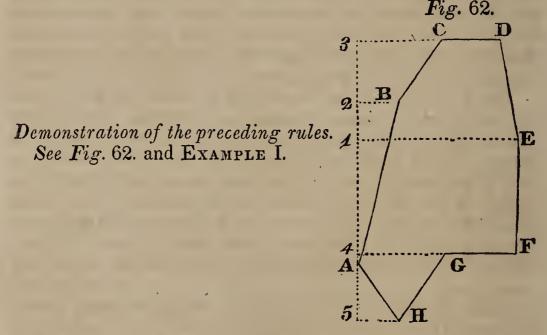
The first number to be placed in the second departure column is 20.74; to this add 45.12, and it makes 65.86 for the second number; to 45.12 add 75.16, and it makes 120.28, for the third number; to 75.16 add 84.72, and it makes 159.88 for the fourth number; to 84.72 add 84.72, and it makes 169.44 for the fifth number; to 84.72, add 44.77, and it makes

129.49 for the sixth number, to 44.77 add 21.02, and it makes 65.79 for the seventh number; to 21.02 add 0.0,

and it makes 21.02 for the eighth number.

6. When the work is thus far prepared, multiply the several numbers in the second departure column by the northings or southings standing against them respectively; place the products of those multiplied by the northings in the column of north areas, and of those multiplied by the southings in the column of south areas; add up these two columns, and substract the less from the greater; the remainder will be double the area of the field in square rods or square chains and links, which ever measure was used in the survey.

[In the preceding explanations, the meridian is supposed to pass through the extreme west angle of the field. It is best always to take the extreme east or west angle.]



The dotted line A 2 represents the northing, and the line 2 B the easting, made by the first course; these multiplied together, that is, 77.15×20.74=1600.0910, which is double the area of the triangle A 2 B, as is evident from the rule to find the area of the triangle, Prob. IX. Rule I. This number is to be placed for the first number in the column of north areas. The line 3 C represents the sum of the eastings made by the first and second courses, which is 45.12, the second number in the first departure column; if to this you add 20.74, the length of the line 2 B, you have 65.86, which is the second number in the second departure column, and which represents the sum of the two lines 3 C and 2 B. These two lines, with the line 2 3, which represents the

northing made by the second course, and the line BC, one of the sides of the field, form a right angled trapezoid. Now, by the rule to find the area of such a trapezoid, see Prob. X., 65.86×31.66=2085.1276, double the area of the trapezoid 2 BC3. Place this product for the second number in the column of north areas.

To the line 3 C add C D 30.04, that easting made by the third course, and you have 75.16, which is the sum of the eastings made by the three first courses, and the third number in the first departure column. To this add 9.56, the easting of the fourth course, and you have 84.72, the length of the line 1 E, which represents the sum of the eastings made by the four first courses, and is the fourth number in the first departure column. These two, viz., the lines 3 D 75.16, and 1 E 84.72, added together, make 159.88, the fourth number in the second departure column; which being multiplied by 49.15, the length of the line 3 1, which represents the southing made by the fourth course, will give double the area of the trapezoid 1 E D 3. The number thus produced is 7858.1020, which is to be placed for the first number in the column of south areas.

The fifth course being due south, it is evident the sum of the eastings will remain the same as at the end of the fourth course; that is, the line 4 F equals the line 1 E, which is 84.72. These added, make 169.44, the fifth number in the second departure column. This, being multiplied by 54.10, the length of the line E F, which is the southing of the fifth course as corrected in balancing, and the same as the line 1 4, will give double the area of the parallelogram 1 E F 4, which is 9166.7040, the second number in the column of south areas.

From the line 4 F 84.72, substract 39.95, which is a west course and it leaves 4 G 44.77, the sum of the eastings, or the meridian distance, at the end of the sixth course, and the sixth number in the first departure column. From this substract 23.75, the westing made by the 7th course, and you have 21.02, the length of the line 5 H, which is the meridian distance at the end of the seventh course, and the seventh number in the first departure column. The line 4 G 44.77, added to the line 5 H 21.02, make 65.79, the seventh number in the second departure column. This being multiplied by 32.21, the length of the line 4 5, which is the southing of the seventh course, will give double the area of the trapezoid 4 G H 5, which is 2119.0959, the third number in the column of south areas.

The line H 5, 21.02, is the westing of the last course, and

the last number in the second departure column. This being multiplied by 26.65, length of the line 5 A, and the northing of the last course, produces 560.1830, which is double the area of the triangle A 5 H, and the last number in the column of north areas.

Note. It will be observed that against the third and sixth courses there are no areas; the reason is, that these courses being one east and the other west, there is no northing or southing to be multiplied into them; regard can therefore be had to them only in forming the departure columns.

By inspecting the figure, and attending to the preceding illustrations, it will be seen that the three north areas represent double the area of the triangle A 2 B, the trapezoid 2 B C 3, and the triangle A 5 H, all of which are without the boundary lines of the field: also, that the three south areas represent double the area of the trapezoid 3 DE 1, the parallelogram 1 E F 4, and the trapezoid 4 G H 5; and that these include not only the field, but also what was included in the north areas. Therefore the north areas substracted from the south, the remainder will be double the area of the field, contained within the black lines.

#### ADDITIONAL DIRECTIONS AND EXPLANATIONS.

The northings and southings may be added and substracted instead of the eastings and westings; then there will be two latitude columns instead of departure columns, and the numbers in the second latitude column must be multiplied into the eastings and westings, and you will have east and west areas.

When the course is directly north and south, the distance must be set in the north or south column; when east or west, in the east or west column. There will therefore sometimes be no number to be added to or substracted from the number last set in the latitude or departure column; then the number last placed in the column must be brought down and set against such course; as in Example I. at the 5th course. It may also sometimes be the case, that there will be no number to multiply into the number in the second latitude or departure column; then that number must be omitted, and against such course there will be no area, as in Example I. at the 3d and 6th courses.

When the northings or southings, eastings or westings, beginning at the top, will not admit of a continual addition of the one and the substraction of the other, without run-

ning out before you get through the several courses, you may begin at such a course in the field book as will admit of a continual addition and substraction; and when you get to the bottom, go to the top, and you will end in cipher at the course next above that where you began.

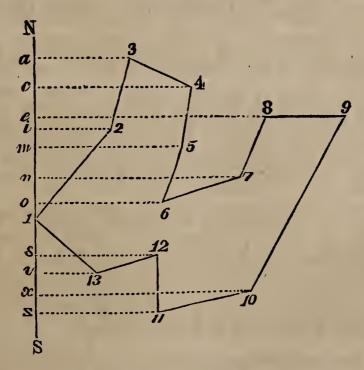
EXAMPLE II.

No.	Courses.	Dist.	N.	s.	E.	w.	1 Dep. Col.	2 Dep. Col.	North areas.	South areas.
1.	N. 36° 45′ E.	76.8	61.5		46.0		46.0	46.0	2829.00	
2.		56.0	51.7		21.4		67.4			
3.	S. 76 45 E.	48.0	• •	11.0	46.7		114.1	181.5	• • •	1996.50
4.	S. 15 00 W.	43.4	• •	41.9		11.2	102.9	217.0		9092.30
5.	S. 16 45 W.	40.5	1	38.8	• •	11.7	91.2	194.1		7531.08
6.	N. 75 00 E.	54.8	14.2		52.9		144.1	235.3	3341.26	
7.	N. 20 30 E.	41.2	38.6		14.4	. •	158.5	302.6	11680.36	
	East	64.8			64.8	• •	223.3	381.8		• • •
9.	S. 33 30 W.	141.2	<b>'••</b>	117.7		77.9	145.4	368.7	• • •	[4339 <b>5.99</b> ]
10.	S. 76 00 W.	64.0	• •	15.5	• •	62.1				3544.85
	North	36.0	36.0		• •		83.3		5997.60	
12.	S. 84 00 W.	46.4		4.9		46.1				590.45
13.	N. 53 15 W.	46.4	27.8		• • 1	37.2	00.0	37.2	1034.16	• • •

110 Acres, 2 Roods, and 23 Rods.

## DEMONSTRATION.

Fig. 63.



The area standing against the 1st course, is the triangle 12i, lying without the field.

That against the 2d course is the trapezoid 23ai, lying without the field.

That against the 3d course is the trapezoid 34ac, and it is a south area, lying partly within and partly without the field.

That against the 4th course is the trapezoid 45cm, and it is also a south area.

That against the 5th course is the trapezoid 56mo, and it is also a south area.

That against the 6th course is the trapezoid 67no, and it is a north area, a part of which is already contained in two different products. In this area, and in the two succeeding areas, all of that part of the figure which lies above the line o6, is considered void, and it may again be covered by both north and south products.

The area against the 7th course is the trapezoid 78en, and

it is a north area.

Against the 8th course there is no latitude.

The area against the 9th course is the trapezoid 9,10,ex and it is a south area.

That against the 10th course is the trapezoid 10, 11, xz, and it is a south area.

That against the 11th station is the parallelogram 11, 12, sz, and is a north area.

That against the 12th station is the trapezoid 12, 13, sv, and it is a south area.

That against the 13th station is the triangle 13,1,v, and it is a north area.

When the field is very irregularly shaped, it will often happen that parts of the same area will be contained in several different products in the column of areas. As often as a space is covered by a north product, so often will it be covered by a south product; but in the final result, the sum of one column being substracted from that of the other, will leave what is included within the boundary lines of the field.

This method of calculating the area of a field by the northings, southings, eastings, and westings, divides the field, with a certain quantity of the adjoining ground, into right angled triangles, right angled trapezoids, parallelograms, or squares, as may be seen by the figures. It may therefore with propriety be called RECTANGULAR SURVEYING.\*

### A USEFUL PROBLEM.

TO FIND THE TRUE AREA OF A FIELD WHICH HAS BEEN MEASURED BY A CHAIN TOO LONG OR TOO SHORT.

Calculate the area as if the chain was of a true length,

then institute the following proportion.

As the square of the length of the true chain; Is to the area, as found by the chain made use of; So is the square of the length of that chain; To the true area of the field.

#### EXAMPLE.

Suppose a field, measured by a two rod chain 3 inches too long, is found to contain 41 acres 1 rood and 33 rods, what is the true area.

As the square of 33 feet, the true length of a two rod chain; is to 41 acres 1 rood and 33 rods; so is the square of 33 feet 3 inches, the length of the chain used in the survey; to 42 acres and 13 rods. 33 feet=396 inches. 396×396=156816 square inches.

41 acres 1 rood 33 rods $\pm$ 6633 rods.

33 feet 3 inches=399 inches. 399×399=159201 square inches.

 $159201 \times 6633 \div 156316 = 6733$  rods.  $6733 \div 160 = 42$  acres 13 rods, the true area.

# PART II.

### LAYING OUT LAND.

PROBLEM I. To lay out any number of acres in the

form of a square.

Annex 5 ciphers to the number of acres, which will turn them into square links, the square root of which will be the side of the square in links.

Example I. It is required to lay out 810 acres in the

form of a square.

Answer. Each side of the square must be 9000 links, or 90 chains.

PROBLEM II. To LAY OUT ANY NUMBER OF ACRES IN THE FORM OF A PARALLELOGRAM, WHEREOF ONE SIDE IS GIVEN.

Divide the number of acres when turned into square links, by the given side; the quotient will be the side required.

EXAMPLE. What must be the longest side of a rectangle, which is to contain 25 acres, when the shortest side is 5 chains and 50 links?

Answer. 2500000÷550=4545 links for the longest side.

PROBLEM III. To LAY OUT ANY NUMBER OF ACRES IN A FIELD, 3, 4, 5, 6, &c. TIMES AS LONG AS IT IS BROAD.

Divide the acres when turned into square links, by the ratio between the length and breadth; the square root of the quotient will be the shortest side.

Example. It is required to lay out 100 acres 5 times as

long as it is broad.

Answer. 10000000÷5=2000000, the square root of which is 1414 links for the shortest side, and the longest will be 7070 links.

PROBLEM IV. To make a triangle which shall contain a given number of acres, being confined to a certain base.

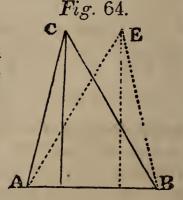
Double the given number of acres, to which, annex 5 ciphers, and divide by the base; the quotient will be the perpendicular height in links.

EXAMPLE. Upon a base of 40 chains, to lay out 100 acres

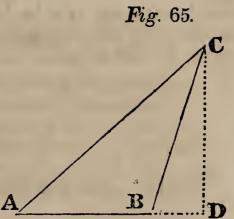
in a triangular form.

Answer. 5000 links, or 50 chains, will be the length of the perpendicular.

The perpendicular may be erected from any part of the base: thus, the triangle ABC, see Fig. 64, is the same as ABE, each containing 100 acres.



When the given base is so situated that a perpendicular of sufficient length cannot be erected therefrom, continue the base as from B to D, Fig. 65, from which erect the perpendicular D C, and complete the triangle A B C, which will contain 100 acres.



# PART III.

### DIVIDING LAND.

As different fields are so variously, and many of them irregularly shaped, and as they are required to be divided in many different proportions, it is difficult to give rules which will apply to particular cases. The business of dividing land must therefore be left, in a great measure, to the skill and judgment of the surveyor; who, if he is well acquainted with trigonometry, and with measuring land, will not find it difficult, after a little practice, to divide a field in such a manner as shall be desired. If he has before him a plot of the field, and knows the number of parts into which it is to be divided, and the proportion which each part is to bear to the others, he will readily find out where the dividing lines are to be drawn.

A few Rules and Examples will be given for the general instruction of the learner.

PROBLEM I. To cut off any number of acres from a square or rectangle.

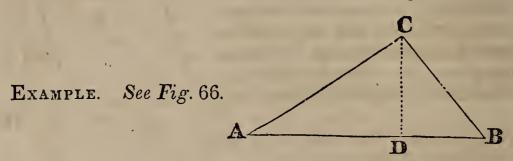
Say, as the whole number of acres in the field; is to the length of the square or length or breadth of the rectangle; so is the number of acres proposed to be cut off; to their proportion of the length or breadth.

PROBLEM II. To cut off any number of acres by a line from any angle of a triangle.

Measure the base, or side opposite the angle from which

the dividing line is to be drawn; then say, as the number of acres in the whole triangle; is to the whole base; so is the given number of acres; to their part of the base.

Fig. 66.

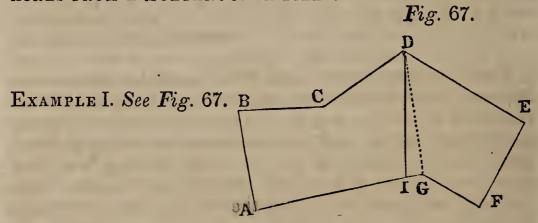


In the triangle A B C, which contains 48 acres, it is required to cut off 18 acres, by a line proceeding from C to the base A B, which is 40 chains.

As 48: 40::18:15

Lay 15 chains on the base from B to D, and draw the line C D. The triangle will then be divided as was proposed; B C D, containing 18 acres.

PROBLEM III. To take off any given number of acres from a multangular field.



Let A B C D, &c. be the plot of a field containing 11 acres,

from which it is required to cut off 5 acres.

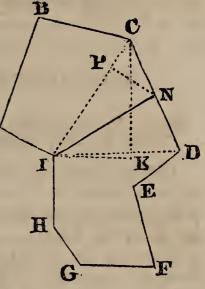
Join two opposite corners of the field, as D and G, with the line D G, (which you may judge to be near the partition line,) and find the area of the part DE F G, which, suppose, may want 140 rods of the quantity proposed to be cut off. Measure the line D G, which, suppose to be 70 rods; divide 140 by 35, the half of D G, and the quotient 4 will be the length of the perpendicular of a triangle, whose, base is 70 and the area 140. Lay off 4 rods from G to I, and draw the line D I, which will be the dividing line.\*

\*This explanation supposes DG and AG at right angles to each other. When they are not at right angles, the height GI must not be measured on the side of the field.—ED.

EXAMPLE II. See Fig. 68.

Fig. 68.

Let ABCD, &c. be a tract of land to be divided into two equal parts, by a line from I to the opposite side CD; to find arithmetically on what part of the line CD the dividing line IN will fall; or to find the distance CN.



# FIELD BOOK.

				I	Rods.	1					Rods.
AB.	N.	199	0′	E.	108	FG.	We	st			70.9
BC.	S.	77	0	E.	91	GH.	N.	360	0'	W.	47
CD.	S.	27	0	E.	115	HI.	No	rth			64.3
DE.	S.	52	0	W.	58	IA.	N.	62	15	W.	59
EF.	S.	15	30	E.	76			$\mathbf{A}$	cres	Rood	Rods.
						Ţ	Whole	area	$\iota$ 152	— 1 -	-25

Find the area of the part I A B C, according to Section III. page 64, as follows: set the latitude and departure of the three first sides, I A, A B, and B C, in their proper columns, in a traverse table; and place as much southing, viz. 109.1, equal to the line C K, and as much westing, viz. 71.7, equal to the line K I, as will balance the columns. This southing and westing will be the latitude and departure made by the line C I. The area of I A B C will be found to be 8722 rods, which is less than half the area of the whole field by 3470 rods, the quantity to be contained in the triangle I C N.

Find the bearing and distance of CI by RIGHT ANGLED

TRIGONOMETRY, CASE IV. as follows:\*

As C K, the southing of C I, 109, nearly - 2.037426 : radius - - - - - 10.000000 :: K I, the westing of C I, 71.7 - - - 1.855519 - - - - 11.855519 2.037426 : tangent course S. 33° 20′ W. - - - 9.818093

<sup>\*</sup> The mode given above is undoubtedly the most correct, but the use of the traverse table will save many figures. From that table the course and distance of CI, may be found at sight.—ED.

As sine course 33° 20′: departure K I, 71.7 :: radius	-	-	-		-	9.739975 1.855519 10.000000
: Distance I C 130.5	-	-		-6	-	11.855519 9.739975 2.115544

Note. In this way the course and distance may be found from any angle of a field to another.

Having found the line C I, divide 3470, the number of rods to be contained in the triangle I C N, by one half the line C I, viz. 65.25; the quotient will be the length of the perpendicular P N, viz. 53.18.

Now, by the bearings of CI and CD, it appears that they form an angle of 60° 20′; wherefore, in the triangle CPN, are given the side PN 53.18, and the angle at C 60° 20′, to find the hypothenuse CN.

As sine P C N 60° 20′		•	•	9.938980
: side P N 53.18	•	-	-	1.725748
:: radius -		•	-	10.000000
				11.725748
				9.938980
: hyp. C N 61.2		-	-	1.786768

Thus the dividing line must go from I to a point on the line C D, which is 61.2 rods from C. The bearing and distance of this line may be found by the directions given above for finding the bearing and distance of the line C I. Or, they may be found by oblique trigonometry, CASE III.

# ANOTHER METHOD OF FINDING THE DISTANCE C N.

Having ascertained the latitude and departure of the line C I, set them down in a traverse table; find the latitude and departure of the line C D, and place them in the table; the difference between the northing of the line I C, and the southing of the line C D, will be the southing of the line D I, viz. 6.6; and the sum of the eastings of those lines, as they are both easterly, will be the westing of the line D I, viz. 123.9. Proceed to calculate the area of the triangle I C D, which will be found to be 6522 rods, nearly.

Note. As in this triangle two sides and their contained angle are given, the area may be found by Prob. IX. Rule 4. page 42.

Having found the area of this triangle, proceed to find

CN according to Prob. II. page 75, as follows:

As the area of the triangle; is to C D the base; so is the quantity to be contained in the triangle I C N; to C N, its proportion of the base.

As 6522: 115:: 3470: 61.19.

# A THIRD METHOD OF FINDING THE DISTANCE C N.

To the logarithm of double the area to be contained within the triangle I C N, add radius; from this sum substract the logarithmic sine of the angle at C; and from the remainder substract the logarithm of the side I C; the last remainder will be the logarithm of the side C N.

The double area of the triangle ICN, is 6940; the angle

at C is 60° 20'; the side I C is 130.

Double area 6940 Radius	•			3.841359 10.000000
Sine I C N 60° 20'				13.841359 9.938980
Side I C 130.5				3.902379 2.115544*
Side C N 61.21		-	•	1.786835

Note. Radius may be added by placing a unit before the index of the logarithm for the double area, without the trouble of setting down the ciphers.

#### BY NATURAL SINES.

Divide the double area by the natural sine of the given angle, and that quotient by the given side; the last quotient will be the side C N.

Nat. sine of the angle at C 60° 20′ 0.86892 6940÷0.86892=7986.92 7986.92÷130.5=61.2

<sup>\*</sup> The log. of IC, as found by calculation on page 77, is employed, instead of taking from the tables, that of 130.5, which is not the exact length of IC.—ED.

From the above the following general rule may be drawn. To find the side of a triangle when the area is given, and also one of the sides, and the angle contained between the given side and the side required

To the logarithm of double the area add radius; from this sum substract the logarithmic sine of the given angle, and from the remainder substract the logarithm of the given side; the last remainder will be the logarithm of the side required.

OR, BY NATURAL SINES: DIVIDE THE DOUBLE AREA BY THE NAT. SINE OF THE GIVEN ANGLE, AND THAT QUOTIENT BY THE GIVEN SIDE; THE LAST QUOTIENT WILL BE THE SIDE REQUIRED.

### CONCLUDING REMARKS.

Other methods of surveying fields are taught by some authors on this subject. The preceding, however, will be found most useful in actual practice. Other instruments besides those mentioned in this book are sometimes used; such as the plain table, semicircle, perambulator, theodolite, &c. But of these instruments very little use is made in New England; and they are not often to be met with. For general practice, none will be found more useful than a common chain, and a compass upon Rittenhouse's construction.

It will be observed that in this work there is no descriptions of mathematical and surveying instruments. The compiler omitted such descriptions, from a belief that nothing which can be written on the subject will enable a person to understand them, without an actual inspection of the instruments themselves, and some instruction from those acquainted

with them.

The general principles here taught may be applied to the surveying of townships, roads, rivers, harbours, &c.

# APPENDIX.

OF THE DECLINATION AND VARIATION OF THE MAGNETIC NEEDLE, AND OF THE ATTRACTIONS TO WHICH IT IS SUBJECT.

THE declination of the needle is the number of degrees it deviates from the true north, either east or west. This differs in different places, and in the same place at different times. [At Hartford, Conn., the declination was, in 1829, 603' west of the true meridian of the earth; and was increasing by an annual variation of about 3'.]

The following method of ascertaining the variation, by the north star, has been adopted by many surveyors, as the most eligible to be practised on land. It was communicated to the compiler by Moses Warren, Esq., of Lyme, an experi-

enced surveyor, with permission to publish it.

The star, commonly called the north star, is not directly north, but revolves round the pole in a small circle, once in 24 hours.\* It can therefore be due north only twice in that period; and that is within a very few minutes of the time, when a star, called Alioth, in the constellation of Ursa major, or the great bear, is directly over or under it. There is also another star nearly in an opposite direction from the pole, called Gamma, in the constellation of Cassiopeia. When these three stars are vertical, the north star is very near the meridian; and when they are horizontal, it is at its greatest elongation, that is, at its greatest distance east or west of the pole, and on the same side as the star in Cassiopeia. The variation may be calculated when the star is on the meridian, or when at its greatest elongation; more accurately, however, at the latter period, because its motion be-

<sup>\*</sup> More exactly, 23 hours, 56 minutes, and 4 seconds.—ED.

ing then nearly vertical for some time, gives the observer

opportunity to complete his observation.\*

To find the elongation of this star in any latitude, its declination must be known: that is, its distance north of the equator. This being found, institute the following proportion:

As co-sine of the latitude; is to radius; so is co-sine of the

declination; to sine of the elongation.

The declination of the north star, January 1, 1810, was 88° 17′ 28″, and increasing at the rate of about 19 seconds

and one half annually.

In the following table, the elongation is calculated for ten successive years, ending with 1840, and for seven different latitudes. The calculation is made for the first of July, and of course gives the mean angle for the year.

TABLE SHOWING THE ELONGATION OF THE NORTH STAR.

<sup>\*</sup> The following figure exhibits a view of the relative situation of these stars, as they appear, when in a horizontal position; or when the north star is in its greatest eastern elongation.

<sup>†</sup> This angle is usually called azimuth.—ED.

The elongation for the latitude of the observation being calculated or taken from the above table, proceed to find its

range according to the following directions:

Take a pole, 18 or 20 feet in length; to the end of it fasten a small line; raise it to an elevation of 45° or 50°; and support it by two crotches of suitable height, to keep it firm in its place. At the end of the line, near the ground, fasten a weight of half a pound or more, which should swim in water to prevent the air from moving the line. Southward of the line fix a compass sight, or other piece of metal or wood, with a narrow, perpendicular aperture, at a convenient height from the ground, say about 2 or  $2\frac{1}{2}$  feet; and let it be so fixed that it can be moved a small distance east or west at pleasure. Let an assistant hold a light either N. E. or N. W. of the line, nearly as high as the range from the sight to the north star, in such a position that the line may plainly be seen; then, (the three stars above mentioned being parallel, or nearly so, with the horizon,) move the sight-vane east or west, until, through the aperture, the line is seen to cut the star; and continue to observe, at short intervals, till the star is seen at its greatest elongation. Let a lighted candle be placed in an exact range with the sight-vane and line, at the distance of 20 rods or more, which should stand perpendicularly, be made fast, extinguished, and left till morning. Then the sight-vane, the line, and the candle, will be the range of elongation, which observe accurately with a compass; and if the elongation be east and the variation west, the former must be substracted from the latter; and if they are both west, they must be added, and their difference or sum will be the true variation.\*

### OF THE ATTRACTION OF THE NEEDLE.

It is well known that any iron substance has an influence upon the magnetic needle, attracting it one way or the other upon the point where it would settle, were there no such attraction. A surveyor should therefore be careful to see that no iron is near the compass when taking a bearing. But as the earth, in certain spots, contains, near its surface, iron, or other minerals, which attract the needle, it will frequently

<sup>\*</sup> The author, in common with many writers, employs the term variation, as synonymous with declination. Variation is properly, however, the change of declination.—ED.

happen that it will point wrong. To ascertain whether this is the case, the surveyor, at each station, should take a back view of the one last left; and if he finds that the compass does not reverse truly, he may be sure, provided the compass be accurately graduated and placed horizontally, that he either made a mistake at the last station, or that in one or the other, or both of the stations, the needle was attracted from the true point. When he finds a place where he suspects there is an attraction, he should go a few rods backward or forward, and see whether the needle points differently. In this way he may prevent mistakes in his field notes, which would arise from putting down a wrong course. To take back sights is particularly necessary in running long lines, and laying out new lands, where the needle is the only thing to guide the surveyor.

By practice and experience, a knowledge will be acquired on this subject, and with regard to many other things in surveying, which cannot be taught by books; and after all the directions which can be written, the practitioner will frequent-

ly find occasion for the exercise of his own judgment.

A RULE TO FIND THE DIFFERENCE BETWEEN THE PRE-SENT VARIATION OF THE COMPASS, AND THAT AT A TIME WHEN A TRACT WAS FORMERLY SURVEYED, IN ORDER TO TRACE OR RUN OUT THE ORIGINAL LINES.

Go to any part of the premises, where any two adjacent corners are known; and if one can be seen from the other, take their bearing; which, compared with that of the same line in the former survey, shows the difference. But if one corner cannot be seen from the other, run the line according to the given bearing, and observe the nearest distance between the line so run, and the corner; and then work the following proportion:

As the length of the whole line, Is to 57.3 degrees,\* So is the said distance, To the difference of variation required.

#### EXAMPLE.

Suppose it be required to run a line, which, some years ago, bore N. 45° E., distance 20 chains, and in running this

\* 57.3 degrees is the radius of a circle (nearly) in such parts that the circumference contains 360.

line by the given bearing, the corner is found 20 links to the left hand; what is the present bearing of this line?

Ch. Deg. L.

Ch. Deg. L.
As 20 : 57.3 : : 20

100 20

2000 1146.0
60

2000)68760(34 Minutes.

Answer— 34 minutes to the left hand is the allowance required, and the line in question bears N. 44° 26′ E.

The compiler of this work acknowledges himself under obligations to George Gillet, Esq., Surveyor General of the state of Connecticut, for the following illustrations, remarks, and miscellaneous questions, considering them calculated to be useful to the learner, and the practical surveyor.

### PRACTICAL TRIGONOMETRY.

The learner must understand decimals, and the nature and use of logarithms, before he can make any proficiency in this branch. Difference of latitude is the distance between the parallels of the beginning and of the terminating point of a line, or of any number of lines, whether northerly or southerly. Departure is the distance between the meridians of the beginning and of the terminating point, or the distance made either east or west from any particular meridian on any course.

These distances are also called northings or southings,

eastings or westings, as different cases may happen.

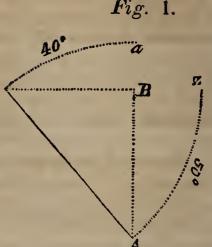
When a course and distance are given, the distance is the hypothenuse of a right angled triangle, of which the latitude and departure are the legs. The angle which the course makes with the meridian, is opposite to the departure. Substract the course from 90°, and the remainder will be the quantity of the angle opposite to the latitude.

# CASE I.

In the annexed triangle, the side AC, is given N. 40° W. 50 rods. The latitude and departure, or the northing and westing, are Crowniand

required.

A B is a meridian, or a north and south line. The angle at A contains 40°, and that at C, 50°, as appears by their respective arches. B C, is an east and west line, of course the angle at B contains 90°,



or it is a right angle. A C is made radius. From the point at A, the arch C a is described. From the point at C, the arch A z is described. B C is the sine of the angle at A, or of the arch C a, and A B is the co-sine. A B is the sine of the angle at C, or of the arch A z, and B C is the co-sine. Sines and co-sines lie within their respective arches. Each side is proportioned to its opposite angle, and each angle to its opposite side.

# TO FIND THE REQUIRED SIDES, TAKE THE FOLLOWING RULE.

For the latitude, make radius, the angle at B, the first term,—the logarithm of the side A C 50, the second; the sine of the angle at C, the third, and the fourth will be the logarithm of the latitude A B. For the departure, take the same first and second terms, the sine of the angle at A for the third, and the fourth will be the logarithm of the departure B C.

### SEE THEM WORKED:

As radius, - 10.000000 : side A C, 50 rods, 1.698970 : : sine of C, 50°, 9.884254	: side A C, 50 rods, 1.698970
Radius, 11.583224	11.507037 Radius, 10.000000
: Latitude 38.30 rods, 1.583224	d :departure, 32.14 rods, 1.507037

Required the latitu	ide and de	eparture of S. 28°, W	7.88 rods.
As radius -	10.000000	As radius, -	10.000000
: distance 88, logarithm,	1.944483	: distance, 88 rods,	1.944483
:: cosine of course 28°	9.945935	: distance, 88 rods, :: sine of the course 28	3° 9.671609
	11.890418		11.616092
	10.000000		10.000000
			t
: latitude, 77.70,	1.890418	: departure, 41.31,	1.616092
Required the latitu	ide and de	parture of N. 75°, E.	245 rods.
As radius, -	10.000000	As radius, -	10.000000
distance 245, -	2.389166		2.389166
: co-sine of course, 75°	9.412996		9.984944
	11 000100		10.264110
	11.802162		12.374110
	10.000000		10.000000

The logarithm of the distance may be set down in two places; and the sine of the course may be placed under one, and the co-sine under the other, and when they are added, the unit at the left hand, in each case, may be cancelled, which will be the same as substracting radius.

1.802162 : departure, 236.65,

# CASE II.

Fig. 2.

Suppose you run north from A to B, 220 rods; then east 150 rods to C. What is your course and distance from C to A? First find the course. In this case, make the side A B radius. With your dividers on the point at A, describe the arch Ba, then on the point at C, describe the arch Bz. In describing the last arch BC is made radius. Each arch contains as many degrees as its opposite angle.

: latitude, 63.41,

As the sides AB and BC, both lie without their respective arches, they are tangents. BC is the tangent of the angle at A, or of the arch Ba, and AB is the co-tangent. AB is the tangent of the angle at C, or of the arch Bz, and BC is the co-tangent.

Note. When an angle is required, a side must be the first term. When a side is required, an angle must be the first term.

To find the course from C to A, Fig. 2, adopt the follow-

ing rule.

Suppose yourself standing at the angle A; make the side AB radius, then state: as the log. of the side AB 220; is to radius; so is the log. of the side BC, 150, to the tangent of the angle at A. See the example worked. As log. of AB,

220—2.342423 : R. 10,0000000 : : log. B C, 150—2.176091 2.176091

> 12.176091 2.342423

: Tang. of A 34° 17′ 9.833668

In the column of tangents, under 34° against 17′, you will find the last term, or that which is nearest to it. The course from A to C is N: 34° 17′ E., or from C to A, S. 34° 17′ W. Next find the distance.

# CASE III.

TO FIND THE DISTANCE.

Make the side A C radius. From the B point at A describe the arch Cx. In this case, the side B C is a sine, as it lies within the arch. Take the following rule.

As the sine of the angle at A, is to the side BC, so is radius to the side

A C. See the example worked.

A.
9.750729
2.176091
10.000000
12.176091
9.750729
2.425362

Fig. 3.

Suppose you begin at a pine, and run north 125 rods to a hemlock, then east 216½ rods to a spruce, what is the course and distance from the spruce to the pine? By Case II. find the course, and by Case III. the distance. Suppose yourself standing at the pine, and making the northing radius, the proportion will be,

: tang. at the pine, 60°, 10.238548

The course from the spruce to the pine is S 60° W.

Note. As the easting is greater than the northing, the course is over 45°, therefore look at the bottom of the page to find it.

To find the distance from the spruce to the pine, make that side radius, and the proportion will be, as the sine of the angle at the pine; is to the easting; so is radius to the distance required: or, as the sine of the angle at the spruce; is to the northing; so is radius to the distance from the spruce to the pine.

As sine at the pme 60°: the easting 2165,: radius	9.937531 2.335458 10.000000	As sine at the spruce 3 : northing, 125, : radius,	0° 9.698970 2.096910 10.000000
	12.335458 9.937531		12.096910 9.698970
required dist. 250 rods,	2.397927	: required dist. 250 rods	2.397940

The following courses and distances of a survey are given, and the course and distance of the closing line are re-

quired.

Beginning at a maple tree, thence running as follows:—S. 80° W. 90 rods, N. 15° W. 95 rods, N. 85° E. 45 rods, S. 10° E. 40 rods, N. 85° E. 42 rods, to a beech tree. First, arrange the given courses and distances in a table, having a blank line for the course, distance, latitude, and departure of the closing line. Find by the traverse table the latitude and departure of each course and distance, and insert them in their respective columns as follows:—

No.	Courses.	Dist.	N.	S.	E.	W·
1	S. 80° W.	90.0		15.63		88.63
2	N. 15° W.	95.0	91.76			24.59
3	N. 85° E.	45.0	3.92		44.83	
4	S. 10° E.	40.0		39.39	6.95	
5	N. 85° E.	42.0	3.66		41.84	
				44.32	19.60	
			99.34	99.34	113.22	113.22

Substract the sum of the southings from that of the northings, and 44.32 will remain to fill the blank in the column of southings. Also, substract the sum of the eastings from that of the westings, and 19.60 will remain to fill the blank in the column of eastings.

These numbers or distances are the legs of a right angled

triangle, the hypothenuse of which is the closing line.

You are now standing at the beech tree. Make the southing radius, and to find the course, the proportion will be,

As the southing 44.32, radius, : the easting 19.60,	$1.646600 \\ 10.000000 \\ 1.292256$
	11.292256 1.646600
:: tangent of the course, 23° 51'	9.645656

The course of the closing line is S. 23° 51' E. which may fill the blank in the column of courses.

To find the distance, make the line from the beech to the maple, or the closing line, radius, and the easting will be a sine, then state,

As the sine of the course 23° 51′ 9.606751 : the easting, 19.60. 1.292256 : radius, 10.000000 11.292256 9.606751 : the distance, 48.48 rods, 1.685505

The distance is 48.48 rods, which may be entered in the blank space in the column of distances, and the survey will

be complete.

In the table of logarithms, against 484, in the column under 8, the last term, or the logarithm which is nearest to it, is found: 8 must be annexed to 484, and as the index is a unit, or 1, the two left hand figures are integers, and the others are decimals.

Former editions of this work contained several cases in Rectangular Trigonometry, which depended on secants for solution, but as secants are not retained in the tables which accompany this edition, those cases are also excluded from it. In Practical Surveying, no case will occur, which cannot be solved by these tables, nor can one occur, which depends on a solution by Rectangular Trigonometry, and which cannot be solved by the cases here treated of; therefore, secants are of no use to the practical surveyor.

Young learners meet with much perplexity in giving decimals their proper places when calculating latitudes and departures by inspection from the traverse table. This sub-

ject claims some attention.

What is the latitude and departure of N. 84° E. 70 rods and 2 links?

The distance is 70.08 rods. The decimal is 8.100 of a rod. Over 84° in the traverse table against 70, the lat. is

7.32, and the dep. is 69.62.

Against 8, over latitude is 0.84, so nigh a unit that one may be added to the second decimal in the lat., and over dep. is 7.98, so near 8 that that number may be added to the second decimal in the departure. Ans. lat. 7.33, dep. 69.70.

When a course departs 10° from a meridian, and it is required to add the lat. and dep. of 10 links or .40 of a rod to the lat. and dep. of the number of rods contained in the distance; under 10° against 40, the lat. is 39.39, and the dep. is 6.95. As the two right hand figures of the latitude are under 50, they may be rejected, and as the two right hand fig-

ures of the dep. are over 50, a unit, or 1, may be added to the left hand figure and the two last rejected, and the answer will stand, lat. .39, dep. .07. If the decimal is called 4 tenths, the separating point in both lat. and dep. may be carried over one figure, towards the right, adding a unit to the dep., and the right hand figure in each rejected, and the result will be the same. 75°, 5 links or 2 tenths; lat. 0.52, dep. 1.93; carry over the point, lat. .05; dep. .19. 65°, five links or two tenths, lat. 0.85, dep. 1.81. lat. .08, dep. .18. 81°, 15 links or 6 tenths, lat. 0.94, dep. 5.93; lat. .09, dep. .59. 28°, 2 links or 8-100, lat. .07, dep. .04. 7°, 15 l. or 6 tenths, lat. 60, dep. .07.

What is the latitude and departure on N. 10°, E. 6.5 rods? This need not be taken by two inspections, one for the integer and another for the decimal, but under 10°, against 65,

the latitude is 64.01, and the departure is 11.29.

The separating point may be placed between the two first figures in each, and as the fourth figure in the departure is 9, a unit may be added to the third, the fourth figure in each may be omitted, and the latitude is 6.40 rods, and the departure is 1.13 rods.

# PRACTICAL SURVEYING.

No. I.

EXPLANATION OF THE COMPASS, WITH DIRECTIONS HOW TO USE IT, AND HOW TO PROVE THE ACCURACY OF IT.

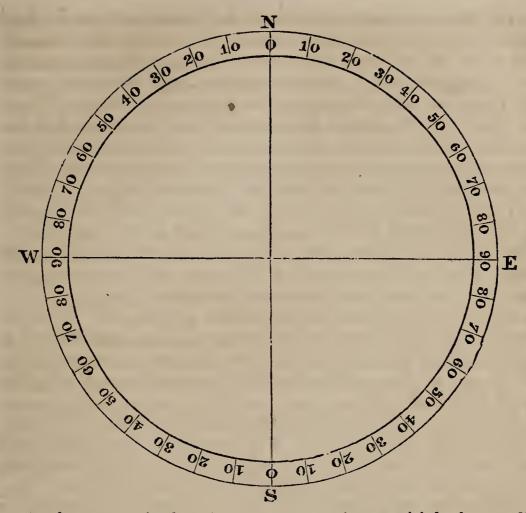
In surveying, each angular point is considered the centre

of a circle divided into 360 equal parts, called degrees.

The circle is also divided into four equal parts, called quadrants, by north and south, and east and west lines, crossing each other at right angles on the centre. Each quadrant is divided into nine equal divisions, and each division contains ten degrees.

The following figure represents the card, or the graduation

of the compass.



At the centre is the pivot or centre-pin on which the needle turns. The compass is fixed on the head of a staff, and it may be directed to any object on any course whatever, while the needle retains its polarity. Courses are counted either east or west from their respective meridians. To be more explicit, the angle which a course makes with its meridian, is written north or south, so many degrees east or west.

Fix the above circle to the four cardinal points, and suppose your course runs from the centre through the point 40, to the right of N.; the direction of it is N. 40° E., or in the opposite direction S. 40° W. To take this course, turn the north end of the compass to the object at the terminating point of the line. This will turn the point 40 at the left of N. directly against the north end of the needle, then count the degrees from N. to the north end.

Suppose your course runs from the centre through the point 80 below W., the direction of it is S. 80° W., or in the opposite direction N. 80° E. To take this course, turn the south end of the compass to the object, and the point 80 above W., will be at the north end of the needle, and that at 80 below E. at the south end of it. In like manner take all other courses.

In some compasses which are sufficiently correct for field surveying, when one end of the needle settles at any degree, the other end will not settle exactly against the same degree on the opposite side. Even compasses of the first rate, when they are not well levelled, are liable to this error. Therefore, all courses should be taken from the same end of the needle, which may be the north end. For example, suppose your course is southeasterly or southwesterly, direct the compass to the object, and at whatever degree the north end of the needle settles, enter it in your field book, even if the south end differs a few minutes from that degree. Also keep the same end of the compass northerly and southerly on courses in that direction, and the same end easterly and westerly in the latter direction.\*

By following these directions, the survey will be taken more correctly, than when the ends of the compass are frequently changed, and the northerly courses are taken by the north end of the needle, and the southerly courses by the

south end of it.

When a needle is well magnetized, the inside of the cap smooth, and the centre-pin nicely pointed, the needle will traverse lively and long: but before it stops at the true point,

will have an almost imperceptible tremulous motion.

When the needle settles quick, by giving the compass or the staff a light rap, it will commonly move a little, sometimes a quarter, a half, or a whole degree. This is certain evidence that something is out of order. Either the needle is not well magnetized, the inside of the cap is rough, or the centre-pin is blunt, which causes friction. The centre-pin ought to be as nicely pointed as a fine sewing-needle. Whether the compass is in order or not, the rap should be given after the needle has settled.

The centre-pin is the part of a compass which fails first The point is easily broken or blunted, and is always in danger. When the point is injured, it is not easily renewed so as to be equal to its first state. Therefore, too great care

cannot be taken of a good compass.

When a new compass is procured, it may be recommended to have one or more extra centre-pins with it, that when one

fails another may be in readiness.

To prove the accuracy of a compass, set each end of it to some distant object at every ten degrees around the circle. If, in every instance, each end of the needle settles at the

<sup>\*</sup> This practice has been recommended by the most celebrated mathematical instrument makers.

same degree on the opposite side, the compass is accurate, and is of the first rate; but if there should be found a difference of five minutes on a part or around the whole circle, the compass would be considered as one of the second rate, and by following the foregoing directions, a survey might be taken with it to a good degree of accuracy.

A compass which does not come within one or the other of the foregoing descriptions, ought not to be used on valuable land.

When a compass is not in use, it should be placed where it can have no motion, and the needle should be left on the centre-pin. By keeping its polarity, the magnetic power of

the needle will strengthen rather than weaken.

Compasses differ in their directions. Those of the first rate have been known to vary within the space of a quarter or a third of a degree, when no defect could be discovered in the mechanical part of them. As correct a survey may be taken with one as with another of this description. The question then naturally arises, which of these varying compasses is right? The answer is, all are right; neither of them points directly to the poles of the earth, except on the line of no declination.\* All that can be said of them is, that one makes a greater declination than another, and that which makes the least, cannot have the preference. It has also been ascertained, that different needles do not point alike at the same place. French writers on magnetism have treated on this subject.

It was well known to the celebrated Rittenhouse, that his compasses did not agree, and he was never satisfied as to the To remedy this defect, if it can be called a defect, he constructed his compass with a nonius, or vernier scale, (as some term it,) that all of them might be so regulated by a meridian as to agree. The meridian should be established by the motion of the heavenly bodies, and made permanent by durable monuments. All courses, which are matters of record, ought to be taken from the true, instead of the magnetic Such meridians should be established at convenient distances from each other, so that, whenever a survey is to be taken in the vicinity of one of them, a surveyor might set his compass on it, and note the declination found, and that declination, together with the meridian from which it was taken, should be inserted in the deed, or instrument, by which the land is conveyed, and should be a part of the record. This would assist a surveyer, at any future period, in retracing those lines, by setting his compass on the same meridian, and

<sup>\*</sup> As compasses differ in their direction, they will differ in locating this line.

allowing the difference in declination since the preceding survey. This would tend greatly to the security of landed property, and it is the only method by which magnetic courses can be regulated. Without this regulation, one correct compass may be used to as good advantage as another. So Dr. Rittenhouse viewed the matter: so the common practice of the country has established it.

# No. II.

### ON THE IRREGULARITIES OF THE MAGNETIC NEEDLE.

By a statute of this state, applicants for the appointment of county surveyor, are required to be well skilled, in point of science, in the theory of the most approved method of surveying lands. It is also as necessary that they should be as well skilled in practical surveying. Practical knowledge must be acquired by experience, but no one can have a thorough knowledge of correct practice, without being acquainted with the imperfections of the magnetic needle.

It is supposed, by most people, that this instrument, in all places, points directly to the poles of the earth, and that its direction remains as permanent as the poles themselves, an infallible guide.\* This is a mistaken idea. A few remarks on this subject will here be offered, and some facts respecting it stated.

\* There is one line around the globe on which there is no declination. The general course of this line, on this side of the globe, is from northwest to southeast, but it is crooked and irregular in its course. This line is not stationary, but is ever changing its position, and notwithstanding the great variety of its directions, it never crosses itself. According to Dr. Holly's chart, made in 1700, this line crossed the meridian of London in 55° south latitude, crossed the equator in 17° west longitude; from thence by various windings to the island of Bermuda; from thence nearly a west course, until it struck the continent near Charleston, in South Carolina.

About 1756, another chart was made, when the line had fallen so far to the west, that it struck the continent near the coast of Florida. On the east side of this line, the magnetic needle points to the west of north, and on the west side, it points to the east of north, and a regular increase of either east or west declination is found from it on its opposite sides.

The line of no declination now runs through Pennsylvania, and through the eastern part of Virginia and of North Carolina, and it leaves the coast at Cape Hatteras.†

At New Orleans, in 1813, the declination was east about eight degrees. The same year, an article appeared in a Philadelphia paper, from which the following was extracted:

At Philadelphia, "1701, declination 8° 30' W.; in 1793, 1° 30' W.;

Notwithstanding the utility of the magnetic needle, it cannot be relied on, when great accuracy is required, on account of the irregularities to which it is subject, viz., its annual and diurnal variations, and, what is the cause of still greater perplexity, its local attractions. When an old course is given to renew a line, it cannot be depended on, on account of the change in declination, between the time of the first running, and the renewal of it.

1794, the needle was observed to recede to the west; 1804, 2° W.; 1813, 2° 27′ W.;" and the west declination was then increasing. According to observations made at Albany, by the late Mr. De Witt, Surveyor General of the State of New York, for many years, the needle has declined to the west.

Observations made at Yale College, New Haven, and by Nathaniel Goodwin, Esq., of Hartford, agree with those of the late Mr. De Witt.

In June, 1805, the writer commenced observing the declination of the magnetic needle, at Hebron, in Connecticut, and he has continued his observations to the present date, June, 1835. The same compass, with the same needle, has been set at the same place, and to the same object. During that period, the north end of the needle declined to the west 1° 20′. At the former date, the declination was 4° 50′ W. The annual motion of the needle has not been uniformly steady. In some years it was more rapid than in others, and, in one or two instances, for a period of three or four years, none, except the diurnal motion, could be discovered. The west declination is still increasing.

While at so many places in the northern states, and at many more which might be mentioned, the west declination has increased, at Salem, in Massachusetts, according to the observations of Dr. Bowditch,

it has steadily decreased.

In 1580, at London, the magnetic needle pointed eleven degrees and a half to the east of north, which proves that the line of no declination

was then east of that place.

The east declination diminished until 1657, when the line of no declination arrived there, and passed by; of course, west declination commenced, and at the close of the last century, it had increased to twenty-four degrees.

The line of no declination must have made rapid progress through the Atlantic, and through a great part of the United States, to have arrived at Charleston in 1700, and at the coast of Florida in 1756

rived at Charleston in 1700, and at the coast of Florida in 1756.

It is unaccountable, how the west declination at London should increase, while at Philadelphia it diminished, when both places were on

the same side of the line of no declination.

The mystery is solved with equal difficulty, how the west declination at Salem should diminish, while at Philadelphia, Albany, New Haven, and at Hartford, it increased. The declination of the needle has long been a subject of much perplexity. Observations have been made in abundance. Many facts have been ascertained, but they are not reducible to system.

The polarity of the needle, with its variations and irregularities, is a hidden mystery, which is never to be searched out by man. It is sufficient in itself, without any other evidence, to cause the reflecting mind to wonder at, admire, and adore the wisdom, knowledge, and

power of Him, who planned, and who still directs it.

No annual rate can be fixed on as a certain rule for the declination of the needle, as its motion is much more rapid in some years than in others. By observations made at London, during a period of more than two hundred years, it appears that, in some years, the motion of the needle was rapid, in others, but little could be discovered, and, in some years, the motion was retrograde. There is no regularity in its motion

at any place, for any length of time.

The diurnal motion of the needle has long been known. As the sun rises in the forenoon, it has an effect on the unknown something which gives polarity to the needle, and turns the north end of it to the west. In the afternoon and night following, the needle returns to its position. Observations for the diurnal motion have been made in abundance, both in Europe and America. The result on both continents has been nearly the same. In summer, about a sixth or a quarter of a degree is usually found. In winter, but very little can be discovered. Perhaps, in a hot climate, the diurnal motion may be greater.

Local attraction is found oftener in hilly, broken lands, filled with ledges, than in level, feasible land, where there are no ledges. As the sources of attraction are generally unknown, and are out of sight, their situation should be determined by experiment. They sometimes cause the needle to deviate more than a degree, and often occasion a more trifling inaccuracy. In some instances, differences have been found, of more than five degrees, within the distance of forty rods.

Although the magnetic needle is not that infallible guide which most people suppose, yet it is a very useful instrument, and, in our country, cannot be wholly dispensed with in land surveying; but the surveyor who is best acquainted with it,

will make as little use of it as he can.

# No. III.

## ON PRACTICAL SURVEYING.

Surveying is a branch of business which will admit of dilagence, but it will not bear to be hurried. Sufficient time must be allowed to take courses, measure distances, and to make calculations correctly, even if the employer does not see the necessity of being so particular.

In taking a survey, go around with the sun, or keep the land which you survey on your right hand, not that you can work more correctly, or that it will have any effect in plot-

ing or in calculating, but when you put your courses and distances on your map, they will follow around from the left to the right, as you perform any other writing, and your map will appear to better advantage than when you write against courses and distances.

Wherever you begin, set your compass on the first angle,

and cause a stake or a flag-staff to be erected at the next.

If the first bound is a rock, erect a stake on it, and set your compass any where between the two stakes, or you may go back of the first angle, and take the range of the stakes.

When the boundary line is not straight, place the flag at the first angle, and go forward to a convenient place for the

next, and take your course by a back sight.

When a line is of such a length that you cannot see the end, and do not know the exact direction of it, leave a flag at the beginning, and go forward as far as you can have a fair view of it, and set your compass to the flag. Pursue that course to the end, and if your strike the bound, you need not boast of superior skill, for it will be by accident. A line run in this manner, is commonly termed a random line.

When the course of a random line is not in a direction to the bound, continue it to a point from which, by turning at a right angle, you will strike the bound, then measure the distance from the end of the random line to the bound, and this distance and the length of the random line will be the legs of a right angled triangle, the hypothenuse of which will be the true distance, and the bearing of the hypothenuse, the true course.

When the course of a random line is northwesterly or southeasterly, and it strikes to the right of the bound, the angle formed by the true and the random line, must be added to the course of the latter, but if to the left, it must be substracted.

When the random course is northeasterly or southwesterly, and it strikes to the right of the bound, the angle must

be substracted, but if to the left, it must be added.

When a line crosses a hill, cause a stake or flag to be erected at each end of it, and set your compass on the top of the hill, directly between them. If bushes or a hedge obstruct the sight on the line, make an offset at each end, or take the course by a random line.

When a distant tree near the line can be seen at the beginning of it, the bearing of the tree may be taken, and the

distance measured, and from the tree to the bound, and the bearing of the bound from the tree, may be taken by a back sight, and the course and distance may be calculated by a traverse.

#### EXAMPLE.

Suppose from the beginning of a line, a tree bears N. 5° W. and the distance is 50 rods; from the tree to the end of the line, is N. 5° E., 50 rods, the course of the line is north,

and the distance is 99 rods and 151 links.

When a line crosses water which cannot be measured with a chain, cause a stake to be erected on the opposite side, directly in the line. Then turn from the line at right angles, and measure until the course on which you ran from the line, and the bearing of the stake, form an angle of 45°, then the distance from the angle to the point of turning off, and from that to the stake, will be precisely the same, which may be added to the distance already found.

If it is not convenient to measure so far as to form an angle of 45°, stop at any proper distance, and take the bearing of the stake, and having ascertained the angle, calculate the distance across the water by the following proportion. As the sine of the angle at the stake: is to its opposite side::

so is the co-sine of that angle: to the side required.

#### EXAMPLE.

Suppose the bearing of the stake is N. 84° W., you may turn to the right or to the left; if to the former, your course will be N. 6° E., and if you measure 16 rods, and then take the bearing of the stake, which may be S. 74° W., the angle at the stake will contain 22°. State the question as follows:

: Dist. across the water - 1.597711 39.6 rods

If it is not convenient to turn from the line at right angles, turn at an acute or an obtuse angle, measure a suitable distance, take the bearing of the stake, and calculate the distance by oblique trigonometry.

### EXAMPLE.

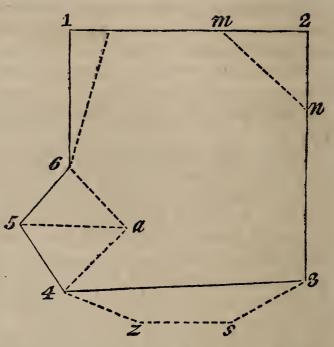
Suppose, on the same line you turn and run N. 27° W. 15 rods and 3 links, the stake on the opposite shore will bear S. 74° W. The angle at the stake will contain 22°, that at the point of turning from the line, 57°, of course the other angle will contain 101°. In this case, all the angles and the side opposite to that at the stake, are given. The distance across the water may be calculated by the first case of oblique trigonometry.

When a line crosses a ledge too high and too steep to be measured with a chain, whether the ascent or descent is before you, erect a flag at the top of it, take a station at the bottom, and ascertain the distance by the method of ascertaining it across the water, which will give the base of the hill from your station to a point directly under the flag.

In taking courses, on account of local attractions, the compass should be set at least twice on each line, even if you have a fair view of the whole length of it. Should there be a difference in the traverse of the compass at the two places, a third should be selected. Should the compass traverse alike at two places, the surveyor may conclude that he has found the true course, but when no two places are found where the compass has the same traverse, the surveyor should enter a medium course in his field book, noting such courses, as he may still have occasion to correct them in his calculation.

If, in such cases, he is at a loss what course to enter in his field book, and suspects that some minutes may be added to, or substracted from the course which he enters, he should prefix to such courses the sign of addition or substraction, as the case may be, which will often assist him in balancing his surveys. It would be no easy matter to describe all the different methods which may be selected in different cases in taking the field work of surveys. An example of only one case will be given here, which is represented by the following figure.

The survey was begun at the corner numbered 1. The corner numbered 2, was in a pond. The course and distance were taken from 1 to m; then from m to n. The angle at 2 was a right angle; of course there was a right angled triangle, wherein the angles and hypothenuse were given to find the sides m2 and From n to 3, the course and distance



were taken on the line. The next line ran through a thicket in a swamp. Courses and distances were taken from 3 to s, thence to z, thence to 4, and the course and distance of the line 3—4 were calculated by a traverse from those courses and distances. At the angle 5, a tree stood on a high clump of rocks, inaccessible on either line terminating at that point. The course from 4 to 5 was taken at 4. Next, the course and distance were taken from 4 to a, and from a the course was taken to 5. Next the course and distance were taken from a to 6, and from 6 the course was taken to 5. Two oblique triangles, with the angles and one side in each, were given, to find the side 4—5 and 5—6, which give the base of the hill.

The closing line ran through thick bushes and water, and the course and distance were taken on the dotted line to the line 1—2, at a point twenty rods from 1. The course and distance of 6—1, were calculated accordingly.

Whenever a line runs through or over a place where it is difficult to take either course or distance correctly, if, by taking a traverse around, at a little distance from the line, the surveyor can have level, cleared land, and then calculate the true course and distance from the courses and distances of the traverse lines, he will be more likely to ascertain the correct course and distance, than he would by attempting to run on the line. By practice and experience, a method for taking courses and distances, in all cases, will become familiar.

In a hilly country, the two-pole chain is preferable, and is more commonly used, because it can be better levelled.

In measuring hills and inclined surfaces, the horizontal distance must be taken. A plummet should be suspended from the end of a chain when it is levelled.

When hills are very steep, the surveyor should assist the chainmen, and when the best is done in levelling and plumbing the chain, judgment must frequently be called into exercise.

Even when elevations and descents are easy, there is danger of making too much measure. In such cases, chainmen often make allowances, but the surveyor will do better to keep them to close measure, and from the shape of the ground, judge what allowances ought to be made. An experienced, judicious surveyor, will form a more correct judgment in such cases, than inexperienced men.

If a surveyor is acquainted with the rise or descent of hills, the traverse table will aid him. For example, from the surface of a hill which rises on an angle of five degrees, one link

for every ten rods may be deducted.

Particular care must be taken to have the chain carried on a straight line. When a tally is ended, and the hinder chainman carries forward the sticks, they must be counted, When on counting the sticks it is discovered that one is lost, the chainmen should not leave the chain and go back to find it, but, from the last mark, should measure back to the point where the tally commenced, to see whether the full tally was measured, or whether one chain was lost from it. Many blunders have been left undetected by not taking this care. A careful, accurate chainman, never loses a stick, or miscounts a tally.

Distances may be taken by chains and links, or by rods and decimal parts, as best suits the surveyor. When a survey is calculated by chains and links, the numbers by which the process is performed, are smaller than when it is calculated by rods and decimal parts. Every method by which the

numbers are diminished, is an improvement.

Young surveyors should practice much for their own instruction, and should make correct practice familiar, before

they offer their services.

A young surveyor should bear in mind, that if he is detected in one error in the beginning of his practice, it will be more to his disadvantage than to be detected in two, when he shall become well established. If an error is committed in a survey, it is not against the surveyor, provided he detects and corrects it; but if he cannot do this, it is sufficient evidence of his deficiency in point of knowledge and skill.

# No. IV.

# DIRECTIONS FOR RUNNING AND ESTABLISHING LINES.

Many people suppose that a surveyor, at the beginning of a line, by intuition, or by some magic art, can set his compass directly to the terminating point, whatever obstructions may intervene, and that he needs no assistance; but this is a mistaken idea.

In running a line of considerable length, a surveyor should have two assistants to carry the chain, two to carry flags, in whose ability and correctness he can confide, and a fifth to carry an axe. If the surveyor is not furnished with such a number of assistants, his employer need not place too much confidence in his work.

The flag staves should be as much as two and a half or three inches in diameter, or what would be better, two strips of a board of that width, and seven or eight feet in length. If they are not so wide, they cannot be seen through the sights of the compass at any great distance. On one end of each staff, a flag, either white or red, of a yard in length, should be wound tight, and not left to hang loose and flutter in the wind. The latter colour will be more clearly seen through bushes, especially when the ground is covered with snow, and the brighter the colour the better. Being thus manned and equipped, at the beginning of a line, he must set his compass as near the true line as he can, or, he may set up one of the flags at the place of beginning, and go forward as far as he can have a view of the back flag. There set his compass on the random line, and send the other assistant as far forward as he can conveniently see the flag. When each flag is clearly seen through the sights of the compass, the back flag must be brought forward, and placed where the compass In this manner he must proceed on his random line, taking care each time he sets his compass, to turn the sights to the back flag. Great care must be taken to keep the flags perpendicular; also, the surveyor must keep the staff and the sights of the compass perpendicular. A little leaning of the flags, or turning the sights of the compass from a perpendicular, will make a crooked line. In taking his sights to the flags, he must look as near the ground as he can, and when practicable, the flag should be turned downwards, on account of the danger of being leaned when kept up.

All obstructions, such as bushes, brush, &c., must be cleared away. The random line must be measured, and at con-

venient distances, perhaps at every twenty rods, stakes must be set directly in it. Every stake must be numbered, that no mistake may be made in calculating, when they are afterwards removed and placed on the true line. If, in the course of the random line, the needle does not traverse as at first, or does not traverse alike at different places, no regard should be paid to it, the flags must direct the course; neither should the surveyor be turned aside or terrified by the cry of either of the parties, you are wrong, you are wrong, (for he will most certainly hear it,) but he must continue his random line, until, turning at right angles, either to the right or to the left, as the case may be, he can exactly strike the bound, or the point where a bound is to be erected; there he may stop, and measure the distance from that place to the bound. He may then calculate the course and distance of the true line, as before taught; but for setting the stakes in the true line, he may take the following directions.

Suppose the whole length of the random line is 200 rods, and the distance from the termination of it to the bound is 90 links, the calculation for setting the stakes on the true line may be made thus:—As the whole distance: is to 90 links: so is the distance of any stake: to the distance that such

stake is to be moved.

If the stakes are 20 rods apart, the answer is, the first stake is to be moved nine links, the second 18 links, and so on, adding nine links at each stake, until the whole are moved at right angles from the random to the true line. Many crooked lines and consequent disputes between farmers, have arisen from the want of this care and attention. When a long line is to be run over a number of ridges, and across intervening valleys, it should first be run and established from one ridge to another, and the intermediate spaces in the valleys may be taken afterwards. By taking long sights, there will be less danger of turning from a straight line.

In all cases, the forward flag should be carried as far as it can be distinctly seen, unless it is at the termination of a

line.

On account of the irregularity of the magnetic needle, the difference between compasses, and the incorrect manner in which most of the former surveys were made, no rule can be given which may be relied on, with certainty, in renewing lost bounds. In such cases, the best evidence must be taken which can be produced. When an old line is to be renewed, where the bounds have been lost, the surveyor may verify or prove his accuracy in various modes. If he finds, for example, that the lots on each side of the line contain their due

quantity, or possess their full width, he will have reason to believe that the line is accurately run; if not, he may allow for the excess or deficiency in either of these lots, and thus discover the true position of the line.

It would be difficult to mention all the circumstances which may govern, or which may serve as evidence in such cases.

# No. V.

#### ON BALANCING SURVEYS.

In every survey which is taken without an error, either in courses or in distances, the sum of the northings will equal that of the southings; and the sum of the eastings that of the westings; but this is not always an infallible proof that the survey is accurate, for two errors may be committed, one of which will exactly balance the other, which no rule will de-

tect; but such cases do not often occur.

In practical surveying, it is next to an impossibility, in any case, to work so correctly that the survey will exactly close without some correction. The difference between the two columns of latitude, and between those of departure, are the legs of a right angled triangle, the hypothenuse of which will be the distance which the survey will fail of closing. In a survey of one hundred acres, whatever may be the number of the angles, the difference between the two columns of latitude, and the two columns of departure, ought not to exceed a rod for each, but to come within those limits, if possible.

If, in such a survey, either of the differences should exceed a rod, where the land is valuable and easily surveyed, it would be better to take a re-survey, or so far as to detect the

error

These differences, as before taught in this work, must be balanced before the column of meridian distances can be

formed, or a correct plot of the survey be drawn.

The small differences between the columns in surveys which are substantially correct, commonly arise from an excess of measure, on account of the irregularity of surface, and from errors of the compass, caused by local attraction, and diurnal motion.

Some authors have given rules for balancing surveys, which, in theory, appear plausible, but, in practice, they are not with out exceptions.\* In correction, these rules are indiscriminately applied to every line in the survey, which pre-

<sup>\*</sup> It is argued, by theorists, that by these rules all will be agreed. This is admitted, but then, all may be agreed in error.

supposes that a proportional error must have been committed on each and all, both in courses and in distances; when in almost every survey, a part of the lines are on land so level and so clear from obstructions of any kind, that if the surveyor and chainmen attend to their business, they will not be likely to commit much error on them, while other lines on other parts of the same survey are attended with so many difficulties, that when they have done their best, it will scarcely be possible for them to avoid some error, and the surveyor who takes the survey will best judge on what lines the errors were committed, and whether they were in the courses or in the distances. In all cases, the corrections should be made on the lines containing the errors.

When the errors are in the courses, they should be corrected, and when the errors are in the distances, the correction should be in them, or the correction may be in both courses and distances, as the surveyor may judge proper.

Surveys are commonly balanced by substracting half the sum of the differences, from the numbers in the larger col-

umns, and by adding them to those in the less.

This, in most instances, is a correct method, but in certain cases, there are exceptions to it. For example, the boundary lines of three sides of a farm are on level land where there are no obstructions. The other side is on rough land filled with broken precipices. In such a case, most, if not all the correction, should be on the lines on the rough side. In some instances, most of the error may be in the course of a single long line.

It is not uncommon on high hills that the traverse of the needle differs a quarter or half of a degree, or more, from its traverse in valleys and on plains below. In such cases, courses should be corrected. In general, the compass is subject to more error than the chain. As rules cannot be given for correcting surveys in all cases, this must be left in a great measure to the judgment and experience of the surveyor.

As a general rule, corrections should be made principally on long lines, and the correction may be in proportion to the difficulties with which the surveying of them is attended.

When a course is north or south, or east or west, or near either of those points, a few minutes may be added to it or substracted from it, when necessary to favour the balancing. If the distance is of considerable length, it is probable that the course may contain some error.

When a course is nearly equidistant between any two of the four cardinal points, if the correction of it increases the latitude and diminishes the departure, or if it diminishes the latitude and increases the departure, so as to favour the balancing, there is double evidence that the course contains some error. If by diminishing the distance on such a course, both the latitude and departure are so diminished as to favour the balancing, it is good evidence of an excess of measure.

In correcting surveys, there is less danger from diminishing distances than there is from increasing them. Cases may occur in which distances may be increased, but the surveyor

should be very cautious about it.

As it is of importance that surveys should be correctly balanced before they are calculated, and as the work is commonly attended with some difficulty, a few examples are given for the assistance of the student. In each survey, the courses and distances are entered in the tables as they were taken in the field.

EXAMPLE I.

No.	Courses.	Dist.	N.	S.	E.	W.
1	N. 40° 30′ W.	53.0	40.30			34.42
2	N. 10 15 E.	74.4	73.21 .00		13.24	
3	S. 85 30 E.	125.5		9.85 10.25	125.11	
4	S. 7 15 W.	71.8		71.22		9.06
5	S. 2 15 E.	31.2		31.18	1.23	
6	N. 84 00 W.	35.5	3.71 .50			35.31
7	W.	40.0		.10		40.00
8	S. 80 00 W.	21.0		3.65 .75		20.68
			117.22	115.90	139.58	139.47
	Balanced,		116.70	116.70	139.58	139.58

The difference between the sum of the northings and that of the southings is one rod and 8 links, and the difference between the sum of the eastings and that of the westings is  $2\frac{3}{4}$  links. The taking of the course on the third line was attended with difficulty, and probably it contains some error, therefore, more than a proportion of the correction is made on the southing of it. There is also evidence that the first course contains some error, as the diminishing of the northing and the increasing of the westing favours the balancing. Twenty links are added to the different southings, and thirteen links are substracted from the different northings

Where corrections are made, the upper numbers are of no further use. If the corrections are made with red ink, they will all be seen at one view, and the work will appear hand-

somer. This was Mr. Flint's practice.

EXAMPLE II.

No.	Courses.	Dist.	N.	S.	E.	W.			
1	N. 5° 00′ E.	44.4	44.23		3.86 .75				
$\frac{1}{2}$	E.	66.6	.22		66.60				
3	N. 20 00 E.	22.6	21.23		7.72				
4	S. 80 00 E.	59.0		10.25	58.10				
5	S. 8 15 W.	57.0		56.41 .30		8.18			
6	N. 85 30 W.	41.4	3.25			41.27			
7	S. 45 00 W.	28.5		20.15		20.15			
8	S. 7 00 E.	24.4		24.22	2.97 .90				
9	S. 80 15 W.	38.2		$ \begin{array}{r} \hline 6.47 \\ .35 \end{array} $		37.65			
10	W.	20.4				20.40			
11	N. 12 30 W.	49.2	48.04	d		10.65			
	12 30		116.75	117.50	139.25	138.30			
1	Balanc	ed,	117.12	117.12	138.77	138.77			
'	10*								

EXAMPLE III.

No.	Courses.	Dist. Rods.	N.	s.	E.	w.
1	N. 20° 00′ W.	70.0	65.78			23.94 $24.05$
$\frac{1}{2}$	N. 12 30 W.	45.4	44.32			9.83
3	N. 10 00 E.	38.5	37.91		6.69	
4	N. 15 00 W.	38.0	36.71			9.84
5	N. 86 00 E.	80.8	5.65 .75		80.61	
6	S. 88 00 E.	65.2		· 2.27 .18	65.16	
7	N. 84 30 E.	72.0	6.90 7 00		71.67	
8	S. 5 45 E.	100.0		99.50	10.02	
9	W.	71.6	.18			71.60
10	S.	88.6		88.60		.20
11	N. 87 00 W.	50.2	2.63 $.73$			50.13
12	S. 81 15 W.	69.0	1	10.50		68.20
-			199.90	200.87	234.15	$\overline{233.54}$
	Balanced,		200.38	200.38	233.85	233.85

In the correction of the two last surveys, the differences between the two columns of latitude, and between those of departure, in each example, are equally divided between their respective columns. A northing is added to the second course in the second example; also, a northing to the ninth, and a westing to the tenth, in the third example. When courses are entered in the field book, north, south, east, or west, they are as liable to contain errors, and they are as subject to correction, as other courses.

EXAMPLE IV.

No.	Courses.	Dist. rods.	N.	S.	E.	w.
1	N. 7° 45′ E.	41.8	41.42		5.64 .58	•
2	S. 79 00 E.	47.0		8.97 9.15	i	
3	N. 40 00 E.	25.0	19.15	1	16.07	
4	S. 70 00 E.	60.0		20.52	56.38	
5	S. 15 00 E.	15.6	ī	15.07	4.06	
6	N. 89 00 E.	57.0	.99 .80		56.99	
7	S. 3 30 E.	96.5		96.32	5.89 .76	
8	S. 87 45 W.	174.6		6.86 7.20		174.46
9	N. 215 E.	84.2	84.14		3.31	
10	N. 80 00 W.	20.0	3.47 .46			19.70
		,	149.17	147.74	194.48	194.16
	Balanced,		148.46	148.46	194.16	

In the last example, the difference between the northings

and the southings is equally divided.

As it was judged that sufficient distances were made on the two westerly courses, the correction was made on the eastings.

## No. IV.

#### ON RECTANGULAR SURVEYING.

Rectangular surveying\* is a name given to the method

here treated of by the late Governor Treadwell.

In the operation of it the whole survey is reduced to squares and parallelograms, and each of these figures is divided into two right angled triangles of equal shape, or into two trapezoids of equal size and shape, by a boundary line of the field running obliquely through it, except when the boundary line is directly north and south, then the figure is divided into two squares or parallelograms.

The calculations are made from a meridian drawn either at the eastern or at the western extremity of the map; and the areas are produced by multiplying the latitudes by the

longitudes made from this meridian.

All the spaces lying between the field and the meridian, and between the parallels of latitude of the northern and southern extremities of it, also large spaces lying without the figure on the opposite side of it, and between those parallels, are included in the calculation; but that which lies without, is eventually excluded.

Parallels of latitude are drawn from each angle to the

meridian, which are called meridian distances.

In forming the column of meridian distances, when the meridian is drawn at the eastern extremity, the westings are added, and the eastings substracted; but when the meridian is laid on the west side, the eastings are added and the westings substracted.

The meridian distances proceeding from each end of a line are added together, to form the column of double mean distances, which the compiler of the foregoing work called second departure.

Meridian distances and double mean distances,† are more proper terms or names for these columns, than first departure

and second departure.

The meaning of the term meridian distance, is the distance made from any meridian.

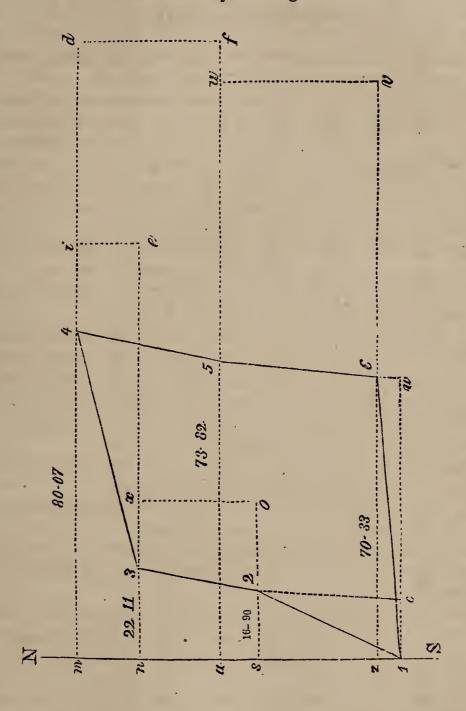
The following survey is calculated from the meridian of

\* Rectangular calculation is as proper.

<sup>†</sup> The compiler of the foregoing work would have made use of these names, but he was afraid of infringing on a certain copy-right which has expired.

the first station which is on the west side of the figure, of course, the eastings are added and the westings substracted.

The whole is illustrated by this figure.



,										
	H. D. N. Areas. S. Areas.				5455.40	5744.38	423.38	11623.16 3351.83	28271.33	Area in rods 160)4135.665
	Areas. S	612.62	1152.35	1586.86				3351.83		ods 160)
	z <u> </u>									in r
	H. D.	8.45	19.50	51.09	76.94	72.07	35.16	_		Area
	Merid Dist.	16.90 33.80	39.01	102.18 160.14	153.89	144.15 144.15 140.66	70.33			
	Merid. D. M. Merid Dist. D. Dist.	16.90	39.01	•	153.89		70.33			
	Merid.	16.90	22.11	80.07	73.82	70.33	00.00			
	×.				6.25	3.49	70.33	80.07		
	<del>_</del>	16.90	5.21	57.96		r		80.07		
	ω				35.45	39.85	6.02	81.32		
	z	36.25	29.54	15.53				81.32		
	Dist. Rods.	40.00	30.00	60.00	36.00	40.00	70.48			
	Courses.	1 N. 25° 00′ E.	N. 10 00 E.	N. 75 00 E.	S. 10 00 W.	5 co w.	85 (15 W.			
	No.	Z	63   X	3   X	\ \alpha \ \text{\alpha} \ \te	\. \. \. \. \. \. \. \. \. \. \. \. \. \	vi   9			

To form the first column marked at the top Merid. Dist. set the easting of the first line 16.90, into the head of the column, which is the meridian distance of 2, or the distance from 2 to s. To this number, add the easting of the second line, and their sum is 22.11, the meridian distance of 3, or the distance from 3 to n. To this number add the easting of the third

line, and their sum is 80.07, the meridian distance of 4, or the distance from 4 to m. From this number, substract the westing of the fourth line, and 73.82 remains, the meridian distance of 5, or the distance from 5 to a. From this number, substract the westing of the fifth line, and 70.33 remains, the meridian distance of 6, or the distance from 6 to z. From this number, substract the westing of the closing line, and 00.00 remains, which proves the work correct so far. When the last substraction does not end in a cipher, an error has been committed somewhere.

In forming the column of double mean distances, take the

following directions:—

Add together two opposite sides of each figure formed by the meridian distances. Set the first meridian distance into the head of the next column, or that marked at the top D. M. D., and it gives one side of the parallelogram 1s—2c. This figure is divided into two equal triangles by the line 1—2. The meridian distance multiplied by the northing of the line 1—2, gives the area of the whole parallelogram, or the double area of one of the triangles. Let this be considered, that which lies without the field. To the line 2s, add 3n, and their sum is 39.01, the length of the parallelogram nxos, which is divided into two equal trapezoids by the line 2—3. The double mean distance 39.01, multiplied by the northing of the line 2—3, gives the area of the parallelogram, or the double area of one of the trapezoids.

Let this be considered that which lies without the field.

To the line 3n, add 4m, and their sum is 102.18, the length of the parallelogram mien, which is divided into two equal trapezoids by the line 3-4. The double mean distance 102.18, multiplied by the northing of the line 3-4, gives the area of the parallelogram, or the double area of one of the trapezoids. Let this be that which lies without the field. To the line 4m, add 5a, and their sum is 153.89, the length of the parallelogram mdfa, which is equally divided by the line 4-5. The double mean distance 153.89, multiplied by the southing of the line 4-5, gives the area of the parallelogram, or the double area of one of the trapezoids.

Let this be that which abuts on the meridian, being partly

within and partly without the field.

To the line 5a, add 6z, and their sum is 144.15, the length of the parallelogram auvz, which is equally divided by the line 5—6. The double mean distance 144.15, multiplied by the southing of the line 5—6, gives the area of the parallelogram, or the double area of one of the trapezoids. Let this

be a5-6z, partly within and partly without the field. To the line 6z, nothing is to be added, of course, it is one side of the parallelogam z6-w1, which is equally divided by the closing line. The distance 70.33, multiplied by the southing of the closing line, gives the double area of the triangle z6-1, partly within and partly without the field.

The three products in the column of north areas, all lie without the field. Those in the column of south areas lie partly within and partly without the field, and they include all the space which is covered by the products in the column

of north areas.

Hence it is plain, that when the sum of the former is substracted from that of the latter, the double area of the field will remain. In this method, when the column of meridian distances and that of double mean distances are correct, the sum of the latter will be double to that of the former.

### PENNSYLVANIA METHOD.

If the writer has been correctly informed, this improvement was made by Dr. Rittenhouse.

Only one column is used for meridian distances, but the

final results are the same as when two columns are used.

This method is not so easily explained to the learner, but is perhaps preferable in practice, because an error may be committed in forming the column of double mean distances which may not be discovered; but in this method, an error cannot be committed in the meridian distances, without being detected. A full explanation of this method would be tedious and perplexing to the learner, without being of the least use in performing practical operations, and probably, if made, but little attention would be paid to it; therefore, only directions how to form the column, and how to apply the numbers in their practical use, will be given.

The operation of this method is substantially the same as that of the other, and the diagram given in that will answer for this. The north and south products are precisely the same in both methods. A further investigation of this method will be left for the learner when he shall be more expe-

rienced.

When the two columns in the other method are proved by addition, the process is longer than in this.

The second column in the foregoing example, marked at

the top, meridian distances, is the method here treated of.

To form the column, add twice or substract twice against

each station. Set the first easting 16.90 into the head of the column at the upper place. Add it to itself, and the sum is 33.80 in the lower place. To this number add the next easting, and they make 39.01 in the upper place. To this number add the same easting again, and they make 44.22 in the lower place. To this number add the third easting, and they make 102.18 in the upper place. To this number add the same easting again, and they make 160.14 in the lower place.

From this number substract the first westing, and 153.89 remains in the upper place. From this number substract the same westing again, and 147.64 remains in the lower place.

From this number substract the second westing, and 144.15 remains in the upper place. From this number substract the same westing again, and 140.66 remains in the lower place. From this number substract the last westing, and 70.33 re-

mains in the upper place.

From this number substract the same westing again, and 00.00 remains. The upper number against each station in this column, is the same as the double mean distance which stands against it; and the remainder of the process may be performed as before directed. Another column may be formed as the eleventh in this example, marked H. D. at the top, which, for distinction, is here called half distance. It contains half the sum of the numbers in the double mean column. These numbers, when multiplied by their respective northings or southings, give the simple areas of the different figures.

This method is preferable in practice, as the multiplications are greatly diminished. When the last decimal in the double mean distances is an odd number, a unit may be taken off, and take half the remainder, rather than annex another decimal: perhaps this would not make the difference of a rod in a survey of three hundred acres. Or the odd numbers in the last place of decimals may be balanced by some-

times adding a unit.

If the numbers are diminished a trifle, it may be remarked, that, on account of uneven surfaces, there is danger of making the distances too much, rather than falling short of the true measure. There are other methods by which surveys may be calculated arithmetically, but none are more correct, and perhaps none are so simple and so easy to be understood as the methods here treated of. These methods may be applied in every case in practical surveying, which depends on a calculation from courses and distances.

Instead of laying the meridian on one side, it may be laid through the map, either at an angle, or so as to bisect a boundary line; but this renders the process more complex and difficult.

#### PENNSYLVANIA METHOD.

This example is calculated by chains and links.

No.	Courses.	Dist.	N.	S.	E.	w.	M. dist. 164.06		
1	S. 88° 15′ W.	35.25		1.08		35.23 .21	128.85 93.64	•	1391580
2	S. 86 30 W.	45.65		2.79		45.57 .54	48.10 02.56		225990
3	N. 2 15 W.	32.55	32.53			1.28	1.28 0.00	416384	
4	N. 87 00 E.	20.25	1.06		20.22		20.22 40.44	212332	
5	N. 3 00 W.	25.40	25.37			1.33	39.11 37.78	9922207	
6	N. 86 45 E.	60.00	3.40		59.90		97.68 157.58		
7	S. 2 45 E.	25.50		25.47	1.22		158.80 160.02		40446360
8	S. 3 30 E.	33.10		33.04	2.02		162.04 164.06		53505608
			62.36	62.38	83.36	83.41		13872043	95569538
									13872043

1.94988 40 37.99520 1 A. Q. Rods. 408 1 38.

The above survey was commenced and terminated at the southeast corner. Against the fourth station, the addition of the eastings in the column of meridian distances begins, and the substraction of the westings terminates directly over it.

The lower number against the 8th station is 164.06. This is placed over the head of the column, and the three first

westings are substracted from it.

If the fourth course had been placed against the first number, and the others had followed in succession, the addition would have began at the head of the column, and the substraction would have ended at the bottom, and the result would have been the same. Perhaps this may be a better method for the student, and for the young surveyor, but one who is experienced can derive no benefit from it.

# No. VII.

#### ON PLOTTING SURVEYS.

Surveys may be plotted by various methods. That which

is commonly practised, is by a scale and protractor.

The latter instrument is a semicircle, graduated like the compass, and it answers the same purpose in laying angles on paper, that the compass does in taking them in the field.

A meridian is drawn for each station or angle in the survey, and the angle which each course makes, with its respective meridian, is laid down with the protractor, and each distance by a scale of even parts. It would be well also to draw a parallel of latitude for each station, as by such parallels the protractor may be kept more truly to the meridians.

A plot may be drawn by laying down the angles by the protractor without meridians or parallels of latitude, as has already been taught in the foregoing work; but the writer never had so good success by this method as he has had by

laying his courses from meridians.

As the scale and protractor are equally subject to error, the surveyor will be more likely to draw a correct plot if he should dispense with the latter instrument, and lay down the boundary lines from the latitude and departure of each, or from the latitude and meridian distance of each station.

To plot from the several latitudes and departures, take the

foregoing survey for an example.\*

As that survey is small, take half a sheet of paper, and draw

meridians across each end of it.

On the left hand meridian, make a point for the beginning. From that point draw a parallel of latitude to intersect the other meridian, perpendicular to, or at right angles with each.

The latitude of the first course is 36.25. Draw another parallel of latitude at that distance above the first.

The latitude of the second course is 29.54. This, added to the first, makes 65.79. Draw another parallel at this distance above the first.

To the sum of the first and second latitudes, add that of the third, and their sum is 81.32. At this distance above the first, draw another parallel. The southing of the fourth course is 35.54. Substract this from the whole sum of the northings, and 45.87 remains. At this distance above the first, draw another parallel. From the last remainder, substract the southing of the fifth course, and 6.02 remains, which is the southing of the closing line. At this distance above the first, draw the last parallel. In like manner, draw the meridian of each station, according to the departure made on each course. The intersection of these lines will be the angles of the figure. If the distances shall not exactly fall into these points, the process will contain some error, either in drafting, or from a scale not accurately divided.

## TO PLOT FROM LATITUDES AND MERIDIAN DISTANCES.

First, form the column of meridian distances. Next draw the meridian of the first station, and the several parallels of latitude, as before directed. On these parallels, lay the meridian distance of each station, viz.—from s to 2, 16.90; from n to 3, 22.11; from m to 4, 80.07; from a to 5, 73.82; from z to 6, 70.33.

From one of these points to another draw the boundary lines. Great care must be taken to keep the latitudes parallel and perpendicular to the meridian. The scale must be correctly divided, the dividers nicely pointed, and the rule must be straight. Whether the protractor is used or not, before a plot of a survey is drawn, it should be balanced, and both courses and distances corrected according to the balancing.

The following example is given as a proof of the necessity

of balancing a survey before the map is drawn.

A farm is to be divided among a number of heirs. A survey of it is taken, and the difference between the two columns of latitude and those of departure, is two rods for each. The survey is balanced and calculated arithmetically, and is found to contain two hundred acres.

The surveyor next draws his map, by which the divisions are to be made, according to the courses and distances as they were taken on the ground. The plan does not close by nearly two rods and three quarters. He next corrects the lines, and maks the map close as well as he can; and when the divisions are made, they may not agree with the first calculation, by two or three acres, or more. Should the map be drawn as before directed, by the latitudes and departures as balanced, or by the latitudes as balanced, and the meridian distances, it would close, and would be in exact conformity to the calculation made arithmetically. If the divisions are made arithmetically, the calculations must be made according to the balancing, or the divisions will not agree with the first calculation.

When a map of a multangular piece of land, of very irregular shape, is to be drawn, whether a calculation or a division is to be made from it, the surveyor should measure across the lot between two opposite angles in some central place, at least once, and in more places, if convenient, and the case requires it. By cross measures, the map may be more correctly drawn, and the divisions should be calculated separately. In such cases, the surveyor will be more likely to ascertain the true contents, than he would by surveying only the boundary lines, and then calculating the whole

together.

### No. VIII.

#### ON DIVIDING LAND.

As lands are divided into so great a variety of shapes, rules cannot be given which will answer in all cases.

In distributions of estates, the divisions are commonly made with scale and dividers. This method will answer well, provided the map is drawn on a large scale, which should not be less than ten rods to an inch.

As more confidence can be placed in arithmetical calculations, it may be recommended to every surveyor to make as little use of the scale and dividers as he can; but in our

country, they cannot, in all cases, be dispensed with.

In dividing lands, it will be acknowledged by every experienced surveyor, that it is a difficult matter to make the amount of a considerable number of divisions agree with the whole, when calculated by itself.

A few examples by arithmetical calculation will be given. Let the preceding figure be divided into two equal parts by a line running eastward from the second angle. At what point on the eastern boundary will it terminate?

As you do not know the point, first calculate the area of

that part which lies above a line from 2 to 5.

Set the courses and distances of the second, third, and fourth courses, into their respective columns, having a blank line for the course, distance, latitude, departure, &c. of the closing line from 5 to 2. On the two first of these courses, the sum of the northings is 45.07 rods, and that of the easting is 63.17 rods, and the course from 4 to 5 contains 35.45 rods of southing and 6.25 rods of westing. The southing and westing of the latter being substracted from the northings and eastings of the two former, leaves a balance of 9.62 rods of southing and 56.92 rods of westing to fill the blank line. The latitude and departure of the closing line being given, the course may be found by the following proportion.

As the latitude is to radius; so is the departure to the tangent of the course. Look in the column of tangents for the course. The course being found, the distance may be found as follows. As the sine of the course is to the departure

so is radius to the distance. See them worked.

Latitude 9.62, and the departure 56.92, given to find the course and distance.

Lat. 9.62 -			0.983175
: radius -			10.000000
:: departure 56.9	2 -		1.755265
radius and dep	p. added		11.755265
lat. brought do	own		0.983175
: tangent of the co	ourse 80	0 25'	10.772090
f 000 05/			0.00000
sine of 80° 25'	-	-	9.993896
: departure 56.92	•		1.755265
:: radius -	-		10.000000
			11 855005
			11.755265
			9.993896
: distance -	57.72		1.761369

The course from 5 to 2 is S. 80° 25' W., and the distance is 57.72 rods. This being ascertained, the contents of that

part of the figure above this line will be found, eleven acres and thirty-four rods, leaving a deficiency of one acre and a half, and thirty-three rods, of making one half of the whole figure.

This quantity is to be laid in a triangle on the line from 2

to 5, and on that from 5 to 6, running to a point at 2.

The question is, what distance from 5 towards 6, will be required to give the contents of the triangle? To answer such a question, the area, the contained angle, and one side of the triangle must be given, to find the length of the contiguous side, including the angle. Having these data, take

the following rule.

To the sine of the given angle, or to its supplement if obtuse, add the logarithm of the given side; substract radius from this sum, and substract the remainder from the logarithm of the double area: the last remainder will be the logarithm of the side required. In this case, the angle formed by the line from 5 to 2, and by that from 5 to 6, contains 75° 25′, the given side is 57.72 rods, the area of the triangle is 273 rods, and the double area is 546 rods. See the rule worked.

Sine of 75° 25'	9 985778		
logarithm of the given side 57.72	1.761369		
cancel the first figure, and R. is			
substracted	1,1.747147		2.737193
logarithm of the double area remainder brought down		-	1.747147
Temamuel blought down	•		1.1 11 111
logarithm of the side required 9.7	7 rods	-	0.990046

Measure from 5 towards 6, 9 rods and 19½ links to a beech tree, from thence on a straight line to 2, and the figure will be equally divided. The true position of the divisional line being established, the course and distance of it may be calculated as before directed.

The course and distance from 2 to 5 are N. 80° 25′ E. 57.72 rods: from 5 to the beech tree, S. 5° W., 9.77 rods. On the first, 9.62 rods of northing and 56.92 of easting are made. On the second, 9.74 rods of southing and .85 of a

rod of westing are made.

The northing of the first course being substracted from the southing of the second, and the westing of the second from the easting of the first, .12 of a rod of northing, and 56.07 rods of westing, are given as data by which the course and distance from the beech tree to 2 may be calculated. The course is N. 89° 53′ W., and the distance is 56.07 rods.

Suppose it is next required to lay out 15 rods in width be-

low and parallel with the dividing line.

As the eastern and western boundary lines both turn obliquely from the dividing line, the question is, what distance

will be required on each to give the required width?

Make the distance on each boundary line the hypothenuse of a right angled triangle, and 15 rods, the width required, one of the legs or the base. The angle at 2, formed by the boundary and dividing lines, contains 114° 53'. Substract 90° from this, and 24° 53' remains, being the angle formed by the given leg (15) and the hypothenuse.

Take the following proportion to find the hypothenuse.

As the co-sine of 24° 53'; is to 15, the given side; so is radius to the distance required. See it worked.

Co-sine of 24° 53'	•	•	•	9.957687
given side 15 rods	-		•	1.176091
:: radius -	•	• `	-	10.
				11.176091
				9.957687
: side required 16.54 rd	ods	-		1.218404

The dividing line and the eastern boundary, at the beech tree, form an angle of 85° 7'. Substract this from 90°, and 4° 53' remains, being the angle by which the east side must be worked.

Co-sine of 4° 53′		-	•	9.998421
: given side 15 rods	•	-	-	1.176091
:: radius	-	•	•	10.
				11.176091
				9.998421
: side required 15.05 roo	ls	•	-	1.177670

The distances required are 15 rods 1½ link on the east-

ern, and 16 rods 13½ links on the western boundary.

Measure from 2 towards 1, 16 rods 13½ links to a spruce tree, and from the beech tree towards 6, 15 rods 11 link to a pine tree, and calculate the distance from the pine to the spruce, and the division will be completed. This calculation must be made by a traverse from the courses and distances already known.

From the spruce to 2, N. 25° E. 16.54 rods; from 2 to the beech, S. 89° 53' E. 56.07 rods; from the beech to the pine S. 5° W. 15.05 rods. Arrange these courses and distances in their proper columns as follows, and calculate the latitude and departure of each, having a blank line for the last.

Courses.	Dist.	N.	s.	Е.	w.
N. 25° 00′ E.	16.54	14.99	1	6.98	
S. 89° 53′ E.	56.07		.12	56.07	
S. 5° 00′ W.	15.05		14.99		1.31
		.12			61.74
		15.11	15.11	63.05	63.05

Having calculated the latitudes and departures, substract the northing of the first course from the sum of the southings of the two last, and .12 of a rod remains to be entered in the blank column of northings; also, substract the westing of the third from the sum of the eastings of the two first, and 61.74 remains to fill the blank column of westings. This balance of northing and of westing is the latitude and departure of the line from the pine to the spruce. The distance is 61.74 rods, and the course agrees with that on the opposite side.

Suppose it is next required to lay out four acres adjoining

and parallel with the line from the pine to the spruce.

As the figure of this division is not regular, no rule can be given by which it can be calculated by one operation, but it

must be done by approximation.

Reduce the quantity of the division to rods, and divide that sum by the length of the known side, and the quotient will be 10.36 rods, but as the south side will be longer than the north, the width cannot be so much.

Assume 10 rods as the width, and calculate the distance on each end by the same process that you did those on the last. The angles in this are the same as in that.

Co-sine of 24 : given side 1		-	-	9.957687 1.000000
:: radius	•	i	•	 10.
				 9.957687
: side require	d 11.03	rods		1.042313

Co-sine of 4° 53′: given side 10 rods: radius		:	9.998421 1.000000 10.
		_	11.000000 9.998421

: side required 10.04 rods - 1.001579

The distances required are 10 rods 1 link on the east, and

11 rods  $\frac{3}{4}$  of a link on the west boundary.

Measure from the spruce towards 1, 11 rods  $\frac{3}{4}$  of a link to a hemlock, and from the pine towards 6, 10 rods 1 link to a maple, and calculate the distance from the latter tree to the hemlock.

From the hemlock to the spruce N. 25° E. 11.03 rods; from the spruce to the pine, S. 89° 53′ E. 61.74 rods; from the pine to the maple S. 5° W. 10.04 rods.

Courses.	Dist.	N.	s.	E.	w.
N. 25° 00′ E.	11.03	10.00		4.66	
S. 89° 53′ E.	61.74		.12	61.74	
S. 5° 00′ W.	10.04		10.00		.87
		.12			65.53
		10.12	10.12	66.40	66.40

The northing and westing in the blank line is the latitude and departure of the line from the maple to the hemlock. The distance required is 65.53 rods. To this distance, add that of the north side, and the sum of both is 127.27 rods. Multiply half of this sum by 10 rods, the width of the division as it now stands, and the product is 636.3 rods. Substract this from 640, and 3.7 rods remain, being a deficiency. To this deficiency annex three ciphers, and divide that sum by the distance from the maple to the hemlock, and the quotient will be nearly 6, which is .06 of a rod, or  $1\frac{1}{2}$  link. To the quantity already found, add this width on the south side, and the division will be completed.

The south division of the whole figure contains twelve acres, three quarters, and twenty-seven rods. This division

now stands in three subdivisions.

The first contains five acres, two quarters and three rods; the second, four acres, and if the foregoing calculations are correct, the third contains three acres, one quarter, and twenty-four rods. See the work proved.

There now remains between the southeast corner and the last subdivision, 5.08 rods, and between the southwest corner

and the same division, 12.37 rods, to be calculated on.

Courses.	Dist.	N.	s.	E.	w.	Merid. Dist.	North. Areas.	South. Areas.
S. 5° 00′ W.	5.08		5.06		.45	141.11 140.66		714.0166
S. 85 05 W.	70.48		6.02		70.33	70.33 00.00		423.3866
N. 25 00 E.	12.37	11.21		5.23		5.23 10.46	58.6283	
			.13	65.55		76.01 141.56		9.8813
		11.21	11.21	70.78	70.78		58.6283	1147.2845 58.6283

1088.6562

$$160) \frac{544.}{480.} (3)$$

A. Qr. Rods. Contents 3 1 24

No. IX.

# ON BOUNDS AND ROADS.

As the magnetic needle cannot be relied on in renewing lost boundaries, it is of the first importance that good, substantial bounds, be kept up. In divisions, or distributions of lands, surveyors ought to see that such bounds are erected. It is their business to cause them to be made, and such bounds ought to be described in deeds, or in the instruments by which lands are conveyed, and to be a part of the record. By proper care and attention to this part of the business, many disputes may be prevented.

Highways are attended with more difficulties of this kind,

than the location of the divisions of real estate. In laying highways, it is the common practice to lay the centre lines, and order the roads to be of a certain width, and stakes are usually set at the angles. Care is not often taken to set bounds on the sides, and when the roads are made the centre bounds are destroyed, and the travelling path is often built on one side of the centre; but as the bounds are lost, it is utterly impossible, after a few years have elapsed, to ascertain by the survey where the road was laid.

Surveyors who are employed on such business ought to describe the angles, or as many as is practicable, in such a

manner that the road may afterwards be found.

It taking surveys of roads, the distance on each proprietor's land must be noted, for the purpose of assessing damages; but these distances need not be entered in the record. The whole distance on each course must be entered in the record, and it is no matter whether it crosses the land of one or of ten different owners.

The following, being a resurvey of a part of the New London and Lyme turnpike road, as was recently taken, is prepared for record, and it may serve as an example.

As there is no object of sufficient permanency directly against the point of the beginning of said road, it may be

found by the following direction.

From a point, 35 links northerly of the northwest corner of B. Brown's stone house, in the range of the west side, run (as the magnetic needle now points\*) S. 66° 25′ W. 1 chain 56 links to the centre of a stone set in the ground beneath the surface, which is the point of beginning of said road—thence, on the same course (S. 66° 25′ W.) 4 chains 60 links, to a point 49½ links northerly of the northwest corner of G. Jones' store, in the range of the west side; thence S. 79° 25′ W. 11 chains 52 links to a point 48 links northerly of the northeast corner of the Norris house, in the range of the east side; thence S. 80° 10′ W. 17 chains 20 links to a point 50 links northerly of the northeast corner of the Chester house, in the range of the east side. The line described by the foregoing survey, is the centre of the road which is four rods in width.

An angle in a road may be described by its bearing and distance from some permanent object, such as the corner of a building, the centre of a well, a point of a rock, a tree, &c. In cases where no permanent object is near an angle, the side bounds ought to be set before the Committee or Com-

missioners, (as they may be named) proceed any further in the location of the road.

When the centre line of a road is laid, the distance which it runs on any proprietor's land may be multiplied by the width of the road, and the product will be the quantity of land taken.

Whether the centre or a side of a road is laid, the lines almost uniformly cross the boundary lines of lots of land in such oblique directions, that if a side is laid, it will require too much time to ascertain the exact quantities of land, which will be taken from different proprietors.

Other advantages will be found by laying the centre line of

a road, which need not here be mentioned.

## DIRECTIONS FOR TAKING MINUTES ON A ROAD.

S. 110 15' E. 17 00 on W. H.'s land.
+ 30 00 on R. S.'s "
+ 89 00 on T. B.'s "
+ 1½ 00 rod on old road.

Whole distance 1371

# No. X.

# ON DISTRIBUTING ESTATES.

As the distribution of estates is connected with surveying, something on that subject may, with propriety, be added to this work.

Surveyors are agreed that written distributions of real estate are often, and too often, returned to Courts, accepted and recorded, which are so unintelligible that it is extremely difficult and sometimes impossible to ascertain, with any degree of certainty, where the divisions of land were originally made.

In distributing estates, surveyors have the minutes, and it properly belongs to them to write the distributions.

To young learners who are coming forward to take an ac-

tive part in this business, some directions may be given.

The divisions of land among heirs, in most cases, are first made on paper. When these are completed and agreed to

by the distributors, erect the bounds between the several divisions. Next, from the map on which the divisions were made, which will be full of marks, and perhaps some blots, copy a neat handsome map on new paper, noting thereon all the courses and distances, and all the bounds, which should be entered in the distribution. Also, note in each division of the map the quantity of land it contains, with the name of the heir to whom it was distributed. This map is to be kept by the heirs. Next write the distribution, and before it shall be returned to Court, see that the heirs have a copy of it.

With a map and a copy of the distribution, the heirs will have a record in their own house, from which, at any future period, they may find the divisions of their land.

The following form of a distribution has been approved

by experienced Judges\* of Probate Courts.

# To the Honourable Court of Probate for the District of Rockingham.

The undersigned, distributors of the estate of Benjamin Banister, Esquire, late of Applebury, within said district, deceased, have distributed said estate, under oath, as follows:

To Philura Banister, widow of said deceased, as her right of dower in said estate, fifty acres of land lying on the front of the farm, bounded as follows:—Beginning at the northwest corner of said farm by the highway, thence running east by Roderick Random's land, 50 rods to a maple tree, thence south parallel with the highway 160 rods to a hemlock tree by Thomas Trunnion's land, thence west by said Trunnion's land 50 rods to the highway, thence north by said highway 160 rods to the place of beginning. Also, the following parts of the dwelling house [describe the parts.] Also, the following parts of the barn [describe the parts, and of other buildings.]

#### PERSONAL ESTATE.

Scott's Bible, \$15. Bed, curtains, &c. \$45. Looking glass, \$15. - - - \$75.00

To BENJAMIN B. BANISTER, the north division of the farm, containing one hundred acres, being partly encumbered by dower, bounded as follows:—Beginning at the north-

<sup>\*</sup> Called Surrogates in some states.

west corner of said farm, thence running east by Roderick Random's lands 200 rods, to a beech tree by Oliver Gulliver's land, thence south by said Gulliver's land, 80 rods to a spruce tree, thence west by land set to Matilda Banister, parallel with said Random's land, 200 rods to a white pine tree by the highway, thence north by said highway, 80 rods to the place of beginning.

Also, one undivided half of all the buildings belonging to

said estate, being partly encumbered by dower.

Said division of real estate is appraised at - \$2500.00

## PERSONAL ESTATE.

One horse, \$100. Two yoke of oxen, \$130. Ox wagon, \$50. - - \$280.00

To Matilda Banister, the south division of the farm, being the remainder and residue of said farm, containing one hundred acres, and is 80 rods in width from front to rear, being partly encumbered by dower, bounded as follows:—North on the division set to Benjamin B. Banister, south on Thomas Trunnion's land, east on Oliver Gulliver's land, west on highway.

Also, one undivided half of all the buildings belonging to

said estate, subject, in part, to incumbrance.

Said division of real estate is appraised at - \$2500.00

## PERSONAL ESTATE.

Bed, curtains, &c. \$45. Mahogany table, \$12. Set of silver spoons, \$18 - - \$75.00

Said widow and said heirs have equal privileges of passing to and from any and every part of the real estate set to each of them in the foregoing distribution, at the usual passways, such as doors, stairs, gates, bars, lanes, paths, &c.

HUGH HUNTER, CHARLES CHALKER.

Applebury, July 30th, 1832. CHRISTOPHER CUTLER.

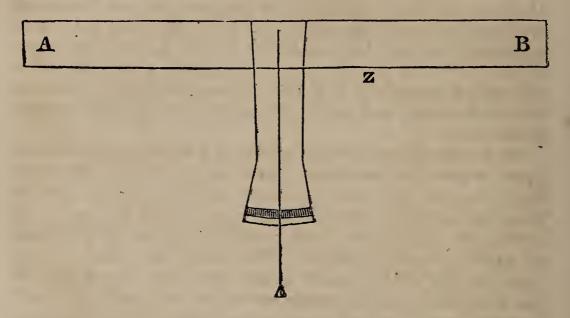
The foregoing caption or preamble is sufficient, as it will appear of record that the distributors were appointed. Forms of distribution must vary according to circumstances.

### No. XI.

## ON LEVELLING.

It is not expected that land surveyors will qualify them-

selves for civil engineers, or that they will furnish themselves with suitable instruments for that business, but every surveyor should furnish himself with an instrument with which he can take levels and angles of elevation\* or depression, with a sufficient degree of accuracy to answer in cases of locating roads, of ascertaining whether water may be carried in an aqueduct from one place to another, and to ascertain the fall of mill seats; also, to answer in all common cases. A cheap, simply constructed instrument, represented by the following figure, is recommended



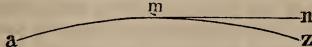
Let A B be a strip of a board three inches wide and three feet in length, or longer if necessary, made perfectly straight on the top. The perpendicular piece, which is dovetailed into the top, should be of such a width at the bottom that it may be graduated either way from the centre, ten or fifteen degrees; and of such a length that the radius by which the graduated arch is swept, should be at least a foot. Great care must be taken in the graduation, to have it done correctly, and by fine lines, and to have the centre perpendicuar or at right angles with the top. The plumb line should be a fine smooth silk thread or hair. At z, a hole should be bored of a suitable size to set it on the head of a compass staff. Such an instrument, if correctly made, will answer all the purposes before mentioned.

Before directions are given for levelling, the difference between the apparent, and the true level, will be explained. The former is a tangent, or a straight line, drawn and con-

<sup>\*</sup> An angle of elevation rises above a horizontal line; a depression falls below it.

<sup>†</sup> This instrument may be improved by fixing sights on the top.

tinued from any point on the globe, the surface continually departing from it. The latter is the curvature of the earth, or a line parallel with it, like two concentric circles, each part of the true level, whatever may be its length, is equidistant from the centre of the earth. The straight line mn, in the following figure, represents the apparent, and the curved line a z, the true level.



Let the above described instrument be set on any part of the ocean, and be levelled by the plummet, the top being even with the surface of the water, and let a line with the top be continued; as the plummet hangs directly towards the centre of the earth, it is evident that this line is a tangent, and at the end of one mile it will be 8 inches, at the end of 10 miles 66 feet 4 inches, and at 20 miles, 266 feet above the surface of the water.

In levelling between two points at a considerable distance apart, where the instrument must be often set, as the plummet, like the spokes in a wheel, each time hangs directly towards the centre of the earth, it will keep the top of the instrument on the true level, provided it is set on the centre of each stationary distance. But when the level is taken from the first to the second station, and from the second to the third, and so on in succession to the end, each level will be a tangent; of course, the apparent level will be taken.

The surveyor should also be furnished with two observation staves, ten feet, or more, in length, divided into feet and inches. These staves should be committed to the care of two skilful men, who will keep them perpendicular at the stations, and who will be correct in their assistance in taking the observations. Suppose the first stationary distance, on which a level is to be taken, is 20 rods. The staves must be erected at each terminating point, and the surveyor must take his station equidistant from each. A target must be raised on each staff as the surveyor may direct.

If the level strikes the back staff 7 feet, and the forward staff 2 feet, above the surface, it is apparent that the rise between the stations is 5 feet; but the substraction need not be made, each observation should be entered in its respective column, under the head of fore heights and back heights, or fore sights and back sights, as the surveyor may choose to term

them.

When the first observation is completed, the back staff should be carried forward to a convenient place, and the

second observation taken as the first. In like manner the rest of the observations must be taken and entered in their

respective columns.

If the sum of the back sights shall exceed the fore sights, the terminating point is higher than the place of beginning; but if the sum of the fore sights shall exceed the back sights, then the terminating point is lower than the point of beginning, as will appear by the following examples.

## FIRST EXAMPLE.

	$F_{0}$	re s	ights.	Back	sights.
	Fe	eet. I	Inches.	Feet.	Inches.
1st Ob	servation				00
2d	66	8	00	2	00
3d	44	8	00	1	00
4th	46	7	00	2	00
5th	46	7	00	2	00
6th		1	00	7	00
7th	66	1	00	8	00
8th	66	1	00	8	00
9th	46	1	00	8	00
10th	66		00	8	00
		41	00	46	00
				41	

Difference 5 00

The terminating point is 5 feet higher than the point of beginning.

#### SECOND EXAMPLE.

	Fc	re.	sights.	Back	sights
	$\mathbf{F}\epsilon$	eet. I	Inches.	Feet.	Inches.
1st	Observation	7	00	0	00
2d	66	8	00	2	00
3d	66	8	00	1	00
4th	66	7	00	2	00
5th	66	7	00	2	00
6th	66 %	1	00	7	00
7th	"	1	00	8	00
8th	66	1	00	8	00
9th	46	1	00	8	00
	_			, <u> </u>	
		41	00	38	00
		38	00		
	Difference	3	00		

The terminating point is 3 feet lower than the point of

beginning.

When the sums of the two columns are equal, the extreme points are on the same level. It will not be necessary to enter the stationary distances in the field notes, unless the whole distance between the two extreme points, or a profile of the surface, is wanted.

On a distance of 80 rods, the difference between the apparent and true level, is half an inch; at half a mile, two

inches.

In levelling to ascertain how high a dam across a stream may be raised without flowing the meadows, or impeding the wheel of a mill above, great caution should be observed, for if a dam is raised to a level with a point 80 or 100 rods above, to which it may be supposed that water may flow without damage, it will rise higher at that point than any one would suppose, who has not investigated the subject. The rise of water at the head of a pond, will depend in a great measure on the width of it, and on the size and force of the stream.

In locating roads, sometimes it is necessary to ascertain the difference between the elevation of the hills on two routes, both proceeding from one and terminating at the same point. Though the difference, of itself, between the rise and fall on two routes, may not in all cases be a correct rule by which to give preference, yet this evidence, with a comparison between the steepness of the hills on two routes, is sufficient.

To perform this service by the slow process of levelling for the conveyance and rise of water, would be attended with an expense which the case would not justify; therefore, a more expeditious method will be pointed out. At convenient distances, take all the angles of elevation and of depression, with the instrument before described, measuring the distance between each station. These angles will be taken more correctly by back sights, as the surveyor can better select proper places for taking them than an inexperienced assistant. The courses or bearings of the several stationary distances, may or may not be taken with a compass.

The elevation of the hills may be ascertained as correctly without the courses as with them. If the courses are taken, it will require more time and expense. Having measured all the stationary distances, and taken all the angles of elevation and depression on a route, arrange them, as in the following table. The first column contains the number of

stations; the second, the distances in rods; the third, the degrees of elevation or depression, with the letter E. or D. against them. The column H. D. contains the horizontal distance made on each line. The horizontal distance, with the elevation or depression against it, is the same as the latitude and departure on a course taken by the compass. The column P. H. contains the perpendicular height at the end of each line above the horizontal line. This column, in this case, is formed by adding the elevations, and by substracting the depressions.

No.	Dist.	0		H. D.	E.	D.	P. H.
1	50.	4	E.	49.88	3.49		3.49
2	40.	5	E.	39.85	3.49		6.98
3	30.	3	E.	29.96	1.57		8.55
4	20.	2	D.	19.99		.70	7.85
5	40.	4	D.	39.90		2.79	5.06
6	50.	3	D.	49.93	,	2.62	2.44
7	45.	1	E.	44.99	.79		3.23
8	40.	4	E.	39.90	2.79		6.02
9	50.	3	E.	49.93	2.62		8.64
10	40.	1	E.	39.99	.87	****	9.51
-					15.62	6.11	

By this calculation it appears that the sum of the elevations amount to 15.62 rods, or to 257 feet  $8\frac{3}{4}$  inches, and the depressions amount to 6.11 rods, or to 100 feet  $9\frac{3}{4}$  inches, which may be thus expressed, 257 feet  $8\frac{3}{4}$  inches rise, and 100 feet  $9\frac{3}{4}$  inches fall. It also appears that the hill at the terminating point is 24 links, or 15 feet 10 inches, higher than the top of the first hill.

By this method of taking elevations, they are the apparent level, but this will answer the purpose for locating roads.

## DIRECTIONS TO MAKE A PROFILE OF THE ABOVE SURVEY.

Lay the plan on a scale of ten rods to an inch. Draw a straight line about  $3\frac{1}{2}$  feet in length for a horizontal line. On this line lay down the several horizontal distances as they stand in the table. At the end of each of these distances lay down the perpendicular height which stands against it, at right angles with the horizontal line. From one of these points to another, draw a line from the beginning to the end, which will represent the surface of the ground.

Profiles of roads, or of certain hills on roads, are good evidence to carry into courts, in disputed cases of this kind. When such testimony is exhibited, the elevations of hills should be given in feet and inches. Also, the rise and fall should be given in this measure.

# MISCELLANIES.

#### TO REDUCE CHAINS AND LINKS TO FEET AND INCHES.

#### RULE.

Multiply the chains and links, or any number of links less than a chain, by 66, the number of feet in a chain, and from the product point off two figures at the right, for decimals. The figures at the left will be feet. Multiply the decimals by 12, the number of inches in a foot, and point off two figures at the right. Those at the left will be inches. Multiply the last decimals by 4, and point off two figures at the right, and that at the left will be quarters of an inch.

#### EXAMPLE.

In 2 chains 22 links, how many feet and inches?

2.22 66	
1332 1332	
146.52 12	

.96 Ans. 146 ft.  $6\frac{1}{4}$  in. nearly.

## TO ASCERTAIN THE NUMBER OF INCHES IN A LINK.

As it will not increase 66 by multiplying it by 1, multiply 66 by 12, and the product will be 7.92 inches.

## TO REDUCE INCHES TO THE DECIMAL OF A FOOT.

#### RULE.

Annex two ciphers to the inches and divide that sum by 12, and the quotient will be the decimal required.

#### EXAMPLE.

What part of a foot is 9 inches?

TO REDUCE FEET AND INCHES TO CHAINS AND LINKS.

#### RULE.

Reduce the inches to the decimal of a foot, and annex that to the feet; or if there are no inches, annex two ciphers to the feet, and divide that sum by 66, and the quotient will be chains and links.

### EXAMPLE.

In 440 feet 3 inches, how many chains and links?

66)440.25(6.67 396

> 442 396

465 462

3 Ans. 6 ch. 67 links.

When a piece of land is calculated by chains and links, and the contents stand in acres and decimal parts of an acre, it may be multiplied by the price of an acre, and the product will be the amount.

#### EXAMPLE.

A piece of land 16 chains and 75 links in length, and 12 chains and 25 links in breadth, is sold for \$25.25 per acre, what is the price of it?

Length			16.75	
Breadth	• •	•	12.25	
	•			
			8375	
			3350	
			3350	
			1675	
			1010	
Acres and de	cimal parts	,	20.51875	
	•	100	25.25	
			~0.~0	
			00 200 200	
		1	0259375	
		4	103750	
			59375	
		410	3750	
	l marrian	Ø519	00 84975	on @519 10
	Answer,	\$310	.09.04379,	or \$518.10.

What is the length of a side of a square which contains 6040 acres?

Logarithm of 966400 ½5.985157

2.992578. Answer, 983.06 rods.

What is the length of a side of a square which contains 4 acres, or 640 rods?

Logarithms of  $640 \frac{1}{2} 2.806180$ 1.403090. Answer, 25.3 rods.

A four sided figure, described by the following courses and distances, is divided, into two triangles to find arithmetically the contents of each, and the amount of both, viz. A, B. N. 10° E. 55 rods, B, C. S. 85° E. 65 rods, C, D. S. 8° W. 60 rods, D, A. N. 80° 35′ W. 66.85 rods. The supplement of the angle contained between the two first sides is 85°, what is the area of the triangle?

Sine of 85° - 9.998344 A, B. 55 rods - 1.740363 B, C. 65 do. - 1.812913

Cancel the first figure 1,3.551620—Double area 3561

 $\begin{array}{c} 160)1780.5(11) \\ 160 \\ \hline \\ 180 \\ 160 \\ \hline \\ A. \quad Q. \quad R. \\ \hline \\ Answer, \quad 11 \quad 0 \quad 20\frac{1}{2} \\ \end{array}$ 

The angle contained between the two last sides is 88° 35', what is area?

Sine of 88° 35′ - 9.999867 C, D. 60 rods - 1.778151 D, A. 66.85 rods - 1.825101

Cancel the first figure 1,3.603119—Double area 4010 160)2005(12

Answer - 12 2 05 320

First triangle 11 0  $20\frac{1}{2}$ Whole contents 23 2  $25\frac{1}{2}$ 

Perhaps the above is as short and as certain a method to calculate the contents of an oblique angled, four sided figure, as can be taken.\*

<sup>\*</sup> Any polygon may be reduced to triangles, and the contents cal culated by the same method.

The method of calculating areas of such figures by multiplying together half the sum of the two opposite sides, is incorrect, or the only certainty there is in it, is that of making, in a greater or less degree, an excess of quantity. In cities, it is the practice to measure lots by feet and inches.

To calculate the areas of such lots, reduce the inches to the decimal of a foot, annex such decimals to the feet to which they belong, and calculate, as by other measure, which will

give the areas in square feet.

When it is required to give the areas of such lots in square rods, and the contents stand in square feet, divide the feet by 272.25, the number of square feet in a rod, and the quotient will be the answer; or the feet and inches given in the distances, may be reduced to chains and links, or to rods and decimal parts of a rod, and the calculations made as in other cases. In measuring city lots, as step-stones and other obstructions may be in the way, extend a rope across the front. Let it be level, drawn tight, and made fast at each end. Measure on the rope; also, measure the other sides with equal accuracy, if necessary.

In the two first editions of this work, a rule was inserted to prove the correctness of the courses in a survey, but it was afterwards discovered by Mr. Flint, and by others, that the rule will prove courses to be correctly taken when they are incor-

rect.

The same rule has recently made its appearance in the American Journal of Science and Arts, and it may take a second tour among surveyors, under the character of an unering rule.

#### FORM OF A FIELD BOOK.

Beginning at a mere-stone at the south-west corner.

#### Rods. Links.

1. N. 25° 00' E. 40 00 to a pine tree.

- 2. N. 10 00 E. 30 00 to a hemlock tree.
- 3. N. 75 00 E. 60 00 to a spruce tree.
- 4. S. 10 00 W. 36 00 to a beech tree.
- 5. S. 5 00 W. 40 00 to a maple tree.
- 6. S. 85 05 W. 70 12 to the place of beginning.

On account of the diurnal motion of the magnetic needle, in the warm season of the year, the courses in all surveys, if practicable, should be taken before 9 o'clock in the morn ing. Let this matter be investigated. A survey is commenced at seven o'clock in the morning, but is not completed until three o'clock in the afternoon. The course of the first line is N. 5° E., and the distance is 70 rods. The departure on this course and distance is 6.10 rods.

When the survey is completed, the bearing of this line is again taken, and the course is N. 5° 10′ E. The departure is now 6.30 rods, five links more than it was in the morning.

Every compass which is in such order as it ought to be, will generally find in the summer, from morning to one o'clock, as great a change as this, often greater, but seldom less.

The writer knows not who invented the following rules for finding contained angles, but they have been extensively adopted into practice.

N. 62° E. When the first letters are alike, and the last N. 44° W. unlike, add the courses.

S. 72° E. When the first letters are alike, and the last s. 25° E. also, substract the less course from the greater.

N. 64° E. When the first letters are unlike and the last alike, add the courses, and substract their sum from 180°.

When the first and the last letters are unlike,

N. 57° W. Substract the less course from the greater, and the remainder from 180°.

To find the quantity of an angle, reverse the preceding course, then both courses will run from the same point. These rules are applied only when the first course is reversed.

#### EXAMPLE.

Two courses are given, viz. S. 62° W., and N. 44° W. to find their contained angle. Suppose yourself standing at the point where these courses meet. Reverse the letters of the first course, and they will stand thus:

The following figures were prepared for the sixth edition of this treatise, by Mr. Barnard.\* There is nothing in the rules-to which they are applied, different in principle from the preceding ones, but they do not require the first course to be reversed.

\* Such notes on the text as are signed ED., were made by Mr. Barnard.

I. If the first letters are alike, and the last also, add the less course to the supplement of the greater.

II. If the first letters are alike, and the last unlike, sub-

stract the sum of the courses from 180°.

III. If the first letters are unlike, and the last alike, add the courses.

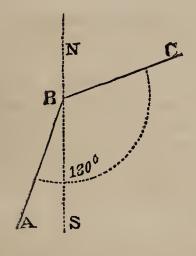
IV. If the first letters are unlike, and the last also, sub-

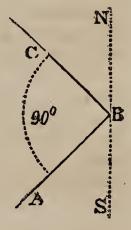
stract the less course from the greater.

"A set of figures like the following, well fixed in the mind, will be a great assistance to the learner."

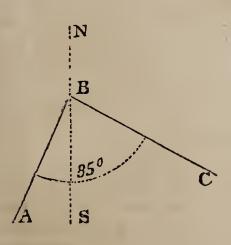
N. 20° E. N. 70 E.

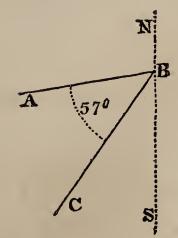
RULE 2d. N. 50° E. N. 40 W.





RULE 3rd. N. 25° E. S. 60 E. RULE 4th. N. 82° E. S. 25 W.





"It will be seen that the required angle, in each case, is A, B, C."

### CONVERGING OF MERIDIANS.

Two meridians cannot be run by the compass parallel to each other, for they will diverge towards the equator, and converge towards the pole.

The length of a degree of longitude in any parallel of latitude, is to the length of a degree upon the equator, as the

co-sine of that latitude is to radius.

The following proportion will give the length of a degree

of longitude in any parallel of latitude.

As radius is to the length of a degree on the equator, so is the co-sine of the latitude, to the length of a degree on that latitude. This rule may be applied either to geographical or to statute miles.

A degree on the equator of geographical measure, is 60 miles; that of statute measure has been estimated at 69½

miles, but this estimate is too great.

The earth is considered a sphere, 7930 statute miles in diameter. By the rules contained in this book for calculating the circumference of a circle, when the diameter is given, the circumference of the earth will be found 24912.8 miles. This number divided by 360, gives a quotient of 69.2, the length of a degree upon the equator.

#### FIRST EXAMPLE.

What is the length of a degree of longitude in geographical miles in latitude 42?

As radius	10.000000
: is to 60 miles	1.778151
: : so is co-sine of latitude 420	9.871073
0	
	11.649224
	10.000000
: Answer, 44.59 miles.	1.649224

#### SECOND EXAMPLE.

What is the length of a degree of longitude in statute miles in latitude 42°?

As radius -	•	•	•	10.000000
: is to 69. 2 miles	•	•	-	1.840106
:: so is co-sine of lat.	420	-		9.871073

11.711179 10.000000 1.711179

Answer, 51.42 miles.

### DIVERGENCE OF THE COMPASS FROM PARAL-LELS OF LATITUDE.

When a meridian crosses a parallel of latitude, the angles on the side opposite to the equator are equal, and each contains less than 90°; of course, those on the other side are equal, and each contains more than 90°. This is demonstrated by the meridians and parallels on a globe. The difference between the first and second angles, depends on their distance from the equator. In 70° of latitude, the two first are less, and the two last are greater than they are in 10° of latitude.

When the compass is set on a parallel of latitude, at right angles with a meridian, it is apparent that each angle contains 90°; of course the compass will not run on that parallel, but will diverge from it, and by continual running will

arrive at and run on the equator.

In 70° of latitude, the compass tends towards the equator faster than it does in 10°, hence it is evident that an east or west line, run by the compass, is not straight, but is curved.

On an extensive plain, let a line be run east or west to the distance of some miles; then from the terminating point, back on the opposite course, the compass will not return on its first track to the place of beginning, but will fall towards the equator.

The divergence of the compass from parallels of latitude, cannot materially affect common land surveying; but lines 10, 20, or 30 miles in length, when designed to be run on particular parallels, will be affected by it, unless calculations

are made to keep the compass on such parallels.

### QUESTIONS.

1. At a certain point, I took the elevation of a tower, 3° 15', then measured towards the tower on an angle of depression 7° 333 feet, to a level with the base of the tower; when I took the elevation again, 8°. Required, the height of the tower, and the distance from the second place of observation to the base; also, how much higher the land was at the place of the first observation, than at the second.

Answer. Height - - 99.6 feet.

Distance required - 708.6 feet.

Difference in height of land 40.58 feet.

2. Two persons made observations on the altitude of a meteor, both being on the same side of it, and in a vertical plane passing through it. The distance between their stations was 200 rods, and at one, the angle of elevation was 36° 25', at the other 32° 50', and at the last the disk of the meteor subtended an angle of 5'. Required, the distance from the last place of observation, also the height and diameter of it.

M. Q. R.

Answer. The distance 5 3 60

Height, 3 0 70

Diameter, 45 feet 5½ inches.

3. From the top of a steeple 165 feet high, the angle of depression of the nearest bank of a river is 11° 15′, that of the opposite bank is 6° 15′. Required, the width of the river.

### Answer, 41.13 rods.

4. What length of cart tire will it take to band a wheel 5 feet in diameter?

### Answer, 15 feet, $8\frac{1}{2}$ inches.

5. A gentleman laid out a garden in a circle, containing one acre, one quarter, and one rod, with a gravelled walk on the outer side of it within the circle, which took up twelve rods of ground. What is the diameter of the circle, and what is the width of the walk?

Answer. The diameter 16 rods—width of the walk 4 feet.

6. Neptune laid out 1,000 square miles of the surface of the sea in a circle, and sold to Æolus all that part of it which lies without a concentric circle of one third of the diameter. What is the diameter, and how much was sold?

Answer. The diameter 35.68 miles. The quantity sold 888.92 square miles.

7. A farmer laid out an elliptical orchard, the longest diameter of which was 30 rods, and the shortest was 20 rods, and enclosed the same with a wall two feet thick within the figure. What is the quantity within the wall, and how much is covered by it?

Answer. Within the wall 2 3 22 Covered by the wall 9.3

8. From a point in an equilateral triangle, I measured the distances to each corner, and found them 20.28, and 31 rods. Required the area and the length of the sides.\*

Answer. The area 5 1 362 Length of each side 45 rods.

9. Required the dimensions of a parallelogram containing one acre and a half, bounded by 64 rods of fence.

### Answer, 12 by 20 rods.

10. The area of a parallelogram is five acres, one quarter, and thirty five rods, and the diagonal is 43 rods. Required the length of the sides.

### Answer, 35 by 25 rods.

11. Required the dimensions of a parallelogram containing twenty-six acres, one quarter, and twenty-four rods, when the length exceeds the breadth by fifty-two rods.

### Answer, 44 by 96 rods.

12. Required the dimensions of a parallelogram containing 250 acres, when the sides are in the proportion of 7 to 3.

### Answer, 3051 by 130.93 rods.

13. John and Jonathan divided a lot of land equally as to value, which contained 600 acres, and which was appraised at \$2 per acre. John's division was valued at 50 cents per acre more than Jonathan's. What were the contents and price per acre of each division. Answer. John's division contained 263 acres and 12 rods, and the price per acre was \$2.28 1-10 nearly.

Jonathan's division contained 336 acres, 3 roods, and 28

rods, and the price per acre was \$1.78 1-10 nearly.

14. The state of Connecticut contains a little more than 4,828 square miles, or 3,090,000 acres, including rivers, harbours, creeks, roads, &c. If this quantity is laid in a square, what will be the length of a side?

\* This may be solved geometrically.

# M. Q. R. Answer, 69 1 75.11.

One word of advice to the young surveyor, who is coming forward to be useful in his occupation, will close the ap-

pendix.

In the choice of assistants to perform practical operations, never call to your aid Sir Richard Rum. He frequently changes his name to brandy, gin, whiskey, &c. He is treacherous, and he causes the head to whirl, the body to reel, and the foot to stumble.

By his might, the strong man has fallen, and the promis-

ing youth has been brought to an untimely grave.

If you employ Sir Richard, your columns of latitude may differ too much for correct work, and your columns of departure may be still worse. He never can render you the least service in establishing your reputation as an accurate surveyor, but there is danger that he may do much to destroy it.

Note.—Such theory as is more curious than useful, however correct it may be, has been excluded from the appendix. The plainest methods have been selected. On some points, the Author has been more minute, on account of the fact that many copies of this book are bought by men who do not expect to be surveyors, and who do not place themselves under instructors.

If some repetition is to be found in this work, the learner will find less fault with it than the critic.

Hebron, (Conn.) June, 1835.

### LOGARITHMS.

The learner, who, for the first time, becomes acquainted with the wonderful properties of Logarithms, may be not a little surprised to find himself introduced to a system of numbers, so new in their nature, and which, surpassing all his former knowledge of figures, afford so many facilities for shortening the labour and lessening the difficulty of arithmetical calculations.

He will admire to find, that by help of these, the labour of hours, and in some calculations, even the labour of days, may be reduced to as many minutes! The invention of Logarithms was justly regarded as "a favour from heaven;" because, in many departments of science, essen-

tial to the happiness of man, they have saved him ages of toil.

Although it does not come appropriately into the design of a work like this, to enter minutely into the history of their invention, nor the yet more difficult process by which they were originally constructed, yet a familiar explanation of their properties and uses, adapted to the apprehension and wants of the practical surveyor, is necessary, in order to his making a proper application of their great advantages in practice.

Logarithms, then, we may first observe, never stand for the numbers themselves, of which they are composed, but invariably for other numbers, of which they are only the representative exponents, or indices. Their great utility in arithmetical operations, consists, chiefly, in this,—that addition takes the place of multiplication, and substraction that of division. That is, to multiply numbers, we have only to add their logarithms; to divide, we have only to substract the logarithm of the divisor from that of the dividend; to raise a number to any power, we multiply its logarithm by the exponent of that power; and to extract the root of any number, we merely divide its logarithm by the number expressing the root to be found.

The constant number upon which the tables in common use are constructed, and which is called the base of the tables, is 10; and every conceivable number, large or small, integral, mixed, or decimal, is

considered as some ascertained power or root of 10.

Indices.	Nun	ibers.		Logarithms.
101 the first power	of ten is	10, whose	exponent is	1.
102 the second pow	ver of ten is	100, whose	exponent is	
103 the third powe	r of ten is 1	,000, whose	exponent is	3.
104 the fourth pow	er of ten is 10	,000, whose	exponent is	4.
105 the fifth power			exponent is	5.
106 the sixth powe	r of ten is 1,000	0,000, whose	exponent is	6.

Note. It may be remarked, that the first power of any number, is that number once repeated, or it is the number itself: The second power of any number is the product of that number multiplied once by itself: The third power of a number, is the product of the number multiplied twice by itself; the fourth power of a number, is the product multiplied three times by itself, &c. The index denoting the power, is called, in common arithmetic, the exponent of that power; and is, in other words, the logarithm of the power.

Logarithms, then, are the Exponents of a series of powers and roots. In the above series, the logarithms indicate how many ciphers belong to their corresponding numbers. Thus, the logarithm 1 stands for 10, or 1 and one cipher; the logarithm 2 stands for 100, or 1 and two ci-

phers; the logarithm 3 for 1000, or 1 and three ciphers, &c. Now, if we multiply 10,000 by 100, the product will be 1,000,000, whose logarithm is 6; but to obtain this, we need only add the logarithms 2 and 4, which stand opposite the numbers to be multiplied. On the contrary, if we divide 1,000,000 by 100, the quotient will be 10,000, whose logarithm is 4: but to obtain this, we need only to substract 2, the logarithm

of the divisor, from 6, the logarithm of the dividend.

Again, the square of 1000, that is, the product of 1000 multiplied by itself, is 1,000,000, whose logarithm is 6; but to obtain the square of 1000, we need only double its logarithm 3. On the other hand, the cube root of 1,000,000 is 100, whose logarithm is 2; but this is obtained by dividing 6, the logarithm of the given number, by 3, the index of the root. Hence it is manifest, that the protracted labour of multiplying or dividing one large number by another, the tedious evolution of roots, and the various mistakes incident to long operations, may be almost entirely obviated by the use of logarithms.

As the logarithm 1 is always 0, and that of 10 is but 1, the logarithms of all numbers below 10, will be decimals; and as the logarithms in the common system increase regularly by 1, according to the integral powers of 10, it follows that the logarithms of all numbers between 10 and 100, will be more than 1, but less than 2—that is, they will be 1 and a decimal; the logarithms of all numbers between 100 and 1000, will be between 2 and 3—that is, they will be 2 and a decimal; and the logarithm of all numbers between 1000 and 10,000, will be between 3

and 4—that is, 3 and a decimal.

A logarithm generally consists of two parts; a whole number, and a decimal. This whole number, or integer, is called the characteristic, or index, of the logarithm, and is always one less than the number of integral figures in the natural number, whose logarithm is sought. As the index of the logarithm is omitted in the tables, it is important to recollect the principle, or rule, by which it is to be supplied, whenever it is wanted in calculation. Thus, the logarithm of 8 is 0.903090. Here, the number (8) consists of but one figure, and the index of its logarithm, being one less, must be 0. Again, the logarithm of 16 is 1.204120. Here, the given number (16) consists of two figures, and the index of its logarithm, being one less, must be 1. Again, the logarithm of 640 is 2.806180. Here, the given number (640) consists of 3 figures, and the index of its logarithm, being one less, must be 2, &c. The rule holds universally true, that the index of a logarithm is always one less than the number of integral figures in the natural number, whose logarithm is sought.

The same rule holds in mixed numbers. The logarithm of 6.40 is 0.806180, the same as for 640, (see the last example,) differing only in the index. Here, the integral part (6) of the given number, consists of but one figure, and the index of its logarithm, being one less, must be 0. And, generally, having obtained the logarithm of any number, large or small, we have only to change the index, agreeably to the above rule, in order to obtain the logarithm of every other number, consisting of the same significant figures, whether they be integral, fractional,

or mixed. Thus:-

The logarithm of 7596	is 3.880585
759.6	2.880585
75.96	* 1.880585
7.596	0.880585
.7596	-1.880585
.07596	-2.880585
.007596	-3.880585

When the natural number is less than 1, the index of its logarithm becomes less than 0, or negative; and is indicated by placing the sign,—, just before, or above it. Suppose it were required to affix the proper index to the logarithm of .000007596. Here, the number of cyphers on the left, including the decimal point, is 6, which being fitted with the negative sign,—, becomes the proper index of the logarithm. And universally, The negative index is always equal to the number of ciphers on the left, including the decimal point.

Before any one can avail himself of the great advantages of logarithms, in expediting the operations of Arithmetic and Trigonometry, he must become so familiar with the tables, that he can readily find the logarithm of any number; and, on the other hand, the number to

which any logarithm belongs.

#### DIRECTIONS FOR TAKING LOGARITHMS AND THEIR NUMBERS FROM THE TABLE.

Note. In the common tables, the *Indices* to the logarithms of the first 100 numbers are inserted. But for all other numbers, the *decimal part* only of the logarithms is given: while the index is left to be supplied, according to the principles already laid down.

PROBLEM I.— To find the logarithm of a number between 1 and 100.

RULE. Look for the proposed number on the left; and against it, in the next column, will be the logarithm with its index.

Example. The logarithm of 50 is 1.698970. The logarithm of 89

is 1.949390.

PROBLEM II. To find the logarithm of any number between 1 and 1000: or of any number consisting of not more than three significant figures, with ciphers annexed.

Rule. Find the given number in the left hand column of the table, and directly opposite, in the next column, is the decimal part of its logarithm, to which apply the index, as already taught.

Example. The logarithm of 140 is 2.146128. The logarithm of 781 is 2.892651; of 358 is 2.553883; of 974 is 2.988559.

The decimal part only of these logarithms are found in the table; the index 2, was affixed to each, because the given numbers consisted, each, of three integral figures. If there had been ciphers annexed to the significant figures of the given numbers, as 1400, 35800, &c., their logarithms would have been precisely the same, with the exception of the index only; and consequently, would be found in the same place in the table. Thus:—

The log. of 1400 is 3.146128. The log. of 781000 is 5.892651. of 35800 4.553883. Of 9740000 6.988559.

Here the decimal part of the logarithm is the same as before; while the index has been increased as many units, as there are ciphers annexed to the given numbers. This rule will hold good in all similar cases.

PROBLEM III. To find the logarithm of any number consisting of four figures, either with or without ciphers annexed.

RULE. Look for the three first figures, on the left hand, and for the fourth figure, at the top of one of the columns; the logarithm will be

found opposite the three first figures, and in the column which, at the

head, is marked with the fourth figure.

By reference to the table, it will be seen, that each page contains ten columns of logarithms, which are severally numbered from 0 to 9. The first column, alone, contains six figures; while every other column has only four figures: but it is to be always remembered that the two first figures of the left hand column, are common to each of the other columns, and were omitted only to avoid repetition. These two initial figures, therefore, are to be prefixed to each of the other four, since every logarithm, in our table, consists of six figures, besides the index. Example. The log. of 3657 is 3.563125. The log. of 6704 is 3.826334. of 5696 is 3.755570.

In the last example, as it will frequently happen, the two initial figures (93) of the logarithm, are not found, in the same line, with the given number, (851,) but in the next below it:—And, universally, whenever the third figure of the logarithm changes, from 9 to 10, the cipher only is retained in the column, while the one is carried down to the next lower initial, on the left. To guard against a mistake here, points have been substituted in place of ciphers; and wherever these points are found, the ciphers are to be reinstated, and the two initials taken from the line below. To be more particular, in the above example; on turning to page 14 of the logarithms, and against 851, the learner will find 92 for the two initial figures, which he must prefix to the other four figures in the first and second columns, but no farther. There he must stop, and taking the two initial figures in the line below, against 852, carry them up to the third. column, where the dots commence, and prefix the same to each of the remaining columns: and so in all similar cases.

PROBLEM IV. To find the logarithm of a number consisting of five or six figures.

Rule. Find the logarithm of the first four figures of the given number, as taught in the last problem. Take the remaining figures and multiply them into the number standing opposite, in the outside column, headed D; from the right of the product, reject as many figures as you multiplied by, and add what is left to the logarithm previously found. This sum, being fitted with a proper index, will be the logarithm required.

EXAMPLE. Required the logarithm of 45263. Thus—
The logarithm of 45260 is
4.655715
The difference D is 96, which being multiplied by 3 gives
28.8

Logarithm of 45263 required,

EXAMPLE 2. Required the logarithm of 758936. Thus—
The logarithm of 758900 is

The difference D is 57, which, being multiplied by 36, gives

20.52

Logarithm of 758936 required, 5.880205

Note. This process of finding the logarithms of large numbers, supposes that they increase in the same ratio as their numbers, which is not strictly true, though sufficiently near the truth for general practice. It may be remarked, however, that these ratios approach that of equality, the larger the numbers, and the less they differ from each other.

The column marked D, contains the average mean differences of the ten logarithms against which they stand, and, consequently, do not always correspond exactly to each of the differences, taken separately;

wherefore, when great accuracy is required, it may be necessary, particularly in the first part of the table, to work by

PROBLEM V.— To find the logarithm of a number consisting of six or seven figures.

Rule. Find the logarithm of the first four figures, as before, and take the difference between this logarithm and the next greater, in the table; multiply this difference by the remaining figures of the given number; reject, from the right of the product, as many figures as you multiply by, and add what is left to the logarithm before found; this sum being fitted with a proper index, will be the logarithm required.

Example. Required the logarithm of 4526375.

To the first four figures, add as many ciphers as there are other figures in the proposed number, then find the logarithm, which substract from the next greater. Thus—

The next greater number is 4527000 and its log. is 6.655810 given number 4526000 6.655715 1000 diff. of numbers, diff. of logs. 95 multiply by the other figures of the given number 375 35.625 for the proportional part to be added to the log. of the first part 6.655715 . 6.655750 and it gives the log. of 4526375, required.

PROBLEM VI.- To find the logarithm of a fraction.

RULE. Substract the logarithm of the denominator from that of the numerator, or, reduce the fraction to a decimal, and take out the logarithm as for a whole number, fitting it with a proper index.

EXAMPLE. Required the logarithm of  $\frac{3}{4}$ , or .75.

The log. of the numerator (3) is

of the denominator (4) is

Log. of  $\frac{3}{4}$ , or .75.

Answer,—1.875061

PROBLEM VII.—To find the Natural Number belonging to any logarithm.

Rule 1. If the logarithm be found within the limits of the table; that is, if its index do not exceed 3; then, neglecting the index, look down in the column of logarithms, under 0, for the two or three first figures of your given logarithm, and if you exactly find all the figures of the given logarithm in that column, you will have the corresponding number in the adjoining column, on the left.

RULE 2. If the logarithm be not found, exactly, in the column under 0, look through the other columns, on the right, till you find it exactly, or very nearly; and in the column of numbers directly against it, you will have the first three figures of the number sought, to which join the figure at the top of the column, in which the logarithm was found, and you will have the number required.

Note. When the number is found, you must point off decimals from it, or annex ciphers to it, if necessary, to make it correspond with the *Index* of your logarithm, as already taught.

#### EXAMPLES.

Logarithms.	Numbers.
3.880585	7596
2.402089	252.4
1.514946	32.73
0.629919	4.265
1.811508	.6479
-2.907680	.08085
-3.962464	.009172

When great accuracy is required, and the given logarithm is not exactly, or very nearly, found in the table, it will be necessary to reverse the rule, under Problem IV. or V. Thus:

Rule 3. From the given logarithm substract the next less, in the table; annex to the difference as many ciphers as you wish the number of figures in the answer to exceed four. Then divide this difference by the common difference in the side column D, and annex the quotient to the natural number belonging to the less logarithm, and you will have the number required.

Example 1. Required the natural number belonging to the logarithm

next less log. 3.441049
3.440909 corresponding number 2760

divide by com. D = 157)14000(quotes .89

Number required, 2760.89

EXAMPLE 2. Required the number corresponding to the logarithm -3.441049.

The operation in this example, is the same as in the first. Having found the corresponding number, as before, prefix the number of ciphers indicated by the negative index, thus, 0.00276089.

PROBLEM VIII.—Directions for taking the logarithmic sines and tangents, and the logarithmic co-sines and co-tangents, from the table.

Note. Logarithmic sines and tangents are the logarithms of the natural sines and tangents, which represent the length of the different sides of triangles.

RULE 1. If the given angle is less than 45°, look for the degrees at the top of the table, and the minutes on the left; then opposite the minutes, and under the word sine, at the head of the column, will be found the logarithmic sine; under the word tangent, will be found the logarithmic tangent, &c., of the angle required. Thus—

Sine of 12° 35' is 9.338176 Co-sine of 21° 40' is 9.968179 Tangent of 38° 5' is 9.894111 Co-tangent of 9° 55' is 10.757300

Note. The first figure is the index, and the other figures are the decimal part of the logarithms.

Rule 2. If the given angle is between 45° and 90°, look for the degrees at the bottom of the table, and for the minutes on the right; then, opposite to the minutes, and over the word sine, at the foot of the col-

umn, will be found the sine; over the word tangent, will be found the tangent, &c., of the angle sought. Thus—

Sine of 81° 20' is 9.995013 Co-sine of 89° 15' is 8.116926 Tangent of 73° 25' is 10.526081 Co-tangent of 54° 5' is 9.859932

Rule 3. If the given angle is between 90° and 180°; substract it from 180°, and take out the tabular sine or co-sine, tangent or co-tangent, of the remainder. Thus—

Sine of 99° is the sine of 81° Co-s. of 111° 55′ is the co-s. of 68° 5′ Tangent of 102° is the tang. of 78° Co-t. of 127° 8′ is the co-t. of 52° 52′

Having thus found the *supplement* of the angle, when it is *obtuse*, that is, when it exceeds 90°, with this supplement, take out the tabular sine or co-sine, tangent or co-tangent, by Rule 1st or 2d.

Rule 4. If there are seconds in the given angle; find the tabular number for the degrees and minutes, as before; then multiply the opposite number in the adjoining column D, by the seconds, cut off two figures from the right of the product, and add what remains to the logarithm, before found, for sines and tangents, but substract it for co-sines and co-tangents, and the sum or difference will be the angle required. Thus—

1. Required the log. sine of 28° 42′ 5″.  Sine of 28° 42′ is  D=384 multiplied by 5″ =	9.681443 19.20
Sine of 28° 42′ 5″ Ans.	9.681462
2. Required co-tangent of 39° 17′ 10″.  Co-tangent of 39° 17′ is  D = 430 multiplied by 10 =	10.087244 43.00
Co-tangent 39° 17′ 10″ Ans.	10.087201

PROBLEM IX.-- To find the logarithmic secant or co-secant of an angle.

RULE 1. To find the logarithmic secant of an angle: substract the logarithmic co-sine of the same angle from 20.000000.

RULE 2. To find the logarithmic co-secant of an angle: substract the logarithmic sine of the same angle from 20.000000.

PROBLEM X.—To find the degrees and minutes corresponding to any logarithmic sine or tangent.

RULE 1. Look in the column of the same name with what you wish to find, for the sine or tangent which is nearest to the given one; and if the title be at the head of the column, take the degrees at the top of the table, and the minutes on the left; but if the title be at the foot of the column, take the degrees at the bottom, and the minutes on the right.

EXAMPLE. Find the number of degrees and minutes corresponding

to the logarithmic sine 9.673971.

The nearest sine in the table is 9.673977. The title of sine is at the head of the column in which the number is found, and the degrees at the top of the page are 28, and the minutes on the left are 10. The angle required is, therefore, 28° 10′, neglecting the small surplus fraction of 6, in the last figure of the logarithm.

When the given logarithmic sign or tangent is not found exactly, or very nearly, then, for the seconds,—

RULE 2. From the given logarithm, substract the next less in the table, annex two ciphers to the remainder, and divide it, thus augmented, by the tabular difference D, and the quotient will be the number of seconds to be added to the degrees and minutes of the tabular logarithm, for sines and tangents, but which must be substracted for co-sines and co-tangents.

EXAMPLE. Required the degrees, minutes, and seconds, corresponding to the logarithmic sine of 9.759567.

Given logarithm 9.759567Next less in the table = 9.759492 =  $35^{\circ}$  5' Divide by tab. diff. 300)7500(quotes = 25''

Angle required,= 35° 5′ 25″

#### MULTIPLICATION BY LOGARITHMS.

RULE. Take from the table the logarithms of all numbers to be multiplied, add them together, and their sum will be the logarithm of the product. Then, by means of the table, take out the natural number, corresponding to this sum, for the product sought.

Observe, that whatever is to be carried from the decimal part of the logarithm, is always positive, and must be added to the positive, or sub-

stracted from the negative index or indices.

#### EXAMPLES.

Numbers. 1. Mult. 326 by 85	Logarithms. 2.513218 1.929419	Numbers. 2. Mult.8.25 by 112	Logarithms. 0.916454 2.049218
Prod. 27710	4.442637	Prod. 924.00	2.965672

3. Multiply the following numbers together: 3.902, 597.16, and .0314728.

 Numbers.
 Logarithms.

 3.902
 0.591287

 597.160
 2.776091

 .0314728
 2.497935

 73.3333
 1.865313

Prod. 73.3333 1.865313
Here, the  $\overline{2}$  cancels the 2, and the 1 to carry, from the decimal part of the logarithms, is set down.

4. Multiply 3.586, and 2.1046, and 0.8372, and 0.0294, all together.

 Numbers.
 Logarithms.

 3.586
 0.554610

 2.1046
 0.323170

 0.8372
 7.922829

 0.0294
 2.468347

 0.105762
 7.268956

Here, the 2 to carry cancels the  $\overline{2}$ , and there remains the  $\overline{1}$  to set down for the index of the product.

In practice, however, it is usual to make all the indices positive. This is done by adding 10 to each negative index; observing to reject an equal number from the final result.

Thus, for negative—1, we may put down positive 9. for negative—2, we may put down positive 8. for negative—3, we may put down positive 7, &c.

Because, minus 1, plus 10, equals 9.
minus 2, plus 10, equals 8.
minus 3, plus 10, equals 7, &c.

5. Repeating the third example, we have

Logarithms. Numbers. Logarithms. 3.9020.591287 = 10.5912872.776091 =597.160 2.776091 .0314728 ₹.497935 or 8.497935

Prod. 73.3333 1.865313 1.865313

Here the sum of the indices is 11: from which reject 10, and the result is the same as before.

#### COMPOUND INTEREST BY LOGARITHMS.

RULE. Find the amount of 1 dollar for 1 year; multiply its logarithms by the number of years; and to the product, add the logarithm of the principal. The sum will be the logarithm of the amount for the given time.

From the amount substract the principal, and the remainder will be

the interest.

Example. The last example in Daboll's Arithmetic, under Compound Interest, is as follows: - "What will 50 dollars amount to in 20 years at 6 per cent."

This question wrought out in the most expeditious manner by common arithmetic, would take the student scarcely less than three hours, and the final result would be, if done correctly,

\$160.3567736106422365941496492288974572748800.

But, by logarithms, this sum may be done in as many minutes, and the correct answer, in dollars and cents, obtained with very few figures.

Amount of 1 dollar for 1 year is 1.06 logarithm 0.0253059 Multiply by the time 20 0.5061180 Add log. of principal 50 1.6989700

> Amount as above = \$160.35,7 2.2050880

From the foregoing general principles of the nature and application of logarithms, are derived an infinite number of specific rules, adapted to particular cases.

#### OF THE TABLE OF NATURAL SINES AND TANGENTS.

To those who are unacquainted with logarithms, it will be interesting to know, that all the cases in right and oblique angled trigonometry, contained in this work, or which are necessary in rectangular

surveying, may, by the help of natural sines and tangents, be solved exactly in the same way, and with the same facility, as he would solve a simple question in the Rule of Three. Natural sines are merely decimals, bearing the same proportion to unity, or 1, that the corresponding number of degrees and minutes bears to radius, or 90°. Natural tangents bear the same proportion to unity, or 1, that the corresponding number of degrees and minutes bears to 45°, because it is a well known principle, that the sine of 90°, and the tangent of 45°, are each equal to radius. That is, I is assumed as the natural sine of 90° in the table of natural sines, and as the tangent of 45° in the table of tangents, and every other number in each of these tables, is calculated accordingly.

GENERAL RULE. 1. State the question in every case, as already taught: 2. Multiply the second and third terms together, and divide

the product by the first.

The manner of taking natural sines and tangents from the tables, is the same as for logarithmic sines and tangents; only that there is in the tables, no column of differences as in the latter, for the more readily finding the odd seconds, when required. But these may be found by making a proportion for the aliquot parts.

There are some problems to which natural tangents afford a much

more simple and ready solution, than any process by logarithms. The

following one, in heights and distances, will illustrate this.

The altitude of an inaccessible object taken at an unknown distance from its base, is 55° 54'; and when taken again at the distance of 93 feet from the place of the first observation, in a direct line with it, the altitude is 33° 20': Required, the height of the object.

Rule. Divide the difference of the natural co-tangents of the an-

gles of elevation, by the distance between the stations. Thus-Co-tangent of 33° 20' is 1.52043 of 55° 54' is .67705

feet. .84338)93.0000(110.27 Ans. Divide by the diff. =

Note. This is the shortest solution possible, and perfectly easy.

Again: Given the latitude and departure, in transverse sailing or

surveying, to find the course.

RULE. Divide the departure by the latitude, the quotient will be the natural tangent of the course: or, divide the latitude by the departure, and the quotient will be the co-tangent of the course. Universally, If in any right angled triangle, the perpendicular be divided by the base, the quotient will be the tangent of the angle at the base; and if the base be divided by the perpendicular, the quotient will be the tangent of the angle at the vertex of the perpendicular.

OF THE TRAVERSE TABLE, OR TABLE OF LATITUDE AND DEPARTURE.

This is calculated for degrees and quarters of degrees, and for any distance up to 100 rods, chains, &c.; by which the northings and southings, eastings and westings, made in a survey, may be found.

PROBLEM XII.— To find the latitude and departure, or northing, &c. for any course and distance.

If the course be less than 45°, look for it at the top, but if more than 45°, at the bottom of the page, and look for the distance in the right or left hand column; against the distance, and directly under or over the course, stand the northing, &c. in whole numbers and decimals.

If the course be less than 45°, the northing or southing will be great-

er than the easting or westing; but if more than 45°, the easting or

westing will be the greatest.

When the distance exceeds 100, take any two or more numbers, which, added together, will equal the distance, and find the latitude and departure for each of these numbers; add the several latitudes together, and the sum will be the whole latitude; and so for the departure. And when the distance is in chains and links, or whole numbers and decimals, find the latitude, &c. for the chains or whole numbers, and then for the links and decimals, remembering to remove the decimal point in the table further to the left, according to the given decimal.

1. Required the latitude and departure for 45 rods, on a course N. 15° 15′ W.

Under 15° 15', and against 45, is 43.42 for the northing, and 11.84 for the westing.

2. Required the latitude and departure for 120 rods, on a course S.

58° 30′ É.

Take one third of 120, which is 40; against this number, over 58° 30′, is 20.90 for the latitude, and 34.11 for the departure. These multiplied by 3 give 62.70 for the southing, and 102.33 for the easting.

3. Required the latitude and departure for 37.36 rods, or 37 chains

and 36 links, on a course N. 26° 45' E.

For 37. 0.36 37.36	Lat. 33.04 .32	Dep. 16.65 .16
37.36	33.36	16.81

Northing 33.36, Easting 16.81.

Note. When the minutes are not 15, 30, or 45, the northings, &c. may be had by proportion, or they may be calculated by natural sines, or by trigonometry.

PROBLEM XIII.—To calculate the northing or southing, &c. for any course and distance, by natural sines.

Find the nat. sine and co-sine of the course, and into each of these multiply the distance; the products will be the latitude and departure required.

Required the latitude and departure for 6 chains and 22 links on a

course N. 38° 27′, W.

Nat. sine of 38° 27′, 0.62183 6.22	Nat. co-sine, 0.78315 6.22		
124366	156630		
124366	156630		
373098	469890		
3.8677826 Answer. Northing, 4.87.	4.8711930 Westing, 3.87.		

## USEFUL NUMBERS, AND THEIR LOGARITHMS.

	Numbers.	Logarith.
Circumference of a circle to diameter, 1)	2.14150005050	0.4021400
Area of a circle to radius,	[3.14159265359]	0.4971499
Surface of a sphere to diameter, 1)	6.28318530718	0.7980799
Circumference of a circle to radius, 1 Solid contents of a sphere to diameter. 1	0.26516930718 $0.52359877560$	-1.8950899
Solid contents of a sphere to diameter, 1 Solid contents of a sphere to radius, 1	4.18879020479	0.6220886
Square of 3.14159265359	9.86960440109	0.9942997
Square root of 3.14159265359  Square root of 3.14159265359	1.77245385091	0.3342337
1-360 of 3.14159265359	0.00872664626	-3.9408474
1-24 of 3.14159265359	0.13089969390	-1.1169387
1-4 of do. or area of cir. to diam. 1	0.78539816340	-1.8950899
365th root of \$1.05, or amount of \$1. for 1 day,	-	
365th root of \$1.06, or amount of \$1. for 1 day,		0.00006933
12th root of \$1.05, or amount of \$1. for 1 mo.		0.00176577
12th root of \$1.06, or amount of \$1. for 1 mo.		0.00210882
360 degrees expressed in seconds,	1296000	
Arc, equal to radius, in degrees,	57.295780	
in minutes,	3437.74677	3.5362739
in seconds,	206264.8	5.3144251
Length of an arc of 1"= sine of 1"	0.000004848	-6.6855749
of $2'' = \sin \theta$ of $2''$	0.000009696	-6.9866049
of $3'' = \sin \theta$ of $3''$	0.000014544	-5.1626961
of $1' = \text{sine of } 1'$	0.000290888	
of 1°	0.017453293	-2.2418774
Sine of 1°	0.017452406	
Mile, reduced to rods,	320	
yards,	1760	
feet,	5280	
inches,	63360	
Square mile, in acres,	640	
square rods,	102400	
square yards,	3097600	
square feet,	27178400	
square inches,	4014489600	
Equatorial diameter of the earth, in miles,	7924 2535680	3.8989445
in rods,	13946240	
in yards, in feet,	41838720	
in inches,		
Circumference of the Equator, in miles,	24893.98	
in feet,	131440217	
in inches,	1577282608	}
Radius of Earth's orbit, in miles,	95273869	7.9789738
Sun's horizontal parallax,	8".57760	
Log. sine =tangent of 8".5776	0 .07.00	5.6189407
The same same of the same same same same same same same sam		3.0200.

### A TABLE

OF

### LOGARITHMS OF NUMBERS

FROM 1 TO 10,000.

-			بيور سيبيدين			_	
N.	Log.	N.	Log.	N.	Log.	N.	Log.
1	0.000000	26	1.414973	51	1.707570	76	1.880814
2	0.301030	27	1.431364	52	1.716003	77	1.886491
3	0.477121	28	1.447158	53	1.724276	78	1.892095
4	0.602060	29	1.462398	54	1.732394	79	1.897627
5	0.698970	30	1.477121	55	1.740363	80	1.903090
$\overline{6}$	0.778151	31	1.491362	$\overline{56}$	1.748188	81	$\overline{1.908485}$
7	0.845098	32	1.505150	57	1.755875	82	1.913814
8	0.903090	33	1.518514	58	1.763428	83	1.919078
9	0.954243	34	1.531479	59	1.770852	84	1.924279
10	1.000000	35	1.544068	60	1.778151	85	1.929419
li	$\overline{1.041393}$	36	1.556303	$\overline{61}$	1.785330	$ \overline{86} $	1.934498
12	1.079181	37	1.568202	62	1.792392	87	1.939519
13	1.113943	38	1.579784	63	1.799341	88	1.944483
14	1.146128	39	1.591065	64	1.806180	89	1.949390
15	1.176091	40	1.602060	65	1.812913	90	1.954243
$\overline{16}$	1.204120	41	$\overline{1.612784}$	$\overline{66}$	1.819544	$ \overline{91} $	1.959041
17	1.230449	42	1.623249	67	1.826075	92	1.963788
18	1.255273	43	1.633468	68	1.832509	93	1.968483
19	1.278754	44	1.643453	69	1.838849	94	1.973128
20	[1.301030]	45	1.653213	70	1.845098	95	1.977724
$\overline{21}$	$\overline{1.322219}$	46	1.662758	71	1.851258	$\overline{96}$	$\overline{1.982271}$
22	1.342423	47	1.672098	72	1.857333	97	1.986772
23	1.361728	48	1.681241	73	1.863323	98	1.991226
24	1.380211	49	1.690196	74	1.869232	99	1.995635
25.	1.397940	50	1.698970	75	1.875061	100	2.000000

N. B. In the following table, in the last nine columns of each page, where the first or leading figures change from 9's to 0's, points or dots are introduced instead of the 0's through the rest of the line, to catch the eye, and to indicate that from thence the annexed first two figures of the Logarithm in the second column stand in the next lower line.

N.	0	1	2	3	4	5	6	7	8	9	D.
100	000000	0434	0868	1301	1734	2166	2598	3029	3461	3891	432
101	4321	4751	5181	5609	6038	6466	6894	7321	7748	8174	428
102	8600	9026	9451	9876	.300	.724	1147	1570	1993		424
103	012837	3259	3680	4100	4521	4940	5360	5779	6197	6616	419
104	7033	7451	7868	8284	8700	9116	9532	9947	.361	.775	416
105	021189	1603	2016	2428	2841	3252	3664	4075	4486	4896	412
106	5306	5715	6125	6533	6942	7350 1408	7757	$\begin{array}{c} 8164 \\ 2216 \end{array}$	8571	8978 3021	408
$\begin{array}{c} 107 \\ 108 \end{array}$	$9384 \\ 033424$	9789 3826	$\frac{.195}{4227}$	$\begin{array}{c} .600 \\ 4628 \end{array}$	1004 5029	5430	1812 5830	$\begin{array}{c} 2210 \\ 6230 \end{array}$	$\frac{2619}{6629}$	7028	404 400
109	7426	7825	8223	8620	9017		9811	.207	.602	.998	396
$\frac{103}{110}$					$\frac{3017}{2969}$	$\frac{3111}{3362}$	$\frac{3011}{3755}$	$\frac{120}{4148}$	$\frac{1002}{4540}$	$\frac{1000}{4932}$	$\frac{393}{393}$
111	$\begin{array}{c} 041393 \\ 5323 \end{array}$	1787 5714	$\frac{2182}{6105}$	2576 6495	6885	7275	7664	8053	8442	8830	389
112	$\begin{array}{c} 3323 \\ 9218 \end{array}$	9606	9993	.380	.766		1538	1924	2309	2694	386
113	053078	3463	3846	4230	4613	4996	5378		6142	6524	382
114	6905	7286	7666	8046	8426	8805	9185	9563	9942	.320	379
115	060698	1075	1452	1829	2206		2958	3333	3709	4083	376
116	4458	4832	5206	5580	5953		6699	7071	7443		372
117	8186	8557	8928	9298	9668	38	.407	.776	1145		369
118	071882	2250	2617	2985	3352	3718	4085	4451	4816	5182	366
119	5547	5912	$\frac{6276}{}$	6640	7004	7368	7731	8094	8457	8819	363
120	079181	9543	9904	.266	.626	.987	1347	1707	2067	2426	360
121	082785	3144	3503	3861	4219	4576	4934	5291	5647	6004	357
122	6360	6716	7071	7426	7781	8136	8493	8845	9198	9552	355
123	9905	.258	.611	.963	$\begin{array}{c} 1315 \\ 4820 \end{array}$	1667	2618	2370	2721	3071	351
$\begin{bmatrix} 124 \\ 125 \end{bmatrix}$	$\begin{array}{c} 093422 \\ 6910 \end{array}$	3772 7257	4122 7604	4471 7951	8298	5169 8644	5518 8990	5866 9335	$\begin{array}{c} 6215 \\ 9681 \end{array}$	$\begin{array}{c} 6562 \\ 26 \end{array}$	349 346
126	100371	0715	1059	1403	1747	2091	2434	2777	3119	3462	343
127	3804	4146	4487	4828	5169	5510	5851	6191	6531	6871	340
128	7210	7549	7888	8227	8565	8903	9241	9579	9916	.253	338
129	110590	0926	1263	1599	1934	2270	2605	2940	3275	3609	335
130	$\overline{113943}$	4277	4611	$\overline{4944}$	5278	5611	5943	6276	6603	$\overline{6940}$	$\overline{333}$
131	7271	7603	7934	8265	8595	8926	9256	9586	9915	.245	330
132	120574	0903	1231	1560	1888	2216	2544	2871	3198	3525	328
133	3852	4178	4504	4830	5156	5481	5806	6131	6456	6781	325
134	7105	7429	7753	8076	8399	8722	9045	9368	9690	12	323
135 136	130334 3539	0655 3858	$0977 \\ 4177$	$\begin{array}{c} 1298 \\ 4496 \end{array}$	4814			2580 5769			321
137	6721	7037	7354	7671	7987	8303	8618	8934	9249	9564	318 315
138	9879	.194	.503	822	1136	1450	1763	2076	2389	2702	314
139	143015	3327	3639	3951	4263	4574	4885	5196	5507	5818	311
140	$\overline{146128}$	$\overline{6438}$	6748	7058	7367	7676	7985	$\overline{8294}$	8603	8911	309
141	9219		9835	.142	.449	.756	1063	1370	1676	1982	307
142	152288	2594	2900	3205	3510	3815	4120	4424	4728		305
143	5336		5943	6246	6549	6852	7154	7457	7759		303
144	8362	8664	8965	9266	9567	9868	.168	.469	.769	1068	301
145	161368	1667	1967	2266	2564	2863	3161	3460	3758	4055	299
146 147	4353 .7317	$\frac{4650}{7613}$	4947 7908	$\begin{array}{c} 5244 \\ 8203 \end{array}$	5541 8497	5838 8792	6134	6430	6726	7022	297
148	170262	0555	0848		1434	1726	$\frac{9086}{2019}$	$9380 \\ 2311$	9674 2603	$\frac{9968}{2895}$	295 293
149	3186	3478	3769	4060	4351	4641	4932	5222	5512	5802	291
$\frac{150}{150}$	176091	$\frac{6381}{6381}$	$\frac{6670}{6670}$	$\frac{1000}{6959}$	$\frac{1001}{7248}$	$\frac{7536}{7536}$	$\frac{7825}{7825}$	8113	$\frac{3312}{8401}$	8689	$\frac{231}{289}$
151	8977		9552	9839	.126	.413	.699	.985	$\frac{3401}{1272}$	1558	287
152	181844		2415	2700	2985	3270	3555	3839	4123	4407	285
153	4691	4975	5259	5542	5825	6108	6391	6674	6956	7239	283
154	7521	7803	8084	8366	8647	8928	9209	9490	9771	51	281
155	190332		0892	1171	1451	1730	2010	2289	2567	2846	279
156 157	$\begin{array}{c} 3125 \\ 5899 \end{array}$		3681	3959	4237			5069			278
158	8657		$\begin{array}{c} 6453 \\ 9206 \end{array}$		7005 9755	$\begin{bmatrix} 7281 \\ \dots 29 \end{bmatrix}$	$\begin{array}{c} 7556 \\ .303 \end{array}$	7832			276 274
159	201397		1943								
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27	1 0		1 0	1 0		1 -		~ 1			-
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160	204120	4391	4663				5746		6286	6556	
161 162	$\begin{array}{r} 6826 \\ 9515 \end{array}$	$\begin{array}{c} 7096 \\ 9783 \end{array}$	7365	7634 .319	7904 .586	8173 .853	8441 1121	$\begin{array}{c} 8710 \\ 1338 \end{array}$	8979	9247	
163	$\begin{array}{c} 3513 \\ 212188 \end{array}$	2454	$\begin{array}{c} \cdot .51 \\ 2720 \end{array}$	2986	3252	3518	3783	4049	$\begin{array}{ c c } 1654 \\ 4314 \end{array}$	$1921 \\ 4579$	267 266
164	4844	5109	5373	5638	5902	6166	6430	6694	6957	7221	234
165	7484	7747	8010	8273	8536	8798	9060	9323	9585	9846	262
166	220108	0370	0631	0892	1153	1414	1675	1936	2196	2456	261
167	2716	2976	3236	3496	3755	4015	4274	4533	4792	5051	259
168	5309	5568	5826	6084	6342	6600	6858	7115	7372	7630	258
169	7887	8144	8400	8657	8913	9170	9426	$\underline{9682}$	9938	.193	256
170	230449	0704	0960	1215	1470	1724	1979	2234	2488	2742	254
171	2996	3250	3504	3757	4011	4264	4517	4770	5023	5276	
172	5528	5781	6033	6285	6537	6789	7041	7292	7544	7795	
173	8046	8297	8548	8799	9049	9299	9550	9800	50	.300	
174 175	240549 3038	$\begin{array}{c} 0799 \\ 3286 \end{array}$	$\begin{array}{c} 1048 \\ 3534 \end{array}$	$\begin{array}{c} 1297 \\ 3782 \end{array}$	1546 4030	$1795 \\ 4277$	$\begin{array}{c} 2044 \\ 4525 \end{array}$	$\frac{2293}{4772}$	2541 5019	2790 5266	249 248
176	5513	5759	6006	6252	6499	6745	6991	7237	7482	7728	
177	7973	8219	8464	8709	8954	9198	9443	9687	9932	.176	
178	250420	0664		1151	1395	1638	1881	2125	2368	2610	243
179	2853	3096	3338	3580	3822	4064	4306	4548	4790	5031	242
180	$\overline{255273}$	$\overline{5514}$	$\overline{5755}$	$\overline{5996}$	$\overline{6237}$	$\overline{6477}$	$\overline{6718}$	6958	$\overline{7198}$	$\overline{7439}$	$\overline{241}$
181	7679	7918	8158	8398	8637	8877	9116	9355	9594	9833	
182	260071	0310	0548	0787	1025	1263	1501	1739	1976	2214	238
183	2451	2688	2925	3162	3399	3636	3873	4109	4346	4582	237
184	4818	5054	5290	5525	5761	5996	6232	6467	6702	6937	235
185	7172	7406	7641	7875	8110	8344	8578	8812	9046	9279	234
186	9513	9746	9980	.213	.446	.679	.912	1144	1377	1609	233
187 188	271842 4158	2074 4389	$\begin{array}{c} 2306 \\ 4620 \end{array}$	2538 4850	$\begin{array}{c} 2770 \\ 5081 \end{array}$	3001 5311	3233 5542	$\frac{3464}{5772}$	$\begin{array}{c} 3696 \\ 6002 \end{array}$	$\begin{array}{c} 3927 \\ 6232 \end{array}$	$\begin{array}{c} 232 \\ 230 \end{array}$
189	6462	6692	6921	7151	7380	7609	7838	8067	8296	8525	229
$\frac{100}{190}$	$\frac{278754}{278754}$	$\frac{3002}{8982}$	$\frac{9211}{9211}$	$\frac{1}{9439}$	9667	$\frac{1005}{9895}$	$\frac{1000}{123}$	$\frac{351}{.351}$	$\frac{578}{.578}$	$\frac{3806}{806}$	$\frac{229}{228}$
191	281033	1261	1488	1715	1942	2169	2396	$\begin{array}{c} -351 \\ 2622 \end{array}$	2849	3075	227
192	3361	3527	3753	3979	4205	4431	4656	4882		5332	226
193	5557	5782	6007	6232	6456	6681	6905	7130	7354	7578	225
194	7802	8026	8249	8473	8696	8920	9143	9366	9589	9812	223
195	290035		0480				1369	1591	1813	2034	222
196	2256	2478	2699		3141	3363	3584	3804		4246	221
197	4466	4687	4907		5347		5787	6007	6226	6446	220
198	6665		7104	7323	7542		7979	8198	8416	8635	219
100	8853	$\frac{9071}{10000000000000000000000000000000000$	$\frac{9289}{1101}$	$\frac{9507}{1001}$	9725		.161	.378	.595	·813	$\frac{218}{218}$
200	301030	1247	1464	1681	1898	2114	2331	2547	2764	2980	217
$\begin{bmatrix} 201 \\ 202 \end{bmatrix}$	3196	3412	3628	3844	4059	4275	4491 6639	4706	$\frac{4921}{7068}$	5136	216
202	5351 7496	5566 7710	5781 7924	5996 8137	$\begin{array}{c} 6211 \\ 8351 \end{array}$	6425 8564	8778	6854 8991	$\begin{array}{c} 7008 \\ 9204 \end{array}$	$7282 \\ 9417$	$\begin{array}{c} 215 \\ 213 \end{array}$
204	9630	9843	56	.268	.481	.693	.906	1118	1330	1542	212
205	311754		2177	2389	2600	2812	3023	3234	3445	3656	211
206	3867		4289	4499			5130	5340	5551	5760	210
207	5970	6180	6390	6599	6809	7018	7227	7436	7646	7854	209
208	8063		8481	8689		9106	9314	9522	9730	9938	208
209	320146	0354	0562	0769	0977	1184	1391	1598	1805	2012	$\frac{207}{}$
210	322219		2633		3046	3252	3458	3665	3871	4077	206
211	4282	4488	4694		5105	5310	5516	5721	5926	6131	205
212	6336	6541	6745		7155	7359	7563	7767	7972	8176	204
213 214	$8380 \\ 330414$	8583 0617	8787	$\begin{array}{c} 8991 \\ 1022 \end{array}$	$9194 \\ 1225$	$9398 \\ 1427$	$\begin{array}{c} 9601 \\ 1630 \end{array}$	$\frac{9805}{1832}$	$\frac{8}{2034}$	211 $2236$	203 202
215	2438		$\begin{array}{c} 0819 \\ 2842 \end{array}$	3044	3245	3447	3649	3850		4253	202
216	4454	4655		5057	5257	5458	5658	5859		6260	201
217	6460	6660	6860	7060	7260	7459	7659,	7858		8257	200
218	8456	8656	8855	9054	9253	9451	9650'	9349	47	.246	199
219	340444	0642	0841	1039	1237	1435	1632	1830	2028	2225	198
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ı	220	342423	2620	2817	3014	3212	3409	3606	3802	3999	4196	197
K	221	4392	4589	4785	4981	5178	5374	5570	5766	5962	6157	196
ı	222	6353	6549	6744	6939	7135	7330	7525	7720	7915	8110	195
ı	223 224	$8305 \ 350248$	$\begin{array}{c} 8500 \\ 0442 \end{array}$	$\begin{array}{c} 8694 \\ 0636 \end{array}$	8889 0829	$\begin{array}{c} 9083 \\ 1023 \end{array}$	9278 1216	$\begin{array}{c} 9472 \\ 1410 \end{array}$	$\begin{array}{c} 9666 \\ 1603 \end{array}$	9860	54	194 193
ı	225	2183	2375	2568	2761	2954	3147	3339	$\begin{array}{c} 1003 \\ 3532 \end{array}$	$\begin{array}{c} 1796 \\ 3724 \end{array}$	$\frac{1989}{3916}$	193
1	226	4108	4301	4493	4685	4876	5068	5260	5452	5643	5834	192
ı	227	6026	6217	6408	6599	6790	6981	7172	7363	7554	7744	191
1	228 229	7935 9835	$8125 \\ 25$	8316 $.215$	$8506 \\ .404$	8696 .593	8886 .783	$9076 \\ .972$	9266 1161	$\begin{array}{c} 9456 \\ 1350 \end{array}$	9646 1539	190 189
ı	$\frac{223}{230}$	$\frac{3633}{361728}$	$\frac{120}{1917}$	$\frac{.215}{2105}$	$\frac{.404}{2294}$	$\frac{.533}{2482}$	$\frac{2671}{2671}$	$\frac{2859}{2859}$	$\frac{1101}{3048}$	$\frac{1330}{3236}$	$\frac{1555}{3424}$	$\frac{103}{188}$
ı	231	3612	3800	3988	4176	4363	4551	4739	4926	5113	5301	188
1	232	5488	5675	5862	6049	6236	6423	6610	6796	6983	7169	187
ı	233	7356	7542	7729	7915	8101	8287	8473	8659	8845	9030	186
ı	234 235	$\frac{9216}{371068}$	$\begin{array}{c} 9401 \\ 1253 \end{array}$	$\begin{array}{c} 9587 \\ 1437 \end{array}$	$\frac{9772}{1622}$	9958 1806	$\begin{array}{c} .143 \\ 1991 \end{array}$	$\frac{.328}{2175}$	$\frac{.513}{2360}$	$\begin{array}{ c c } .698 \\ 2544 \end{array}$	$\begin{array}{c} .883 \\ 2728 \end{array}$	185 184
	236	2912	3096	3280	3464	3647	3831	4015	4198	4382	4565	184
ı	237	4748	4932	5115	5298	5481	5664	5846	6029	6212	6394	183
Į	238	6577	6759	6942	7124	7306	7488	7670	7852	8034	8216	182
ł	$\frac{239}{249}$	8398	$\frac{8580}{2000}$	8761	8943	$\frac{9124}{2024}$	9306	9487	9668	$\frac{9849}{1000}$	30	$\frac{181}{101}$
ı	240 241	380211 2017	$\begin{array}{c} 0392 \\ 2197 \end{array}$	$\begin{array}{c} 0573 \\ 2377 \end{array}$	$0754 \\ 2557$	$\begin{array}{c} 0934 \\ 2737 \end{array}$	1115 2917	$\frac{1296}{3097}$	$\frac{1476}{3277}$	1656 <b>34</b> 56	$\begin{array}{c} 1837 \\ 3636 \end{array}$	181 180
I	242	3815	3995	4174	4353	4533	4712	4891	5070	5249	5428	179
ł	243	5606	5785	5964	6142	6321	6499	6677	6856	7034	7212	178
ı	244	7390	7568	7746	7923	8101	8279	8456	8634	8811	8989	178
١	245 246	$   \begin{array}{r}     9166 \\     390935   \end{array} $	$\frac{9343}{1112}$	$\begin{array}{c} 9520 \\ 1288 \end{array}$	$\begin{array}{c} 9698 \\ 1464 \end{array}$	$9875 \\ 1641$	$\frac{51}{1817}$	$\begin{array}{c} .228 \\ 1993 \end{array}$	$\frac{.405}{2169}$	$\begin{array}{c} .582 \\ 2345 \end{array}$	$\begin{array}{c} .759 \\ 2521 \end{array}$	177 176
ı	247	2697	2873	3048	3224	3400	3575	3751	3926	4101	4277	176
ı	248	4452	4627	4802	4977	5152	5326	5501	5676	5850	6025	175
1	<b>24</b> 9	6199	6374	6548	$\frac{6722}{}$	6896	7071	7245	7419	$\frac{7592}{}$	7766	174
ı	250	397940	8114	8287	8461	8634	8808	8981	9154	9328	9501	$\begin{array}{c c} 173 \\ 173 \end{array}$
ł	$\begin{array}{ c c c }\hline 251 \\ 252 \\ \hline \end{array}$	$\begin{array}{c} 9674 \\ 401401 \end{array}$	9847 1573	$\begin{array}{c}20 \\ 1745 \end{array}$	$\frac{.192}{1917}$	$\frac{.365}{2089}$	$\frac{.538}{2261}$	.711 $2433$	$\frac{.883}{2605}$	$\begin{array}{c} 1056 \\ 2777 \end{array}$	$\begin{array}{c} 1228 \\ 2949 \end{array}$	173
ı	253	3121	3292	3464	3635	3807	3978	4149	4320	4492	4663	171
I	254	4834	5005	5176	5346	55.7	5688	5858	6029	6199	6370	171
1	255 256	$\begin{bmatrix} 6540 \\ 8240 \end{bmatrix}$	$6710 \\ 8410$	6881 8579	7051 8749	7221 8918	$7391 \\ 9087$	$7561 \\ 9257$	$\begin{array}{c} 7731 \\ 9426 \end{array}$	7901 9595	$\begin{array}{c} 8070 \\ 9764 \end{array}$	170 169
ı	257	9933	.102	.271	.440	.609	.777	.946	1114	1283	1451	169
1	258	411620	1788	1956	2124	2293	2461	2629	2796	2964	3132	168
ı	259	3300	3467	3635	3803	3970	4137	4305	4472	4639	4806	$\frac{167}{}$
1	260	414973	5140	5307	5474	5641	5808	5974	6141	6308	6474	167
I	261 262	$\begin{array}{c} 6641 \\ 8301 \end{array}$	$6807 \\ 8467$	6973 8633	7139 8798	$\begin{array}{c} 7306 \\ 8964 \end{array}$	7472 9129	$\begin{array}{c} 7638 \\ 9295 \end{array}$	7804 9460	$\begin{array}{c} 7970 \\ 9625 \end{array}$	8135 9791	166 165
1	263	9956	.121	.286	.451	.616	.781	.945	1110	1275	1439	165
	264	421604	1768	1933	2097	2261	2426	2590	2754	2918	3082	164
I	265 266	$\begin{array}{c} 3246 \\ 4882 \end{array}$	$\begin{array}{c} 3410 \\ 5045 \end{array}$	$\begin{array}{c} 3574 \\ 5208 \end{array}$	3737 5371	3901 5534	4065 5697	$\begin{array}{c} 4228 \\ 5860 \end{array}$	4392 6023	$\frac{4555}{6186}$	$\frac{4718}{6349}$	164 163
į	267	6511	6674	6836	6999	7161	7324	7486	7648	7811	7973	162
1	268	8135	8297	8459	8621	8783	8944	9106	9268	9429	9591	162
ł	269	9752	9914	75	.236	.398	.559	.720	.881	$\underline{1042}$	1203	161
ı	270	431364	1525	1685	1846	2007	2167	2328	2488	2649	2809	161
ı	271 272	2969 4569	$\frac{3130}{4729}$	3290 4888	3450 5048	$\frac{3610}{5207}$	$\frac{3770}{5367}$	3930 5526	4090 5685	4249 5844	4409 6004	160 159
	273	6163	6322	6481	6640	6798	6957	7116	7275	7433	7592	159
	274	7751	7909	8067	8226	8384	8542	8701	8859	9017	9175	158
	275	$9333 \\ 440909$	9491	9648	9806	9964	.122	.279	.437	.594	.752	158
	276 277	2480	$\begin{array}{c} 1066 \\ 2637 \end{array}$	$\frac{1224}{2793}$	$\frac{1381}{2950}$	$\frac{1538}{3106}$	$\frac{1695}{3263}$	1852 3419	2009 3576	$\frac{2166}{3732}$	2323 3889	157 157
	278	4045	4201	4357	4513			4981	5137	5293	5449	156
	279	5604	5760		6071	6226	6382	6537	6692	6848	7003	155
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280	1447158	7313	7468	7623	7778	7933	8088	8242	8397	8552	155
281	8706	8861	9015	9170	9324	9478	9633	9787	9941	95	154
282		0403	0557	0711	0865	1018	1172	1326	1479	1633	154
283 284		$1940 \\ 3471$	$\begin{vmatrix} 2093 \\ 3624 \end{vmatrix}$	2247 3777	$\begin{array}{ c c c } 2400 \\ 3930 \end{array}$	2553   4082	2706 4235	2859 4387	$\frac{3012}{4540}$	$\begin{vmatrix} 3165 \\ 4692 \end{vmatrix}$	153
285		4997	5150	5302	5454	5606	5758		6062	6214	153 152
286		6518	6670	6821	6973	7125	7276	7428	7579	7731	152
287		8033	8184	8336	8487	8638	8789	8940	9091	9242	151
288		9543	9694	9845	9995	.146 1649	.296	.447	.597	.748	151
$\frac{289}{2000}$		$\frac{1048}{2549}$	1198	1348	$\frac{1499}{2007}$		$\frac{1799}{2806}$	$\frac{1948}{2445}$	$\frac{2098}{2504}$	$\frac{2248}{2744}$	$\frac{150}{150}$
290 291	462398 3893	$\begin{array}{c} 2548 \\ 4042 \end{array}$	$2697 \\ 4191$	2847 4340	2997 4490	3146 4639	$\frac{3296}{4788}$	3445 4936	3594 5085	3744 5234	150 149
292		5532	5680	5829	5977	6126	6274	6423	6571	6719	149
293		7916	7164	7312	7460	7608	7756	7904	8052	8200	148
294		8495	8643	8790	8938	9085	9233	9380	9527	9675	148
295		9969	.116	$\begin{array}{c} .263 \\ 1732 \end{array}$	.410	.557 $2025$	.704	.851	.998	1145	147
296 297		1438 2903	$1585 \\ 3049$	$\frac{1752}{3195}$	$1878 \\ 3341$	3487	$\begin{array}{c} 2171 \\ 3633 \end{array}$	$\frac{2318}{3779}$	2464 3925	$2610 \ 4071$	146 146
298		4362	4508	4653	4799	4944	5090	5235	5381	5526	146
299		5816	5962	6107	6252	6397	6542	6687	6832	6976	145
300	$\overline{477121}$	$\overline{7266}$	7411	7555	7700	7844	7989	8133	8278	$\overline{8422}$	$\overline{145}$
301	8566	8711	8855	8999	9143	9287	9431	9575	9719	9863	144
302	480007	0151	0294	0438	0582	0725	0869	1012	1156	1299	144
303 304		$\frac{1586}{3016}$	$\frac{1729}{3159}$	$\frac{1872}{3302}$	$\begin{array}{c} 2016 \\ 3445 \end{array}$	$\begin{array}{c} 2159 \\ 3587 \end{array}$	$\begin{array}{c} 2302 \\ 3730 \end{array}$	2445 3872	$2588 \\ 4015$	2731 4157	143 143
305	4300	4442	4585	4727	4869	5011	5153	5295	5437	5579	142
306	5721	5863	6005	6147	6289	6430	6572	6714	6855	6997	142
307	7138	7280	7421	7563	7704	7845	7986	8127	8269	8410	141
308 309	8551	8692	8833	8974	9114	9255	9396	9537	9677	9818	141
	9958	1500	$\frac{.239}{1649}$	.380	$\frac{.520}{1000}$	.661	$\frac{.801}{.0001}$	.941	$\frac{1081}{2481}$	$\frac{1222}{2621}$	$\frac{140}{140}$
$\frac{310}{311}$	491362   2760	$\begin{array}{c} 1502 \\ 2900 \end{array}$	1642 3040	$\frac{1782}{3179}$	$\frac{1922}{3319}$	2062 3458	$\frac{2201}{3597}$	$\frac{2341}{3737}$	2481 3876	2621 4015	140 139
312	4155	4294	4433	4572	4711	4850	4989	5128	5267	5406	139
313	5544	5683	5822	5960	6099	6238	6376	6515	6653	6791	139
314	6930	7068	7206	7344	7483	7621	7759	7897	8035	8173	138
315 316	8311 9687	8448 9824	8586 9962	8724	8862 -236	$8999 \\ .374$	$9137 \\ .511$	$\begin{array}{c} 9275 \\ .648 \end{array}$	9412 .785	$\begin{array}{c} 9550 \\ .922 \end{array}$	138 137
317	501059	1196	1333	1470	1607	1744	1880	2017	2154	2291	137
318	2427	2564	2700	2837	2973	3109	3246	3382	3518	3655	136
319	3791	3927	4063	4199	4335	4471	4607	4743	4878	5014	136
$\overline{320}$	$ \overline{505150} $	5286	5421	5557	5693	5828	5964	6099	6234	6370	136
321	6505	6640	6776	6911	7046	7181	7316	7451	7586	7721	135
322 323	7856 9203	7991 9337	8126 9471	$   \begin{array}{c c}     8260 \\     9606   \end{array} $	8395 9740	9874	8664	8799 .143	8934 .277	$\begin{array}{c} 9068 \\ .411 \end{array}$	135 134
324	510545	0679	0813		1081	1215	1349	1482	1616	1750	134
325	1883	2017	2151	2284	2418	2551	2684	2818	2951	3084	133
326	3218	3351	3484	3617	3750	3883	4016	4149	4282	4414	133
327	4548	4681	4813		5079	5211	5344 6668	5476 6800	5609	5741 7064	133
328 329	5874 71 <b>9</b> 8	6006 7328	6139 7460	6271 7592	6403 7724	6535 7855	7987	8119	6932 8251	8382	$\begin{array}{c} 132 \\ 132 \end{array}$
$\frac{323}{330}$	$\frac{130}{518514}$	8646	$\frac{1400}{8777}$	8909	$\frac{2}{9040}$	$\frac{1}{9171}$	$\frac{9303}{}$	$\frac{3130}{9434}$	$\frac{3566}{9566}$	$\frac{\overline{9697}}{9697}$	131
331	9828	9959	90	.221	.353	.484	.615	.745	.876	1007	131
332	521138	1269	1400	1530	1661	1792	1922	2053	2183	2314	131
333	2444	2575	2705	2835	2966	3096	3226	3356	3486	3616	130
334	3746		4006			4396	4526 5822	4656 5951	4785 6081	4915	130
335 336	5045 6339	5174 6469	5304 6598		5563 6856	5693 6985	7114	7243	7372	$\begin{array}{ c c } 6210 \\ 7501 \end{array}$	129 129
337	7630	7759	7888	8016	8145	8274		8531	8660	8788	129
338	8917	9045	9174	9302	9430	9559	9687	9815	9943	72	128
339	530200	0328	0456	0584	0712	0840	0968	1096	1223	1351	128
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	340	531479			1862			2245	2372	2500	2627	128
	341	2754	2882	3009	3136	$\begin{array}{c}  1990  \\  3264  \end{array}$	3391	3518	3645	3772	3899	127
1	342	4026	4153	4280	4407	4534	4661	4787	4914	5041	5167	127
ı	343	5294	5421	5547	5674	5800	5927	6053	6180	6306	6432	126
ı	344	6558	6685	6811	6937	7063	7189	7315	7441	7567	7693	126
ı	345	7819	7945	8071	8197	8322	8448	8574	8699	8825	8951	126
ı	346 347	$9076 \\ 540329$	$\begin{array}{c} 9202 \\ 0455 \end{array}$	$\begin{array}{c} 9327 \\ 0580 \end{array}$	9452 0705	$\begin{vmatrix} 9578 \\ 0830 \end{vmatrix}$	9703 0955		.9954 $1205$	$\begin{array}{c}79 \\ 1330 \end{array}$	$\begin{array}{c} .204 \\ 1454 \end{array}$	125 125
	348	1579	1704	$\frac{0380}{1829}$	1953	2078	2203	$\begin{array}{c} 1080 \\ 2327 \end{array}$	2452	$\frac{1550}{2576}$	2701	125
	349	2825	2950	3074	3199	3323	3447	3571	3696	38:0	3944	124
	350	544068	$\overline{4192}$	$\overline{4316}$	4440	$\overline{4564}$	4688	$\frac{3}{4812}$	$\overline{4936}$	5060	$\overline{5183}$	$\overline{124}$
	351	5307	5431	5555	5678	5802	5925	6049	6172	6296	6419	124
	352	6543	6666	6789	6913	7036	7159	7282	7405	7529	7652	123
1	353	7775	7898	8021	8144	8267	8389	8512	8635	8758	8881	123
ı	354	9003	9126	9249	9371	9494	9616	9739	9861	9934	.106	123
	355 356	$\begin{array}{c} 550228 \\ 1450 \end{array}$	$\begin{array}{c} 0351 \\ 1572 \end{array}$	$\begin{bmatrix} 0473 \\ 1694 \end{bmatrix}$	0595 1816	$\begin{bmatrix} 0717 \\ 1938 \end{bmatrix}$	$\begin{array}{c} 0840 \\ 2060 \end{array}$	$\begin{array}{c} 0962 \\ 2181 \end{array}$	$\begin{array}{c} 1084 \\ 2303 \end{array}$	$\begin{array}{c} 1206 \\ 2425 \end{array}$	1328 $2547$	$\begin{array}{c} 122 \\ 122 \end{array}$
	357	$\begin{array}{c} 1450 \\ 2668 \end{array}$	2790	2911	3033	3155	3276	3398	3519	3640	3762	121
	358	3883	4004	4126	4247	4368	4489	4610	4731	4852	4973	121
	359	5094	5215	5336	5457	5578	5699	5820	5940	6061	6182	121
	360	556303	$\overline{6423}$	$\overline{6544}$	$\overline{6664}$	$\overline{6785}$	6905	7026	7146	7267	$\overline{7387}$	120
ı	361	7507	7627	7748	7868	7988	8108	8228	8349	8469	8589	120
ı	362	8709	8829	8948	9068	9188	9308	9428	9548	9667	9787	120
ı	363	9907	26	.146	.265	.385	.504	.624	.743	.863	.982	119
B	364 365	561101 $2293$	$\begin{array}{c} 1221 \\ 2412 \end{array}$	$\frac{1340}{2531}$	$\begin{array}{c} 1459 \\ 2650 \end{array}$	1578  $ 2769 $	$\begin{array}{c} 1698 \\ 2887 \end{array}$	$\begin{array}{c} 1817 \\ 3006 \end{array}$	$\frac{1936}{3125}$	$2055 \\ 3244$	$\begin{array}{c} 2174 \\ 3362 \end{array}$	119
ı	366	$\begin{array}{c c} 2293 \\ 3481 \end{array}$	3600	3718	3837	3955	4074	4192	4311	4429	4548	119
ľ	367	4666	4784	4903	5021	5139	5257	5376	5494	5612	5730	118
	368	5848	5966	6084	6202	6320	6437	6555	6673	6791	6909	118
	369	7026	7144	7262	7379	7497	7614	7732	7849	7967	8084	118
	370	568202	8319	8436	8554	8671	8788	8905	9023	9140	9257	117
	371	9374	9491	9608	9725	9842	9959	76	.195	.309	.426	117
	$\begin{array}{c} 372 \\ 373 \end{array}$	570543 1709	$\begin{array}{c} 0660 \\ 1825 \end{array}$	$\begin{array}{c} 0776 \\ 1942 \end{array}$	$\begin{array}{c} 0893 \\ 2058 \end{array}$	1010  $2174$	$\begin{array}{c} 1126 \\ 2291 \end{array}$	$\begin{array}{c} 1243 \\ 2407 \end{array}$	$\begin{array}{c} 1359 \\ 2523 \end{array}$	$\begin{array}{c} 1476 \\ 2639 \end{array}$	1592 2755	117 116
	374	2872	2988	3104	3220	3336	3452	3568	3684	3800	3915	116
	375	4031	4147	4263	4379	4494		4726		4957	5072	
	376	5188	5303		5534	5650			5996	6111	6226	115
	377	6341	6457	6572	6687	6802	6917	7032	7147	7262	7377	
	378	7492	7607	7722	7836	7951	8066	8181	8295	8410	8525	
	$\frac{379}{200}$	8639	$\frac{8754}{2000}$	8868	8983	$\frac{9097}{241}$	$\frac{9212}{255}$	$\frac{9326}{100}$	$\frac{9441}{500}$	$\frac{9555}{200}$	$\frac{9669}{611}$	
	380	579784	9898	12	.126	.241	.355	.469	.583	.697	.811	114
-	$\begin{array}{c} 381 \\ 382 \end{array}$	580925 $2063$	$\begin{array}{c} 1039 \\ 2177 \end{array}$	$\begin{array}{c} 1153 \\ 2291 \end{array}$	$\begin{array}{c} 1267 \\ 2404 \end{array}$	$\begin{array}{ c c }\hline 1381\\ 2518\\ \hline \end{array}$	1495 2631	$\frac{1608}{2745}$	$\begin{array}{c} 1722 \\ 2858 \end{array}$	$\frac{1836}{2972}$	$\begin{array}{c} 1950 \\ 3085 \end{array}$	
	383	3199	3312	3426	3539	3652	3765	3879	3992	4105	4218	
	384	4331	4444	4557	4670	4783	4896	5009	5122	5235	5348	113
	385	5461	5574	5686	5799	5912	6024	6137	6250	6362	6475	113
-	386	6587	6700	6812	6925	7037	7149	7262	7374	7486	7599	112
ı	$\frac{387}{388}$	$\begin{array}{c} 7711 \\ 8832 \end{array}$	7823	7935 9056	8047	8160	8272	8384	8496	8608	8720	112 112
	389	9950	$8944 \\61$	.173	9167 $.284$	9279 .396	$\begin{array}{c} 9391 \\ .507 \end{array}$	9503 $.619$	$9615 \\ .730$	$\begin{array}{c} 9726 \\ .842 \end{array}$	$9838 \\ .953$	112
۱	390	$\frac{591065}{591065}$	$\frac{1176}{1176}$	$\frac{1}{1287}$	$\frac{1204}{1399}$	$\frac{1510}{1510}$	$\frac{.601}{1621}$	$\frac{1732}{1732}$	$\frac{1843}{1843}$	$\frac{1955}{1955}$	$\frac{.000}{2066}$	111
1	391	2177	2288	2399	2510	2621	2732	2843	2954	3064	3175	111
-0-	392	3286	3397	3508	3618	3729	3840	3950	4061	4171	4282	111
ľ	393	4393	4503	4614	4724	4834	4945	5055	5165	5276	5386	110
ı	394	5496	5606	5717	5827	5937	6047	6157	625,	6377	5487	110
	395 396	6597 7695	$\begin{array}{c} 6707 \\ 7805 \end{array}$	6817	6927	7037	7146	7256	7366	7476	7586	$\begin{array}{c} 110 \\ 110 \end{array}$
	397	8791	8900	7914 9009	8024	$\begin{array}{c} 8134 \\ 9228 \end{array}$	8243 9337	8353 9446	8462 9556	8572 9665,	8681 9774	109
	398	9883	9992	.101	.210	.319	.428	.537	.646	.755	.864	109
	399	600973		1191	1299	1408	1517	1625		1843	1951	109
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400	602060	2169	2277	2386	2494	2603	2711	2819	2928	3036	108
401	3144			3469		3686		3902	4010	4118	108
402	4226			4550	4658	4766	4874	4982	5089	5197	108
,403	5305		5521	5628		5844	5951	6059	6166	6274	108
404	6381	6489	6596	6704	6811	6919	7026	7133	7241	7348	107
405	7455	7562	7669	7777	7884	7991	8098	8205	8312	8419	107
406	8526		8740	8847	8954	9061	9167	9274	9381	9488	107
407	9594		9808	9914	21	.128	.234	.341	.447	.554	107
408	610660		0873	0979	1086	1192	1298	1405	1511	1617	106
$\frac{409}{100}$	$\frac{1723}{2}$	$\frac{1829}{1829}$	$\frac{1936}{2000}$	2042	$\frac{2148}{21200}$	$\frac{2254}{2}$	$\frac{2360}{2360}$	$\frac{2466}{2}$	$\frac{2572}{2000}$	2678	$\frac{106}{100}$
410	612784	2890	2996	3102	3207	3313	3419	3525	3630	3736	106
411	$\frac{3842}{4897}$	$\begin{bmatrix} 3947 \\ 5003 \end{bmatrix}$	$\begin{array}{ c c }\hline 4053\\ 5108\\ \end{array}$	$\frac{4159}{5213}$	$\frac{4264}{5319}$	4370	4475	4581 5634	4686 5740	4792 5845	106 105
$\begin{array}{c c} 412 \\ 413 \end{array}$	- 5950	6055	6160	6265	6370	$\begin{array}{c} 5424 \\ 6476 \end{array}$	5529 6581	$\begin{array}{c} 3034 \\ 6686 \end{array}$	6790	6895	105
414	7000	7105	7210	7315	7420	7525	7629	7734	7839	7943	105
415	8048	8153	8257	8362	8466		8676	8780	8884	8989	105
416	9093	9198	9302		9511	9615	9719	9824	9928	32	104
417	620136	0240	0344		0552	0656	0760	0864	0968	1072	104
418	1176	1280	1384	1488	1592	-1695	1799	1903	2007	2110	104
419	2214	2318	2421	2525	2628	2732	2835	2939	3042	3146	104
$\overline{420}$	623249	3353	$\overline{3456}$	$\overline{3559}$	3663	$\overline{3766}$	$\overline{3869}$	$\overline{3973}$	4076	$\overline{4179}$	103
421	4282	4385	4488	4591	4695	4798	4901	5004	5107	5210	103
422	5312	5415	5518	5621	5724	5827	5929	6032	6135	6238	103
423	6340	6443	6546	6648	6751	6853	6956	7058		7263	103
424	7366	7468	7571	7673	7775	7878	7980	8082	8185	$8287 \\ 9308$	102 102
$\begin{array}{ c c }\hline 425 \\ 426 \\ \hline \end{array}$	$\frac{8389}{9410}$	8491 9512	$8593 \\ 9613$	8695 9715	8797 9817	8900 9919	$9002 \\21$	$9104 \\ .123$	9206 $.224$	.326	102
427	630428	0530	0631	0733	0835	0936	1038	1139	$\frac{1241}{1241}$	1342	102
428	1444	1545	1647	1748	1849	1951	2052	2153	2255	2356	101
42:9	2457	2559	2660	2761	2862	2963	3064	3165	3266	3367	101
$\overline{430}$	$\overline{633468}$	3569	3670	3771	$\overline{3872}$	3973	4074	4175	$\overline{4276}$	$\overline{4376}$	$\overline{100}$
431	4477	4578	4679	4779	4880	4981	5081	5182	5283	5383	100
432	5484	5584	5685	5785	5886	5986	6087	6187	6287	6388	100
433	6438	6588	6688	6789	6889	6989	7089	7189	7290	7390	100
434	7490	7590	7690	7790	7890	7990	8090	8190	8290	8389	99
$\begin{array}{c c} 435 \\ 436 \end{array}$	$oxed{8489} \ 9486$			8789	8888 9885	$\begin{array}{c} 8988 \\ 9984 \end{array}$	90881		$\frac{9287}{999}$	9387	99 99
437	640481	$0586 \\ 0581$	0680	$\frac{9785}{0779}$	0879	0978	$\frac{84}{1077}$	.183	$\begin{array}{c} .283 \\ 1276 \end{array}$	$\begin{array}{c} .382 \\ 1375 \end{array}$	99
438	1474	1573	1672	1771	1871	1970	2069	2168	2267	2366	99
439	2465	2563	2662	2761	2860	2959	3053	3156	3255	3354	99
$\overline{440}$	$\overline{643453}$	3551	$\overline{3650}$	$\overline{3749}$	3847	$\overline{3946}$	$\overline{4044}$	$\overline{4143}$	$\overline{4242}$	$\overline{4340}$	98
441	4439	4537	4636	4734	4832	4931	5029	5127	5226	5324	98
442	5422	5521	5619	5717	5815	5913	6011	6110	6208	6306	98
443	6404	6502	6690	6698	6796	6894	6992	7089	7187	7285	98
444	7383	7481	7579	7676	7774	7872	7969	8067	8165	8252	98
445	8360	8458	8555	8653	8750	8848	8945		9140	9237	97
446	9335	9432	9530	9627	9724	9821	9919	16	.113	.210	97
447	650308   1278	$\begin{array}{c} 0405 \\ 1375 \end{array}$	$\begin{array}{c c} 0502 \\ 1472 \end{array}$	$\begin{array}{c} 0599 \\ 1569 \end{array}$	$\begin{array}{c} 0696 \\ 1666 \end{array}$	$\begin{array}{c} 0793 \\ 1762 \end{array}$	$0890 \\ 1859$	$0987 \\ 1956$	$\frac{1084}{2053}$	$\frac{1181}{2150}$	97
449	2246	2343	2440	2536	$\begin{array}{c} 1000 \\ 2633 \end{array}$	2730	$\frac{1839}{2826}$	2923	3019	3116	97
$\frac{110}{450}$	$\frac{2213}{653213}$	$\frac{2313}{3309}$	3405	$\frac{2500}{3502}$	3598		$\frac{2020}{3791}$	$\frac{2320}{3888}$	$\frac{3984}{3984}$	$\frac{3110}{4080}$	$\frac{96}{96}$
451	4177	$\frac{3309}{4273}$	4369	4465	4562	4658	4754	$\frac{3000}{4850}$	4946	5042	96
452	5138	5235	5331	5427	5523	5619	5715	5810	5906	6002	96
453	6098	6194	6290	6386	6482	6577	6673	6769	6864	6960	98
454	7056	7152	7247	7343	7438	7534	7629	7725	7820	7916	96
455	801i	8107	8202	8298	8393	8488		8679	8774	8870	95
456		9060	9155	9250	9346	9441	9536	9631	9726	9821	95
$\begin{array}{c c} 457 \\ 458 \end{array}$	9916 660865	0960	$\begin{array}{c} .106 \\ 1055 \end{array}$	$\begin{array}{c} .201 \\ 1150 \end{array}$	$\frac{.296}{1245}$	$\frac{.391}{1339}$	$\begin{array}{c} .486 \\ 1434 \end{array}$	1581 1529	$\begin{array}{c} \textbf{.676} \\ 1623 \end{array}$	$\frac{.771}{1718}$	95 95
459	1813	1907		2096	2191	$\frac{1559}{2280}$	$\frac{1434}{2380}$	2475	$\begin{array}{c} 1023 \\ 2569 \end{array}$	2663	95
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1	460	662758	2852	2947	3041	3135	3230	3324	3418	3512	3607,	94
1	461	3701	3795	3889	3983	4078	4172	4266	4360	4454	4548	94
1	462 463	$\begin{array}{c} 4642 \\ 5581 \end{array}$	4736 5675	4830 5769	4924 5862	5018 5956	5112 6050	5206 6143	5299 6237	5393 6331	5487 6424	$\begin{array}{c} 94 \\ 94 \end{array}$
ı	464	6518	6612	6705	6799	6892	6986	7079	7173	7266	7360	94
1	165	7453	7546	7640	7733	7826	7920	8013	8106	8199	8293	93
1	466	$8386 \\ 9317$	8479 9410	8572 9503	8665 9596	8759 9689	8852 9782	8945 9875	$\frac{9038}{9967}$	$9131 \\60$	9224	93 93
I	468	670246	0339	0431	0524	0617	0710	0802	0895	0988	1080	93
1	469	1173	$\frac{1265}{}$	1358	1451	1543	1636	1728	1821	1913	2005	93
Į	470	672098	2190	2283	2375	2467	2560	2652	2744	2836	2929	92
1	471 472	$\begin{array}{c} 3021 \\ 3942 \end{array}$	$\begin{array}{c} 3113 \\ 4034 \end{array}$	$\frac{3205}{4126}$	$\begin{array}{c} 3297 \\ 4218 \end{array}$	3390 4310	$\begin{array}{c} 3482 \\ 4402 \end{array}$	3574 4494	3666 4586	$\frac{3758}{4677}$	$\frac{3850}{4769}$	$\begin{array}{c} 92 \\ 92 \end{array}$
1	473	4861	4953	5045	5137	5228	5320	5412	5503	5595	5687	92
1	474	5778	5870	5962	6053	6145	6236	6328	6419	6511	6602	92
1	475 476	6694 7607	6785 7698	6876 7789	$\begin{array}{c} 6968 \\ 7881 \end{array}$	$\begin{array}{c} 7059 \\ 7972 \end{array}$	$\begin{array}{c} 7151 \\ 8063 \end{array}$	7242 8154	$\begin{bmatrix} 7333 \\ 8245 \end{bmatrix}$	7424 8336	7516 8427	91 91
1	477	8518	8609	8700	8791	8882	8973	9064	9155	9246	9337	91
1	478	9428	9519	9610	9700	9791	9882	9973	63	.154	.245	91
1	$\frac{479}{400}$	$\frac{680336}{621041}$	$\frac{0426}{1000}$	$\frac{0517}{1402}$	$\frac{0607}{1510}$	$\frac{0698}{1600}$	$\frac{0789}{1000}$	$\frac{0879}{1504}$	$\frac{0970}{1074}$	$\frac{1060}{10004}$	$\frac{1151}{2055}$	$\frac{91}{00}$
1	480 481	681241 2145	$\begin{array}{c} 1332 \\ 2235 \end{array}$	$\begin{array}{c} 1422 \\ 2326 \end{array}$	1513 2416	1603 2506	$1693 \\ 2596$	1784 2686	$\begin{array}{c} 1874 \\ 2777 \end{array}$	$\frac{1964}{2867}$	$\begin{array}{c} 2055 \\ 2957 \end{array}$	90 90
1	482	3047	3137	3227	3317	3407	3497	3587	3677	3767	3857	90
1	483	3947	4037	4127	4217	4307	4396	4486	4576	4666	4756	90
1	484 485	4845 5742	4935 5831	$5025 \\ 5921$	$\begin{array}{c} 5114 \\ 6010 \end{array}$	$\begin{array}{c} 5204 \\ 6100 \end{array}$	$\begin{array}{c} 5294 \\ 6189 \end{array}$	$5383 \\ 6279$	$\begin{array}{c} 5473 \\ 6368 \end{array}$	5563 6458	5652 6547	90 89
1	486	6636	6726	6815	6904	6994	7083	7172	7261	7351	7440	89
ı	487	7529	7618	7707	7796	7886	7975	8064	8153	8242	8331	89
ı	488 489	$\begin{array}{c} 8420 \\ 9309 \end{array}$	$\begin{array}{c} 8509 \\ 9398 \end{array}$	$8598 \\ 9486$	8687 9575	8776 9664	$8865 \\ 9753$	$\begin{array}{c} 8953 \\ 9841 \end{array}$	$\begin{array}{c} 9042 \\ 9930 \end{array}$	$9131 \\ 19$	$\begin{array}{c} 9220 \\ .107 \end{array}$	89 89
	$\frac{403}{490}$	$\frac{3303}{690196}$	$\frac{3336}{0285}$	$\frac{3400}{0373}$	$\frac{3073}{0462}$	$\frac{3004}{0550}$	$\frac{3733}{0639}$	$\frac{3341}{0728}$	$\frac{3330}{0816}$	$\frac{\cdot \cdot 15}{0905}$	$\frac{107}{0993}$	89
1	491	1081	1170	1258	1347	1435	1524	1612	1700	1789	1877	88
	492	1965	2053	2142	2230	2318	2406	2494	2583	2671	2759	88
	493 494	$\begin{array}{c c} 2847 \\ 3727 \end{array}$	$\left  \begin{array}{c} 2935 \\ 3815 \end{array} \right $	$\begin{array}{c} 3023 \\ 3903 \end{array}$	$\begin{array}{c} 3111 \\ 3991 \end{array}$	$\begin{array}{c} 3199 \\ 4078 \end{array}$	$\frac{3287}{4166}$	$\frac{3375}{4254}$	$\begin{vmatrix} 3463 \\ 4342 \end{vmatrix}$	$\begin{array}{c} 3551 \\ 4430 \end{array}$	$\begin{array}{c} 3639 \\ 4517 \end{array}$	88 88
	495	4605							5219	5307	5394	88
	496	5482	5569	5657	5744	5832	5919	6007	6094	6182	6269	87
1	497 498	$\begin{array}{c} 6356 \\ 7229 \end{array}$	6444 7317	$\begin{array}{c} 6531 \\ 7404 \end{array}$		6706 7578	6793 7665		6968	7055	$\begin{array}{c} 7142 \\ 8014 \end{array}$	87 87
	499	8101	8188	8275	8362	8449	8535	7752 8622	7839 8709	7926 8796	8883	87
1	500	698970	9057	9144		$\overline{9317}$	$\overline{9404}$	$\overline{9491}$	$\overline{9578}$	$\overline{9664}$	$\frac{1}{9751}$	87
	501	9838		11	98	.184	.271	.358	.444	.531	.617	87
	502 503	700704 1568		$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$ \begin{array}{c} 0963 \\ 1827 \end{array} $	$\begin{array}{c} 1050 \\ 1913 \end{array}$	1136	1222	$\begin{array}{c} 1309 \\ 2172 \end{array}$	$\begin{array}{c} 1395 \\ 2258 \end{array}$	$\begin{array}{c} 1482 \\ 2344 \end{array}$	86 86
	504	2431	2517			2775	$1999 \\ 2861$	$2086 \\ 2947$	3033	3119	3205	86
	505	3291	3377	3463	3549	3635	3721	3807	3895	3979	4065	86
1	506 507	4151 5008	$\begin{vmatrix} 4236 \\ 5094 \end{vmatrix}$	$\begin{array}{ c c }\hline 4322\\5179\end{array}$	4408 5265	4494   5350	4579	4665	4751	4837 5693	4922 5778	86 86
1	508	5864	5949	6035		6206	$\begin{array}{ c c c } 5436 \\ 6291 \end{array}$	5522 6376	$\begin{array}{ c c c } 5607 \\ 6462 \end{array}$	6547	6632	85
	509	6718		6888		7059	7144		7315	7400	7485	85
	510	707570		7740		7911	7996	8081	8166	8251	8336	85
	511 512	8421 9270	8506 9355	8591	8676	8761	8846		9015	9100	9185	85
	513	710117		$\begin{vmatrix} 9440 \\ 0287 \end{vmatrix}$		9609 0456	9694	9779 0625	$\begin{array}{ c c c c }\hline 9863\\ 0710\end{array}$	9948 0794	$\begin{array}{c}33 \\ 0879 \end{array}$	85 85
	514	0963	1048	1132	1217	1301	1385	1470	1554	1639	1723	84
1	515 516	1807 2650					2229			2481	2566	84
4	517	3491								$\frac{3323}{4162}$	$\begin{bmatrix} 3407 \\ 4246 \end{bmatrix}$	84 84
	518	4330	4414	4497	4581	4665	4749	4833	4916	5000	5084	84
	<u>519</u>	5167	5251	5335	5418	5502	5586	5669	5753	5836	5920	84
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520	716003	<u>'</u>	-				·			6754	
521	6838		7004			7254			7504		83
522	7671	7754	7837	7920	8003		8169				83
523	8502				8834						83
524	9331	9414		9580					9994	77	83
525	720159					0573				0903	83
526	0986	$\begin{array}{ c c c }\hline 1068\\1893\end{array}$		1233				1563	1646	1728	82
527 528	1811 2634		2798	$\begin{bmatrix} 2058 \\ 2881 \end{bmatrix}$	$\begin{vmatrix} 2140 \\ 2963 \end{vmatrix}$			$\begin{vmatrix} 2387 \\ 3209 \end{vmatrix}$		$\begin{array}{ c c c }\hline 2552\\ 3374\\ \end{array}$	82 82
529	3456				3784				4112	4194	82
$\frac{530}{530}$	$\boxed{\frac{724276}{724276}}$		4440	$\frac{3}{4522}$	$\frac{3101}{4604}$		$\frac{3767}{4767}$	$\frac{1030}{4849}$	$\frac{1112}{4931}$	$\frac{1134}{5013}$	$-\frac{32}{82}$
531	5095		5258	5340	5422	5503			5748	5830	$\begin{bmatrix} 82 \\ 82 \end{bmatrix}$
532	5912	5993	6075		6238			6483	6564	6646	82
533	6727		6890		7053	7134	7216	7297		7460	81
534	7541	7623	7704	7785	7866				8191	8273	81
535	8354		8516		8678	8759		8922	9003	9084	81
536	9165		9327	9408	9489	9570	9651	9732	9813	9893	81
537	9974	55	.136	.217	.298	.378	.459	•540	.621	.702	81
538 539	<b>73</b> 0782   1589	$0853 \\ 1669$	$\begin{array}{c} 0944 \\ 1750 \end{array}$	$\begin{array}{c} 1024 \\ 1830 \end{array}$	$\frac{1105}{1911}$	$\begin{array}{c} 1186 \\ 1991 \end{array}$	$\begin{array}{c} 1266 \\ 2072 \end{array}$	$\begin{array}{c} 1347 \\ 2152 \end{array}$	1428	1508	81
									$\frac{2233}{2000}$	$\frac{2313}{2112}$	81
540 541	732394 3197	$\frac{2474}{3278}$	2555 3358	2635 3438	$\frac{2715}{3518}$	$\begin{array}{c} 2796 \\ 3598 \end{array}$	$2876 \\ 3679$	$\frac{2956}{3759}$	3037	3117	80
542	3999	4079	4160	4240	4320	4400	4480	$\frac{3759}{4560}$	$\frac{3839}{4640}$	$\frac{3919}{4720}$	80 80
543	4800	4880	4960	5040	5120	5200	5279	5359	5439	5519	80
544	5599	5679	5759	5838	5918	5998	6078	6157	6237	6317	80
545	6397	6476	6556	6635	6715	6795	6874	6954	7034	7113	80
546	7193	7272	7352	7431	7511	7590	7670	7749	7829	7908	79 🖔
547	7987	8067	8146	8225	8305	8384	8463	8543	8622	8701	79
548	8781	8860	8939	9018	9097	9177	9256	9335	9414	9493	79
549	9572	$\frac{9651}{2}$	$\frac{9731}{2}$	9810	$\frac{9889}{}$	$\frac{9968}{2772}$	47	.126	.205	.284	79
550	740363	0442	0521	0600	0678	0757	0836	0915	0994	1073	79
551	$\begin{array}{c c} & 1152 \\ \hline & 1939 \end{array}$	$\begin{array}{c} 1230 \\ 2018 \end{array}$	$\begin{array}{c} 1309 \\ 2096 \end{array}$	$\frac{1388}{2175}$	$\begin{array}{c} 1467 \\ 2254 \end{array}$	$\begin{array}{c} 1546 \\ 2332 \end{array}$	$\begin{array}{c} 1624 \\ 2411 \end{array}$	$1703 \\ 2489$	$\frac{1782}{2568}$	1860	79
552 553	$\begin{array}{c} 1959 \\ 2725 \end{array}$	2804	2882	2961	3039	3118	3196	3275	3353	2646 3431	79 { 78 }
554	3510	3588	3667	3745	3823	3902	3980	4058	4136	4215	78
555	4293		4449	4528	4606	4684	4762				78
556	5075	5153	5231	5309	5387	5465	5543	5621	5699	5777	78
557	5855	5933	6011	6089	6167	6245	6323	6401	6479	6556	78
558	6634	6712	6790	6868	6945	7023	7101	7179	7256	7334	78
559	7412	7489	7567	7645	7722	7800	7878	7955	8033	8110	78
560	748188	8266	8343	8421	8498	8576	8653	8731	8808	8885	77
561	8963	9040	9118	9195	9272	9350	9427	9504	9582	9659	77
562 563	9736 750508	9814 0586	9891	$\begin{array}{c} 9968 \\ 0740 \end{array}$	$0.45 \\ 0.817$	$\begin{array}{c} .123 \\ 0894 \end{array}$	$\begin{array}{c} .200 \\ 0971 \end{array}$	$\begin{array}{c} .277 \\ 1048 \end{array}$	.354	$\begin{array}{c} .431 \\ 1202 \end{array}$	77
564	1279	1356	1433	1510	1587	1664	1741	1818	1895	1972	77
565	2048	2125	2202	2279	2356	2433	2509	2586	2663	2740	77
566	2816	2893	2970	3047	3123	3200	3277	3353	3430	3506	77 (
567	3583	3660	3736	3813	3889	3966	4042	4119	4195	4272	77
568	4348	4425	4501	4578	4654	4730	4807	4883	4960	5036	76
569	5112	5189	5265	5341	5417	5494	5570	5646	5722	5799	76
570	755875	5951	6027	6103	6180	6256	6332	6408	6484	6560	76
571	6636	6712	6788	6864	6940	7016	7092	7168	7244	7320	76
572	7396	7472	7548	7624	7700	7775	7851	7927	8003	8079	76
573	8155	8230	8306	8382	8458 9214	8533 9290	8609 9366	8685 9441	8761 9517	8836 9592	76 76
574 575	$\begin{array}{c} 8912 \\ 9668 \end{array}$	8988 9743	9063 9819	$   \begin{array}{c c}     9139 \\     9894   \end{array} $	9214	45	.121	.196	.272	.347	75 75
576	$\begin{array}{c} 3008 \\ 760422 \end{array}$	0498	0573	0649	0724	0799	0875	0950	1025	1101	75
577	1176	1251	1326	1402	1477	1552	1627	1702	1778	1853	75
578	1928	2003	2078	2153	2228	2303	2378	2453	2529	2604	75
579	2679	27541	2829	2904	2978	3053	3128	3203	3278	3353	75
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580	763428	, 3503		_							75
581	4176	4251	4326								
582 583	4923 5669	$\begin{array}{ c c c }\hline 4998\\ 5743\\ \hline\end{array}$		1		5296 6041					
584	6413										
585	7156		7304					7675			
586	7898		8046		8194	8268					74
587	8638		8786		8934	9008	9082				
588	9377	9451	9525	9599	9673	9746				42	
589	770115	0189	0263	0336	0410	0484		$\frac{0631}{}$	0705	0778	74
590	770852	0926	0999	1073	1146	1220	1293	1367	1440	1514	
591	1587	1661	1734	1808	1881	1955		2102	2175	2248	73
592 593	$\frac{2322}{3055}$	$\begin{array}{ c c c c }\hline 2395 \\ 3128 \end{array}$	$\begin{array}{ c c c } 2468 \\ 3201 \end{array}$	$\begin{array}{ c c c }\hline 2542\\ 3274\\ \end{array}$	$\begin{array}{ c c c c }\hline 2615\\ 3348\\ \end{array}$	$\begin{array}{ c c c } 2688 \\ 3421 \end{array}$	$\begin{array}{ c c c c }\hline 2762\\ 3494 \end{array}$	2835 3567	$\begin{array}{ c c c c }\hline 2908 \\ 3640 \\ \end{array}$	$\frac{2981}{3713}$	73
594	3786	3860	3933	4006			4225	$\begin{array}{ c c c c c }\hline 4298 \\ \end{array}$	4371	4444	73
595	4517	4590	4663					5028	5100	5173	73
596	5246	5319	5392	5465	5538	5610	5683	5756	5829	5902	73
597	5974	6047	6120	6193		6338	6411	6483	6556	6629	73
598	6701	6774	6846	6919	6992	7064	7137	7209	7282	7354	73
<u>599</u>	7427	$\boxed{7499}$	7572	$\frac{7644}{}$	7717	7789	7862	7934	8006	8079	72
600	778151	8224	8296	8368	8441	8513	8585	8658	8730	8802	72
601	8874	8947	9019	9091		9236	9308	9380	9452	9524	72
602 603	9596	9669	9741	$9813 \\ 0533$		$9957 \\ 0677$	29	.101	.173	.245	72
604	$\begin{bmatrix} 780317 \\ 1037 \end{bmatrix}$	$\begin{array}{c} 0389 \\ 1109 \end{array}$	$\begin{bmatrix} 0461 \\ 1181 \end{bmatrix}$	1253	1324	1396	$\begin{array}{c} 0749 \\ 1468 \end{array}$	$\begin{array}{c} 0821 \\ 1540 \end{array}$	$\begin{array}{c} 0893 \\ 1612 \end{array}$	$\begin{array}{c} 0965 \\ 1684 \end{array}$	72 72
605	1755	1827	1899		2042	2114	2186	$\begin{array}{c} 1340 \\ 2258 \end{array}$	2329	2401	72
606	2473	2544	2616	2688	2759	2831	2902	2974	3046	3117	72
607	3189	3260	3332			3546	3618	3689	3761	3832	71
608.	3904	3975	4046	4118	4189	4261	4332	4403	4475	4546	71
609	4617	4689	4760	4831	4992	4974	5045	5116	5187	5259	71
610	785330	5401	5472	5543	5615	5686	5757	5828	$\overline{5899}$	$\overline{5970}$	$\overline{71}$
611	6041	6112	6183	6254	6325		6467	6538	6609	6680	71
612	6751	6822	6893		7035	7106	7177	7248	7319	7390	71
$\begin{array}{c} 613 \\ 614 \end{array}$	7460	7531	$\begin{array}{c} .7602 \\ 8310 \end{array}$	7673 8381	$\begin{array}{c} 7744 \\ 8451 \end{array}$	7815 8522	7885 8593	7956	$8027 \\ 8734$	8098	71
615	8168 8875	8239 8946	9016	9087	9157	9228	9299	8663 9369		8804 9510	71 71
616	9581	9651	9722					74		.215	70
61%	790285	0356	0426	0496	0567	0637	0707	0778	0848	0918	70
618	• 0988	1059	1129	1198	1269	1340	1410	1480	1550	1620	70
619	1691	1761	1831	1901	1971	2041	2111	2181	2252	2322	70
620	$\overline{792392}$	2462	2532	2602	2672	2742	2812	$\overline{2882}$	2952	3022	70
621	3092	3162	3231	3301	3371	3441	3511	3581	3651	3721	70
622	3790	3860	3930	4000	4070	4139	4209	4279	4349	4418	70
623	4488	4558	4627	4697	4767	4836	4906	4976	5045	5115	70
$\begin{bmatrix} 624 \\ 625 \end{bmatrix}$	5185 5880	5254 5949	5324 6019	5393 6088	5463 6158	5532 6227	5602 6297	5672 6366	5741 6436	5811 6505	70 <b>6</b> 9
626	6574	6644	6713	6782	6852	6921	6990	7060	7129	7198	<b>6</b> 9
627	7268	7337	7406	7475	7545	7614	7683	7752	7821	7890	69
528	7960	8029	8098	8167	8235	8305	8374	8443	8513	8582	69
629	8651	8720	8789	8858	8927	8996	9065	9134	9203	9272	69
630	799341	9409	9478	$\overline{9547}$	9616	9685	$\overline{9754}$	9823	9892	9961	69
631	800029	0098	0167	0236	0305	0373	0442	0511	0580	0648	69
632	0717	0786	0854	0923	0992	1061	1129	1198	1266	1335	69
633	1404	1472	1541	1609	1678	1747	1815	1884	1952	2021	69
634   635	2089	2158	2226	2295	2363	2432	2500	2568	2637	2705	69
636	2774 3457	2842 3525	2910 3594	$\begin{array}{c c} 2979 \\ 3662 \end{array}$	3047 3730	3116 3798	3184 3867	3252 3935	3321 4003	3389 4071	68 68
637			4276	4344	4412					4753	68
638			4957	5025	5093	5161	5229	5297	5365	5433	68
639			5637	5705	5773				6044	6112	68
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640	806180				6451	6519					
641 642	6858 7535	6926	6994 $7670$	$  \frac{7061}{7738}  $	$ 7129 \\ 7806$	$\begin{array}{ c c } 7197 \\ 7873 \end{array}$	$7264 \\ 7941$	$\begin{bmatrix} 7332 \\ 8008 \end{bmatrix}$		7467 8143	68
643	8211	8279	8346	8414	8481	8549	8616		8751	8818	$\begin{array}{c} 68 \\ 67 \end{array}$
644	8886	8953	9021	9088	9156	9223	9290		9425	9492	67
645	9560	9627	9694	9762	9829		9964		98	.165	67
646	810233	0300	0367	0434	0501	0569		0703	0770	0837	67
647	0904	0971	1039		1173				1441	1508	67
648	1575	1642	1709		1843				2111	2178	67
649	2245	2312	2379		$\frac{2512}{}$	$\boxed{2579}$	$\frac{2646}{}$	$\frac{2713}{}$	2780	2847	67
650	812913	2980	3047	3114	3181	3247	3314	3381	3448	3514	67
651 652	3581 4248	3648	3714		3848	3914	3981	4048	4114	4181	67
653	4913	$\begin{bmatrix} 4314 \\ 4980 \end{bmatrix}$	$\begin{array}{c} 4381 \\ 5046 \end{array}$	4447 5113	$4514 \\ 5179$		$\frac{4647}{5312}$	$\frac{4714}{5378}$	$\frac{4780}{5445}$	4847 5511	67 66
654	5578	5644	5711	5777	5843		5976	6042	6109	6175	66
655	6241	6308	6374	6440	6506		6639		6771	6838	66
656	6904	6970	7036	7102	7169		7301	7367	7433	7499	66
657	7565	7631	7698	7764	7830	7896	7962			8160	66
658	8226	8292	8358		8490		8622	8688		8820	66
659	8885	8951	9017	9083	9149	9215	9281	9346	9412	9478	66
660	819544	9610	9676	9741	9807	9873	9939	4	70	.136	66
661	820201	0267	0333	0399	0464	0530	0595		0727	0792	66
662	0858	0924	0989	1055	1120		1251	1317	1382	1448	66
663	1514 2168	$\begin{array}{c} 1579 \\ 2233 \end{array}$	$\begin{array}{c} 1645 \\ 2299 \end{array}$	$\begin{array}{c} 1710 \\ 2364 \end{array}$	$\frac{1775}{2430}$		$\frac{1906}{2560}$	$\begin{array}{c} 1972 \\ 2626 \end{array}$	$2037 \\ 2691$	2103 2756	65
665	2822	2887	2299 2952	$\frac{2304}{3018}$	3083		3213	$\frac{2020}{3279}$	3344	3409	$\begin{array}{c c} 65 \\ \hline 65 \end{array}$
666	3474	3539	3605	3670	3735		3865	3930	3996	4061	65
667	4126	4191	4256	4321	4386	4451	4516	4581	4646	4711	65
668	4776	4841	4906	4971	5036	5101	5166	5231	5296	5361	65
669	5426	5491	5556	5621	5686	5751	5815	5880	5945	6010	65
670	826075	$\overline{6140}$	6204	$\overline{6269}$	6334	6399	$\overline{6464}$	$\overline{6528}$	$\overline{6593}$	6658	$\overline{65}$
671	6723	6787	6852	6917	6981	7046	7111	7175	7240	7305	65
672	7369	7434	7499	7563	7628	7692	7757	7821	7886	7951	65
673	8015	8080	8144	8209	8273	8338	8402	8467	8531	8595	64
674	$   \begin{array}{r}     8660 \\     9304   \end{array} $	$\begin{array}{c} 8724 \\ 9368 \end{array}$	8789 9432	8853 9497	$\begin{array}{c} 8918 \\ 9561 \end{array}$	$8982 \\ 9625$	9046 9690	$\frac{9111}{9754}$	$\frac{9175}{9818}$	9239 9882	$\frac{64}{64}$
676	9947	11	75	139	.204	.268	.332	396	.460	.525	64
677	830589	0653	0717	0781	0845	0909	0973	1037	1102	1166	64
678	1230	1294	1358	1422	1486	1550	1614	1678	1742	1806	$6\overline{4}$
679	1870	1934	1998	2062	2126	2189	2253	2317	2381	2445	64
680	832509	2573	2637	2700	2764	2828	2892	2956	$\overline{3020}$	3083	$\overline{64}$
681	3147	3211	3275		3402	3466	3530	3593	3657	3721	64
682	3784	3848	3912	3975	4039	4103	4166	4230	4294	4357	64
683	4421	4484	4548		4675		4802	4866	4929	4993	64
684	5056	5120	5183		5310		5437	5500	5564	5627	63
685 686	5691 -63 <b>2</b> 4	5754 6387	5817	5881	5944 6577	$\frac{6007}{6641}$	6071 6704	$\frac{6134}{6767}$	$\frac{6197}{6830}$	6261 6894	63 63
687	6957	$\begin{array}{c} 0.387 \\ 7020 \end{array}$	6451 7083	6514 7146	7210	$\begin{array}{c} 0041 \\ 7273 \end{array}$	7336	7399	7462	7525	63
688	7588	7652	7715	7778	7841	7904	7967	8030	8093	8156	63
689	8219	8282	8345	8408	8471	8534	8597	8660	8723	8786	63
$\overline{690}$	838849	8912	$\frac{1}{8975}$	$\frac{1}{9038}$	9101	$\overline{9164}$	$\overline{9227}$	$\overline{9289}$	$\overline{9352}$	9415	$\overline{63}$
691	9478	9541	9604	9667	9729	9792	9855	9918	9981	43	63
692	840106	0169	0232	0294	0357	0420	0482	0545	0608	0671	63
693	0733	0796	0859	0921	0984	1046	1109	1172	1234	1297	63
694	1359	1422	1485	1547	1610	1672	1735	1797	1860	1922	63
695	1985	2047	2110	2172	2235	2297	2360	2422	2484	2547	62
696 697	2609 3233	2672	2734	2796 3420	2859 3482	2921 3544	2983 3606	3046 3669	$\frac{3108}{3731}$	3170 3793	62 62
698	3855	3295 3918	3357 3980	4042	4104	4166	4229	4291	4353	4415	62
699	4477			4664			4850	4912	4974	5036	62
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700	1845098	15160	5222	5284	5346	5408	5470	5532	5594	5656	62
701	5718		5842	5904		6028	6090		6213	6275	
702	6337	6399	6461	6523		6646	6708		6832	6894	- 62
703	6955	7017	7079	7141	7202	7264	7326			7511	62
704	7573	7634	7696	7758	.7819	7881	7943		8066	8128	62
705	8189	8251	8312	8374	8435	8497	8559		8682	8743	62
706	8805	8866	8928	8989	9051	9112	9174	9235	9297	9358	61
707	9419	9481	9542	9604	9665	9726	9788	9849	9911	9972	61
708	850033	0095	0156	0217	0279	0340	0401	0462	0524	0585	61
709	0646	$\frac{0707}{1}$	$\frac{0769}{}$	$\frac{0830}{1000}$	$\frac{0891}{1}$	$\frac{0952}{}$	1014	1075	1136	$\frac{1197}{1197}$	$\frac{61}{2}$
710	851258	1320	1381	1442	1503	1564	1625	1686	1747	1809	61
711	1870	1931	1992	2053	2114	2175	2236	2297		2419	61
712	2480	2541	2602	2663	2724	2785	2846	2907	2968	3029	61
713	$\begin{vmatrix} 3090 \\ 3698 \end{vmatrix}$	$\begin{array}{c} 3150 \\ -3759 \end{array}$	$\frac{3211}{3820}$	$\begin{bmatrix} 3272 \\ 3881 \end{bmatrix}$	$\frac{3333}{3941}$	$\frac{3394}{4002}$	3455 40'.3	$\begin{array}{c} 3516 \\ 4124 \end{array}$		$\begin{array}{c} 3637 \\ 4245 \end{array}$	$\begin{bmatrix} 61 \\ 61 \end{bmatrix}$
715	4306	4367	4428	4488	4549	4610	4670	4731		4852	61
716	4913	4974	5034	5095	5156	5216	5277	5337	5398	5459	61
717	5519	5580	5640	5701	5761	5822	5882	5943	6003		61
718	6124	6185	6245	6306	6366	6427	6487	6548	6608	6668	60
719	6729	6789	6850	6910	6970	7031	7091	7152	7212	7272	60
720	857332	7393	$\overline{7453}$	$\overline{7513}$	$\overline{7574}$	$\overline{7634}$	$\overline{7694}$	7755	7815	7875	60
721	7935	7995	8056	8116	8176	8236	8297	8357		8477	60
722	8537	8597	8657	8718	8778	8833	8898	8958	9018	9078	60
723	9138	9198	9258	9318	9379	9439	9499	9559	9619	9679	60
724	9739	9799	9859	9918	9978	38	98	.158	.218	.278	60
725	860338	0398	0458	0518	0578	0637	0697	0757	0817	0877	60
726	0937	0996	1056	1116	1176	1236	1295	1355	1415	1475	60
727 728	1534 2131	$\frac{1594}{2191}$	$\begin{array}{c} 1654 \\ 2251 \end{array}$	$\begin{array}{c} 1714 \\ 2310 \end{array}$	$\frac{1773}{2370}$	$\begin{array}{c} 1833 \\ 2430 \end{array}$	$\frac{1893}{2489}$	$\begin{array}{c} 1952 \\ 2549 \end{array}$	$\begin{array}{c} 2012 \\ 2608 \end{array}$	2072 2668	60 60
729	$\begin{bmatrix} 2131 \\ 2728 \end{bmatrix}$	2787	2847	2906	2966	3025	3085	3144		3263	60
730 731	$oxed{863323}{3917}$	$\frac{3382}{3977}$	$\frac{3442}{4036}$	3501 4096	$\frac{3561}{4155}$	$\begin{array}{c} 3620 \\ 4214 \end{array}$	$\frac{3680}{4274}$	3739 4333	$\frac{3799}{4392}$	$\begin{array}{c} 3858 \\ 4452 \end{array}$	59 59
732	4511	4570	4630	4689	4748	4808	4867	4926	4985	5045	59 59
733	5104	5163	5222	5282	5341	5400	5459	5519	5578	5637	59
734	5696	5755	5314	5874	5933	5992	6051	6110		6228	59
735	6287		6405		6524	6533		6701			59
736	6878	6937	6996	7955	7114	7173	7232	7291	7350	7409	59
737	7467	7526	7585	7514	7703	7762	7821	7880	7939	7998	<b>5</b> 9
738	8056	8115	8174	8233	8292	8350	8409	8468	8527	8586	<b>5</b> 9
739	8644	8703	8762	8831	8879	8933	8997	9056	9114	9173	59
740	869232	9299	9349	9403	9466	9525	9584	9642	9701	9760	<b>5</b> 9
741	9818	9877	9935	9994	53	.111	.170	.228	.287	.345	59
742	870404	0462	0521	0579	0533	0596	0755	0813	0872	0930	<b>5</b> 8
743	0989	1047	1196	1164	1223	1281	1339	1398	1456	1515	58
744 745	1573 2156	$\frac{1631}{2215}$	$\begin{array}{c} 1690 \\ 2273 \end{array}$	$\frac{1748}{2331}$	$\frac{1806}{2389}$	$\frac{1865}{2448}$	1923 2506	$\begin{array}{c} 1981 \\ 2564 \end{array}$	$\begin{array}{c} 2040 \\ 2622 \end{array}$	2098 2681	58 58
746	$\begin{bmatrix} 2130 \\ 2739 \end{bmatrix}$	2797	2855	2913	2972	3030	3088	3146	$\frac{2022}{3204}$	3262	58 58
747	3321	3379	3437	3495	3553	3611	3659	3727	3785	3844	58
748	3902	3960	4018	4076	4134	4192	4250	4308	4366	4424	58
749	4482	4540	4598	4656	4714	4772	4830	4888	4945	5003	58
750	875061	5119	$\overline{5177}$	5235	$529\overline{3}$	$\overline{5351}$	5409	$\overline{5466}$	5524	$\overline{5582}$	<b>5</b> 8
751	5640	5698	5756	5813	5871	5929	5987	6045	6102	6160	<b>58</b>
752	6218	6276	6333	6391	6449	6507	6564	6622	6680	6737	58
753	6795	6853	6910	6968	7026	7083	7141	7199	7256	7314	58
754	7371	7429	7487	7544	7602	7659	7717	7774	7832	7889	58
755	7947	8004	8062	8119	8177	8234	8292	8349	8407	8464	57
756 757	8522	8579	8637	8694	3752	8809	8866	8924	8981	9039	57
758	9096 9669	9153   9726	9211 9784	9268 9341	9325	9383 9956	9440	9497	9555	9612	57
759	880242	0299	0356		$\frac{9898}{0471}$	0528	$\begin{array}{c}13 \\ 0585 \end{array}$	$\begin{array}{c}70 \\ 0642 \end{array}$	0699	0.185	57 57
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	<b>A</b>	TABL	<u>.</u> , O.	10011			OM 1	10 10			13
N.	0	1	2	3	4	5	6	7	8	9	D.
760	880814	0871	0928	0985	1042	1099	1156	1213	1271	1328	57
761	1385	1442	1499	1556	1613	1670	1727	1784	1841	1898	57
762	1955	2012	2069	2126	2183	2240	2297	2354	2411	2468	57
763	2525	2581	2638	2695	2752	2809	2866	2923	2980	3037	57
764	3093	3150	3207	3264	3321	3377	3434	3491	3548	3605	57
765	3661	3718	3775	3832	3888	3945	4002	4059	4115	4172	57
766	4229	4285	4342	4399	4455	4512	4569	4625	4682	4739	57
767	4795	4852	4909	4965	5022	5078	5135	5192	5248	5305	57
768	5361	5418	5474	5531	5587	5644	5700	5757	5813	5870	57
769	5926	5983	6039	6096	6152	6209	6265	6321	6378	6434	56
770	886491	6547	6604	6660	$\overline{6716}$	6773	6829	6885	$\overline{6942}$	6998	56
771	7054	7111	7167	7223	7280	7336	7392	7449	7505	7561	56
$77\overline{2}$	7617	7674	7730	7786	7842	7898	7955	8011	8067	8123	56
773	8179	8236	8292	8348	8404	8460	8516	8573	8629	8685	56
774	8741	8797	8853		8965	9021	9077	9134	9190	9246	56
775	9302	9358	9414	9470	9526	9582	9638	9694	9750	9806	56
776	9862	9918	9974	30	86	.141	.197	.253	.309	.365	56
777	890421	0477	0533	0589	0645	0700	0756	0812	0868	0924	56
778	0980	1035	1091	1147	1203	1259	1314	1370	1426	1482	56
779	1537	1593	1649	1705	1760	1816	1872	1928	1983	2039	56
780	892095	$\frac{2150}{2150}$	$\frac{\overline{2206}}{2206}$	$\frac{2}{2262}$	$\frac{\overline{2317}}{2317}$	$\overline{2373}$	$\overline{2429}$	$\frac{2484}{2484}$	$\frac{2540}{2540}$	$\frac{2595}{2595}$	56
781	2651	2707	2762	2818	2873	2929	2985	3040	3096	3151	56
782	$\frac{2031}{3207}$	3262	3318	3373	3429	3484	$\begin{array}{c} 2500 \\ 3540 \end{array}$	3595	3651	$\frac{3131}{3706}$	56
783	$\frac{3207}{3762}$	3817	3873	3928	3984	4039	4094	4150	$\frac{3031}{4205}$	$\frac{3760}{4261}$	55 55
784	4316	4371	4427	4482	4538	4593	4648	4704	4759	4814	55 55
785	$\frac{4310}{4870}$	4925	4980	5036	5091	5146	5201	5257	5312	5367	55 55
786	5423	5478	5533	5588	5644	5699	5754	5809	5864	5920	55 55
787	5975	6030	6085	6140	6195	6251	6306	6361	6416	6471	55
788	6526	6581	6636	6692	6747	6802	6857	6912	6967	7022	55
789	7077	7132	7187	7242	7297	7352	7407	7462	7517	7572	55 55
790	897627	7682	7737	7792	7847	7992	7957	8012	8067	8122	55
791	8176	8231	8286	8341	8396	8451	8506	8561	8615	8670	55
792	8725	8780	8835	8890	8944	8999	9054	9109	9164	9218	55
793	9273	9328	9383	9437	9492	9547	9602	9656	9711	9766	55
794	9821	9875	9930		39	94	.149	.203	.258	.312	55
795	900367		0476		0586				0804	0859	55
796	0913		1022	1077	1131	1186	1240	1295	1349	1404	55
797	1458		1567	1622	1676	1731	1785	1840	1894	1948	54
798	2003		2112	2166	2221	2275	2329	2384	2438	2492	54
799	2547	2601	$\frac{2655}{}$	$\frac{2710}{}$	$\frac{2764}{}$	2818	$\frac{2873}{}$	$\frac{2927}{}$	$\frac{2981}{}$	3036	54
800	903090	3144	3199	3253	3307	3361	3416	3470	3524	3578	54
801	3633		3741	3795	3849			4012	4066		54
802	4174	4229	4283	4337				4553	4607		54
803	4716	4770		4878		4986		5094	5148	5202	54
804	5256	5310	5364					5634	5688	5742	54
805	5796	5850	5904			6066		6173	6227	6281	54
806	6335	6389	6443		6551	6604	6658	6712	6766	6820	54
807	6874	6927	6981	7035	7089	7143	7196	7250	7304	7358	54
808	7411	7465	7519		7626	7680	7734	7787	7841	7895	54
809	7949	8002	8056	8110	8163	8217	8270	8324	8378	8431	54
810	908485	8539	$\overline{8592}$	8646	8699	8753	8807	8860	8914	8967	54
811	9021					9289			9449	9503	54
812	9556		9663						9984	37	53
813	910091	0144	0197		0304	0358	0411	0464	0518		53
814	0624		0731	0784		0891	0944		1051	1104	53
815	1158	1211	1264		1371	1424		1530	1584	1637	53
816	1690	1743	1797		1903	1956	2009	2063	2116	2169	53
817	2222	2275	2328		2435	2488				2700	53
818	2753	2806	2859								53
819	3284		3390								
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820	913814	3867	3920	3973	4026	4079	4132	4184	4237	4290	53
821	4343	4396	4449	4502	4555	4608	4660	4713	4766	4819	53
822	4872	4925	4977	5030	5083	5136	5189	5241	5294	5347	53
823	5400	5453		5558	5611	5664	5716	5769	5822	5875	53
824	5927	5980	6033	6085	6138	6191	6243	6296	6349	6401	53
825	6454	6507	6559	6612	6664	6717	6770	6822	6875	6927	53
826	6980	7033	7085	7138	7190	7243	7295	7348	7400	7453	53
827	7506	7558	7611	7663	7716	7768	7820	7873	7925	7978	52
828	8030	8083	8135	8188	8240	8293	8345	8397	8450	8502	52
829	8555	8607	8659	8712	8764	8816	8869	8921	8973	9026	52
830	919078	9130	9183	9235	9287	9340	9392	9444	9496	9549	52
831	9601	9653		9758	9810	9862	9914	9967	19	.71	52
832	920123	0176	0228	0280	0332	0384	0436	0489	0541	0593	52
833	0645	0697	0749	0801	0853	0906	0958	1010	1062	1114	52
834	1166	1218	1270	1322	1374	1426	1478	1530	1582	1634	52
835	1686	1738	1790	1842	1894	1946	1998	2050	2102	2154	52
836	2206	2258	2310	2362	2414	2466	2518	2570	2622	2674	52
837	2725	2777	2829	2881	2933	2985	3037	3089	3140	3192	52
838	3244	3296	3348	3399	$\frac{3451}{3969}$	3503	3555	3607	3658	3710	52
	3762	3814	3865	$\frac{3917}{1100}$		$\frac{4021}{1522}$	$\frac{4072}{1500}$	$\frac{4124}{1215}$	$\frac{4176}{10000}$	$\frac{4228}{1221}$	52
840	924279	4331	4383	4434	4486	4538	4589	4641	4693	4744	52
841	4796	4848	4899	4951	5003	5054	5106	5157	5209	5261	52
842	5312	5364		5467	5518	5570	5621	5673	5725	5776	52
843	5828	5879	5931	5982	6034	6085	6137	6188	6240	6291	51
844 845	6342	6394	$\begin{array}{c} 6445 \\ 6959 \end{array}$	6497 7011	6548 7062	$6600 \\ 7114$	6651 7165	$6702 \\ 7216$	6754 7268	6805   7319	51
846	6857 7370	$6908 \\ 7422$	7473	7524	7576	7627	7678	7730	7781	7832	51
847	7883	7935	7986	8037	8088	8140	8191	8242	8293	8345	51 51
848	8396	8447	8498	8549	8601	8652	8703	8754	8805	8857	51
849	8908	8959	9010	9061	9112	9163	9215	9266	9317	9368	51
$\frac{310}{850}$		$\frac{3300}{9470}$	$\frac{3510}{9521}$	$\frac{5572}{9572}$	$\frac{9623}{9623}$	$\frac{0100}{9674}$	$\frac{57}{9725}$	$\frac{5776}{9776}$	$\frac{3317}{9827}$	$\frac{3000}{9879}$	
851	929419 9930	9470	32	83	.134	.185	.236	.287	.338	.389	51
852	930440	0491	0542	0592	0643	0694	0745	0796	0847	0898	51 51
853	0949	1000	1051	1102	1153	1204	1254	1305	1356	1407	51
854	1458	1509	1560	1610	1661	1712	1763	1814	1865	1915	51
855	1966		2068		2169	2220	2271	2322	2372	2423	51
856	2474	2524	2575	2626	2677	2727	2778	2829	2879	2930	51
857	2981	3031	3082	3133	3183	3234	3285	3335	3386	3437	51
858	3487	3538	3589	3639	3690	3740	3791	3841	3892	3943	51
859	3993	4044	4094	4145	4195	4246	4296	4347	4397	4448	51
860	934498	4549	4599	$\overline{4650}$	$\overline{4700}$	$\overline{4751}$	4801	4852	4902	4953	50
861	5003	5054	5104	5154	5205	5255	5306	5356	5406	5457	50
862	5507	5558	5608	5658	5709	5759	5809	5860	5910	5960	50
863	6011	6061	6111	6162	6212	6262	6313	6363	6413	6463	50
864	6514	6564	6614	6665	6715	6765	6815	6865	6916	6966	50
865	7016	7066	7117	7167	7217	7267	7317	7367	7418	7468	50
866	7518	7568	7618	7668	7718	7769	7819	7869	7919	7969	50
867	8019	8069	8119	8169	8219	8269	8320	8370	8420	8470	50
868	8520	8570	8620	8670	8720	8770	8820	8870	8920	8970	50
869	-9020	9070	9120	9170	9220	$\frac{9270}{}$	9320	9369	9419	9469	_50
870	939519	9569	9619	9669	9719	9769	9819	9869	9918	9968	50
871	940018	0068	0118	0168	0218	0267	0317	0367	0417	0467	50
872	0516	0566		0666	0716	0765	0815	0865	0915	0964	50
873	1014	1064		1163	1213	1263	1313	1362	1412	1462	50
874	1511	1561	1611	1660	1710	1760	1809	1859	1909	1958	50
875	2008	2058		2157	2207	2256	2306	2355	2405	2455	50
876 877	$\begin{array}{c c} 2504 \\ 3000 \end{array}$	$2554 \\ 3049$	2603	2653	2702	2752	2801	2851	2901	2950	50
878	$\frac{3000}{3495}$	3544		$\frac{3148}{3643}$	$\frac{3198}{3692}$	$\frac{3247}{3742}$	$\frac{3297}{3791}$	3346	3396	3445	49
879	3989				3092 4186			3841 4335	$\frac{3890}{4384}$	$\begin{array}{c} 3939 \\ 4433 \end{array}$	49
===		1000	1000	+107	4100	4200	1200	TOOO	4334	4433	49
N.	0	1 .	2	3	4	5	6	7	8	9	D.
torrustro-	-			100	-	-		COLUMN TOWNS OF THE PARTY.	WILL REST WATER		-

N.	0	1	2	3	4	5	6	7	8	9	D.
880	944483	4532	4581	4631	4680	4729	4779	4828	4877	4927	49
881	4976	5025	5074	5124	5173	5222	5272	5321	5370	5419	49
882	5469	5518	5567	5616	5665	5715	5764	5813	5862	5912	49
883	5961	$6010 \\ 6501$	$6059 \\ 6551$	$\begin{array}{c} 6108 \\ 6600 \end{array}$	$\begin{array}{c} 6157 \\ 6649 \end{array}$	$\begin{array}{c} 6207 \\ 6698 \end{array}$	$6256 \\ 6747$	$\begin{array}{c} 6305 \\ 6796 \end{array}$	$\begin{array}{c} 6354 \\ 6845 \end{array}$	$\begin{array}{c} 6403 \\ 6894 \end{array}$	49
885	$\begin{array}{c} 6452 \\ 6943 \end{array}$	6992	7041	7090	7140	7189	7238	7287	7336	7385	49
886	7434	7483	7532	7581	7630	7679	7728	7777	7826	7875	49
887	7924	7973	8022	8070	8119	8168	8217	8266	8315	8364	49
888	8413	8462	8511	8560	8609	8657		8755	8804		49
889	8902	8951	8999	9048	9097	9146		$\frac{9244}{}$	$\frac{9292}{}$	9341	49
890	949390	9439	9488	9536	9585	9634	9683	9731	9780	9829	49
891	9878	9926	9975	24	73	.121	.170	.219	.267	.316	49
892 893	950365 0851	$\begin{array}{c} 0414 \\ 0900 \end{array}$	$\begin{bmatrix} 0462 \\ 0949 \end{bmatrix}$	$0511 \\ 0997$	$\begin{array}{c} 0560 \\ 1046 \end{array}$	$\begin{array}{c} 0608 \\ 1095 \end{array}$	$\begin{array}{c} 0657 \\ 1143 \end{array}$	$\begin{array}{c} 0706 \\ 1192 \end{array}$	$\begin{array}{c} 0754 \\ 1240 \end{array}$	$\begin{array}{c} 0803 \\ 1289 \end{array}$	49 49
894	$\begin{array}{c} 0001 \\ 1338 \end{array}$	1386	1435	$\frac{0937}{1483}$	1532	1580	$\begin{array}{c} 1143 \\ 1629 \end{array}$	$\frac{1132}{1677}$	1726	1775	49
895	1823	1872	1920	1969	2017	2066	2114	2163	2211	2260	48
896	2308	2356	2405	2453	2502	2550	2599	2647	2696	2744	48
897	2792	2841	2889	2938	2986	3034	3083	3131	3180	3228	48
898	3276	3325	3373	3421	3470	3518	3566	3615	3663	3711	48
899	3760	3808	3856	$\frac{3905}{}$	$\frac{3953}{}$	$\frac{4001}{}$	$\frac{4049}{}$	4098	4146	4194	48
900	954243	4291	4339	4387	4435	4484	4532	4580	4628	4677	48
$\begin{bmatrix} 901 \\ 902 \end{bmatrix}$	$\begin{array}{c} 4725 \\ 5207 \end{array}$	4773 5255	$\begin{array}{c} 4821 \\ 5303 \end{array}$	4869	4918 5399	4966 5447	5014 5495	5062 5543	$5110 \\ 5592$	$5158 \\ 5640$	48 48
903	5688	5736	5784	5351 5832	5880	5928	5976	6024	6072	$\begin{array}{c} 6120 \\ \end{array}$	48
904	6168	6216	6265	6313	6361	6409	6457	6505	6553	6601	48
905	6649	6697	6745	6793	6840	6888	6936	6984	7032	7080	48
906	7128	7176	7224	7272	7320	7368	7416	7464	7512	7559	48
907	7607	7655	7703	7751	7799	7847	7894	7942	7990	8038	48
908	8086	8134	8181	8229	8277	8325	8373	8421	8468	8516	48
$\frac{909}{010}$	8564	8612	8659	8707	$\frac{8755}{3333}$	$\frac{8803}{8803}$	$\frac{8850}{2820}$	8898	$\frac{8946}{64436}$	8994	48
$ 910  \\ 911 $	959041 9518	9089 9566	$9137 \\ 9614$	9185 9661	9232	9280	$9328 \\ 9804$	$9375 \\ 9852$	9423 $9900$	$9471 \\ 9947$	48
912	9995	42	90	.138	9709	$\begin{array}{c} 9757 \\ .233 \end{array}$	.280	.328	.376	.423	48
913	960471	0518	0566	0613	0661	0709	0756	0804		0899	48
914	0946	0994	1041	1089	1136	1184	1231	1279	1326	1374	47
915	1421		1516				1706				47
916	1895	1943		2038	2085	2132		2227	2275	2322	47
917	$2369 \ 2843$	$\begin{array}{c} 2417 \\ 2890 \end{array}$	2464	2511	2559		2653	$\frac{2701}{3174}$	2748	2795	47
919	3316	3363	$\begin{array}{c} 2937 \\ 3410 \end{array}$	$\frac{2985}{3457}$	$\begin{array}{c} 3032 \\ 3504 \end{array}$	$\begin{array}{c} 3079 \\ 3552 \end{array}$	3126 3599	3646	$\frac{3221}{3693}$	$\frac{3268}{3741}$	47
$\frac{\overline{920}}{920}$	$\frac{963788}{963788}$	$\frac{3835}{3835}$	3882	$\frac{3101}{3929}$	$\frac{3977}{3977}$	$\frac{3002}{4024}$		$\frac{3018}{4118}$	$\frac{3035}{4165}$	$\frac{3111}{4212}$	47
921	4260	$\frac{3633}{4307}$	4354	4401	4448			4590			47
922	4731	4778	4825	4872	4919			5061	5108		47
923	5202	5249	5296	5343	5390		5484	5531	5578	5625	47
924	5672	5719	5766	5813	5860	5907		6001	6048	6095	47
925	6142	6189	6236	6283	6329	6376	6423	6470	6517		47
$\begin{array}{c} 926 \\ 927 \end{array}$	6611 7080	$\frac{6658}{7127}$	$6705 \\ 7173$	$\begin{array}{c} 6752 \\ 7220 \end{array}$	$\begin{array}{c} 6799 \\ 7267 \end{array}$	$\begin{array}{c} 6845 \\ 7314 \end{array}$	$\begin{array}{c} 6892 \\ 7361 \end{array}$	$6939 \\ 7408$	6986 $7454$	$\begin{array}{c} 7033 \\ 7501 \end{array}$	47
928	7548	7595	$\begin{array}{c} 7173 \\ 7642 \end{array}$	7688	$\begin{array}{c} 7207 \\ 7735 \end{array}$	7782	7829	7875	7922	7969	47
929	8016	8062	8109	8156	8203		8296	8343	8390	8436	47
$\overline{930}$	968483	$\overline{8530}$	8576	$\frac{8623}{8623}$	8670	8716	$\frac{8763}{8763}$	8810	$\frac{8856}{8856}$	$\frac{1}{8903}$	47
931	8950	8996	9043	9090	9136	9183		9276	9323	9369	47
932	9416	9463	9509	9556	9602	9649	9695	9742	9789	9835	47
933	9882	9928	9975	21	68	.114	.161	.207	.254	.300	47
$\begin{array}{c c} 934 \\ 935 \end{array}$	970347	0393	0440	0486				0672	0719	0765	46
936	$\begin{array}{c} 0812 \\ 1276 \end{array}$	$\begin{array}{c} 0858 \\ 1322 \end{array}$	$0904 \\ 1369$	$0951 \\ 1415$	$\begin{array}{ c c } 0997 \\ 1461 \end{array}$	$\begin{array}{c} 1044 \\ 1508 \end{array}$		$1137 \\ 1601$	$  \begin{array}{c} 1183 \\ 1647 \end{array}  $	$\begin{array}{ c c c }\hline 1229\\ 1693\\ \hline\end{array}$	
937	1740	1786	1832	1879	1925			2064		2157	
938	2203	2249	2295	2342	2388			2527			
939	2666		2758			2897		2389	3035	3082	46
N.	0	1	2	3	1 4	5	6	7	8	9	D.

N.	0	1	2	3	4	5	6	1 7	8	9	D.
$\begin{array}{c} 940 \\ 941 \end{array}$	$     \begin{array}{r}       973128 \\       \hline       3590     \end{array} $	$\frac{3174}{3636}$	$\frac{3220}{3682}$	3266 3728	3313 3774	3359 3820	3405 3866	3451	$\frac{3497}{3959}$		46 46
942	4051		4143		4235	4281	4327	4374	4420	4466	46
943	4512		4604		4696	4742	4788	4834	4880	4926	46
944	4972		5064	5110	5156	5202	5248	5294	5340	5386	46
945	5432	5478	5524	5570	5616	5662	5707	5753	5799	5845	46
946	5891	5937	5983	6029	6075	6121	6167	6212	6258	6304	46
947	6350	6396	6442	6488	6533	6579	6625	6671 7129	6717 7175	6763 7220	46
948 949	6808 7266	6854 7312	6900 7358	6946 7403	6992 7449	7037 7495	7083 7541	7586	7632	7678	46 46
					$\frac{7906}{7906}$			$\frac{1300}{8043}$	8089		$\frac{46}{46}$
950 951	977724 8181	7769 8226	7815 8272	7861 8317	8363	7952 8409	7998 8454	8500	8546	8135 8591	46
952	8637	8683	8728	8774	8819	8865	8911	8956	9002	9047	46
953	9093		9184	9230	9275	9321	9366	9412	9457	9503	46
954	9548	9594	9639		9730	9776	9821	9867	9912	9958	46
955	980003	0049	0094	0140	0185	0231	0276	0322	0367	0412	45
956	0458	0503	0549	0594	0640	0685	0730	0776	0821	0867	45
957	0912	0957		1048		1139	1184	1229	1275	1320	45
958 959	1366 1819	1411 1864	$\frac{1456}{1909}$		$\frac{1547}{2000}$	$\begin{array}{c} 1592 \\ 2045 \end{array}$	$\begin{array}{c} 1637 \\ 2090 \end{array}$	$1683 \\ 2135$	1728 2181	$\begin{array}{c} 1773 \\ 2226 \end{array}$	45 45
960 961	$982271 \\ 2723$	2316 2769	$2362 \\ 2814$	$\begin{array}{c} 2407 \\ 2859 \end{array}$	$2452 \\ 2904$	2497 $2949$	2543 2994	2588 3040	2633 3085	$\begin{array}{c} 2678 \\ 3130 \end{array}$	45 45
962	3175	3220			3356	3401	3446	3491	3536	3581	45
963	3626	3671	3716		3807	3852	3897	3942	3987	4032	45
964	4077	4122	4167		4257	4302	4347	4392	4437	4482	45
965	4527	4572			4707	4752	4797	4842	4887	4932	45
966	4977	5022	5067	5112	5157	5202	5247	5292	5337	5382	45
967	5426		5516		5606	5651	5696	5741	5786	5830	45
968 969	$\begin{array}{c} 5875 \\ 6324 \end{array}$	$\frac{5920}{6369}$	$\frac{5965}{6413}$		$6055 \\ 6503$	$\begin{array}{c} 6100 \\ 6548 \end{array}$	$6144 \\ 6593$	$6189 \\ 6637$	$6234 \\ 6682$	$6279 \\ 6727$	45 45
970 971	986772 7219	6817 $7264$	$6861 \\ 7309$	6906	6951	$6996 \\ 7443$	7040	7085	7130	$7175 \\ 7622$	45
972	7666		7758	7353 7800	7398 7845		7488 7934	7532 7979	7577 8024	8068	45 45
$97\tilde{3}$	8113			8247	8291	8336	8381	8425	8470	8514	45
974	8559					8782		8871	8916	8960	45
975		9049							9361		4.5
976	9450							9761	9806	9850	44
977	9895						.161	.206		.294	44
$\begin{vmatrix} 978 \\ 979 \end{vmatrix}$	$\frac{990339}{.0783}$		0428 $0871$	$\begin{array}{c} 0472 \\ 0916 \end{array}$			$\begin{array}{c} 0605 \\ 1049 \end{array}$	$\begin{array}{c} 0650 \\ 1093 \end{array}$	$0694 \\ 1137$	$\begin{bmatrix} 0738 \\ 1182 \end{bmatrix}$	44 44
980 981	$991226 \\ 1669$						$\begin{array}{c} 1492 \\ 1935 \end{array}$	1536 1979	$1580 \\ 2023$	$\begin{array}{c} 1625 \\ 2067 \end{array}$	44 44
982	2111								2465	2509	44
983	2554										44
984	2995	3039	3083	3127	3172	3216	3260		3348	3392	44
985	3436			3568	3613	3657	3701	3745			44
986	3877						4141	4185	4229	4273	44
987 988	4317	4361						4625		4713	44
989	4757 5196		4845 5284			4977 5416		5065 5504	5108 5547	5152 5591	44
$\frac{303}{990}$	$\frac{5130}{995635}$	$\frac{5240}{5679}$								$\frac{5531}{6030}$	
991	6074		5723 6161			$\frac{5854}{6293}$	5898 6337		$5986 \\ 6424$		44
992	6512	6555									44
993	6949	6993				7168			7299	7343	44
994	7386	7430	7474	7517	7561	7605	7648	7692	7736	7779	44
995	7823			7954	7998	8041	8085	8129	8172		44
996	8259										44
997 998	$\begin{array}{r} 8695 \\ 9131 \end{array}$		8782		8869						44
999	9565		9652	$9261 \\ 9696$		9348 $9783$					44 43
N.	0	1	2	3	4	5	6	7	8	9	D.

## SINES AND TANGENTS.

FOR EVERY

## DEGREE AND MINUTE

OF THE QUADRANT.

N.B. The minutes in the left-hand column of each page, increasing downwards, belong to the degrees at the top; and those increasing upwards, in the right-hand column, belong to the degrees below.

10		o reg	100.) A		LE OF LOG	JARLIN	MIC	
M	.   Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	0.000000		10.000000		10.000000		Infinite.	1 60
1	6.463726		000000		6.463726			59
2 3	764756 940847		000000		764756	293483		58
4	7.065786	$\begin{vmatrix} 208231 \\ 161517 \end{vmatrix}$	000000 000000		7.065786	208231	-00100	
5	162696	131968	000000		162696	131969	12.934214 837304	
6	241877	111575	9.999999		241878	111578	758122	54
7	308824	96653		01	308825	99653	691175	53
8	366816	85254	999999	01	366817		633183	52
9	417968 463725	76263	999999	01	417970		582030	51
$\frac{10}{11}$		68988	999998	$\frac{01}{01}$	$\frac{463727}{7}$	68988	536273	
12	$\begin{bmatrix} 7.505118 \\ 542906 \end{bmatrix}$	62981 57936	9.999998 $999997$	$\begin{vmatrix} 01\\01 \end{vmatrix}$	$7.505120 \\ 542909$	62981	12.494880	49
113	577668	53641	999997	01	577672	57933 53642	$\frac{457091}{422328}$	48 47
14	609853	49938	999996	01	609857	49939	390143	
15	639816	46714	999996	01	639820	46715	360180	45
16	667845	43881	999995	01	667849	43882	332151	44
17 18	694173 718997	41372	999995	01	694179	41373	305821	43
18	718997	$39135 \\ 37127$	999994 999993	$\begin{array}{c} 01 \\ 01 \end{array}$	719003 $742484$	39136	280997	42
20	764754	35315	999993	01	764761	$37128 \\ 35136$	257516	41 40
$\frac{2}{21}$	$ \frac{7.785943}{7.785943} $	33672	9.999992	$\frac{01}{01}$	$\frac{7.785951}{7.785951}$	33673	$\frac{235239}{19.914040}$	$\frac{40}{39}$
$\frac{\tilde{2}}{22}$	806146	$\frac{33072}{32175}$	999991	01	806155	32176	12.214049 193845	39 38
23	825451	30805	999990	01	825460	30806	174540	37
24	843934	29547	999989	02	843944	29549	156056	36
25	861662	28388	999988	02	861674	28390	138326	35
26 27	878695 895085	27317	999988	02	878708	27318	121292	34
28	910879	26323 25399	999987 999986	$\begin{bmatrix} 02 \\ 02 \end{bmatrix}$	895099 910894	26325 25401	104901	33
29	926119	24538	999985	$02 \\ 02$	926134	24540	089106 073866	$\frac{32}{31}$
30	940842	23733	999983	$0\tilde{2}$	940858	23735	059142	$\frac{30}{21}$
31	7.955082	22980	9.999982	$\frac{0}{0}$	$\frac{7.955100}{7.955100}$	22981	$\frac{033142}{12.044900}$	$\frac{30}{29}$
32	968870	22273	999981	02	968889	22275	031111	28
33	982233	21608	999980	02	982253	21610	017747	27
34	995198	20981	999979	02	995219	20983	004781	26
35 36	$\begin{bmatrix} 8.007787 \\ 020021 \end{bmatrix}$	$20390 \\ 19831$	999977 999976	$\begin{vmatrix} 02 \\ 02 \end{vmatrix}$	8.007809	20392	11.992191	25
37	031919	19302	999975	$\begin{vmatrix} 02 \\ 02 \end{vmatrix}$	$\begin{array}{c} 020045 \\ 031945 \end{array}$	19833	979955	24
38	043501	18801	999973	02	043527	$19305 \\ 18803$	968055 956473	23 22
39	054781	18325	999972	$0\tilde{2}$	054809	18327	945191	21
40	065776	17872	999971	02	065806	17874	934194	20
41	8.076500	17441	9.999969	$\overline{02}$	8.076531	17444	11.923469	19
42	086965	17031	999968	02	086997	17034	913003	18
43	097183	16639	999966	02	097217	16642	902783	17
44 45	$107167 \\ 116926$	16265 15908	999964	$\begin{vmatrix} 03 \\ 03 \end{vmatrix}$	$\begin{array}{c} 107202 \\ 116963 \end{array}$	16268	892797	16
46	126471	15566	$999963 \\ 999961$	03	126510	15910 15568	883037	15
47	135810	15238	999959	03	135851	15300 $15241$	873490 864149	14 13
48	144953	14924	999958	03	144996	14927	855004	12
49	153907	14622	999956	03	153952	14627	846048	11
513	162681	14333	999954	03	162727	14336	837273	10
51	8.171280	14054	9.999952	03	8.171328	14057	11.828672	9
52	179713	13786	999950	03	179763	13790	820237	8
53 54	$187985 \\ 196102$	$13529 \\ 13280$	999948	03	188036	13532	811964	7
55	204070	$\frac{13280}{13041}$	999946 $999944$	03	$\frac{196156}{204126}$	$13284 \\ 13044$	803844 795874	6
56	211895	12810	999942	(4)	211953	13044 $12814$	795874 788047	5 4
57	219581	12587	999940	$ 0\hat{4} $	219641	12590	780359	3
58	227134	12372	999938	04	227195	-12376	772805	2
59 60	234557	12164	999936	04	234621	12168	765379	1
=	241855	11963	999934	041	241921	11967	758079	
	Cosine	-	Sine		Cotang.		Tang.	M.
		أنسان المستنا				-		

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	8.241855	11963	9.999934	04	8.2419211	11967	11.758079	60
1	249033	11768	999932	04	249102	11772	750898	59
$\hat{2}$	256094	11580	999929	04	256165	11584	743835	58
$\tilde{3}$	263042	11398	999927	$0\overline{4}$	263115	11402	736885	57
4	269881	11221	999925	$0\overline{4}$	269956	11225	. 730044	56
5	276614	11050	999922	04	276691	11054	723309	55
6	283243	10883	999920	04	283323	10887	716677	54
7	289773	10721	999918	04	289856	10726	710144	53
8	296207	10565	999915	04	296292	10570	703708	52
9	30254.6	10413	999913	04	302634	10418	697366	51
10	308794	10266	999910	04	308884	10270	691116	50
$\overline{11}$	8.314954	$\overline{10122}$	9.999907	$\overline{04}$	8.315046	10126	11.684954	$\overline{49}$
12	321027	9982	999905	04	321122	9987	678878	48
13	327016	9847	999902	04	327114	9851	672886	47
14	332924	9714	999899	05	333025		666975	46
15	338753	9586	999897	05	338956		661144	45
16	344504	9460	999894	05	344610	9465	655390	44
17	350181	9338	999891	05	350289	9343	649711	43
18	355783	9219	999888	05	355895	9224	644105	42
19	361315	9103	999885	05	361430	9108	638570	41
20	366777	8990	999882	05	366895	8995	633105	40
$\overline{21}$	8.372171	8880	9.999879	05	8.372292	8885	11.627708	39
22	377499	8772	999876	05	377622	8777	622378	38
23	382762	8667	999873	05	382889		617111	37
24	387962	8564	999870	05	388092		611908	36
25	393101	8464	999867	05	393234	8470	606766	35
26	398179	8366	999864	05	398315	8371	601685	34
27	403199	8271	999861	05	403338	8276	596662	33
28	408161	8177	999858	05	408304	8182	591696	32
29	413068	8086	999854	05	413213	8091	586787	31
30	417919	7996	999851	06	418068	8002	581932	30
31	8.422717	7909	9.999848	$\overline{06}$	8.422869	7914	11.577131	$\overline{29}$
32	427462	7823	999844	06	427618	7830	572382	28
33	432156	7740	999841	06	432315	7745	567685	27
34	436800	7657	999838	06	436962	7663	563038	26
35	441394	7577	999834	06			558440	25
36	445941	7499	999831	06	446110		553890	24
37	450440	7422	999827	06	450613		549387	23
38	454893	7346	999823	06	455070		544930	22
39	459301	7273	999820	06	459481	7279	540519	21
40	463665	7200	999816	06	463849	7206	536151	20
41	8.467985	7129	9.999812	$\overline{06}$		7135	11.531828	19
42	472263	7060	999809	06	472454		527546	18
43	476498	6991	999805	06	476693		523307	17
44	480693	6924	999801	06			519108	16
45	484848	6859	999797	07	485050		514950	15
46	488963	6794	999793	07	489170		510830	14
47	493040	6731	999790	07	493250		506750	13
48	497078	6669	999786	07	497293		502707	12
49	501080	6608	999782	07	501298		498702	11
$\frac{50}{}$	505045	6548	999778	$\frac{07}{27}$	$\frac{505267}{2}$		494733	
51	8.508974	6489	9.999774	$\overline{07}$	8.509200	6496	11.490800	9
52	512867	6431	999769	07	513098	6439	486902	8
53	516726	6375	999765	07	516961	6382	483039	7
54	520551	6319	999761	07	520790		479210	6
55	524343	6264	999757	07	524583		475414	5
56	528102	6211	999753	07	528349	6218	471651	4
57	531828	6158	999748	07	532080		467920	3
58	535523	6106	999744	$\begin{vmatrix} 07\\07 \end{vmatrix}$	535779 539447	6113 606 <b>2</b>	464221	$\begin{bmatrix} 2 \\ 1 \end{bmatrix}$
59 60	$539186 \\ 542819$	$\begin{array}{c} 6055 \\ 6004 \end{array}$	999740 $999735$				460553 456916	$\begin{bmatrix} 1 \\ 0 \end{bmatrix}$
		0004		. 07		0014		
	Cosine		Sine		Cotang.		Tang.	M.
								_

20	(2	Degre	ees.) A	TAL	BLE OF LO	)GARIT.		
M.	Sine	D.	Cosine	D.	Tang,	D.	Cotang.	
01	8.542819	6004	9.999735	07	8.543084	6012	11.456916	60
1	546422	5955	999731	07	546691	5962	$\begin{array}{c c} 453309 \\ 449732 \end{array}$	59 58
2	549995 553539	5906 5858	$\begin{array}{c} 999726 \\ 999722 \end{array}$	07 08	550268 553817	5914 5866	446183	57
$\begin{vmatrix} 3 \\ 4 \end{vmatrix}$	557054	5811	999717	08	557336	5819	442664	56
5	560540	5765	999713	08	560828	5773	439172	55
6	563999	5719	999708	08	564291	5727	435709	54
7	567431	5674	999704	08 08	567727 571137	5682 5638	432273 428863	53 52
8 9	570836 574214	5630 5587	999699 999694	08	574520	5595	425480	51
10	577566	5544	999689	08	577877	5552	422123	50
11	8.580892	5502	9.999685	$\overline{08}$	8.581208	5510	11.418792	$\overline{49}$
12	584193	5460	999680	08	584514	5468	415486	48
13	587469	5419	999675	08	587795	$5427 \\ 5387$	$\begin{array}{c c} & 412205 \\ \hline & 408949 \end{array}$	47 46
14	590721 593948	5379 5339	999670 999665	80	591051 $594283$	5347	405717	45
15	597152	5300	999660	08	597492	5308	402508	44
17	600332	5261	999655	08	600677	5270	399323	43
18	603489	5223	999650	08	603839	5232	396161	42
19	$\begin{array}{c} 606623 \\ 609734 \end{array}$	5186	999645	09 09	$606978 \\ 610094$	5194 5158	393022 389906	41
$\frac{20}{21}$		5149	$\frac{999640}{0.000005}$	$\frac{03}{09}$	8.613189	$\frac{5130}{5121}$	11.386811	$\frac{10}{39}$
$\begin{bmatrix} 21 \\ 22 \end{bmatrix}$	$8.612823 \\ 615891$	5112 5076	9.999635	09	616262	5085	383738	38
23	618937	5041	999624	09	619313	5050	380687	37
24	621962	5006	999619	09	622343	5015	377657	36
25	624965	4972	999614	09	625352	4981	374648	35
26	$\begin{array}{c} 627948 \\ 630911 \end{array}$	4938	999608 999603	09 09	$\frac{628340}{631308}$	$\begin{array}{c} 4947 \\ 4913 \end{array}$	$371660 \\ 368692$	34   33
27 28	633854	$\frac{4904}{4871}$	999597	09	634256	4880	365744	32
29	636776	4839	999592	09	637184	4848	362816	31
30	639680	4806	999586	09	640093	4816	359907	30
31	8.642563	4775	9.999581	09	8.642982	4784	11.357018	29
32	645428	4743	999575	09	645853	$4753 \\ 4722$	354147 351296	28 27
1 33	$648274 \\ 651102$	$\begin{array}{c} 4712 \\ 4682 \end{array}$	999570 $999564$	$\begin{vmatrix} 09 \\ 09 \end{vmatrix}$	$648704 \\ 651537$	4691	348463	
34 35	653911	4652	999558	10	654352		345648	25
36	656702	4622	999553		657149	4631	342851	24
37	659475	4592	999547		659928	$4602 \\ 4573$	340072	23
38	$\begin{array}{c c} 662230 \\ 664968 \end{array}$	$\begin{array}{c} 4563 \\ 4535 \end{array}$	999541 999535	10	662689 665433	4544	337311 334567	22 21
39 40	667689	4506	999529	10	668160		331840	20
$\frac{1}{41}$	8.670393	4479	9.999524	$\overline{10}$	8.670870	4488	11.329130	19
42	673080	4451	999518	10	673563	4461	326437	18
43	675751	4424	999512		676239	4434	323761	17
44	678405	4397	999506		678900 $681544$	4417 4380	$\begin{vmatrix} 321100 \\ 318456 \end{vmatrix}$	16 15
45 46	$\begin{bmatrix} 681043 \\ 683665 \end{bmatrix}$	$\begin{array}{c} 4370 \\ 4344 \end{array}$	999500 $999493$		1		315828	
47	686272	4318	999487	10	686784	4328	313216	13
48	688863	4292	999481	10		4303	310619	12
49	691438	4267	999475				308037 305471	11 10
$\frac{50}{51}$	693998	4242	$\frac{999469}{0.000463}$		$\frac{694529}{8.697081}$	$\begin{array}{ c c c c c }\hline 4232\\\hline 4228\\\hline \end{array}$	$\frac{303471}{11.302919}$	$\frac{10}{9}$
$\overline{\frac{51}{52}}$	$\begin{array}{r} 8.696543 \\ 699073 \end{array}$	$\frac{4217}{4192}$	9.999463 $999456$		699617		300383	8
53	701589	4168	999450		702139	4179	297861	7
54	704090	4144	999443	11	704646	4155	295354	
55	706577	4121	999437				292860 290382	5
56 57	709049	$\begin{array}{c} 4097 \\ 4074 \end{array}$	999431 $999424$				2911382	3
58	713952		999418		I		285465	
59	716383	4029	999411	11	716972	4040	283028	1
60	718800	4006	999404	111	719396	4017	280304	
	Cosine	,	Sine		Cotang.		Tang.	M.
-	-			-			-	

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	(8.718800)	4006 (	9.999404	11	8.719396	4017	11.280604	60
1	721204	3984	999398	11	721806	3995	278194	59
2	723595	3962	999391	11	724204	3974	275796	58
3	725972	3941	999384	11	726588	3952	273412	57
4 5	$oxed{728337}{730688}$	3919 3898	$\frac{999378}{999371}$	11 11	728959 $731317$	3930 3909	$271041 \ 268683$	56 55
6	733027	3877	999364	12	733663	3889	266337	54
7	735354	3857	999357	$\tilde{12}$	735996	3868	264004	
8	737667	3836	999350	12	738317	3848	261683	
9	739969	3816	999343	12	740626	3827	259374	
10	742259	3796	999336	12	742922	3807	257078	50
11	8.744536	3776	9.999329	12	8.745207	3787	11.254793	
12	746802	3756	999322	12	747479	3768	252521	48
13	749055	3737	999315 $999308$	12	749740	3749 3729	250260	47
14	751297 753528	$\begin{array}{c c} 3717 \\ 3698 \end{array}$	999300	12 12	751989 754227	3710	$248011 \\ 245773$	
16	755747	3679	999294	12	756453	3692	243547	
17	757955	3661	999286	12	758668	3673	241332	
18	760151	3642	999279	12	760872	3655	239128	42
19	762337	3624	999272	12	763065	3636	236935	
$\underline{20}$	$\frac{764511}{}$	3606	999265	12	765246	3618	$\frac{234754}{}$	
21	8.766675	3588	9.999257	12	8.767417	3600	11.232583	
22	768828	3570	999250	13	769578	3583	230422	
23	770970	3553 3535	999242	13	771727 773866	3565 3548	228273	
24 25	773101 $775223$	3518	$\begin{array}{c} 999235 \\ 999227 \end{array}$	13 13	775995	3531	$226134 \\ 224005$	
$\frac{26}{26}$	777333	3501	999220	13	778114	3514	221886	
27	779434	3484	999212	13	780222	3497	219778	
28	781524	3467	999205	13	782320	3480	217680	
29	783605	3451	999197	13	784408	3464	215592	
30	785675	3431	999189	$\frac{13}{}$	786486	3447	213514	1
31	8.787736	3418	9.999181	13		3431	11.211446	
32	789787	3402	999174	13	790613		209387	
33 34	791828 793859	$\frac{3386}{3370}$	999166 $999158$	13 13		3399 3383	207338 205299	
35	795881	3354	999150			3368	203269	
36	797894		999142	13			201248	
37	799897		999134				199237	
38	801892		999126				197235	
39	803876		999118				195242	
$\frac{40}{41}$	805852	3278	999110				$\frac{193258}{1101939}$	
41	8.807819	3263	9.999102			3278	11.191283	
42 43	809777 811726		$oxed{999094} 999086$			3262 3248	189317 187359	
44	813667		999077				185411	16
45	815599		999069			3219	183471	15
46	817522	3191	999061	14	818461	3205	181539	
47	819436		999053				179616	
48	821343		999044				$\begin{vmatrix} 177702 \\ 175795 \end{vmatrix}$	
49 50	823240 825130		$oxed{999036} 999027$				173795	
$\frac{50}{51}$	$\frac{8.827011}{8.827011}$	]	$\frac{999027}{9.999019}$	l —	$\frac{8.827992}{8.827992}$		$\frac{173037}{11.172008}$	-
52	828884	3122	9.999019				170126	
53	830749		999002	1		3110	168252	7
54	832607		998993		833613	3096	166387	6
55	834456	3069	998984	14	835471	3083	164529	5
56	835297		998976			3070	162679	4
57	838130	3043	998967				160837	3 2
58 59	839956 841774		998958 $998950$			$\frac{3045}{3032}$	159002 $157175$	ĩ
60			998941				155356	
	Cosine	1 3004		1		3010	Tang.	M.
	Cosme		Sine		Cotang.	200	rang.	141.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotone	l
-	8.843585	3005					Cotang.	
$\begin{bmatrix} 0 \\ 1 \end{bmatrix}$	845387	2992	$9.998941 \\ 998932$	15 15	8.844644	3019	11.155356 153545	60
2	847183	2980	998923	15	848260	2995	151740	59 58
3	848971	2967	998914	15	850057	2982	149943	57
4	850751	2955	998905	15	851846	2970	148154	56
5	852525	2943	998896	15	853628	2958	146372	55
$\begin{array}{c c} 6 \\ 7 \end{array}$	854291 856049	2931	998887 $998878$	15 15	855403 857171	2946	144597	54
8	857801	2919 2907	998869	15	858932	$2935 \\ 2923$	142829 $141068$	53
9	859546	2896	998860	15	860686	2911	139314	52 51
10	861283	2884	998851	15	862433	2900	137567	50
11	8.863014	2873	9.998841	$\overline{15}$	8.864173	2888	11.135827	$\frac{3}{49}$
12	864738	2861	998832	15	865906	2877	134094	48
13	866455	2850	998823	16	867632	2866	132368	47
14 15	868165 869868	2839	$\begin{array}{c} 998813 \\ 998804 \end{array}$	16 16	869351	2854	130649	46
16	871565	$\frac{2828}{2817}$	998795	16	$871064 \ 872770$	$\begin{array}{c} 2843 \\ 2832 \end{array}$	$\begin{array}{c} 128936 \\ 127230 \end{array}$	45
17	873255	2806	998785	16	874469	2821	127230 $125531$	44 43
18	874938	2795	998776	16	876162	2811	123838	43
19	876615	2786	998766	16	877849	2800	122151	41
20	878285	2773	998757	$\frac{16}{}$	879529	2789	120471	40
21	8.879949	2763	9.998747	16	8.881202	2779	11.118798	$\overline{39}$
22	881607 883258	2752	998738	16	882869	2768	117131	38
23   24	883238	2742 2731	$\begin{array}{c} 998728 \\ 998718 \end{array}$	$\frac{16}{16}$	$884530 \\ 886185$	$\frac{2758}{2747}$	115470	37
25	886542	$\begin{bmatrix} 2731 \\ 2721 \end{bmatrix}$	998708	16	887833	2737	113815 $112167$	36
26	888174	2711	998699	16	889476	2727	110524	35 34
27	889801	2700	998689	16	891112	2717	108888	33
28	891421	2690	998679	16	892742	2707	107258	32
29	893035	2680	998669	17	894366	2697	105634	31
$\frac{30}{21}$	894643	2670	998659	$\frac{17}{18}$	895984	2687	104016	30
31 32	8.896246 897842	2660 2651	9.998649	$\frac{17}{17}$	8.897596	2677	11.102404	29
33	899432	2641	998639 998629	17	$899203 \\ 900803$	$\begin{array}{c} 2667 \\ 2658 \end{array}$	$100797 \\ 099197$	28 27
34	901017	2631	998619	17	902398	2648	097692	26
35	902596	2622	998609	17	903987	2638	096013	25
36	904169	2612	998599	17	905570	2629	094430	24
37	905736	2603	998589	$\frac{17}{17}$	907147	2620	092853	23
38 39	907297 $908853$	$2593 \\ 2584$	998578 $998568$	17	$908719 \ 910285$	$\frac{2610}{2601}$	$091281 \\ 089715$	22   21
40	910404	2575	998558	17	911846	$\begin{array}{c} 2001 \\ 2592 \end{array}$	088154	20
$\frac{1}{41}$	8.911949	2566	$\frac{0.998548}{9.998548}$	$\frac{1}{17}$	$\frac{312313}{8.913401}$	$\frac{2583}{2583}$	$\frac{000194}{11.086599}$	$\frac{20}{19}$
42	913488	2556	998537	17	914951	$\begin{array}{c} 2574 \\ 2574 \end{array}$	085049	18
43	915022	2547	998527	17	916495	2565	083505	17
44	916550	2538	998516	1.8	918034	2556	081966	16
45	918073	2529	998506	18	919568	2547	080432	15
46 47	$919591 \\ 921103$	2520 2512	998495 $998485$	18 18	$921096 \ 922619$	$\begin{array}{c} 2538 \\ 2530 \end{array}$	078904	14 13
48	$\begin{array}{c c} 921103 \\ 922610 \end{array}$	$\begin{array}{c} 2512 \\ 2503 \end{array}$	998474	18	$\begin{array}{c} 922019 \\ 924136 \end{array}$	$\begin{array}{c} 2530 \\ 2521 \end{array}$	$077381 \ 075864$	12
49	924112	2494	998464	18	925649	2512	074351	11
50	925609	2486	998453	18	927156	2503	072844	10
51	8.927100	2477	9.998442	18	8.928658	2495	$\overline{11.071342}$	9
52	928587	2469	998431	18	930155	2486	069845	8
53	930068	2460	998421	18	931647	2478	068353	7
54   55	$\begin{array}{c} 931544 \\ 933015 \end{array}$	$\begin{array}{c} 2452 \\ 2443 \end{array}$	998410 $998399$	18 18	$933134 \\ 934616$	$\begin{array}{c} 2470 \\ 2461 \end{array}$	$066866 \ 065384$	6
56	934481	$\begin{array}{c} 2445 \\ 2435 \end{array}$	998399	18	934010 $936093$	$\begin{array}{c} 2401 \\ 2453 \end{array}$	U63384 U63907	5 4
57	935942	2427	998377	18	937565	2445	062435	3
58	937398	2419	998366	18	939032	2437	060968	2
59	938850	2411	998355	18	940494	2430	059506	1
60	940296	2403	998344	18	941952	2421	058048	0
	Cosine		Sine		Cotang.		Tang.	M.

M.	Sine	D.	Cosine	D.		D.		1
0	8.940296		9.9983444		8.9419520		Cotang.	00
1	941738	2394	998333	19	943404	$\begin{array}{c} 2421 \\ 2413 \end{array}$	$11.058048 \\ 056596$	60 59
2	943174	2387	998322	19	944852	2405	055148	58
3	944606	2379	998311	19	946295	2397	053705	57
4	946034	2371	998300	19	947734	2390	052266	56
5	947456	2363	998289	19	949168	2382	050832	55
6	948874	2355	998277	19	950597	2374	049403	54 53
7 8	950287 $951696$	$\begin{array}{c} 2348 \\ 2340 \end{array}$	$998266 \\ 998255$	$\begin{array}{c} 19 \\ 19 \end{array}$	952021   953441	$\frac{2366}{2360}$	$\begin{array}{c c} 047979 \\ 046559 \end{array}$	52
G	953100	2332	998243	19	954856	2351	045144	51
10	954499	2325	998232	19	956267	2344	043733	50
11	8.955894	2317	9.998220	$\overline{19}$	8.957674	2337	11.042326	49
12	957284	2310	998209	19	959075	2329	040925	48
13	958670	2302	998197	19	960473	2323	039527	47
14:	960052	2295	998186	19	961866	2314	038134	46
15 16	$\begin{array}{r} 961429 \\ 962801 \end{array}$	2288 2280	998174 $998163$	19 19	$963255 \ 964639$	$\begin{array}{c} 2307 \\ 2300 \end{array}$	$036745 \\ 035361$	45
17	964170	2273	998151	19	966019	2293	033981	43
18	965534	2266	998139	20	967394	2286	032606	42
19	966893	2259	998128	20	968766	2279	031234	41
20	968249	2252	998116	$\frac{20}{20}$	970133	2271	029867	40
21	8.969600	2244	9.998104	$\overline{20}$	8.971496	2265	11.028504	39
22	970947	2238	998092	20	972855	2257	027145	38
23	972289	2231	998080	$\frac{20}{20}$	974209 $975560$	$2251 \\ 2244$	$\begin{array}{c c} 025791 \\ 024440 \end{array}$	37 36
24 25	$\begin{array}{c} 973628 \\ 974962 \end{array}$	$\begin{array}{c c} 2224 \\ 2217 \end{array}$	998068 998056	$\frac{20}{20}$	976906	2237	0234440	35
26	976293	2210	998044	$\tilde{20}$	978248	2230	021752	34
27	977619	2203	998032	20	979586	2223	020414	33
28	978941	2197	998020	20	980921	2217	019079	32
29	980259	2190	998008	20	982251	2210	017749	31
30	981573	2183	997996	$\frac{20}{100}$	983577	2204	016423	$\frac{30}{100}$
31	8.982883	2177	9.997984	20	8.934899	2197	11.015101	29
32	$984189 \\ 985491$	$\begin{array}{c c} 2170 \\ 2163 \end{array}$	997972 $997959$	$\frac{20}{20}$	986217 $987532$	$\frac{2191}{2184}$	$013783 \\ 012468$	28 27
33 34	986789	2157	997947	$\tilde{20}$	988842	2178	011158	26
35	988083	2150	997935	21	990149	2171	009851	25
36	989374	2144	997922	21	991451	2165	008549	24
37	990660	2138	997910	21	992750	2158	007250	23
38	991943	2131	997897	21	$\begin{array}{c} 994045 \\ 995337 \end{array}$	$\begin{array}{c} 2152 \\ 2146 \end{array}$	$005955 \ 004663$	22 21
39 40	9932229934497	$\begin{array}{c} 2125 \\ 2119 \end{array}$	997885 $997872$	$\begin{vmatrix} 21\\21 \end{vmatrix}$	996624	$\frac{2140}{2140}$	$004005 \\ 003376$	20
41	$\frac{934497}{8.995768}$	$\frac{2119}{2112}$	$\frac{337872}{9.997860}$	$\frac{z_1}{21}$	$\frac{330024}{8.997908}$	2134	$\frac{003370}{11.002092}$	$\frac{20}{19}$
41	997036	$\begin{array}{c} 2112 \\ 2106 \end{array}$	9.997800 $997847$	$\frac{21}{21}$	999188	$\frac{2134}{2127}$	000812	18
43	998299	2100	997835	$\tilde{2}\bar{1}$	9.000465	2121	10.999535	17
44	999560	2094	997822	21	001738	2115	998262	16
45	9.000816	2087	997809	21	003007	2109	996993	15
46	002069	2082	$997797 \\ 997784$	$\frac{21}{21}$	$004272 \\ 005534$	$\frac{2103}{2097}$	995728 $994466$	14 13
47 48	$003318 \ 004563$	$\begin{array}{c} 2076 \\ 2070 \end{array}$	$997784 \\ 997771$	$\frac{z_1}{21}$	$005534 \\ 006792$	2091	993208	12
49	004903 $005805$	2064	997758	$\tilde{2}^1$	008047	2085	991953	11
50	007044	2058	997745	21	009298	2080	990702	0,
$\overline{51}$	9.008278	2052	$\overline{9.997732}$	$\overline{21}$	9.010546	2074	10.989454	$\overline{9}$
52	009510	2046	997719	21	011790	2068	988210	8
53	010737	2040	997706	21	013031	2062	986969	7
54	011962	2034	997693	22	014268	$\begin{array}{c} 2056 \\ 2051 \end{array}$	985732	6
55 56	$013182 \\ 014400$	$\begin{array}{c} 2029 \\ 2023 \end{array}$	$\begin{array}{c} 997680 \\ 997667 \end{array}$	$\frac{22}{22}$	$015502 \ 016732$	$\begin{array}{c} 2051 \\ 2045 \end{array}$	984498 $983268$	5 4
57	015613	$\begin{bmatrix} 2025 \\ 2017 \end{bmatrix}$	997654	22	017959	2040	982041	3
58	016824	2012	997641	$\tilde{2}\tilde{2}$	019183	2033	980817	2
59	018031	2006	997628	22	020403	2028	979597	1
60	019235	2000	997614	22	021620	2023	978380	0
	Cosine		Sine	1	Cotang.		Tang.	M.
-	THE RESERVE OF THE PERSON NAMED IN	-				-	-	-

24 M	Sine	Degre D.	Cosine	TAB		D.	Cotang.	
				-				
0	9.019235	2000	9.997614	22	9.021620	2023	10.978380	60
1	020435	1995	997601 997588	22 22	$\begin{array}{c c} 022834 \\ 024044 \end{array}$	2017 2011	$977166 \ 975956$	59 58
2 3	$\begin{array}{c} 021632 \\ 022825 \end{array}$	1989 1984	997574	22	$024044 \\ 025251$	2006	974749	57
4	024016	1978	997561	22	026455	2000	973545	56
5	025203	1973	997547	$\tilde{2}\tilde{2}$	027655	1995	972345	55
6	026386	1967	997534	$\tilde{23}$	028852	1990	971148	54
7	027567	1962	997520	23	030046	1985	969954	53
8	028744	1957	997507	23	031237	1979	968763	52
9	029918	1951	997493	23	032425	1974	£67575	51
10	031089	1947	997480	23	033609	1969	966391	50
$\overline{11}$	9.032257	1941	9.997466	$\overline{23}$	9.034791	1964	10.965209	49
12	033421	1936	997452	23	035969	1958	964031	48
13	034582	1930	997439	23	037144	1953	962856	47
14	035741	1925	997425	23	038316	1948	961684	46
15	036896	1920	997411	23	039485	1943	960515	45
16	038048	1915	997397	23	040651	1938	959349	44
17 18	$039197 \\ 040342$	1910 1905	$\begin{array}{c} 997383 \\ 997369 \end{array}$	23 23	$\begin{array}{c} 041813 \\ 042973 \end{array}$	$\begin{array}{c} 1933 \\ 1928 \end{array}$	958187 $957027$	43 42
18 19	040342	1899	997355	23	042973	1928	955870	42
$\frac{13}{20}$	042625	1894	997341	$\tilde{23}$	045284	1918	954716	40
$\frac{20}{21}$	$\frac{042025}{9.043762}$	1889	$\frac{337311}{9.997327}$	$\frac{20}{24}$	$\frac{010201}{9.046434}$	1913	$\frac{001110}{10.953566}$	$\frac{10}{39}$
$\frac{21}{22}$	044895	1884	997313	24	047582	1913	952418	38
23	046026	1879	997299	$\tilde{24}$	048727	1903	951273	37
24	047154	1875	997285	24	049869	1898	950131	36
25	048279	1870	997271	24	051008	1893	948992	35
26	049400	1865	997257	24	052144	1889	947856	34
27	050519	1860	997242	24	053277	1884	946723	33
28	051635	1855	997228	24	054407	1879	945593	32
29	052749	1850	997214	24	055535	1874	944465	31
30	053859	1845	997199	$\frac{24}{}$	056659	1870	943341	30
31	054966	1841	9.997185	24	9.057781	1865	10.942219	29
32	056071	1836	997170	24	058900	1869	941100	28
33	057172	1831	997156	24	060016	1855	939984	27
34 35	$\begin{array}{c c} 058271 \\ 059367 \end{array}$	$\begin{array}{c} 1827 \\ 1822 \end{array}$	$\begin{array}{c} 997141 \\ 997127 \end{array}$	24 24	$\begin{array}{c c} 061130 \\ 062240 \end{array}$	$\begin{array}{c} 1851 \\ 1846 \end{array}$	$938870 \\ 937760$	26 25
36	060460	1817	997112	24	063348	1842	936652	24
37	061551	1813	997098	24	064453	1837	935547	23
38	062639	1808	997083	25	065556	1833	934444	22
39	063724	1804	997068	25	066655	1828	933345	21
40	064806	1799	997053	25	067752	1824	932248	20
$\overline{41}$	9.065885	1794	9.997039	$\overline{25}$	9.068846	1819	10.931154	19
42	066962	1790	997024	25	069938	1815	930062	
43	068036	1786	997009	25	071027	1810	928973	17
44	069107	1781	996994	25	072113	1806	927887	
45	070176	1777	996979	25	073197	1802	926803	
46	071242	1772	996964	25	074278	1797	925722	
47	072306	1768	996949	25	075356	1793	924644	
48 49	$073366 \\ 074424$	1763 1759	996934 $996919$	25   25	076432	1789 1784	923568 922495	
50	075480	1755	996919	25	078576	1784	922495 $921424$	
$\frac{50}{51}$	$\frac{076430}{9.076533}$	$\frac{1750}{1750}$	$\frac{336364}{9.996889}$	$\frac{25}{25}$	$\frac{0.079644}{9.079644}$	1776		1
52	077583	1750	9.996889 $996874$		080710	1776	$\begin{bmatrix} 10.920356 \\ 919290 \end{bmatrix}$	
53	078631	1742	996858	25	081773		919290	
54	079676	1738	996843		082833		917167	
55	080719	1733	996828		083891	1759	916109	
56	081759	1729	996812	26	084947	1755	915053	
57	082797	1725	996797	26	086000	1751	914000	3
58	083832	1721	996782		087050		912950	2
59	084864	1717	996766		086098		911902	
60	085894	1713	996751	26	089144	1738	910856	0
	Cosine		Sine		Cotang.		Tang.	M.
4				G-	-			1

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.085894	1713	9.996751	26	9.089144		10.910856	60
1 2	$oxed{086922}{087947}$	1709 1704	996735 $996720$	26 26	$090187 \\ 091228$	1734 1730	909813 $908772$	59 58
3	088970	1700	996704	26	092266		907734	57
4	089990	1696	996688	26	093302	1722	906698	56
5	091008	1692	996673	26	094336		905664	55
6 7	$oxed{092024} \ 093037$	1688 1684	996657 $996641$	26 26	095367 $096395$		904633 903605	54 53
8	094047	1680	996625	26	097422		902578	52
9	095056	1676	996610	26	098446		901554	51
10	096062	1673	996594	26	099468	1699	900532	$\frac{50}{100}$
11 12	$   \begin{bmatrix}     9.097065 \\     098066   \end{bmatrix} $	1668	9.996578	27	9.100487 $101504$		10.899513	49 48
13	099065	1665 1661	996562 996546	27 27	101504 $102519$		898496 897481	47
14	100062	1657	996530	27	103532		896468	$\overline{46}$
15	101056	1653	996514	27	104542		895458	45
16	$\begin{array}{ c c c c c }\hline 102048 \\ 103037 \\ \hline \end{array}$	1649	996498 996482	27	$105550 \\ 106556$		894450 893444	44 43
18	103037	$\begin{array}{c} 1645 \\ 1641 \end{array}$	996465	$\begin{bmatrix} 27 \\ 27 \end{bmatrix}$	$\begin{array}{c} 100350 \\ 107559 \end{array}$		892441	42
19	105010	1638	996449	27	108560		891440	41
20	105992	1634	996433	27	109559		890441	40
21	9.106973	1630	9.996417	$\overline{27}$	9.110556		10.889444	39
22 23	$\begin{array}{ c c c c c }\hline 107951 \\ 108927 \\ \hline \end{array}$	$\begin{array}{c} 1627 \\ 1623 \end{array}$	$\begin{array}{c} 996400 \\ 996384 \end{array}$	27 27	111551 112543		888449 887457	38
24	108927	1619	$996364 \\ 996368$	27	113533		886467	36
25	110873	1616	996351	27	114521		885479	35
26	111842	1612	996335	27	115507	1639	884493	34
27	112809	1608	996318	27	116491		883509	33
28 29	113774 114737	$\begin{array}{c} 1605 \\ 1601 \end{array}$	$\begin{array}{r} 996302 \\ 996285 \end{array}$	28 28	117472 $118452$		882528 881548	$\begin{vmatrix} 32 \\ 31 \end{vmatrix}$
30	115698	1597	996269	28	119429		880571	30
31	9.116656	1594	9.996252	$\frac{28}{28}$	9.120404		10.879596	$\overline{29}$
32	117613	1590	996235	28	121377	1618	878623	28
33 34	118567	1587	996219	28	122348		877652	
35	119519 120469	1583 1580	996202 $996185$	28   28	$egin{array}{ccc} 123317 \ 124284 \end{array}$		876683 875716	
36	121417	1576	996168		125249		874751	24
37	122362	1573	996151	28	126211		873789	
38	123306	1569	996134		127172		872828	
40	124248 125187	$\begin{array}{c} 1566 \\ 1562 \end{array}$	$oxed{996117} 996100$		$\begin{array}{ c c c c c }\hline & 128130 \\ & 129087 \\ \hline \end{array}$		871870 870913	
$\frac{1}{41}$	$\frac{125167}{9.126125}$	$\frac{1502}{1559}$	$\frac{330100}{9.996083}$		$\frac{125001}{9.130041}$		$\frac{0.0310}{10.869959}$	
42	127060	1556	996066		130994		869006	
43	127993	1552	996049	29	131944	1581	868056	
44 45	128925	1549	996032		$\begin{array}{c c} & 132893 \\ & 133833 \end{array}$		867107 866161	
46	129854 130781	1545 1542	996015 995998		133838		865216	15
47	131706	1539	995980		135726	1567	864274	13
48	132630	1535	995963	29	136667	1564	863333	12
49 50	133551	1532	995946		137608 138549		862395 861458	
51	134470	1529	$\frac{995928}{0.005011}$	· \	$\frac{138547}{9.139476}$	-	$\frac{801458}{10.860524}$	
52	$\begin{vmatrix} 9.135387 \\ 136303 \end{vmatrix}$	1525 1522	9.995911 $995894$		14040		859591	
53	137216	1519	995876		141340	1548	858660	7
54	138128	1516	995859	29	142269	1545	857731	6
55 56	139037		995841	29	14319 14412		856804	
57	139944 $140850$		995823		14412		855879 854956	
58	141754		995788		14596		854034	
59	142655	1500	995771	29	14688	5 1529	853115	1
60	143555	1496	995753	3   29	14780	3 1526	852197	
	Cosine		Sine	1	Cotang.		Tang.	M.

20	(0	Degre	es.) A T	'AB	LE OF LOC	JARITH		
M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.143555	1496	19.995753		9,147803	1526	10.852197	
1	144453	1493	995735	30	148718	1523	851282	59
2 3	145349	1490	995717	30	$149632 \\ 150544$	$1520 \\ 1517$	850368 849456	58 57
4	$\begin{vmatrix} 146243 \\ 147136 \end{vmatrix}$	$1487 \\ 1484$	995699 995681	30	151454	1514	848546	56
5	148026	1481	995664	30	152363	1511	847637	55
$\tilde{6}$	148915	1478	995646	30	153269	1508	846731	54
7	149802	1475	995628	30	154174	1595	845826	53
8	150686	1472	995610	30	155077	1502	844923	52
9 10	$\begin{array}{c c} 151569 \\ 152451 \end{array}$	$\begin{array}{c} 1469 \\ 1466 \end{array}$	995591 995573	30 30	$oxed{155978} 156877$	1499 1496	$oxed{844022}{843123}$	21 50
-					$\frac{150377}{9.157775}$		$\frac{643125}{10.842225}$	
11 12	$\begin{bmatrix} 9 & 153330 \\ 154208 \end{bmatrix}$	$\begin{array}{c} 1463 \\ 1460 \end{array}$	9.995555 $995537$	30 30	158671	$\frac{1493}{1490}$	841329	49 48
13	155083	1457	995519	30	159565	1487	840435	47
14	155957	1454	995501	31	160457	1484	839543	46
15	156830	1451	995482	31	161347	1481	838653	45
16	157700	1448	995464	31	162236	1479	837764	44
17	158569	1445	995446	31	$163123 \\ 164008$	$\begin{array}{c} 1476 \\ 1473 \end{array}$	826877	43 42
18 19	$oxed{159435}{160301}$	$\begin{array}{c} 1442 \\ 1439 \end{array}$	995427   995409	31 31	164892	1470	$835992 \\ 835108$	41
20	161164	1436	995390	31	165774	1467	834226	40
$\frac{1}{21}$	$\overline{9.162025}$	1433	${9.995372}$	$\frac{31}{31}$	9.166654	1464	10.833346	$\frac{1}{39}$
$2\overline{2}$	162885	1430	995353	31	167532	1461	832468	38
23	163743	1427	995334	31	168409	1458	831591	37
24	164600	1424	995316	31	169284	1455	830716	36
25 26	$165454 \\ 166307$	$\begin{array}{c c} 1422 \\ 1419 \end{array}$	$\frac{995297}{995278}$	31 31	170157 $171029$	$\begin{array}{c} 1453 \\ 1450 \end{array}$	$829843 \\ 828971$	35 34
27	167159	1419	995260	31	171899	$\begin{array}{c} 1430 \\ 1447 \end{array}$	828101	33
$\tilde{2}8$	168008	1413	995241	32	172767	1444	827233	32
29	168856	1410	995222	32	173634	1442	826366	31
30	169702	1407	995203	32	174499	1439	825501	30
31	9.170547	1405	9.995184	32	9.175362	1436	10.824638	29
32	171389	1402	995165	32	176224	1433	823776	28
33 34	$\begin{array}{c} 172230 \\ 173070 \end{array}$	$\begin{array}{c c} 1399 \\ 1396 \end{array}$	995146 995127	$\begin{array}{c c} 32 \\ 32 \end{array}$	$\frac{177084}{177942}$	$\begin{array}{c} 1431 \\ 1428 \end{array}$	822916 822058	27 26
35	173908	1394	995108	32	178799	1425	821201	25
36	174744	1391	995089	32	179655	1423	820345	24
37	175579	1388	995070	32	180508	1420	819492	23
38	176411	1386	995051	32	181360	1417	818640	22
$\begin{vmatrix} 39 \\ 40 \end{vmatrix}$	$\frac{177242}{178072}$	$\begin{array}{c} 1383 \\ 1380 \end{array}$	$   \begin{array}{r}     995032 \\     995013   \end{array} $	32 32	$182211 \\ 183059$	$\begin{array}{c} 1415 \\ 1412 \end{array}$	$817789 \\ 816941$	21 20
$\frac{40}{41}$	$\frac{178072}{9.178900}$	$\frac{1300}{1377}$	$\frac{333013}{9.994993}$	$\frac{32}{32}$	$\frac{183003}{9.183907}$	$\frac{141/3}{1409}$	$\frac{810941}{10.816093}$	$\frac{20}{19}$
42	179726	1374	994974	32	184752	1409	815248	18
43	180551	1372	994955	32	185597	1404	814403	17
44	181374	1369	994935	32	186439	1402	813561	16
45	182196	1366	994916	33	187280	1399	812720	15
$\begin{bmatrix} 46 \\ 47 \end{bmatrix}$	183016 183834	$\begin{array}{c c} 1364 \\ 1361 \end{array}$	$\begin{array}{c} 994896 \\ 994877 \end{array}$	33 33	$\frac{188120}{188958}$	1396	$811880 \\ 811042$	14 13
48	184651	$\frac{1301}{1359}$	994857	33	189794	$1393 \\ 1391$	811042	13
49	185466	1356	994838	33	190629	1389	809371	11
50	186280	1353	994818	33	191462	1386	808538	10
$\overline{51}$	9.187092	1351	$\overline{9.994798}$	33	9.192294	1384	10.807706	9
52	187903	1348	994779	33	193124	1381	806876	8
53 54	188712 $189519$	1346 1343	994759 994739	33	$\begin{array}{c} 193953 \\ 194780 \end{array}$	$1379 \\ 1376$	$806047 \\ 805220$	7 6
55	190325	1341	994719	33	195606	1374	804394	5
56	191130	1338	994700	33	196430	1371	803570	4
57	191933	1336	994680	33	197253	1369	802747	3
58	192734	1333	994660	33	198074	1366	801926	2
59 60	$\begin{array}{c} 193534 \\ 194332 \end{array}$	$\begin{array}{c c} 1330 \\ 1328 \end{array}$	$994640 \\ 994620$	33	198894	1364	$   \begin{array}{r}     801106 \\     800287   \end{array} $	0
		1026		JU	199713	1361		
1	Cosine		Sine		Cotang.		Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D	Cotang.	
0	9.194332	1328	9.994620	33	9.199713		110.800287	60
1	195129 195925	$\begin{array}{c} 1326 \\ 1323 \end{array}$	994600 994580	33	$\begin{vmatrix} 200529 \\ 201345 \end{vmatrix}$	$\begin{array}{c} 1359 \\ 1356 \end{array}$	799471 798655	59 58
2 3	196719	1321	994560	34	202159	1354	797841	57
4	197511	1318	994540	34	202971	1352	797029	56
5	198302	1316 1313	994519 $994499$	34 34	$\begin{vmatrix} 203782 \\ 204592 \end{vmatrix}$	$1349 \\ 1347$	796218	55
6 7	$\begin{array}{c} 199091 \\ 199879 \end{array}$	1313	994479	34	204392	$\begin{array}{c} 1347 \\ 1345 \end{array}$	795408 794600	54 53
8	200666	1308	994459	34	206207	1342	793793	52
9	201451	1306	994438	34	207013	1340	792987	51
$\frac{10}{11}$	$\left  \frac{202234}{9.203017} \right $	$\frac{1304}{1301}$	$\frac{994418}{9.994397}$	$\frac{34}{34}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	1338	792183	$\frac{50}{49}$
$\overline{\frac{11}{12}}$	203797	$\begin{array}{c} 1301 \\ 1299 \end{array}$	994377	$\begin{vmatrix} 34 \\ 34 \end{vmatrix}$	209420	$\begin{array}{c} 1335 \\ 1333 \end{array}$	$\begin{bmatrix} 10.791381 \\ 790580 \end{bmatrix}$	49
13	204577	1296	994357	34	210220	1331	789780	47
14	205354	1294	994336	34	211018	1328	788982	46
15 16	206131 $206906$	$\begin{array}{c} 1292 \\ 1289 \end{array}$	994316 $994295$	34 34	211815 $212611$	$\begin{array}{c} 1326 \\ 1324 \end{array}$	788185 787389	45
17	207679	1287	994274	35	213405	1321	786595	43
18	208452	1285	994254	35	214198	1319	785802	42
$\frac{19}{20}$	209222 $209992$	$\begin{array}{c} 1282 \\ 1280 \end{array}$	$994233 \\ 994212$	35 35	214989 $215780$	$\frac{1317}{1315}$	785011 $784220$	41 40
$\frac{20}{21}$	$\frac{209392}{9.210760}$	$\frac{1260}{1278}$	$\frac{994212}{9.994191}$	$\frac{35}{35}$	$\frac{213160}{9.216568}$	$\frac{1313}{1312}$	$\frac{784220}{10.783432}$	$\frac{1}{39}$
$\frac{21}{22}$	211526	$\begin{array}{c} 1275 \\ 1275 \end{array}$	994171	35	217356	1310	782644	38
23	212291	1273	994150	35	218142	1308	781858	37
24	$213055 \\ 213818$	$\begin{array}{c} 1271 \\ 1268 \end{array}$	994129 $994108$	35 35	$218926 \ 219710$	$\frac{1305}{1303}$	781074 780290	36 35
25 26	214579	$\begin{array}{c} 1203 \\ 1266 \end{array}$	994087	35	$\begin{bmatrix} 219710 \\ 220492 \end{bmatrix}$	1303 $1301$	779508	$\frac{35}{34}$
27	215338	1264	994066	35	221272	1299	778728	33
28	216097	1261	994045	35	222052	1297	777948	$\frac{32}{21}$
29   30	$2168541 \\ 217609$	$\begin{array}{c} 1259 \\ 1257 \end{array}$	994024 $994003$	35 35	222830 $223606$	$\begin{array}{c} 1294 \\ 1292 \end{array}$	$\begin{bmatrix} 777170 \\ 776394 \end{bmatrix}$	31 30
$\frac{30}{31}$	$\frac{218363}{9.218363}$	$\frac{1255}{1255}$	9.993981	$\frac{3}{35}$	$\boxed{\frac{9.224382}{9.224382}}$	$\frac{1290}{1290}$	10.775618	$\frac{1}{29}$
32	219116	1253	993960	35	225156	1288	774844	28
33	219868	1250	993939	35 35	$oxed{225929} \ 226700$	1286	774071	27 26
34 35	$egin{array}{c} 220618 \ 221367 \end{array}$	$\begin{array}{c} 1248 \\ 1246 \end{array}$	993918 993896	36	227471	$\begin{array}{c} 1284 \\ 1281 \end{array}$	773300 772529	25
36	222115	1244	993875	36	228239	1279	771761	24
37	222861	1242	993854	36 36	$oxed{229007}{229773}$	1277	770993	23 22
38 39	$223606 \ 224349$	$1239 \\ 1237$	993832 $993811$	36	230539	$\begin{array}{c} 1275 \\ 1273 \end{array}$	770227 $769461$	21
40	225092	1235	993789	36	231302	1271	768698	20
$\overline{41}$	$\overline{9.225833}$	1233	$\overline{9.993768}$	$\overline{36}$	9.232065	1269	10.767935	19
42	226573	1231	$\begin{array}{c} 993746 \\ 993725 \end{array}$	36 36	232826 $233586$	$\begin{array}{c} 1267 \\ 1265 \end{array}$	767174 766414	18 17
43 44	$egin{array}{c} 227311 \ 228048 \ \end{array}$	$\begin{array}{c} 1228 \\ 1226 \end{array}$	993725	36	234345	$\begin{array}{c} 1265 \\ 1262 \end{array}$	765655	16
45	228784	1224	993681	36	235103	1260	764897	15
46	229518	1222	993660	36	235859	1258	764141	$\begin{array}{c} 14 \\ 13 \end{array}$
47 48	$230252 \\ 230984$	$\begin{array}{c} 1220 \\ 1218 \end{array}$	993638 $993616$	36 36	236614 $237368$	$\begin{array}{c} 1256 \\ 1254 \end{array}$	$763386 \ 762632$	$\frac{13}{12}$
49	231714	1216	993594	37	238120	1252	761880	11
50	232444	1214	993572	$\frac{37}{27}$	$\frac{238872}{}$	1250	761128	$\frac{10}{10}$
51	9.233172	1212	9,993550	$\frac{\overline{37}}{37}$	9.239622 $240371$	$\begin{array}{c} 1248 \\ 1246 \end{array}$	10.760378	9 8
52 53	$233899 \ 234625$	$\begin{bmatrix} 1209 \\ 1207 \end{bmatrix}$	993528 $993506$	37	240371 $241118$	$\begin{array}{c} 1240 \\ 1244 \end{array}$	759629 758882	7
54	235349	1205	993484	37	241865	1242	758135	6
55	236073	1203	993462	37 37	242610 $243354$	1240	757390	5
56 57	236795 $237515$	$1201 \\ 1199$	$993440 \\ 993418$	$\frac{37}{37}$	243334 $244097$	$\begin{array}{c} 1238 \\ 1236 \end{array}$	756646 755903	3
58	238235	1197	993396	37	244839	1234	755161	2
59	238953	1195	993374	37	245579	1232	754421	1 0
60	239670	1193	993351	37	246319	1230	753681	
	Cosine 1		Sine		Cotang.		Tang.	М.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.239670	1193	9.993351	37	9.246319	1230	10.753681	60
1	240386	1191	993329	37	247057	1228	752943	59
2 3	$241101 \\ 241814$	1189 1187	$\begin{array}{c} 993307 \\ 993285 \end{array}$	37 37	$oxed{247794} \ 248530$	$\begin{array}{c} 1226 \\ 1224 \end{array}$	752206 751470	
4	242526	1187	993262	37	249264	1224	750736	57 56
5	243237	1183	993240	37	249998	1220	750002	55
6	243947	1181	993217	38	250730	1218	749270	54
7	244656 $245363$	1179 1177	993195 $993172$	38 38	$251461 \\ 252191$	$\frac{1217}{1215}$	748539 747809	53
8 9	246069	1175	993149	38	252191 252920	1213	747080	52 51
10	246775	1173	993127	38	253648	1211	746352	50
$\overline{11}$	9.247478	1171	9.993104	$\overline{38}$	9.254374	1209	10.745626	$\overline{49}$
12	248181	1169	993081	38	255100	1207	744900	48
13 14	248883 $249583$	$\begin{array}{c} 1167 \\ 1165 \end{array}$	993059 $993036$	38 38	255824 $256547$	$\begin{array}{c} 1205 \\ 1203 \end{array}$	744176 743453	46
15	250282	1163	993013	38	257269	1203	742731	45
16	250980	1161	992990	38	257990	1200	742910	44
17	251677	1159	992967	38	258710	1198	741290	43
18 19	252373 $253067$	$\begin{array}{c c} 1158 \\ 1156 \end{array}$	992944 $992921$	38 38	$259429 \ 260146$	$\begin{array}{c} 1196 \\ 1194 \end{array}$	740571 739854	42 41
$\begin{vmatrix} 19\\20 \end{vmatrix}$	253761	1154	992898	38	260863	$1194 \\ 1192$	739137	40
$\frac{20}{21}$	$\frac{1}{9.254453}$	$\frac{-1152}{1152}$	$\overline{9.992875}$	$\frac{38}{38}$	$\frac{261578}{9.261578}$	1190	10.738422	$\frac{10}{39}$
22	255144	1150	992852	38	262292	1189	737708	38
23	255834	1148	992829	39	263005	1187	736995	37
24 25	$256523 \\ 257211$	$\begin{array}{c c} 1146 \\ 1144 \end{array}$	$\frac{992806}{992783}$	39 39	263717 $264428$	$\begin{array}{c} 1185 \\ 1183 \end{array}$	736283 735572	36 35
26	257898	1142	992759	39	265138	1181	734862	34
27	258583	1141	992736	39	265847	1179	734153	33
28	259268	1139	992713	39	266555	1178	733445	32
29   30	$259951 \ 260633$	1137 1135	$992690 \\ 992666$	39 39	$267261 \ 267967$	1176 1174	732739 732033	$\begin{array}{c} 31 \\ 30 \end{array}$
$\left \frac{30}{31}\right $	$\frac{260033}{9.261314}$	$\frac{1133}{1133}$	$\frac{992600}{9.992643}$	$\frac{39}{39}$	$\frac{207907}{9.268671}$	$\frac{1174}{1172}$	$\frac{732033}{10.731329}$	$\frac{50}{29}$
32	261994	1131	992619	39	269375	1170	730625	28
33	262673	1130	992596	39	270077	1169	729923	27
34 35	263351 $264027$	$\begin{array}{c c} 1128 \\ 1126 \end{array}$	$992572 \\ 992549$	39 39	$270779 \ 271479$	$\begin{array}{c} 1167 \\ 1165 \end{array}$	729221 728521	26 25
36	264703	1124	992525	39	272178	1164	727822	24
37	265377	1122	992501	39	272876	1162	727124	23
38	266051	1120	992478	40	273573	1160	726427	22
39 40	266723 $267395$	$\begin{array}{c c} 1119 \\ 1117 \end{array}$	$992454 \\ 992430$	40	$\frac{274269}{274954}$	$\frac{1158}{1157}$	725731 725036	21 20
$\frac{1}{41}$	$\frac{267937}{9.268065}$	1115	$\frac{9.992406}{9.992406}$	$\frac{40}{40}$	$\frac{274304}{9.275658}$	1155	$\frac{723030}{10.724342}$	$\frac{20}{19}$
42	268734	1113	992382	40	276351	1153	723649	18
43	269402	1111	992359	40	277043	1151	722957	17
44	$\begin{array}{c} 270069 \\ 270735 \end{array}$	1110	992335	40	277734	1150	722266	16
$\begin{array}{c c} 45 \\ 46 \end{array}$	270735 271400	$\frac{1108}{1106}$	992311 $992287$	$\frac{40}{40}$	278424 279113	$\frac{1148}{1147}$	721576 $720887$	15 14
47	272064	1105	992263	40	279801	1145	720199	13
48	272726	1103	992239	40	280488	1143	719512	12
49 50	$\begin{bmatrix} 273388 \\ 274049 \end{bmatrix}$	$\begin{array}{c} 1101 \\ 1099 \end{array}$	$992214 \\ 992190$	$\frac{40}{40}$	281174 281858	1141	718826	11
$\frac{50}{51}$	$\frac{274049}{9.274708}$	$\frac{1099}{1098}$	$\frac{992190}{9.992166}$	$\frac{40}{40}$	$\frac{281838}{9.282542}$	$\frac{1140}{1138}$	$\frac{718142}{10.717458}$	$\frac{10}{9}$
52	275367	1098	9.992160 $992142$	40	$\frac{9.282542}{283225}$	1136	716775	8
53	276024	1094	992117	41	283907	1135	716093	7
54	276681	1092	992093	41	284588	1133	715412	6
55 56	$oxed{277337} 277991$	$\begin{array}{c} 1091 \\ 1089 \end{array}$	$992069 \\ 992044$	41 41	285268 285947	$\begin{array}{c} 1131 \\ 1130 \end{array}$	714732 714053	5 4
57	278644	$\begin{array}{c} 1089 \\ 1087 \end{array}$	992044	41	286624	1128	714035	3
58	279297	1086	991996	41	287301	1126	712699	2
59 60	279948 $280599$	$\begin{array}{c} 1084 \\ 1082 \end{array}$	991971	41	287977	1125	712023	1
00	Cosine	1082	991947	41	288652	1123	711348	0 M
	Cosine		Şine		Cotang.		Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.280599	1082	9.991947		9.288652	1123	10.711348	
1	281248	1081	991922	41	289326	1122	710674	
2 3	$oxed{281897} 282544$	$\begin{array}{c} 1079 \\ 1077 \end{array}$	991897 $991873$	$\begin{array}{c}41\\41\end{array}$	2899999 $290671$	1120 1118	$710001 \\ 709329$	58
4	283190	1076	991848	41	291342	1117	708658	57 56
5	283836	1074	991823	$\frac{1}{41}$	292013	1115	707987	55
6	284480	1072	991799	41	292682	1114	707318	54
7	285124	1071	991774	42	293350	1112	706650	53
8	285766	1069	991749	42	294017	1111	705983	52
9	$286408 \ 287048$	$\begin{array}{c} 1067 \\ 1066 \end{array}$	991724	42	$294684 \ 295349$	$\frac{1109}{1107}$	705316	51
$\frac{10}{11}$			$\frac{991699}{0.001054}$	$\frac{42}{13}$			704651	$\frac{50}{10}$
12	9.287687 $288326$	$\begin{array}{c} 1064 \\ 1063 \end{array}$	9.991674 $991649$	$\begin{vmatrix} 42 \\ 42 \end{vmatrix}$	$9.296013 \\ 296677$	$\begin{array}{c} 1106 \\ 1104 \end{array}$	$10.703987 \\ 703323$	49
13	288964	1061	991624	42	$\frac{290077}{297339}$	1104	703523	48
14	289600	1059	991599	$\frac{12}{42}$	298001	1101	701999	46
15	290236	1058	991574	42	298662	1100	701338	45
16	290870	1056	991549	42	299322	1098	700678	44
17	291504	1054	991524	42	299980	1096	700020	43
18	$292137 \ 292768$	$\frac{1053}{1051}$	991498	42	$300638 \ 301295$	1095	699362	42
19 20	292708	1051 $1050$	991473 991448	$\begin{array}{c c} 42 \\ 42 \end{array}$	301295	$\begin{array}{c} 1093 \\ 1092 \end{array}$	698705 698049	41 40
$\left \frac{20}{21}\right $	$\frac{233333}{9.294029}$	$\frac{1033}{1048}$		$\frac{42}{42}$	$\frac{301301}{9.302607}$	$\frac{10.02}{1090}$	10.697393	$\frac{10}{39}$
$\begin{bmatrix} 21 \\ 22 \end{bmatrix}$	294029	1048	9.991422 $991397$	$\begin{vmatrix} 42 \\ 42 \end{vmatrix}$	303261	1090	696739	38
23	295286	1045	991372	43	303914	1087	696086	37
24	295913	1043	991346	43	304567	1086	695433	36
25	296539	1042	991321	43	305218	1084	694782	35
26	297164	1040	991295	43	305869	1083	694131	34
27	297788 $298412$	1039	991270	43	306519 $307168$	$\begin{array}{c} 1081 \\ 1080 \end{array}$	$\begin{array}{ c c c c c } \hline 693481 \\ \hline 692832 \\ \hline \end{array}$	33
28 2)	293412 299034	$\begin{array}{c} 1037 \\ 1036 \end{array}$	$991244 \\ 991218$	43 43	307815	1078	692832 $692185$	32 31
30	299655	$\begin{array}{c} 1030 \\ 1034 \end{array}$	991193	43	308463	1077	691537	30
$\frac{31}{31}$	9.300276	$\frac{1032}{1032}$	$\frac{9.991167}{9.991167}$	$\frac{1}{43}$	9.309109	1075	10.690891	$\frac{\overline{29}}{29}$
32	300895	1031	991141	43	309754	1074	690246	28
33	301514	1029	991115	43	310398	1073	689602	27
34	302132	1028	991090	43	311042	1071	688958	26
35	302748	1026	991064		311685	1070	688315	
36 37	$303364 \ 303979$	$\begin{array}{c c} 1025 \\ 1023 \end{array}$	991038 $991012$	$\begin{array}{c c} 43 \\ 43 \end{array}$	$312327 \\ 312967$	$\begin{array}{c} 1068 \\ 1067 \end{array}$	$\begin{bmatrix} 687673 \\ 687033 \end{bmatrix}$	24 23
38	304593	1023	990986	43	313608	1065	686392	22
39	305207	1020	990960	43	314247	1064	685753	21
40	305819	1019	990934	44	314885	1062	685115	20
$\overline{41}$	9.306430	1017	9.990908	$\overline{44}$	9.315523	1061	$\overline{10.684477}$	$\overline{19}$
42	307041	1016	990882	44	316159	1060	683841	18
43	307650	1014	990855	44	316795	1058	683205	17
44	$308259 \ 308867$	1013 1011	990829 990803	44	$317430 \\ 318064$	$\begin{array}{c} 1057 \\ 1055 \end{array}$	682570 $681936$	16 15
$\begin{array}{c} 45 \\ 46 \end{array}$	308807	1011	990803	44	318697	$1055 \\ 1054$	681303	14
47	310080	1008	990750	44	319329	1053	680671	13
48	310685	1007	990724	44	319961	1051	680039	12
49	311289	1005	990697	44	320592	1050	679408	11
$\frac{50}{}$	311893	1004	990671	44	321222	1048	678778	$\frac{10}{10}$
51	9.312495	1003	9.990644	44	9.321851	1047	10.678149	9
52	$\frac{313097}{212000}$	1001	990618		322479	$\begin{array}{c} 1045 \\ 1044 \end{array}$	677521 676894	8
53 54	$313698 \ 314297$	$\begin{array}{c} 1000 \\ 998 \end{array}$	990591 $990565$	44 44	$   \begin{array}{r}     323106 \\     323733   \end{array} $	$\begin{array}{c} 1044 \\ 1043 \end{array}$	676267	6
55	$\frac{314297}{314897}$	998	990538	44	324358	1043	675642	5
56	315495	996	990511	45	324983	1040	675017	4
57	316092	994	990485	45	325607	1039	674393	3
58	316689	993	990458	45	326231	1037	673769	2
59	317284	991	990431	45	326853 327475	1036 103 <b>5</b>	$\begin{array}{ c c c c c } & 673147 \\ & 672525 \end{array}$	$\frac{1}{0}$
60	317879	990	990404	45		1099		
	Cosine		Sine	Dog	Cotang.		Tang.	

М.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.317879	990	9.9904041		9.327474	1035		$\overline{\overline{60}}$
1	318473	988	990378	45	328095	1033		59
2	319066	987	990351	45	328715	1032	671285	58
3	319658	986	990324 990297	45 45	$329334 \\ 329953$	1030	670666 670047	57 56
<sup>7</sup> 4 5	$320249 \\ 320840$	$\begin{array}{c} 984 \\ 983 \end{array}$	990297	45	330570	1029	669430	55
6	321430	982	990243	45	331187	1026	668813	54
7	322019	980	990215	45	331803		668197	53
8	322607	979	990188	45	332418	1024	667582	52
9	$323194 \\ 323780$	$\begin{array}{c} 977 \\ 976 \end{array}$	$990161 \\ 990134$	45 45	<b>33</b> 3033 <b>33</b> 3646	$\begin{array}{c c} 1023 \\ 1021 \end{array}$	666967 666354	51 50
$\frac{10}{11}$	$\frac{323780}{9.324366}$	$\frac{-975}{}$	$\frac{330101}{9.990107}$	$\frac{10}{46}$	9.334259		$\overline{10.665741}$	$\frac{30}{49}$
12	324950	973	990079	46	334871	1019	665129	48
13	325534	972	990052	46	335482	1017	664518	47
14	326117	970	990025	46	336093		663907	46
15	326700	$\begin{array}{c} 969 \\ 968 \end{array}$	985997 989970	$\begin{array}{ c c } 46 \\ 46 \end{array}$	$336702 \\ 337311$	1015	663298 662689	45 44
16 17	$327281 \ 327862$	966	989942	46	337919	_	662081	43
18	328442	965	989915	46	338527		661473	42
19	329021	964	989887	46	339133		660867	41
20	329599	962	989860	46	339739	t	660261	40
$ \overline{21} $	9.330176	961	9.989832	46	9.340344	1007	10.659656	39
22	330753 331329	$\begin{array}{c} 960 \\ 958 \end{array}$	989804 $989777$	46 46	$340948 \\ 341552$	1006	659052 658448	38 37
23 24	331903	957	989749	47	342155	1003	657845	36
$\tilde{25}$	332478	956	989721	47	342757	1002	657243	35
26	333051	954	989693	47	343358	1000	656642	34
27	333624	$\begin{array}{c} 953 \\ 952 \end{array}$	$989665 \\ 989637$	47	343958 344558		$\begin{vmatrix} 656042 \\ 655442 \end{vmatrix}$	33 32
28 29	334195 334766	950	989609	47	345157	997	654843	31
$\begin{vmatrix} \tilde{3}0 \\ 3 \end{vmatrix}$	335337	949	989582	47	345755	996	654245	30
$\frac{31}{31}$	9,335906	948	9.989553	47	9.346353	994	10.653647	$\overline{29}$
32	336475	946	989525	47	346949	993	653051	28
33	337043	945	989497	47	347545		652455	27
34 35	337610 338176	$\begin{array}{c} 944 \\ 943 \end{array}$	$989469 \\ 989441$	47	348141 348735	$\begin{array}{c} 991 \\ 990 \end{array}$	651859 651265	26 25
36	338742	941	989413		349329	988	650671	24
37	339306	940	989384	47	349922		650078	23
38	339871	939	989356	47	350514		649486	22
$\begin{array}{c} 39 \\ 40 \end{array}$	$340434 \\ 340996$	$\begin{array}{c} 937 \\ 936 \end{array}$	$989328 \\ 989300$	47	$\frac{351106}{351697}$	$\begin{array}{c} 985 \\ 983 \end{array}$	$\begin{bmatrix} 648894 \\ 648303 \end{bmatrix}$	21 20
$\frac{40}{41}$	$\frac{340550}{9.341558}$	$\frac{350}{935}$	$\frac{9.989271}{9.989271}$	$\frac{1}{47}$	$\frac{0.01037}{9.352287}$	$\frac{-969}{982}$	$\frac{0.0000}{10.647713}$	$\frac{20}{19}$
42	342119	934	989243	47	352876	981	647124	18
43	342679	932	989214	47	353465	980	646535	17
44	343239	931	989186	47	354053		645947	16
45 46	343797 344355	$930 \\ 929$	989157 $989128$	47	$\begin{array}{r} 354640 \\ 355227 \end{array}$	$\begin{array}{c} 977 \\ 976 \end{array}$	645360 644773	15 14
40	344912	$\begin{array}{c c} 929 \\ 927 \end{array}$	989100	48	355813		644187	13
48	345469	926	989071	48	356398	974	$\boxed{ 643602}$	12
49	346024	925	989042	48	356982		643018	11
$\frac{50}{2}$	346579	924	989014		$\frac{357566}{2140}$	1	642434	10
51	9.347134	922	9.988985	48	9.358149		10.641851 641269	9
52 53	$\begin{vmatrix} 347687 \\ 348240 \end{vmatrix}$		$988956 \\ 988927$	48 48	358731 $359313$	969 968	640687	8
54	348792		988898		359893		640107	6
55	349343	917	988869	48	360474	966	639526	5
56	349893		988840	48	361053		638947	4
57 58	350443 350992		988811 988782	49	$ \begin{array}{c c} 361632 \\ 362210 \end{array} $		638368	3 2
59	351540		988753		362787	961	637213	1
60	352088		988724		363364		636636	0
	Cosine		Sine		Cotang.	1	Tang	M.
Paner.						-		

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	1
0	19.352088	911	9.988724	49	9.363364		10.636636	60
1	352635	910	988695	49	363940	959	636060	
2	353181	909	988666	49	364515	958	635485	53
3	353726	908	988636	.49	365090	957	634910	
5	354271 354815	907 905	988607 988578	49 49	$365664 \\ 366237$	$\begin{array}{c} 955 \\ 954 \end{array}$	$\begin{bmatrix} & 634336 \\ & 633763 \end{bmatrix}$	56 55
6	355358	904	988548	49	366810	953	633190	54
7	355901	903	988519	49	367382	352	632618	53
8	356443	902	988489	49	367953	951	632047	52
9	356984	901	988460	49	368524	950	631476	51
$\frac{10}{11}$	357524	899	$\frac{988430}{2000401}$	$\frac{49}{40}$	$\frac{369094}{6.000000}$	$\frac{949}{040}$	630906	$\frac{50}{40}$
11 12	$\begin{vmatrix} 9.358064 \\ 358603 \end{vmatrix}$	898 897	$9.988401 \\ 988371$	49	$9.369663 \\ 370232$	$\begin{array}{c} 948 \\ 946 \end{array}$	$\begin{bmatrix} 10.630337 \\ 629768 \end{bmatrix}$	49 48
13	359141	896	988342	49	370799	$\begin{array}{c} 940 \\ 945 \end{array}$	629201	47
14	359678	895	988312	50	371367	944	628633	
15	360215	893	988282	50	371933	943	628067	45
16	360752	892	988252	50	372499	942	627501	44
17 18	$\begin{vmatrix} 361287 \\ 361822 \end{vmatrix}$	$\begin{bmatrix} 891 \\ 890 \end{bmatrix}$	988223 $988193$	50 50	$373064 \ 373629$	$\begin{array}{c} 941 \\ 940 \end{array}$	$\begin{array}{c c} 626936 \\ 626371 \end{array}$	43 42
19	$\begin{vmatrix} 361622 \\ 362356 \end{vmatrix}$	889	988163	50	374193	939	$\begin{vmatrix} 625807 \\ 625807 \end{vmatrix}$	41
$\frac{10}{20}$	362889	888	988133	50	374756	938	625244	40
$\overline{21}$	9.363422	887	9.988103	50	9.375319	937	$\overline{10.624681}$	$\overline{39}$
22	363954	885	988073	50	375381	935	624119	38
23	364485	884	988043	50	376442	934	623558	37
$\begin{bmatrix} 24 \\ 25 \end{bmatrix}$	$365016 \ 365546$	883 882	$988013 \\ 987983$	50 50	377003	933	$egin{array}{c} 622997 \ 622437 \end{array}$	36
$\frac{25}{26}$	$\frac{355340}{366975}$	881	987953	50	377563 $378122$	$\begin{array}{c} 932 \\ 931 \end{array}$	621878	35 34
$\tilde{27}$	356604	880	987922	50	378681	930	621319	33
28	367131	879	987892	50	379239	929	620761	32
29	367659	877	987862	50	379797	928	620203	31
$\frac{30}{21}$	368185	876	987832	$\frac{51}{2}$	$\frac{380354}{2000000000000000000000000000000000000$	$\frac{927}{2}$	619646	$\frac{30}{20}$
$\begin{vmatrix} \overline{31} \\ 32 \end{vmatrix}$	$\frac{9.368711}{369236}$	875	$9.987801 \\ 987771$	$\overline{51}$	9.380910	$\begin{array}{c} 926 \\ 925 \end{array}$	10.619090	29
33	369761	874 873	987740	51 51	$381466 \\ 382020$	$\begin{array}{c} 925 \\ 924 \end{array}$	$egin{array}{c} 618534 \ 617980 \ \end{array}$	28 27
34	370285		987710	51	382575	923	617425	$\tilde{2}6$
35	370808	871	987679	51	383129	922	616871	25
35	371330	870	987649	51	383682	921	616318	24
37 38	$371852 \\ 372373$	$\begin{array}{c} 869 \\ 867 \end{array}$	987618 $987588$	51 51	$384234 \ 384786$	$\begin{array}{c} 920 \\ 919 \end{array}$	$615766 \ 615214$	23 22
$\begin{vmatrix} 39 \\ 39 \end{vmatrix}$	372894	866	987557	51	385337	918	614663	21
40	373414	865	987526	51	385888	917	614112	20
$\overline{41}$	$\overline{9.373933}$	864	9.987496	$\overline{51}$	9.336433	915	10.613562	$\overline{19}$
42	374452	863	987465	51	386987	914	613013	18
43	374970	862	987434	51	387536	913	612464	17
44 45	$\frac{375487}{376003}$	$\begin{array}{c} 861 \\ 860 \end{array}$	$987403 \\ 987372$	52 52	$388084 \\ 388631$	$\begin{array}{c} 912 \\ 911 \end{array}$	$611916 \\ 611369$	16 15
46	376519	859	987341	52	389178	910	610822	14
47	377035	858	997310	52	.389724	909	610276	13
48	377549	857	987279	52	390270	908	609730	12
49	378063	856	987248	52	390815	907	609185	11
$\frac{50}{51}$	378577	854	$\frac{987217}{2007100}$	$\frac{52}{50}$	$\frac{391360}{0.0000000000000000000000000000000000$	906	608640	$\frac{10}{9}$
51 52	$\frac{9.379089}{379601}$	$\begin{array}{c} 853 \\ 852 \end{array}$	$9.987186 \\ 987155$	52 52	$\begin{vmatrix} 9.391903 \\ 392447 \end{vmatrix}$	$\begin{array}{c} 905 \\ 904 \end{array}$	$\frac{10.608097}{607553}$	9 8
53	380113	851	987133	52	$\frac{392447}{392989}$	903	607933	7
54	380624	850	987092	52	393531	902	606469	6
55	381134	849	987061	52	394073	901	605927	5
56     57	381643	848	987030	52	394614	900	605386	4
58	$382152 \\ 382661$	$\begin{array}{c} 847 \\ 846 \end{array}$	$986998 \\ 986967$	52 52	$395154 \\ 395694$	899 898	$604846 \\ 604306$	$\frac{3}{2}$
59	383168	845	986936	52	396233	897	603767	ĩ
60	383675	844	986904	52	396771	896	603229	0
	Cosine	1	Sine		Cotang.		Tang.	M.
					7		1	

M.	Sina	1	1 Casino	1 D	l m	1 -		
-		D.	Cosine	D.		D.	Cotang.	
$0 \\ 1$			9.986904 $986873$		$\begin{vmatrix} 9.396771 \\ 397309 \end{vmatrix}$	00	10.603229	
2	384687		986841		397846	896	602691	
3	385192		986809		398383	894	601617	
4		840	986778	53	398919	893	601081	56
5 6		839	986746		399455	892	600545	
7		838 837	986714 986683	53	399990 400524	891	600010	
8		836	986651	53	401058	890 889	599476 598942	
9	388210	835	986619		401591	888	598409	
10	l ———	834	986587	53	402124	887	597876	
11	9.389211	833	9.986555		9.402656	886	10.597344	$\overline{49}$
12 13	389711	832	986523		403187	885	596813	48
14		831 830	986491 986459	53 53	$\begin{array}{c c} 403718 \\ 404249 \end{array}$	884	596282	
15	391206	828	986427	53	404778	883 882	595751 595222	
16	391703	827	986395	53	405308	881	594692	
17	392199	826	986363	54	405836	880	594164	
18	392695	825	986331	54	406364	879	593636	42
$\begin{array}{c} 19 \\ 20 \end{array}$	393191 393685	$\begin{array}{c} 824 \\ 823 \end{array}$	986299 986266	54	406892	878	593108	
$\frac{20}{21}$	$\frac{333033}{9.394179}$	$\frac{822}{822}$	$\frac{980200}{9.986234}$	$\frac{54}{54}$	$\frac{407419}{0.407045}$	877	$\frac{592581}{100000000000000000000000000000000000$	$\frac{40}{20}$
22	394673	821	986202	54 54	$9.407945 \\ 408471$	876	10.592055	
23	395166	820	986169	54	408471	875 874	591529 $591003$	
21	395658	819	986137	54	409521	874	590479	
25	396150	818	.986104	54	410045	873	589955	
26 27	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	817	986072	54	410569	872	589431	34
23	397621	816	986039 $986007$	54 $54$	$411092 \\ 411615$	871	588908	
29	398111	815	935974	54	412137	$\begin{array}{c} 870 \\ 869 \end{array}$	588385 587863	
30	398600	814	985942	54	412658	868	587342	30
31	9.399088	813	9.985909	$\overline{55}$	$\overline{9.413179}$	867	$\overline{10.586821}$	$\left  \frac{30}{29} \right $
32	399575	812	985876	55	413699	866	586301	28
33 34	$\begin{array}{ c c c c }\hline 400062 \\ 400549 \\ \hline \end{array}$	811	985843	55	414219	865	585781	27
35	401035	$\begin{array}{c} 810 \\ 809 \end{array}$	985811 $985778$	55 55	$\frac{414738}{415257}$	864	585262	26
36	401520	808	985745	55	415775	$\begin{array}{c} 864 \\ 863 \end{array}$	584743 584225	25 24
37	402005	807	985712	55	416293	862	583707	
38	402489	806	985679	55	416810	861	583190	22
33 40	$\begin{array}{c c} 402972 \\ 403455 \end{array}$	805	985646	55	417326	860	582674	21
$\frac{40}{41}$		804	$\frac{985613}{0.005500}$	$\frac{55}{55}$	417842	859	582158	20
42	$\begin{vmatrix} 9.403938 \\ 404420 \end{vmatrix}$	$\begin{array}{c} 803 \\ 802 \end{array}$	9.985580	55	9.418358	858	10.581642	19
43	404901	801	985547 $985514$	55	$\frac{418873}{419387}$	857 856	581127	18
44	405382	800	985480	55	419301	855	580613 580 <b>09</b> 9	17 16
4.5	405862	799	985447	55	420415	855	579585	15
46 47	406341	798	985414	56	420927	854	579073	14
48	$\frac{406820}{407299}$	797 796	$985380 \\ 985347$	56	421440	853	578560	13
49	407777	790 795	985347 $985314$	56 56	$\begin{array}{c} 421952 \\ 422463 \end{array}$	852 851	578048	12
50	408254	794	985280	56	422974	850	577537 577026	11 10
51	9.408731	794	9.985247	$\frac{\overline{56}}{}$	$\frac{1223484}{9.423484}$	849	$\frac{577626}{10.576516}$	
52	409207	793	985213	56	423993	848	576007	9 8
53 54	409682	792	985180	56	424503	848	575497	7
55	$\frac{410157}{410632}$	$\begin{bmatrix} 791 \\ 790 \end{bmatrix}$	985146	56	425011	847	574989	6
56	411106	789	985113 985079	56 56	$\begin{array}{c} 425519 \\ 426027 \end{array}$	846 845	574481	5
57	411579	788	985045	56	$\frac{426027}{426534}$	845	573973 573466	4
58	412052	787	985011	56	427041	843	572959	$\frac{3}{2}$
59   60	412524	786	984978	56	427547	843	572453	ĩ
001		785		56	428052	842	571948	Õ
	Cosine	10	Sine	1	Colang.	1	Tang	M.
					The state of the last of the l	-		

75 Degrees.

		SINES F	IND IANG		(10	Degree		၁၁
M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.412996		9.984944		9.428052	842	10.571948	60
1	413467		984910	57	428557	841	571443	59
2	413938		984876	57	429062	840	570938	58
3	414408		984842	57	429566	839	570434	57
4 5	$\begin{vmatrix} 414878 \\ 415347 \end{vmatrix}$		984808 984774	57 57	$\begin{array}{ c c c c }\hline & 430070 \\ & 430573 \\ \hline \end{array}$	838 838	569930 569427	56 55
6	415815		984740	57	430373	837	568925	54
7	$\frac{416013}{416283}$		984706	57	431577	836	568423	53
8	416751		984672	57	432079	835	567921	52
9	417217		984637	57	432580	834	567420	51
10	417684	776	984603	57	433080	833	566920	50
11	9.418150	775	9.984569	$\overline{57}$	9.433580	832	10.566420	49
12	418615		984535	57	434080	832	565920	48
13	419079		984500	57	434579	831	565421	47
14	419544		984466	57	435078	830	564922	46
15	$\begin{array}{c c} 420007 \\ 420470 \end{array}$		984432	58	435576	829	564424	45 44
16 17	$420470 \\ 420933$		984397 984363	58 58	$436073 \\ 436570$	828 828	563927 563430	43
18	421395		984328	58 ·	437067	827	562933	42
19	$\frac{121857}{421857}$		984294	58	437563	826	562437	41
20	422318		984259	58	438059	825	561941	40
$\overline{21}$	9422778	$\frac{767}{}$	9.984224	$\frac{50}{58}$	9.438554	824	$\overline{10.561446}$	39
22	423238	766	984190	58	439048	823	560952	38
23	423697	765	984155	58	439543	823	560457	37
24	424156	764	984120	58	440036	822	559964	36
25	424615	763	984085	58	440529	821	559471	35
26	425073		984050	58	441022	820	558978	34
27 28	$\begin{array}{r} 425530 \\ 425987 \end{array}$		984015	58	$441514 \\ 442006$	819	558486 557994	33 32
29	425987 $426443$		$\begin{array}{c} 983981 \\ 983946 \end{array}$	58 58	$\frac{442000}{442497}$	819 818	557503	31
$\begin{bmatrix} 29 \\ 30 \end{bmatrix}$	426899	759	983911	58	442988	817	557012	30
$\frac{30}{31}$	$\frac{120000}{9.427354}$	758	$\frac{0.983875}{9.983875}$	$\frac{58}{58}$	$\frac{112000}{9.443479}$	$\frac{-317}{816}$	$\frac{556521}{10.556521}$	$\frac{30}{29}$
32	427809		983840	59	443968	816	556032	28
33	428263		983805	59	444458	815	555542	27
34	428717		983770	59	444947	814	555053	26
35	429170	754	983735		445435	813	554565	25
36	429623	753	983700	59	445923	812	554077	24
37	430075	752	983664	59	446411	812	553589	23
$\begin{array}{c} 38 \\ 39 \end{array}$	$430527 \\ 430978$	752 751	$\begin{array}{c} 983629 \\ 983594 \end{array}$	59 59	$446898 \\ 447384$	811 810	553102 552616	22 21
40	431429	750	983558	59	447870	809	552130	20
$\frac{40}{41}$	$\frac{431423}{9.431879}$	$-\frac{730}{749}$	$\frac{363536}{9.983523}$	$\frac{59}{59}$	$\frac{447876}{9.448356}$		$\frac{552130}{10.551644}$	$\frac{20}{19}$
$\frac{41}{42}$	432329	749	983487	59 59	$\frac{9.448330}{448841}$	$\begin{array}{c} 809 \\ 808 \end{array}$	551159	18
43	432778	748	983452	59	449326	807	550674	17
44	433226	747	983416	59	449810	806	550190	16
45	433675	746	983381	59	450294	806	549706	15
46	434122	745	983345	59	450777	805	549223	14
47	434569	744	983309	59	451260	804	548740	13
48	435016	744	$983273 \ 983238$	60 60	451743	803	548257 547775	12
49 50	$\begin{array}{r} 435462 \\ 435908 \end{array}$	$\begin{array}{c c} 743 \\ 742 \end{array}$	983202	60	452225 $452706$	$\begin{array}{c} 802 \\ 802 \end{array}$	547775	$\begin{array}{c c} 11 \\ 10 \end{array}$
$\frac{50}{51}$	$\frac{43.5308}{9.436353}$	$\frac{742}{741}$	$\frac{363262}{9.983166}$	$\frac{60}{60}$	$\frac{4.2100}{9.453187}$	$\frac{802}{801}$	$\frac{547234}{10.546813}$	$\frac{10}{9}$
$\begin{vmatrix} 51 \\ 52 \end{vmatrix}$	436798	741	983130	60	453668	800	546332	8
$\begin{bmatrix} 5\tilde{3} \\ 5\tilde{3} \end{bmatrix}$	437242	740	983094	60	454148	799	545852	7
54	437686	739	983058	60	454628	799	545372	6
55	438129	738	983022	60	455107	798	544893	5
56	438572	737	982986	60	455586	797	514414	4.
57 58	439014	736	982950	60 60	456064	796	543936	$\begin{vmatrix} 3 \\ 2 \end{vmatrix}$
58 59	$439456 \\ 439897$	736 735	$982914 \\ 982878$	60	$456542 \\ 457019$	796 795	543458 542981	1
60	440338	734	982842	60	457496	795 794	542504	0
	Cosine		Sine		Cotang.		Tang.	M.
			Direc		ontains.		Tung.	

M	. Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.440338	734	19.982842		19.457496	<u> </u>	10.542504	160
1	440778	733	982805	60	457973		542027	59
2			982769		458449	793	541551	58
3			982733		458925	792	541075	57
4			982696		459400	791	540600	56
5			982660		459875	790	540125	55
6 7	$442973 \\ 443410$	729	982624 982587		460349	790	539651	54
8		727	982551		460323 461297	789 788	539177	53
$\tilde{9}$	444284		982514		461770	788	538703 538230	52
10		726	982477		462242	787	537758	50
$\overline{11}$	9.445155	725	9.982441	$\overline{61}$	$\overline{9.462714}$	786	10.537286	$\frac{3}{49}$
12		724	982404		463186	785	536814	48
13		723	982367	61	463658	785	536342	47
14	446459	723	982331		464129	784	535871	46
15	446893	722	982294		464599	783	535401	45
16 17	447326	721	982257		465069	783	534931	44
18	447759 448191	720	982220	62	465539	782	534461	43
19	448623	$720 \\ 719$	982183 982146	62	466008 466476	781	533992	42
20	449054	718	982109	62	466945	780 780	533524	41
$\frac{21}{21}$	$\frac{110001}{9.449485}$	$\frac{713}{717}$	$\frac{9.982072}{9.982072}$	$\frac{62}{62}$	$\frac{400943}{9.467413}$		533055	$\frac{40}{20}$
22	449915	716	982035	62	467880	779 778	10.532587 532120	39   38
23	450345	716	981998	62	468347	778	531653	37
24	450775	715	981961	62	468814	777	531186	36
25	451204	714	981924	62	469280	776	530720	35
26	451632	713	981886	62	469746	775	530254	34
27	452060	713	981849	62	470211	775	529789	33
28 29	452488 452915	712	981812	62	470676	774	529324	32
30	453342	$\frac{711}{710}$	$981774 \\ 981737$	62 62	471141 471605	773	528859	31
$\frac{31}{31}$	$9.\overline{453768}$	$\frac{710}{710}$	$\frac{331737}{9.981699}$	$\frac{62}{63}$	$\frac{471003}{9.472068}$	773	528395	$\frac{30}{20}$
32	454194	709	981662	63	472532	772 771	$10.527932 \\ 527468$	29 28
33	454619	708	981625	63	472995	771	527005	27
34	455044	707	981587	63	473457	770	526543	$\tilde{2}6$
35	455469	707	981549		473919	769	526081	25
36 37	$\begin{vmatrix} 455893 \\ 456316 \end{vmatrix}$	706 705	981512	63	474381	769	525619	24
38	456739	703	$981474 \\ 981436$	63 63	$\frac{474842}{475303}$	768	525158	23
39	457162	704	981399	63	475763	$\begin{array}{c} 767 \\ 767 \end{array}$	$524697 \\ 524237$	22 21
40	457584	703	981361	63	476223	766	523777	20
$\overline{41}$	9.458006	702	$\overline{9.981323}$	$\overline{63}$	$\overline{9.476683}$	765	$\frac{523117}{10.523317}$	$\frac{20}{19}$
42	458427	701	981285	63	477142	765	522858	18
43	458848	701	981247	63	477601	764	522399	17
44	459268	700	981209	63	478059	763	521941	16
45	459688	699	981171	63	478517	763	521483	15
46 47	$460108 \ 460527$	$\begin{array}{c c} 698 \\ 698 \end{array}$	981133	64	478975	762	521025	14
48	460946	697	$981095 \\ 981057$	$\begin{vmatrix} 64 \\ 64 \end{vmatrix}$	$\frac{479432}{479889}$	761	520568	13
49	461364	696	981019	64	480345	761 760	$520111 \mid 519655 \mid$	12
50	461782	695	980981	64	480801	759	519199	11 10
$\overline{51}$	9.462199	695	9.980942	$\frac{64}{64}$	$\frac{100001}{9.481257}$	759	$\frac{513133}{10.518743}$	$\frac{10}{9}$
52	462616	694	980904	64	481712	758	518288	8
53	463032	693	980866	64	482167	757	517833	7
54	463448	693	980827	64	482621	757	517379	6
55 56	463864	692	980789	64	483075	756	516925	5
57	464279 464694	691 690	$   \begin{array}{c c}     980750 \\     980712   \end{array} $	64	483529	755	516471	4
58	465108	690	980673	64   64	483982 484435	755	516018	3
59	465522	689	980635	64	484887	754 753	515565 515113	2
60	465935	688		64	485339	753	514661	0
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-				-	0		Tung.	

1		Cotang.	D.	1 Tang	In				
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4					65	980480			$\tilde{3}$
6         468407         684         980325         65         488492         748         511508         5           8         469227         683         980286         65         488491         747         511059         5           10         470046         681         980247         65         489390         747         510610         5           11         9.470455         680         980130         65         490733         745         500207         4           12         470863         680         980130         65         490733         745         509207         4           13         471271         679         980091         65         491180         744         508373         4           16         472492         677         979973         65         492519         743         507927         4           16         472492         677         979934         66         492965         742         507035         4           18         47310         675         979855         66         493854         740         506148         4           20         474115         674         979766									4
T									
8         469637         682         980286         65         488941         747         511059         5           10         470046         681         980208         65         488938         746         510162         5           11         9.470455         680         9.80169         65         498933         746         10.509714         4           12         -470863         680         980130         65         490733         745         509267         4           14         471679         678         980012         65         491627         744         508823         4           15         472086         678         980012         65         492073         743         507927         4           16         472492         677         979973         65         492073         743         507925         4           17         472898         676         979855         66         493410         741         506590         4           18         473304         675         979855         66         493410         741         506540         1         506144         1         1         507035         4									
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12	- 1	510162	746	489838	65	980208	681	470046	
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$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		501278	734	498722		979420	667 -	478142	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				9.499163	$\overline{66}$	9.979380			$\overline{31}$
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$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	3 16	495146	725	504854			658	483712	
$egin{bmatrix} 47 & 484895 & 656 & 978736 & 67 & 506159 & 724 & 493841 & 1 \ 48 & 485289 & 655 & 978696 & 68 & 506593 & 723 & 493407 & 1 \end{bmatrix}$	1   15		725	505289	67	978817	657		45
48   485289   655   978696   68   506593   723   493407   1									
				506502					
		492973	722	507027	68	978655	655	485682	49
$oxed{50}$   $486075$   $654$   $978615$   $68$   $507460$   $722$   $492540$   $1$	10								
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\bar{7} \mid \overline{9}$	10.492107	$\overline{721}$	9.507893					
52   486860   653   978533   68   508326   721   491674	1 8	491674	721	508326	68	978533	653	486860	52
53 487251 652 978493 68 508759 720 491241	1 7								
$egin{bmatrix} 54 & 487643 & 651 & 978452 & 68 & 509191 & 719 & 490809 \ 55 & 488034 & 651 & 978411 & 68 & 509622 & 719 & 490378 \ \end{bmatrix}$									
57   488814   650   978329   68   510485   718   489515	5   3								
1.58   489204   649   978288   68   510916   717   489084	1 2	489084	717	510916	68	978288	649	489204	.58
			716		68		648		00
Cosine   Sine   Cotang.   Tang.   M	M.	Tang.		Cotang.		Sine		Cosine	

	(10 Degrees.) A TABLE OF LOGARITHMIC								
M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.		
0	9.489982		9.978206		9.511776	716	10.488224	60	
1	490371	648	978165	68	512206	716	487794	59	
$\frac{2}{3}$	490759 491147	647	978124	68	512635	715	487365	58	
4	491535	646 646	$978083 \ 978042$	69 69	513064	714	486936	57	
5	491922	645	978001	69	$513493 \\ 513921$	714	486507	56	
6	492308	644	977959	69	513921 $514349$	713 713	$486079 \\ 485651$	55	
7	492695	644	977918	69	514777	713	$\frac{485031}{485223}$	54 53	
8	493081	643	977877	69	515204	712	484796	52	
9	493466	642	977835	69	515631	711	484369	51	
10	493851	642	977794	69	516057	710	483943	50	
11	9.494236	641	9.977752	$\overline{69}$	9.516484	710	10.483516	$\overline{49}$	
12	494621	641	977711	69	516910	709	483090	48	
13	495005	640	977669	69	517335	709	482665	47	
14 15	495388	639	977628	69	517761	708	482239	46	
16	495772 496154	639	977586	69	518185	708	481815	45	
17	496537	$\begin{array}{c} 638 \\ 637 \end{array}$	$977544 \ 977503$	70 70	518610 $519034$	707	481390	44	
18	496919	637	977461	70	$519034 \\ 519458$	706 706	$480966 \\ 480542$	43	
19	497301	636	977419	70	519458 $519882$	706	480118	42 $41$	
20	497682	636	977377	70	520305	705	479695	40	
$\overline{21}$	9.498064	635	9.977335	$\frac{70}{70}$	$\frac{520728}{9.520728}$	704	$\frac{173033}{10.479272}$	$\frac{1}{39}$	
22	498444	634	977293	70	521151	704	478849	38	
23	498825	634	977251	70	521573	703	478427	37	
24	499204	633	977209	70	521995	703	478005	36	
25	499584	632	977167	70	522417	702	477583	35	
26 27	499963	632	977125	70	522838	702	477162	34	
28	$500342 \\ 500721$	$\begin{array}{c} 631 \\ 631 \end{array}$	$977083 \ 977041$	70	523259	701	476741	33	
29	501099	630	976999	70 70	$523680 \ 524100$	701	476320	32	
30	501476	629	976957	70	524100 $524520$	700 699	$475900 \\ 475480$	$\begin{vmatrix} 31 \\ 30 \end{vmatrix}$	
$\overline{31}$	$\frac{1}{9.501854}$	629	$\frac{9.976914}{9.976914}$	$\frac{10}{70}$	$\frac{524920}{9.524939}$		$\frac{475480}{10.475061}$		
32	502231	$\begin{array}{c} 623 \\ 628 \end{array}$	976872	71	525359	$\begin{array}{c} 699 \\ 698 \end{array}$	474641	29 28	
33	502607	628	976830	$7\overline{1}$	525778	698	474222	27	
34	502984	627	976787	71	526197	697	473803	$\tilde{2}6$	
35	503360	626	976745	71	526615	697	473385	25	
36	503735	626	976702	71	527033	696	472967	24	
37 38	$504110 \ 504485$	625	976660	71	527451	696	472549	23	
39	504460	$\begin{array}{c} 625 \\ 624 \end{array}$	976617 $976574$	71 71	527868	695	472132	22	
40	505234	$\begin{array}{c c} 624 \\ 623 \end{array}$	976532	$71 \mid$	$528285 \ 528702$	$\begin{array}{c} 695 \\ 694 \end{array}$	$471715 \\ 471298$	21	
$\frac{1}{41}$	$\frac{505201}{9.505608}$	$\frac{623}{623}$	$\frac{376332}{9.976489}$	$\frac{1}{71}$	$\frac{328702}{9.529119}$			$\frac{20}{10}$	
42	505981	623	9.976446	$\begin{vmatrix} 71 \\ 71 \end{vmatrix}$	529119 $529535$	693 693	$0.470881 \\ 470465$	19	
43	506354	622	976404	71	529950	693	470465	18 17	
44	506727	621	976361	$7\overline{1}$	530366	692	469634	16	
45	507099	620	976318	71	530781	691	469219	15	
46	507471	620	976275	71	531196	691	468804	14	
47	507843	619	976232	72	531611	690	468389	13	
48 49	508214 508585	$\begin{array}{c} 619 \\ 618 \end{array}$	$976189 \\ 976146$	72	532025	690	467975	12	
50	508956	618	976146	$\begin{bmatrix} 72 \\ 72 \end{bmatrix}$	532439 532853	689	467561	11	
$\frac{50}{51}$	$\frac{500330}{9.509326}$	$\frac{617}{617}$	$\frac{976103}{9.976060}$	$\frac{72}{72}$		689	467147	$\frac{10}{10}$	
$\frac{51}{52}$	509696	616	9.976060	$\begin{vmatrix} 72 \\ 72 \end{vmatrix}$	$9.533266 \\ 533679$	688	10.466734	9	
53	510065	616	975974	$7\frac{2}{7}$	534092	$\begin{array}{c} 688 \\ 687 \end{array}$	$466321 \\ 465908$	8 7	
54	510434	615	975930	$7\tilde{2}$	534504	687	465496	6	
55	510803	615	975887	72	534916	686	465084	5	
56	511172	614	975844	72	535328	686	464672	4	
57 58	$511540 \ 511907$	613	975800	72	535739	685	464261	3	
59	512275	$\begin{array}{c c} 613 \\ 612 \end{array}$	975757 975714	$\begin{bmatrix} 72 \\ 72 \end{bmatrix}$	536150	685	463850	2	
60	512642	$612 \mid$	975670	72	$536561 \ 536972$	684 684	463439 $463028$	0	
	Cosine	1	Sine	1		704			
	30.110		pine		Cotang.		Tang.	M.	

M.   Sine   D.   Cosine   D.   Tang.   D.   Cotang.	-							,	
1         513009         611         975627         73         537382         688         462618         59           2         513757         610         975496         73         538202         682         461799         57           5         514472         609         975496         73         538202         681         460898         55           6         514837         608         975408         73         539429         681         460671         54           7         515202         608         975365         73         539937         680         460163         53           8         515566         607         975277         73         540245         680         459755         52           9         515900         607         975189         73         541061         679         459347         51           10         51657         605         9776189         73         541065         678         458939         50           11         91.516657         605         9776189         73         541065         678         458947         541065           12         517020         605         9776	M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
2         513375         611         975583         73         537792         688         462208         58           4         514107         609         975496         73         538611         682         461389         56           5         514472         609         975498         73         539020         681         460980         56           6         514827         608         975408         73         539429         681         460980         56           7         515202         608         9755277         73         540653         69         46975255         52           9         515930         607         975277         73         540653         679         458937         51           10         516294         606         975237         73         541665         679         458939         50           11         9.516657         605         9.976189         73         541876         678         458125         48           12         517020         605         9975145         73         541876         678         458125         48           12         51746         604         97511									
3         513741         610         975639         73         538202         682         461398         56           5         514472         609         975452         73         539020         681         460980         55           6         514837         608         975408         73         539429         681         460980         55           7         515202         608         975385         73         539429         681         460671         53           9         515930         607         975237         73         5404653         679         459347         51           10         516294         696         975233         73         541061         679         459347         51           12         517020         605         975145         73         541675         678         458122         48           13         517382         604         975013         73         542281         677         457312         46           15         518107         603         974925         74         543499         676         455690         42           15         51910         601         974880 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>									
4         514107         609         975496         73         538611         682         461389         56           5         514827         608         975408         73         539429         681         460571         54           7         515202         608         975365         73         539429         681         460571         54           9         515900         607         975277         73         540653         679         459347         51           10         516294         606         975237         73         540653         679         459347         51           11         9.516590         605         9.976189         73         9.541468         678         10.458532         49           11         9.516657         605         9.976189         73         9.541468         678         10.458532         49           12         517326         604         975057         73         542688         677         45712         47           14         51746         603         974969         74         54399         676         456690         43           15         518107         603	3								
5         514472         609         975462         73         539020         681         460957         55           7         515202         608         975365         73         539337         680         460163         53           8         515566         607         975277         73         540245         680         469765         52           10         516294         696         975233         73         541061         679         458934         51           11         9.516657         605         9.975189         73         9.541468         678         10.458532         49           12         517020         605         975145         73         541667         678         468125         48           13         517382         604         975013         73         542881         677         457312         46           15         518107         603         974990         74         543499         676         456906         45           16         518468         603         974997         543499         676         456904         44           18         519191         601         974836									
7         515202         608         975331         73         540245         680         459755         52           9         515930         607         975321         73         540653         679         459347         51           10         516294         696         975233         73         541061         679         468939         50           11         9.516657         605         9.975185         73         9.541468         678         10.488532         49           12         517020         605         975145         73         541875         678         10.488532         48           13         517382         604         975013         73         542881         677         467712         46           15         518107         603         974909         74         543499         676         456906         45           16         518468         603         974999         74         543490         676         456904         44           18         519910         601         974836         74         544310         675         456690         454476           20         519911         600	5	514472			73		681	460980	
8         515566         607         975321         73         540645         680         459755         52           10         516294         696         975233         73         540613         679         459347         51           11         9.516657         605         9.975185         73         541661         679         458939         51           12         517020         605         9.975185         73         541675         678         458125         48           13         517382         604         975101         73         54288         677         457719         47           14         517745         604         975013         73         54288         677         457312         46           15         518107         603         9759013         73         54288         677         457312         46           15         518107         603         974980         74         543499         676         456590         42           18         519190         601         974880         74         544310         675         455290         456905         43           19         520631 <th< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<>									
9         515930         607         975277         73         540653         679         459393         50           11         9.516657         605         9.975189         73         9.541468         678         10.458532         9           12         517020         605         9.975145         73         541875         678         458125         48           13         517382         604         975101         73         542818         677         457719         47           14         517745         604         975007         73         54288         677         457712         47           15         518107         603         974996         74         543499         676         456906         45           15         519190         601         974880         74         544310         675         456690         42           20         519911         600         974742         74         545119         674         458281         40           21         9.520271         600         9.74748         74         9.45524         673         10.454476         39           22         526631         599						539837			
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13		9.516657	605	9.975189	1	9.541468	678		
14	12	517020			73		678	458125	48
15	_								
16         518468         603         974925         74         543499         676         456501         44           17         518829         602         974925         74         543905         675         456095         42           18         519190         601         974880         74         544105         674         455285         41           20         519911         600         974792         74         545119         674         455285         41           21         9.520271         600         9.74793         74         54519         673         10.454476         39           22         520631         599         974659         74         546318         672         453669         32           24         521349         598         974670         74         546735         672         453669         36           25         521707         598         974570         74         547343         671         452362         35           26         522781         596         974481         74         547343         671         452460         34           27         522781         596									
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20         519911         600         974792         74         545119         674         454881         40           21         9.520631         599         9.74793         74         545524         673         10.454476         38           22         520631         599         974659         74         545928         673         454072         38           24         521349         598         974614         74         546735         672         453669         37           26         522066         597         974525         74         547743         671         452862         36           27         522424         596         974481         74         547343         670         452057         33           28         522781         596         974367         74         548345         670         451653         31           30         523495         595         974371         75         549149         669         450851         30           31         9.523852         594         974257         75         54950         668         10.450450         29           32         52408         594									
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23         520990         599         974659         74         546331         672         453669         37           24         521349         598         974670         74         547138         671         452862         36           26         522066         597         974525         74         547340         671         452460         34           27         522424         596         974436         74         548745         670         451655         32           28         522781         596         974436         74         548745         670         451655         32           29         523138         595         974347         75         549149         669         450851         30           31         9.523552         594         9.74257         75         549149         669         450851         30           32         524208         594         9.74257         75         549551         668         450049         28           33         424564         593         974167         75         550752         667         449648         27           34         524920         593         9									
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28         522781         596         9744361         74         548345         670         451655         32           30         523495         595         974347         75         549149         669         450851         30           31         9.523852         594         9.974302         75         549150         668         10.450450         29           32         524208         594         9.74257         75         549550         668         10.450450         29           33         434564         593         974121         75         550352         667         449648         27           34         524920         593         974167         75         550352         667         449648         25           35         525630         591         974077         75         551552         666         448848         25           36         525630         591         974032         75         551952         665         448048         23           37         525984         591         974032         75         551952         665         447649         22           40         527046         589									
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$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$									
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\overline{31}$	9.523852	594	$\overline{9.974302}$	$\overline{75}$	9.549550	668	$\overline{10.450450}$	$\overline{29}$
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$									
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$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		525984	591	974032	75	551952	665	448048	23
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$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	44	528458	587	973716	76	554741	662		16
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$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$									4
$egin{array}{ c c c c c c c c c c c c c c c c c c c$	57	533009	580	973124	76	559885	656	440115	3
60   534052   578   972986   77   561066   655   438934   0									
50   551650   516   512660   11   561660   566									
Cosine   Sine   Cotang.   Tang.   M.	=		1 578		, , , ,	,	1 000		
	_	Cosine	1	Sine		Cotang.		Tang.	MI.

38	(~	Degre	ees.) A	TAD				n one of
M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.5340521	578	9.972986	77	9.561066	655	10.438934	60
1	534399	577	972940	77	561459	654	438541 $438149$	59 58
2	534745	577	972894	77	561851	654	437756	57
3	535092	577	$972848 \\ 972802$	77	562244 562636	653 653	437364	56
4	535438 535783	576 576	972755	77	563028	653	436972	55
5 6	536129	575	972709	77	563419	652	436581	54
7	536474	574	972663	77	563811	652	436189	53
8	536818	574	972617	77	564202	651	435798	52
9	537163	573	972570	77	564592	651	435408	51 50
10	537507	573	972524	77	564983	650	435017	
11	9.537851	572	9.972478	77	9.565373	650	10.434627	49 48
12	538194	572	972431	78	565763	649	$\frac{434237}{433847}$	47
13	538538	571	972385	78	566153 $566542$	$\begin{array}{c c} 649 \\ 649 \end{array}$	433458	46
14	538880	571	$972338 \\ 972291$	78 78	$\begin{array}{c} 566932 \\ \hline \end{array}$	648	433068	45
15 16	539223 539565	570 570	972245	78	567320	648	432680	44
17	539907	569	972198	78	567709	647	432291	43
18	540249	569	972151	78	568098	647	431902	42
19	540590	568	972105	79	568486	646	431514	41
20	540931	568	972058	78	568873	646	431127	$\frac{40}{20}$
$\overline{21}$	9.541272	567	9.972011	78	9.569261	645	10.430739	39
22	541613	567	971964	78	569648	645	430352	38 37
23	541953	566	971917	78	570035	645	$\frac{429965}{429578}$	36
24	542293	566	971870	78	570422 570809	$\begin{array}{c} 644 \\ 644 \end{array}$	429191	35
25	542632	565	971823 $971776$	78 78	571195	643	428805	34
26 27	542971 543310	565 564	971729	79	571581	643	428419	33
$\tilde{2}8$	543649	564	971682	79	571967	642	428033	32
29	543987	563	971635	79	572352	642	427648	31
30	544325	563	971588	79	572738	642	427262	30
$\overline{31}$	9.544663	562	9.971540	79	9.573123	641	10.426877	29
32	545000	562	971493	79	573507	641	426493	28
33	545338	561	971446	79	573892	640	426108	27   26
34	545674	561	971398	79	574276	640	425724 425340	25
35	546011	560	$\begin{array}{c c} 971351 \\ 971303 \end{array}$	79	574660 575044	$\begin{array}{c} 639 \\ 639 \end{array}$	424956	24
36 37	546347 546683	560 559	971256		575427	639	424573	23
38	547019	559	971208		575810	638	424190	22
39	547354	558	971161	79	576193	638	423807	21
40	547689	558	971113	79	576576	637	423424	20
$\overline{41}$	9.548024	557	9.971066	80	9.576958	637	10.423041	19
42	548359	557	971018		577341	636	422659	18
43	548693	556	970970		577723		422277	16
44	549027	556	970922		578104		$\begin{array}{ c c c c c }\hline & 421896 \\ & 421514 \\ \hline \end{array}$	15
45	549360	555	970874		578486		421133	14
46	549693	555 554	970827 970779		579248		420752	13
47 48	550026 550359	554	970731		579629		420371	12
49	550692		970683		580009	634	419991	11
50	551024	553	970635		580389		419611	10
51	9.551356	552	9.970586	80	9.580769		10.419231	9
52	551687	552	970538	80	581149	632	418851	8
53	552018	552	970490		581528		418472	7
54			970442		581907		418093	6 5
55			970394		582286		417714 417335	4
56		550	970345		582665 583043		417335	3
57 58			970297		583422		416578	2
59			970200		583800		416200	1
60			970152		584177		415823	0
=	1 Cosine	1	Sine	1	Cotang.	I	1 Tang.	M.
100	Cosmic		Dillo		Johang.	1		1

M.	Sine	D.	Cosine	D.	Tang,	D.	Cotang.	
U	9.554329	548	9.970152	81	9.584177	629	10.415823	60
1 2	554658 554987	548 547	970103 $970055$	81 81	584555 584932	$\begin{array}{c} 629 \\ 628 \end{array}$	$415445 \\ 415068$	59 58
$\frac{\tilde{3}}{3}$	555315	547	970006	81	585309	628	414691	57
4	555643	546	969957	81	585686	627	414314	56
5	555971	546	969909 969860	81 81	586062 586439	627	$egin{array}{cccc} 413938 \ 413561 \end{array}$	55 54
6 7	556299 556626	545 545	969811	81	586815	$\begin{array}{c} 627 \\ 626 \end{array}$	413185	53
8	556953	544	969762	81	587190	626	412810	52
9	557280	544	969714	81	587566	625	412434	51
$\frac{10}{10}$	557606	543	$\frac{969665}{2000000000000000000000000000000000000$	$\frac{81}{22}$	587941	625	412059	$\frac{50}{10}$
11 12	9,557932 558258	$\begin{array}{c} 543 \\ 543 \end{array}$	9.969616	82 82	$9.588316 \\ 588691$	$\begin{array}{c} 625 \\ 624 \end{array}$	$10.411684 \\ 411309$	49 48
13	558583	542	969518	82	589066	624	410934	47
14	558909	542	969469	82	589440	623	410560	46
15	559234	541	969420	82	589814	623	410186	45
16	559558 559883	541 540	969370 $969321$	82	590188 590562	$\begin{array}{c} 623 \\ 622 \end{array}$	409812 409438	44 43
18	560207	540	969272	82	590935	622	409065	42
19	560531	539	969223	82	591308	622	408692	41
20	560855	539	969173	82	591681	621	408319	$\frac{40}{30}$
21	9.561178	538	9.969124	82	9.592054	621	10.407946 407574	$\frac{\overline{39}}{38}$
22 23	561501 $561824$	538 537	$\begin{array}{r} 969075 \\ 969025 \end{array}$	82 82	592426 $592798$	$\begin{array}{c} 620 \\ 620 \end{array}$	407202	37
23 24 25	562146	537	968976	$8\tilde{2}$	593170	619	406829	36
	562468	536	968926	83	593542	619	406458	35
26	562790	536	$\begin{array}{ c c c c }\hline 968877 \\ 968827 \\ \hline \end{array}$	83	593914 $594285$	618 618	406086 405715	34 33
27 28	563112 563433		968777	83	594656	618	405715	$\begin{vmatrix} 33 \\ 32 \end{vmatrix}$
29	563755	535	968728	83	595027	617	404973	31.
30	.564075		968678	83	595398		404602	30
31	9.564396	534	9.968628	83	9.595768	617	10.404232	29
32 33	564716 565036	533	$\begin{array}{ c c c c c }\hline 968578 \\ 968528 \\ \hline \end{array}$	83	596138 596508	616 616	403862 403492	28 27
34	565356	532	968479	83	596878	616	403122	$\begin{vmatrix} \tilde{2}6 \end{vmatrix}$
35	565676		968429		597247	615	402753	25
36	565995 566314		$ \begin{array}{c c} 968379 \\ 968329 \end{array} $		$\begin{array}{ c c c c c }\hline 597616 \\ 597985 \\ \hline \end{array}$	615	402384 402015	24
38	566632		968278		598354	615 614	401646	23 22
39	566951	530	968228	84	598722	614	401278	21
40	567269		$\frac{968178}{}$	1	<u>599091</u>	613	400909	$\frac{20}{}$
41	9.567587		9.968128	84	9.599459	613	10.400541	19
42 43	567904 568222		968078 $968027$		$\begin{bmatrix} 599827 \\ 600194 \end{bmatrix}$		400173	18 17
44	568539		967977		690562		399438	16
45	568856		967927		600929	611	399071	15
46	569172		$oxed{967876} 967826$		601296		398704	14
是4万	569488 569804		967775		601662	611	398338 397971	13 12
43	570120		967725		602395		397605	111
50	570435	525	967674	1	602761	610	397239	10
51	9.570751	525	9.967624	84	9.603127	609	10.396873	9
52 53	571066 571380		967573 $967522$		$\begin{array}{c c} 603493 \\ 603858 \end{array}$	609	396507 396142	8 7
54	571695		967471	85	$\begin{vmatrix} 605838 \\ 604223 \end{vmatrix}$		395777	6
55	572009	523	967421	85	604588	608	395412	5
56	572323		967370		604953		395047	4
57 58	572636 572950		967319 967268		$\begin{bmatrix} 605317 \\ 605682 \end{bmatrix}$		394683 394318	$\begin{vmatrix} 3\\2 \end{vmatrix}$
59	573263		967217		606046		393954	1 î
60	573575		967166		606410		393590	0
1	Cosine	1	Sine	Ī	Cotang.		Tang.	M.
L	1				1			1

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	1
0	9.573575		9.967166	85	9.606410	606	10.393590	<u></u>
1	573888	520	967115	85	606773	606	393227	59
2 3	574200 574512	$\begin{array}{c} 520 \\ 519 \end{array}$	$967064 \\ 967013$	85 85	607137 $607500$	$\begin{array}{c} 605 \\ 605 \end{array}$	$392863 \\ 392500$	58
4	574824	519	966961	85	607863	604	392137	57 56
5	575136	519	966910	85	608225	604	391775	55
6	575447	518	966859	85	608588	604	391412	54
7 8	575758 576069	518 517	966808 $966756$	85 86	$608950 \\ 609312$	$\begin{array}{c} 603 \\ 603 \end{array}$	$391050 \\ 390688$	53 52
9	576379	517	966705	86	609674	603	390326	51
10	576689	516	966653	86	610036	602	389964	50
11	9.576999	516	9.966602	86	9.610397	602	10.389603	$\overline{49}$
12 13	577309 577618	516 515	$966550 \\ 966499$	86 86	$610759 \\ 611120$	$\begin{array}{c} 602 \\ 601 \end{array}$	389241 $388880$	48
14	577927	515	966447	86	611480	601	388520	47
15	578236	514	966395	86	611841	601	388159	45
16	578545	514	966344	86	612201	600	387799	44
17 18	578853 579162	$\begin{array}{c c} 513 \\ 513 \end{array}$	$966292 \\ 966240$	86 86	$612561 \\ 612921$	600 600	$\frac{387439}{387079}$	43 42
19	579470	513	966188	86	613281	599	386719	41
20	579777	512	966136	86	613641	599	386359	40
$\overline{21}$	9.580085	512	9 966085	87	9.614000	598	10.386000	39
22 23	580392 580699	$\begin{array}{c} 511 \\ 511 \end{array}$	$\begin{array}{c} 966033 \\ 965981 \end{array}$	87	$614359 \\ 614718$	598	385641	38
24	581005	$\frac{511}{511}$	965928	87 87	615077	598 597	385282 384923	37 36
25	581312	510	965876	87	615435	597	384565	35
26	581618	510	965824	87	615793	597	384207	34
27 28	$581924 \\ 582229$	$\begin{array}{c} 509 \\ 509 \end{array}$	$965772 \\ 965720$	87	$616151 \\ 616509$	596 596	383849 383491	33
29	582535	509	965668	87	616867	596 596	383133	$\frac{32}{31}$
30	582840	508	965615	87	617224	595	382776	30
$\overline{31}$	9.583145	508	9.965563	87	9617582	595	10.382418	29
32	583449	507	965511	87	617939	595	382061 381705	28
33 34	583754 584058	507 506	965458 $965496$	87	$\begin{array}{c} 618295 \\ 618652 \end{array}$	$\begin{array}{c} 594 \\ 594 \end{array}$	381795	$\begin{bmatrix} 27 \\ 26 \end{bmatrix}$
35	584361	506	965353	88	619008		380992	25
36	584665	506	965301	88	619364	593	380636	24
37 38	$584968 \\ 585272$	505 505	965248 $965195$	88	$\begin{array}{c c} 619721 \\ 620076 \end{array}$	593 593	$380279 \\ 379924$	23 22
39	585574	504	965143	88	620432	592	379568	21
40	585877	504	965090	88	620787	592	379213	20
41	9.586179	503	9.965037	88	9.621142	592	10.378858	19
42	586482 586783	503	$964984 \\ 964931$	88	$\begin{array}{ c c c c c } & 621497 \\ & 621852 \end{array}$	591 591	378503 378148	18 17
43	587085	$\begin{array}{c} 503 \\ 502 \end{array}$	964879	88	$621802 \\ 622207$	590	378148	16
45	587386	502	964826	88	622561	590	377439	15
46	587688	501	964773	88	622915		377085	14
47 48	587989 588289	501 501	$964719 \\ 964666$	88 89	$\begin{array}{c c} 623269 \\ 623623 \end{array}$	589 589	376731 376377	13 12
49	588590	500	964613		623976		376024	11
50	588890	500	964560	89	624330	588	375670	10
$\overline{51}$	9.589190	499	9.964507	$\overline{89}$	9.624683		10.375317	9
52	589489	499	964454		625036		374964	8 7
53 54	589789 590088	$\begin{array}{c c} 499 \\ 498 \end{array}$	$964400 \\ 964347$		$\begin{array}{c c} 625388 \\ 625741 \end{array}$	587 587	374612 374259	6
55	590387	498	964294	89	626093	587	373907	5
56	590686	497	964240	89	626445	586	373555	4
57	590984		964187		626797		373203	3
58 59	591282 591580		964133 964080		$\begin{array}{c c} 627149 \\ 627501 \end{array}$		372851 372499	2
60	591878		964026		627852		372148	
	Cosine		Sine	1	Cotang.		Tang.	M.

1	1 ~:	1 7	1 ~ :	1	J 72	70		
M.	Sine	D.	Cosine	D.	Tang.	.D.	Cotang.	0.5
0	$\begin{vmatrix} 9.591878 \\ 592176 \end{vmatrix}$	$\begin{vmatrix} 496 \\ 495 \end{vmatrix}$	$\begin{array}{r r} 9.964026 \\ 963972 \end{array}$	89	$\begin{bmatrix} 9.627852 \\ 628203 \end{bmatrix}$	585 585	$10.372148 \\ 371797$	60
$\frac{1}{2}$	592473	495	963919	89	628554	585	371446	59 58
2 3	592770	495	963865	90	628905	584	371095	57
4	593067	494	963811	90	629255	584	370745	56
5	593363	494	963757	90	629606	583	370394	55
6 7	593659 593955	493 493	$\begin{array}{c} 963704 \\ 963650 \end{array}$	90	629956 $630306$	583 583	$370044 \\ 369694$	54 53
8	594251	493	963596	90	630656	583	369344	52
9	594547	492	963542		631005	582	368995	51
10	594842	492	963488	90	631355	582	368645	50
11	9.595137	491	9.963434	$\overline{90}$	9.631704	582	10.368296	$\overline{49}$
12	595432	491	963379	90	632053	581	367947	48
13 14	595727 $596021$	491 490	$963325 \\ 963271$	90 90	$\begin{array}{c} 632401 \\ 632750 \end{array}$	581	$367599 \\ 367250$	47 46
15	596315	490	963277	90	633098	581 580	366902	45
16	596609	489	963163	90	633447	580	366553	44
17	596903	489	963108	91	633795	580	366205	43
18	597196	489	963054	91	634143	579	365857	42
$\begin{array}{c} 19 \\ 20 \end{array}$	597490 597783	$\begin{array}{c}488\\488\end{array}$	9629999962945	91 91	$634490 \\ 634838$	579 579	$365510 \\ 365162$	$\begin{array}{c c} 41 \\ 40 \end{array}$
1	$\frac{397765}{9.598075}$							
21 22	598368	487 487	$9.962890 \\ 962836$	91 91	$9.635185 \\ 635532$	$\begin{array}{c} 578 \\ 578 \end{array}$	$10.364815 \\ 364468$	39 38
23	598660	487	962781	91	635879	578	364121	37
24	598952	486	962727	91	636226	577	363774	36
25	599244	486	962672	91	636572	577	363428	35
26	599536	485	962617	91	636919	577	363081	34
27 28	$     \begin{array}{r}       599827 \\       600118     \end{array} $	$\begin{array}{c} 485 \\ 485 \end{array}$	962562 $962508$	91 91	637265 637611	577 576	$362735 \\ 362389$	33 32
29	600409	484	962453	91	637956	576	362044	31
30	600700	484	962398	92	638302	576	361698	30
$\overline{31}$	9.600990	484	9.962343	$\overline{92}$	9.638647	575	10.361353	$\overline{29}$
32	601280	483	962288	92	638992	575	361008	28
33	601570	483	962233	92	639337	575	360663	27
34 35	$601860 \\ 602150$	$\begin{array}{c} 482 \\ 482 \end{array}$	$962178 \\ 962123$	$\begin{array}{c} 92 \\ 92 \end{array}$	$639682 \\ 640027$	574 574	$360318 \\ 359973$	26 25
36	602439	482	962067	92	640371	574	359629	24
37	602728	481	962012	92	640716	573	359284	23
38	603017	481	961957	92	641060	573	358940	22
39 40	$\begin{array}{c} 603305 \\ 603594 \end{array}$	481 480	$961902 \\ 961846$	92	$641404 \\ 641747$	573	$358596 \\ 358253$	$\begin{vmatrix} 21\\20 \end{vmatrix}$
$\frac{40}{41}$	$\frac{603394}{9.603882}$		$\frac{961840}{9.961791}$	$\frac{92}{00}$		572	$\frac{358253}{10.357909}$	-
41	$\begin{vmatrix} 9.603882 \\ 604170 \end{vmatrix}$	$\begin{array}{c} 480 \\ 479 \end{array}$	$9.961791 \\ 961735$	92 92	$\begin{array}{c} 9.642091 \\ 642434 \end{array}$	572 572	357566	19 18
43	604457	479	961680	92	642777	572	357223	17
44	604745	479	961624	93	643120	571	356880	16
45	605032	478	961569	93	643463	571	356537	15
46   47	605319 $605606$	$\begin{array}{c} 478 \\ 478 \end{array}$	$961513 \\ 961458$	93 93	$\begin{array}{c} 643806 \\ 644148 \end{array}$	571	$356194 \\ 355852$	14 13
47	$\begin{array}{c} 605892 \\ 605892 \end{array}$	$\begin{array}{c} 478 \\ 477 \end{array}$	$961438 \\ 961402$	93	644490	570 570	355510	12
49	606179	477	961346	93	644832	570	355168	11
50	606465	476	961290	93	645174	569	354826	10
$\overline{51}$	9.606751	476	$\overline{9.961235}$	$\overline{93}$	9.645516	569	10.354484	9
52	607036	476	961179	93	645857	569	354143	8
53	607322	475	961123	93	646199	569	353801 353460	$\begin{vmatrix} 7 \\ 6 \end{vmatrix}$
54 55	$\frac{607607}{607892}$	475 474	$961067 \\ 961011$	93 93	$646540 \\ 646881$	568 568	353 <b>J</b> 19	5
56	608177	474	960955	93	647222	568	352778	4
57	608461	474	960899	93	647562	567	352438	3
58	608745	473	960843	94	647903	567	352097	2
59 60	609029 $609313$	473	$960786 \ 960730$	$\begin{array}{c c}94\\94\end{array}$	$\begin{array}{c} 648243 \\ 648583 \end{array}$	567	351757 351417	$\begin{vmatrix} 1 \\ 0 \end{vmatrix}$
		473		34		566	<u> </u>	
	Cosine		Sine	1	Cotang.		Tang.	MI.

42	(~ 1	Degr	ees.) A	TAE	SLE OF LO	GARIT.	ATALICO	
М.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.609313	473	9.960730		9.648583	566	10.351417	60
1	609597	472	960674	94	$\begin{array}{c} 648923 \\ 649263 \end{array}$	566 566	$\begin{vmatrix} 351077 \\ 350737 \end{vmatrix}$	59 58
2 3	609880 610164	$\begin{array}{c c}472\\472\end{array}$	960618 960561	94   94	649602	566	350398	57
4	610447	471	960505	94	649942	565	350058	56
5	610729	471	960448	94,	650281	565	349719	55
6	611012	470	960392	94	650620	565	349380	54
7	611294	470	$\begin{array}{c} 960335 \\ 960279 \end{array}$	94   94	650959 $651297$	564 564	$349041 \begin{vmatrix} 348703 \end{vmatrix}$	53 52
8 9	611576 611858	470 469	960222	94	651636	564	348364	51
10	612140	469	960165	94	651974	563	348026	50
11	9.612421	469	9.960109	$\overline{95}$	9.652312	563	10.347688	49
12	612702	468	960052	95	652650	563	347350	48
13	612983	468	959995	95	652988 653326	$\begin{array}{c c} 563 \\ 562 \end{array}$	$347012 \begin{vmatrix} 346674 \end{vmatrix}$	47
14 15	$613264 \\ 613545$	467 467	$\frac{959938}{959882}$	95 95	653663	$\frac{562}{562}$	346337	45
16	613825	467	959825	95	654000	562	346000	44
17	614105	466	959768	95	654337	561	345663	43
18	614385	466	959711	95	654674	561	345326	42
19 20	614665 614944	$\begin{array}{c} 466 \\ 465 \end{array}$	$\begin{array}{c} 959654 \\ 959596 \end{array}$	95 95	655011   655348	$\begin{array}{c} 561 \\ 561 \end{array}$	$egin{array}{c} 344989 \ 344652 \ \end{array}$	41 40
$\frac{20}{21}$	$\frac{014944}{9.615223}$	465	$\frac{353530}{9.959539}$	$\frac{35}{95}$	$\frac{05.0510}{9.655684}$	560	$\frac{10.344316}{10.344316}$	$\frac{10}{39}$
$\begin{bmatrix} 21\\22 \end{bmatrix}$	615502	465	959482	95	656020	560	343980	38
$\tilde{23}$	615781	464	959425	95	656356	560	343644	37
24	616060	464	959368	95	656692	559	343308	36
25	616338	464	$\begin{array}{c} 959310 \\ 959253 \end{array}$	96	657028 657364	559 559	$egin{array}{c} 342972 \ 342636 \ \end{array}$	35 34
$\begin{array}{c} 26 \\ 27 \end{array}$	$616616 \\ 616894$	$\begin{array}{c} 463 \\ 463 \end{array}$	959195	$\begin{array}{c} 96 \\ 96 \end{array}$	657699	559 559	342301	$\frac{34}{33}$
28	617172	462	959138	96	658034	558	341966	32
29	617450	462	959081	96	658369	558	341631	31
30	$\boxed{617727}$	462	959023	$\frac{96}{}$	658704	558	341296	30
31	9.618004	461	9.958965		9.659039	558	$\begin{array}{r} 10.340961 \\ 340627 \end{array}$	29
32 33	618281 618558	$\begin{array}{c} 461 \\ 461 \end{array}$	958908 $958850$	96 96	659373 $659708$	557 557	340627	28 27
34	618834	460	958792		660042	557	339958	26
35	619110	460	958734		660376	557	339624	25
36	619386	460	958677	96	660710 $661043$	556 556	339290 338957	24 23
37 38	619662	$\begin{array}{c} 459 \\ 459 \end{array}$	958619 958561	96	661377	556	338623	22
39	620213	459	958503		661710	555	338290	21
40	620488	458	958445	97	662043	555	337957	20
41	9.620763	458	9.958387	$\overline{97}$	9 662376	555	10.337624	19
42	621038	457	958329	97	$\begin{array}{ c c c c c } & 662709 \\ & 663042 \end{array}$	554	337291	18
43 44	$\begin{bmatrix} 621313 \\ 621587 \end{bmatrix}$	$\begin{array}{c} 457 \\ 457 \end{array}$	$\begin{array}{c} 958271 \\ 958213 \end{array}$	97	663375	554	336958 336625	16
45	621861	456	958154	97	663707	554	336293	15
46	622135	456	958096	97	664039	553	335961	14
47	622409	456	958038	97	664371	553	335629	13
48 49	$\begin{array}{c c} 622682 \\ 622956 \end{array}$	455 455	957979 957921	97	664703		335297 334965	12
50	623299	$\begin{array}{c} 455 \\ 455 \end{array}$	957863		665366		334634	10
$\frac{51}{51}$	$\frac{62320}{9.623502}$	454	9.957804		9.665697	1	10.334303	9
52	623774	454	957746	98	666029	552	333971	8
53	624047	454	957687		666360		333640	7
54 55	624319	453	$\begin{array}{ c c c c c }\hline 957628 \\ 957570 \\\hline \end{array}$		666691		333309 332979	6 5
56 56		453 453	957570		667352		332648	4
57	625135		957452		667682	550	332318	3
58	625406	452	957393	98	668013		331987	2
59			957335		668343		331657 331328	$\begin{vmatrix} 1 \\ 0 \end{vmatrix}$
60		451	957276	198		550		
	Cosine		l Sine		Cotang.	1	Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.625948	451	9.957276	98	9.668673	550	10.331327	60
$\frac{1}{2}$	$626219 \\ 626490$	$\begin{array}{c} 451 \\ 451 \end{array}$	957217 $957158$	98 98	$\frac{669002}{669332}$	549 549	330998 330668	59 58
3	626760	450	957099	98	669661	549	330339	57
4	627030	450	957040	98	669991	548	330009	56
5	627300	450	956981	98 99	670320	548	329680	55
6 7	$\begin{array}{c} 627570 \\ 627840 \end{array}$	$\begin{array}{c} 449 \\ 449 \end{array}$	$956921 \\ 956862$	99	$\frac{670649}{670977}$	$\begin{array}{c} 548 \\ 548 \end{array}$	$329351 \ 329023$	54 53
8	628109	449	956803	99	671306	547	328694	52
9	628378	448	956744	99	671634	547	328366	51
$\frac{10}{10}$	$\frac{628647}{2000000000000000000000000000000000000$	448	$\frac{956684}{20005}$	$\frac{99}{100}$	671963	547	328037	$\frac{50}{10}$
11 12	$9.628916 \\ 629185$	447 447	9.956625 956566	99 99	$9.672291 \\ 672619$	547 546	$\frac{10.327709}{327381}$	49 48
13	629453	447	956506	99	672947	$\begin{array}{c} 540 \\ 546 \end{array}$	$\frac{327551}{327053}$	47
14	629721	446	956447	99	673274	546	326726	46
15	629989	446	956387	99	673602	546	326398	45
16 17	$630257 \\ 630524$	$\begin{array}{c} 446 \\ 446 \end{array}$	956327 $956268$	99 99	$\frac{673929}{674257}$	545 545	$326071 \ 325743$	44 43
18	630792	445	956208	100	674584	545	325416	42
19	631059	445	956148	100	674910	544	325090	41
$\frac{20}{}$	631326	445	956089	$\frac{100}{100}$	675237	544_	324763	<u>40</u>
21	9.631593	444	9.956029 $955969$	100	9.675564	544	10.324436	39
22 23	$631859 \\ 632125$	444 444	955909	100	$675890 \ 676216$	$\begin{array}{c} 544 \\ 543 \end{array}$	$324110 \\ 323784$	$\begin{array}{c} 38 \\ 37 \end{array}$
24	632392	$\hat{4}\hat{4}\hat{3}$	955849	100	676543	543	323457	36
25	632658	443	955789	100	676869	543	323131	25
$\begin{bmatrix} 26 \\ 27 \end{bmatrix}$	632923 $633189$	$\begin{array}{c} 443 \\ 442 \end{array}$	955729 955669	$\begin{bmatrix} 100 \\ 100 \end{bmatrix}$	$\frac{677194}{677520}$	$\begin{array}{c} 543 \\ 542 \end{array}$	$322806 \\ 322480$	$\begin{bmatrix} 34 \\ 33 \end{bmatrix}$
28	633454	$\begin{array}{c} 442 \\ 442 \end{array}$	955609	100	677846	542	322154	32
29	633719	442	955548	100	678171	542	321829	31
30	633984	441	955488	100	678496	542	321504	30
31	9.634249	441	9.955428	101	9.678821	541	10.321179	29
32 33	$634514 \\ 634778$	$\begin{array}{c} 440 \\ 440 \end{array}$	$955368 \\ 955307$	$\begin{bmatrix} 101 \\ 101 \end{bmatrix}$	$\begin{array}{c} 679146 \\ 679471 \end{array}$	541 541	$320854 \\ 320529$	28 27
34	=635042	440	955247	101	679795	541	320205	26
35	635306	439	955186		680120	540	319880	25
$\begin{bmatrix} 36 \\ 37 \end{bmatrix}$	$\begin{array}{r} 635570 \\ 635834 \end{array}$	439 439	$955126 \\ 955065$		$680444 \\ 680768$	540 540	$egin{array}{cccccccccccccccccccccccccccccccccccc$	24 23
38	636097	$\begin{array}{c} 439 \\ 438 \end{array}$	955005		681092	540	318908	22
39	636360	438	954944	101	681416	539	318584	21
$\frac{40}{}$	-636623	438	$\frac{954883}{}$		681740	500	318260	$\frac{20}{}$
41	9.636886	437	9 954823		9.682063	539	10.317937	19
42 43	$637148 \\ 637411$	$\begin{array}{c} 437 \\ 437 \end{array}$	$\begin{array}{c c} 954762 \\ 954701 \end{array}$	101	$\begin{array}{c c} 682387 \\ 682710 \end{array}$	539 538	$\begin{array}{c} 317613 \\ 317290 \end{array}$	18
44	637673	437	954640		683033	538	316967	16
45	637935	436	954579	101	683356	538	316644	15
46	638197	436	954518	$\begin{vmatrix} 102 \\ 102 \end{vmatrix}$	683679 684001	538	$ \begin{array}{c c} 316321 \\ 315999 \end{array} $	14
47	$\begin{array}{c c} 638458 \\ 638720 \end{array}$	$\begin{array}{c} 436 \\ 435 \end{array}$	$oxed{954457} 954396$		684001 $684324$	537 537	315676	
49	638981	435	954335	102	684646	537	315354	11
50	639242	435	954274	102	684968	537	315032	10
$\overline{51}$	9.639503	434	9.954213			536	10.314710	
52	639764	434	954152 $954090$		685612 685934	536 536	314388 314066	8 7
$\begin{array}{c} 53 \\ 54 \end{array}$	$640024 \\ 640284$	$\begin{array}{c} 434 \\ 433 \end{array}$	$954090 \\ 954029$				313745	
55	640544	433	953968	102	686577	535	313423	5
56	640804	433	953906			535	313102	
57 58	641064	432	$\begin{array}{ c c c c c }\hline 953845 \\ 953783 \\ \hline \end{array}$			535	312781 312460	3 2
58 • 59	$\begin{array}{c c} 641324 \\ 641584 \end{array}$	$\begin{array}{c} 432 \\ 432 \end{array}$	953722				312139	
60	641842		953660				311818	
	Cosine		Sine		Cotang.		Tang.	M.
	,							1

0   9.641842   431   9.953660   103   9.688182   534   10.311818   60   1   642101   431   9.953690   103   688502   534   311478   53   642618   430   9.55337   103   688823   534   311477   58   3   642618   430   9.553475   103   688943   533   310857   57   6487333   430   9.53413   103   689443   533   310857   57   643650   429   9.53228   103   690423   533   309897   54   643650   429   9.55328   103   690423   533   309897   54   644665   429   9.55328   103   690423   533   309897   54   64443   428   9.55241   104   692019   531   307861   48   48   48   48   48   48   48   4	M	Sine	D.	Cosine	D.	Tang.	l p	1 Cotons	1
1	-						D.	Cotang.	1 00
2									
3	2	642360	431			688823			
648373   430   953813   103   669463   533   310537   56     648393   430   953825   103   669783   533   310217   55     7   64850   429   953290   103   669103   533   309977   54     8   643908   429   953166   103   690742   532   309957   54     9   644165   429   953104   103   691062   532   309957   54     10   644423   428   953042   103   691381   532   308619   50     11   9   644680   428   9.59298   104   692109   531   307851   80781   11     12   644936   428   9.59298   104   692019   531   307851   80781   11     13   645193   427   952855   104   692338   531   307862   47     14   645460   427   95273   104   692556   531   307344   46     15   645706   427   952731   104   692556   531   307344   40     16   644506   426   952666   104   693933   530   306707   44     17   646218   426   952666   104   693933   530   3068707   42     18   646474   426   952546   104   693933   530   3068707   42     20   646729   425   952481   104   693933   530   3068707   42     20   646729   425   952481   104   693930   530   3068707   42     21   9   647240   425   952481   104   693930   530   3068707   42     22   64744   424   952241   104   693930   530   3065707   42     23   647749   424   952241   104   693518   529   304482   37     24   64804   424   952241   104   695501   529   304482   37     25   648258   424   952240   104   695501   529   304482   37     25   648258   424   952240   104   695501   529   304482   37     27   64866   423   951917   105   697103   528   302393   32     28   649020   423   951917   105   697103   528   302393   32     29   649274   422   951851   105   697400   527   302264   30     29   649274   422   951851   105   697400   527   302264   30     30   649527   422   951850   105   696376   527   302264   30     31   9.649781   422   951850   105   699316   526   300688   425     32   65039   419   951159   106   700786   527   302264   30     32   65039   419   951159   106   700786   527   302269   30688   31   40088   30688   30688   30689   527   30088						689143			
6 643393 430 953290 103 690103 533 309877 54 8 643908 429 953166 103 690742 532 309578 52 953104 103 691062 532 309578 52 10 644165 429 953104 103 691062 532 308539 52 10 644423 428 953042 103 691062 532 308539 52 10 644423 428 953042 103 691062 532 308539 52 10 644423 428 953042 103 691062 532 308539 52 11 9.644680 428 9.59298 104 9.691381 532 308619 50 12 644936 428 9.59298 104 692338 531 307981 82 13 645193 427 952855 104 692338 531 307981 82 14 645460 427 952731 104 692356 531 307344 46 16 645962 426 952606 104 693293 530 306707 44 17 646218 426 952606 104 693293 530 306707 44 17 646218 426 952606 104 693293 530 306388 43 18 646474 426 952606 104 693930 530 306707 42 19 646729 425 952481 104 693930 530 306707 42 19 646729 425 952481 104 693930 530 306707 42 19 646729 425 952481 104 693930 530 306707 42 19 646729 425 952481 104 693930 530 306707 42 19 646729 425 952481 104 693930 530 306707 42 2 64744 424 952241 104 695201 529 305434 40 22 64744 424 952241 104 695518 529 305434 40 22 64744 424 952241 104 695518 529 304482 37 22 647640 424 952241 104 695518 529 304482 37 22 64860 424 952241 104 695518 529 304482 37 22 64860 424 952241 104 695518 529 304482 37 22 64860 424 952241 104 695518 529 304482 37 22 64866 424 952241 104 695518 529 304482 37 22 64860 424 952241 104 695518 529 304482 37 22 64866 529 42 951861 105 696470 528 303530 34 35 28 303530 34 35 28 303530 34 35 28 303530 34 35 28 303530 34 35 30 36432 34 35 32 30 36482 37 35 36432 34 35 36 36 36 36 36 36 36 36 36 36 36 36 36		642877	430					310537	56
Total		643135	430						
8 643908 429 953166 103 690742 532 309388 51 10 644423 428 953042 103 691062 532 309388 51 11 9.644680 428 9.95298 104 9692019 531 307981 48 12 644936 428 952918 104 692019 531 307981 48 13 645193 427 952855 104 692338 531 307662 47 14 645450 427 952731 104 692656 531 307344 46 15 645706 427 952731 104 692656 531 307344 46 16 64562 426 952666 104 693293 530 306707 44 18 646474 426 952606 104 693293 530 306707 44 18 646474 426 952606 104 693293 530 306707 44 18 646729 425 952441 104 693491 530 306707 44 19 646729 425 952441 104 693293 530 306707 44 19 646729 425 952441 104 693293 530 306752 41 20 646984 425 952419 104 694566 529 304349 40 21 9.647240 425 9.952356 104 994566 529 304393 305752 41 22 647494 424 952221 104 695201 529 304799 38 23 647749 424 952221 104 695518 529 304482 37 24 648004 424 952221 104 695518 529 304482 37 25 648528 424 952168 105 695836 529 304482 37 26 648512 423 952043 105 695875 528 303213 33 27 648766 423 951990 105 696470 528 303530 33 28 649020 423 951917 105 696470 528 303530 34 29 649274 422 951854 105 697420 527 302580 31 30 649527 422 951854 105 699305 527 302580 31 30 649527 422 951854 105 699305 527 302580 31 31 9.649781 422 951665 105 699316 526 300684 25 33 66792 421 951539 105 699632 527 302284 30 31 9.649781 422 951651 105 699316 526 30099 26 40 652052 419 951522 106 700578 525 299422 1 31 9.649781 422 951605 105 699316 526 30099 26 40 652052 419 951522 106 700578 525 299422 1 41 9.65255 418 95103 106 699347 526 300684 25 36 651044 420 951412 105 699632 524 2995784 16 40 653057 418 950951 106 702466 524 297534 15 40 653057 418 950951 106 702466 524 297534 15 40 653057 418 950951 107 704666 524 297534 15 40 653057 418 950954 107 704666 524 297534 15 40 653057 418 950954 107 704666 524 297534 15 40 653057 418 950954 107 704366 522 295984 10 40 654309 416 950584 107 704666 524 297537 15 40 656004 414 950013 107 704666 524 297534 15 40 656004 414 950010 107 706603 522 295937 8 40 656004 414 950010 107 706603 522 295937 8 40 656004 414 950010 107 706603 522 295337 8 40 666799									
9		0 417000							
10		644165		953104	103				
11	9	644423	428	953042	103				
12				9.952980	104	9.691700			N
14							531	307981	
15									
16								307344	
17						603903			
18	17					693612			
19			426						
Section   Sine   Cotange   Cotange   Sine   Cotange   Cotange   Sine   Cotange   Cotange						694248			
22		1			104	694566	529	305434	
23   647749   424   952231   104   695518   529   304482   37   648004   424   952168   105   695836   529   304164   36   36   688258   424   952106   105   696153   528   303347   35   26   648512   423   952043   105   696470   528   303347   33   328   649020   423   951917   105   697687   528   302397   32   30   649527   422   951854   105   697420   527   302580   31   30   649527   422   951854   105   697420   527   302580   31   30   649527   422   951854   105   697420   527   302264   30   31   9.649781   422   9.951728   105   698369   527   302264   30   32   650034   422   9.951665   105   698369   527   301631   28   33   650287   421   951602   105   698365   526   301315   27   301631   28   33   650287   421   951539   105   699001   526   300999   26   35   650792   421   951476   105   699385   526   301315   27   301631   28   36   651044   420   951412   105   699632   526   3009684   25   36   651044   420   951349   106   699947   526   300968   24   37   651297   420   951349   106   699947   526   300968   24   39   651800   419   951222   106   700263   525   299737   22   40   652052   419   9511259   106   700363   525   299107   20   42   652555   418   950968   106   701637   524   298163   17   44   653057   418   950905   106   701208   524   298163   17   44   653368   417   950778   106   702466   524   297534   15   46   653558   417   950778   106   702466   524   297534   15   46   653558   417   950778   106   702466   524   297534   15   46   653558   416   950394   107   704663   522   295337   8   654059   416   950586   106   703723   523   206591   12   49   654399   416   950586   106   703723   523   206591   12   49   49   49   49   49   49   40   40							529	10.305117	39
24         648004         424         952168         105         695836         529         304464         36           25         648258         424         952168         105         696153         528         303347         35           26         648512         423         952043         105         696470         528         303331         33           28         649020         423         951917         105         697103         528         302897         32           29         649274         422         951854         105         697736         527         302264         30           30         649527         422         951791         105         697736         527         302264         30           31         9.649781         422         9.51665         105         698369         527         301631         28           32         650287         421         951602         105         698695         526         301315         27           34         650589         421         951602         105         698695         526         300684         25           35         650792         421									
25									
26									
28	26								
289   649920   423   951917   105   697103   528   302897   32   300   649527   422   951854   105   697420   527   302580   31   31   9.649781   422   9.951791   105   697736   527   302264   30   32   650034   422   9.951792   105   6986953   527   10.301947   29   33   650287   421   951665   105   698695   526   301315   27   30   34   650539   421   951539   105   699605   526   300684   25   36   651044   420   951412   105   699632   526   300684   25   36   651044   420   951412   105   699632   526   300684   25   38   651549   420   951349   106   699947   526   300053   23   38   651549   420   951286   106   700263   525   299737   22   40   652052   419   951159   106   700893   525   299107   20   41   9.652304   419   9.951096   106   701837   524   298163   17   47   653808   418   950968   106   702466   524   297534   15   46   653558   417   950778   106   702466   524   297534   15   47   653808   417   950778   106   703409   523   296591   12   49   654309   416   950586   106   703409   523   296591   12   49   654808   416   950586   106   703723   523   296591   12   49   654808   416   950586   106   703723   523   296591   12   49   654808   416   950586   106   703723   523   296591   12   49   654808   416   950586   106   703723   523   296591   12   49   654808   416   950586   106   703723   523   296591   12   49   654808   416   950586   106   703723   523   296591   12   49   654808   416   950586   106   703723   523   296591   12   49   654808   416   950586   107   704663   522   2955337   8   655356   415   950266   107   705603   521   294497   556   656551   414   950010   107   706541   521   294397   556   656099   413   948945   107   707664   520   292834   0   40   413   948981   107   707666   520   292834   0   40   413   948981   107   707666   520   292834   0   40   413   948981   107   707666   520   292834   0   414   415   413   418		648766				696787			
Sine       Sine       Sine       Sine       Sine   Sine   Sine   Sine   Sine   Sine   Sine						697103			
31   9.649781   422   9.951728   105   9.698053   527   10.301947   29   32   650034   422   951665   105   698685   526   301631   28   34   650287   421   951602   105   698685   526   300999   26   35   650792   421   951476   105   699316   526   300999   26   36   651044   420   951412   105   699316   526   3000584   25   37   651297   420   951349   106   699347   526   300053   23   38   651549   420   951286   106   700263   525   299737   22   40   652052   419   951129   106   700893   525   299107   20   41   9.652304   419   9.951032   106   701523   524   298477   18   44   653057   418   950968   106   702152   524   297848   16   6530557   418   950958   106   702152   524   297848   16   6530557   418   950951   106   702466   524   297848   16   6530557   418   950951   106   702466   524   297848   16   6530557   418   950958   106   702152   524   297848   16   6530557   418   950958   106   702466   524   297848   16   6530557   418   950958   106   702466   524   297848   16   653057   418   950958   106   702466   524   297848   16   653057   418   950958   106   702466   524   297848   16   653057   418   950958   106   702466   524   297848   16   653057   418   950958   106   702466   524   297584   15   653308   417   950714   106   702466   523   296050   13   49   654309   416   950586   106   703409   523   296095   10   296095   10   296095   10   296095   10   296095   10   296095   10   296095   10   296095   10   296095   10   296095   10   296095   10   296095   10   296095   10   296095   10   296095   10   296095   20   296095   20   296095   20   296095   20   296095   20   296095   20   296095   20   296095   20   296095   20   296095   20   296095   20   296095   20   296095   20								302580	31
32         650034         422         951665         105         698369         527         301631         28           34         650287         421         951602         105         698685         526         301315         27           34         650539         421         951539         105         699001         526         300999         26           35         650792         421         951476         105         699316         526         300999         26           36         651044         420         951349         106         699347         526         3000684         25           37         651297         420         951349         106         699947         526         300053         23           38         651800         419         951222         106         700578         525         299737         22           40         652052         419         951159         106         70701208         524         299107         20           41         9.652304         419         9.951096         106         701523         524         298163         17           43         652806         418									30
33   650287   421   951602   105   698685   526   301315   27   34   650539   421   951539   105   699001   526   300999   26   35   650792   421   951476   105   699316   526   300684   25   36   651044   420   951412   105   699632   526   300368   24   37   651297   420   951349   106   699947   526   300368   24   38   651549   420   951286   106   700263   525   299737   22   40   652052   419   951159   106   700893   525   299107   20   41   9.652304   419   9.951096   106   701823   524   42   652555   418   950968   106   701823   524   43   652806   418   950968   106   701823   524   44   653057   418   950968   106   702152   524   298467   18   45   653308   418   950968   106   702466   524   297534   15   46   653558   417   950778   106   702466   524   297534   15   47   653808   417   950778   106   702466   524   297534   15   48   654059   417   950650   106   703409   523   296297   12   48   654309   416   950586   106   703409   523   296591   12   49   654309   416   950586   106   703409   523   296591   12   50   654558   416   950522   107   704036   522   295964   10   51   9.654808   416   950586   106   703723   523   296277   106   51   9.654808   416   950586   106   703409   523   296277   10   52   655556   415   950266   107   704977   522   295023   7   54   655556   415   950266   107   705290   522   294710   6   55   655805   416   950394   107   705916   521   294084   4   57   656302   414   950138   107   706641   521   294084   4   58   656551   414   950010   107   706641   521   294084   4   58   656551   414   950010   107   706641   521   293459   2   59   656794   413   949945   107   706654   521   293459   2   60   657047   413   949881   107   707166   520   292834   0									
34         650539         421         951539         105         699001         526         300999         26           36         650792         421         951476         105         699316         526         300684         25           36         651044         420         951412         105         699632         526         300368         24           37         651297         420         951349         106         699947         526         300053         23           38         651549         420         951286         106         700263         525         299737         22           39         651800         419         951522         106         700578         525         299422         21           40         652052         419         951159         106         700893         525         299422         21           41         9.652304         419         9.951096         106         701523         524         298477         18           42         652806         418         950961         106         701523         524         298477         18           45         653308         418									
35   650792   421   951476   105   699316   526   300684   25   36   651044   420   951412   105   699632   526   300368   24   37   651297   420   951349   106   699947   526   300053   23   23   23   23   24   24   24   2									
36         651044         420         951412         105         699632         526         300368         24           37         651297         420         951349         106         699947         526         300053         23           38         651549         420         951286         106         700263         525         299737         22           39         651800         419         951222         106         700578         525         299452         21           40         652052         419         951159         106         700893         525         299107         20           42         652555         418         951032         106         701523         524         298463         17           43         652806         418         950968         106         701523         524         297848         16           45         653308         418         950951         106         702466         524         297534         15           46         653558         417         950778         106         702780         523         296297         14           47         653808         417	35								
37         651297         420         951349         106         699947         526         300053         23           38         651549         420         951286         106         709263         525         299737         22           39         651800         419         951222         106         700578         525         299452         21           40         652052         419         951159         106         700893         525         299107         20           41         9.652304         419         9.951096         106         7.701208         524         10.298792         10           42         652555         418         951032         106         701523         524         298477         18           43         652806         418         950968         106         702152         524         297848         17           45         653308         418         950941         106         702466         524         297848         15           47         653808         417         950778         106         702780         523         296905         13           48         654059         417			420						
Sine   Cotang.   Tang.   M.   M.   M.   M.   M.   M.   M.						699947			
40         652052         419         951159         106         700893         525         299107         20           41         9.652304         419         9.951096         106         9.701208         524         10.298792         10           42         652555         418         951032         106         701523         524         298477         18           43         652806         418         950905         106         701837         524         298477         18           44         653057         418         950905         106         702466         524         297848         16           45         653308         418         950941         106         702466         524         297534         15           47         653808         417         950778         106         702780         523         296905         13           48         654059         417         950650         106         703409         523         296591         12           49         654309         416         950522         107         704036         522         295964         10           52         655058         416									
41         9.652304         419         9.951096         106         9.701208         524         10.298792         19           42         652555         418         951032         106         701523         524         298477         18           43         652806         418         950968         196         701837         524         298163         17           44         653057         418         950905         106         702152         524         297848         16           45         653308         418         950841         106         702466         524         297534         15           46         653558         417         950778         106         702780         523         297220         14           47         653808         417         950714         106         703409         523         296591         13           48         654059         417         950650         106         703723         523         296277         11           50         654558         416         950522         107         704036         522         295964         10           51         9.654808         416 <td></td> <td></td> <td></td> <td></td> <td></td> <td>700578</td> <td></td> <td></td> <td></td>						700578			
42         652555         418         951032         106         701523         524         298477         18           43         652806         418         950968         196         701837         524         298163         17           44         653057         418         950905         106         702152         524         297848         16           45         653308         418         950941         106         702466         524         297534         15           46         653558         417         950778         106         702780         523         297220         14           47         653808         417         950714         106         703095         523         296905         13           48         654059         417         950650         106         703409         523         296591         12           49         654309         416         950586         106         703723         523         296277         11           50         654558         416         950394         107         704663         522         295964         10           51         655058         416		·							
43         652806         418         950968         106         701837         524         298163         17           44         653057         418         950905         106         702152         524         298163         17           45         653308         418         950841         106         702466         524         297534         15           46         653558         417         950778         106         702780         523         297220         14           47         653808         417         950650         106         703095         523         296905         13           48         654059         417         950650         106         703409         523         296591         12           49         654309         416         950586         106         703723         523         296277         11           50         654558         416         9.950458         107         704036         522         295964         10           51         9.654808         416         9.950394         107         704663         522         295337         8           52         655058         416									
44         653057         418         950905         106         702152         524         297848         16           45         653308         418         950841         106         702466         524         297534         15           46         653558         417         950778         106         702780         523         297220         14           47         653808         417         950714         106         703095         523         296905         13           48         654059         417         950650         106         703409         523         296591         13           49         654309         416         950586         106         703723         523         296277         11           50         654558         416         950522         107         704036         522         295964         10           51         9.654808         416         950394         107         704663         522         295337         8           52         655058         416         950394         107         704977         522         295337         8           53         655305         415									
45         653308         418         950841         106         702466         524         297534         15           46         653558         417         950778         106         702780         523         297220         14           47         653808         417         950714         106         703095         523         296905         13           48         654059         417         950650         106         703409         523         296591         12           50         654558         416         950586         106         703723         523         296277         11           51         9.654808         416         950522         107         704036         522         295964         10           52         655058         416         950394         107         704663         522         2959337         8           53         655058         415         950330         107         704977         522         295023         7           54         655536         415         950266         107         705290         522         294710         6           55         655805         415	44					702152			
46         653558         417         950778         106         702780         523         297220         14           47         653808         417         950714         106         703095         523         296905         13           48         654059         417         950650         106         703409         523         296277         11           49         654309         416         950586         106         703723         523         296277         11           50         654558         416         950522         107         704036         522         295964         10           51         9.654808         416         9.950458         107         704036         522         295964         10           52         655058         416         9.50394         107         704663         522         295337         8           53         655307         415         950330         107         704977         522         295023         7           54         655556         415         950266         107         705290         522         294710         6           55         6565805         415	45	653308	418	950841		702466			
47         653808         417         950714         106         703095         523         296905         13           49         654309         416         950650         106         703409         523         296591         12           50         654558         416         950522         107         704036         522         295964         10           51         9.654808         416         9.950458         107         704036         522         295964         10           52         655058         416         950394         107         704663         522         295337         8           53         655307         415         950330         107         704977         522         295023         7           54         655556         415         950266         107         705290         522         294710         6           55         656054         414         950138         107         705603         521         294084         4           57         656302         414         950074         107         706228         521         293772         3           58         656551         414         <					106	702780	523		
$\begin{array}{c c c c c c c c c c c c c c c c c c c $							523	296905	
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$									12
51         9.654808         416         9.950458         107         9.704350         522         10.295650         9           52         655058         416         950394         107         704663         522         10.295650         9           53         655307         415         950330         107         704977         522         295023         7           54         655556         415         950266         107         705290         522         294710         6           55         655805         415         950202         107         705603         521         294397         5           56         656054         414         950138         107         705916         521         294084         4           57         656302         414         950074         107         706228         521         293772         3           58         656551         414         950010         107         706854         521         293459         2           59         656799         413         949881         107         707166         520         292834         0           Cosine         Sine         Cotang.									
52         655058         416         950394         107         704663         522         295337         8           53         655307         415         950330         107         704977         522         295023         7           54         655556         415         950266         107         705290         522         294710         6           55         655805         415         950202         107         705603         521         294397         5           56         656054         414         950138         107         705916         521         294084         4           57         656302         414         950074         107         706228         521         293772         3           58         656551         414         950010         107         706541         521         293459         2           59         656799         413         949845         107         706854         521         293146         1           60         657047         413         949881         107         707166         520         292834         0    Cosine									
53         655307         415         950330         107         704977         522         295023         7           54         655556         415         950266         107         705290         522         294710         6           55         655805         415         950202         107         705603         521         294397         5           56         656054         414         950138         107         705916         521         294084         4           57         656302         414         950074         107         706228         521         293772         3           58         656551         414         950010         107         706541         521         293459         2           59         656799         413         949451         107         706854         521         293146         1           60         657047         413         949881         107         707166         520         292834         0    Cosine									
54         655556         415         950266         107         705290         522         294710         6           55         655805         415         950202         107         705603         521         294397         5           56         656054         414         950138         107         705916         521         294084         4           57         656302         414         950074         107         706228         521         293772         3           58         656551         414         950010         107         706541         521         293459         2           59         656799         413         949945         107         706854         521         293146         1           60         657047         413         949881         107         707166         520         292834         0           Cosine         Sine         Cotang.         Tang.         M.									
55         655805         415         950202         107         705603         521         294397         5           56         656054         414         950138         107         705916         521         294084         4           57         656302         414         950074         107         706228         521         293772         3           58         656551         414         950010         107         706541         521         293459         2           59         656799         413         949945         107         706854         521         293146         1           60         657047         413         949881         107         707166         520         292834         0           Cosine         Sine         Cotang.         Tang.         M.		655556	415						
50         656054         414         950138         107         705916         521         294084         4           57         656302         414         950074         107         706228         521         293772         3           58         656551         414         950010         107         706541         521         293459         2           59         656799         413         9494945         107         706854         521         293146         1           60         657047         413         949881         107         707166         520         292834         0           Cosine         Sine         Cotang.         Tang.         M.				950202	107	705603			
57         656302         414         950074         107         706228         521         293772         3           58         656551         414         950010         107         706541         521         293459         2           59         656799         413         949945         107         706854         521         293146         1           60         657047         413         949881         107         707166         520         292834         0           Cosine         Sine         Cotang.         Tang.         M.						705916	521	294084	4.
59         656799         413         949945         107         706854         521         293446         1           60         657047         413         949881         107         707166         520         292834         0           Cosine         Sine         Cotang.         Tang.         M.									3
60         657047         413         949881         107         707166         520         292834         0           Cosine         Sine         Cotang.         Tang.         M.			413						
Cosine   Sine   Cotang.   Tang.   M.	60								
County. 1 ang. M.		Cosine 1	1				020		
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M	Sine	Ď	Cosine	D	Tang.	Ď.	Cotang.	
0	9.657047	413	9.949881	107			10.292834	60
$\frac{1}{2}$	657295 $657542$	$\begin{array}{c} 413 \\ 412 \end{array}$	$949816 \\ 949752$	$\frac{107}{107}$	707478 $707790$	$\begin{array}{c} 520 \\ 520 \end{array}$	$292522 \\ 292210$	59 58
$\tilde{3}$	657790	412	949688	108	708102	520	291898	57
4	658037	412	949623	108	708414	519	291586	56
5 6	658284 658531	$\begin{array}{c} 412 \\ 411 \end{array}$	$949558 \\ 949494$	$\frac{108}{108}$	708726 $709037$	519 519	$291274 \\ 290963$	55 54
7	658778	411	949429	108	709349	$\begin{array}{c} 519 \\ 519 \end{array}$	290651	53
8	659025	411	949364	108		519	290340	52
9	$\begin{array}{c} 659271 \\ 659517 \end{array}$	$\begin{array}{c} 410 \\ 410 \end{array}$	$949300 \\ 949235$	$\frac{108}{108}$	$709971 \\ 710282$	518 518	290029 $289718$	51
$\frac{10}{11}$	$\frac{059317}{9.659763}$	$\frac{410}{410}$	$\frac{949233}{9.949170}$	$\frac{108}{108}$		$\frac{518}{518}$	$\frac{289118}{10.289407}$	$\frac{50}{49}$
12	660009	409	949105	108	710904	518	289096	48
13	660255	409	949040	108	711215	518	288785	47
14	660501 $660746$	$\begin{array}{c c} 409 \\ 409 \end{array}$	$948975 \\ 948910$	$\frac{108}{108}$	711525 $711836$	517 517	$288475 \\ 288164$	46
15 16	660991	409	948845	108	711030	517	287854	45
17	661236	408	948780	109	712456	517	287544	43
18	661481	408	948715	109	712766	516	287234	42
19 20	661726 $661970$	$\begin{array}{c} 407 \\ 407 \end{array}$	$948650 \\ 948584$	$\begin{array}{c} 109 \\ 109 \end{array}$	$713076 \\ 713386$	$\begin{array}{c} 516 \\ 516 \end{array}$	$286924 \\ 286614$	$\begin{vmatrix} 41 \\ 40 \end{vmatrix}$
$\frac{20}{21}$	$\frac{001370}{9.662214}$	$\frac{407}{407}$	$\frac{9.948519}{9.948519}$	$\frac{100}{109}$	$\frac{7133696}{9.713696}$	$\frac{310}{516}$	$\frac{260014}{10.286304}$	$\frac{10}{39}$
$\frac{\tilde{2}}{22}$	662459	407	948454	109	714005	516	285995	
23	662703	406	948388	109	714314	515	285686	37
24 25	662946	406	$\begin{array}{c} 948323 \\ 948257 \end{array}$	$\begin{bmatrix} 109 \\ 109 \end{bmatrix}$	714624 $714933$	515	$285376 \ 285067$	36 35
26	$\begin{bmatrix} 663190 \\ 663433 \end{bmatrix}$	$\begin{array}{c c} 406 \\ 405 \end{array}$	948297 $948192$	109	714933	515 515	284758	34
27	663677	405	948126	109	715551	514	284449	33
28	663920	405	948060	109	715860	514	284140	32
29 30	664163 664406	$\begin{array}{c c} 405 \\ 404 \end{array}$	947995 $947929$	110 110	716168 $716477$	514 514	283832 283523	31 30
$\frac{30}{31}$	9.664648	404	$\frac{9.947863}{9.947863}$	$\frac{110}{110}$	9.716785	$\frac{-514}{514}$	$\overline{10.283215}$	$\frac{\overline{29}}{29}$
32	664891	404	947797	110	717093	513	282907	28
33	665133	403	947731	110	717401	513	282599	27
34 35	665375 665617	$\begin{array}{c c} 403 \\ 403 \end{array}$	947665 $947600$		717709 $718017$	513 513	$282294 \\ 281983$	26 25
36	665859	402	947533	110	718325	513	281675	24
37	666100		947467		718633	512	281367	23
38	666342 666583	$\begin{array}{c c} 402 \\ 402 \end{array}$	$\begin{array}{ c c c c c }\hline 947401 \\ 947335 \\ \hline \end{array}$	$\begin{array}{c c} 110 \\ 110 \end{array}$	$718940 \\ 719248$	512 512	$egin{array}{c} 281060 \ 280752 \end{array}$	
40	666824	401	947269	110		512	280445	
$\overline{41}$	9.667065	401	9.947203		$\overline{9.719862}$	512	10.280138	$\overline{19}$
42	667305	401	947136		720169	511	279831	18
43	$\begin{bmatrix} 667546 \\ 667786 \end{bmatrix}$	401	$\begin{array}{c c} 947070 \\ 947004 \end{array}$		720476 $720783$	511 511	279524 $279217$	17 16
45	668027	400	946937		721089	511	278911	15
46	-668267	490	946871	111	721396	511	278604	14
47	668506	399	946804		721702	510	278298	13
48 49	668746 668986	399	946738 $946671$	111	722009 $722315$	510 510	$\begin{vmatrix} 277991 \\ 277685 \end{vmatrix}$	12
50	669225	399	946604		722621	510	277379	10
$\overline{51}$	9.669464	398	9.946538		9.722927	510	$\boxed{10.277073}$	9
52	669703	398	946471	111	723232	509	276768	8
53 54	669942	$\frac{398}{397}$	$\begin{array}{c c} 946404 \\ 946337 \end{array}$		723538 $723844$	509 509	$276462 \\ 276156$	7 6
55	670419	397	946270			509	275851	5
56	670658	397	946203	112	724454	509	275546	4
57 58	670896		946136		724759	508	275241	3 2
59	671134	396	$\begin{array}{ c c c c c }\hline 946069 \\ 946002 \\ \end{array}$			508 508	274935 274631	1
60	671609		945935				274326	_
	Cosine	1	Sine	1	Cotang.	i	Tang.	M.
		1	1	1				

4(	(2	o Deg	rees.) A	TAI	RLE OF LO	GARIT	HMIC	
M	.   Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
1			19.945935				10.274323	
1			945868				27402]	
2	672084		945800			507	273716	
3			945733			507	273412	
4			945666			507	273108 272803	
5 6			945598 945531	112		507 507	272499	
7	673268		945351			506	272195	
8	673505		945396			506	271891	
9	673741		945328	113		506	271588	
10	673977		945261	113		506	271284	
11	9.674213	393	9.945193	113	9.729020	506	10.270980	49
12	674448		945125			505	270677	
13	674684		945058			505	270374	47
14	674919	392	944990	113		505	270071	46
15	675155	,	944922	113		505	269767	45
16	675390	391	944854	113		505	269465	
17	675624	391	944786	113	730838	504	269162	
18	675859		944718	113	731141	504	$268859 \\ 268556$	42
19 20	676094 676328	391	$\begin{array}{ c c c c c }\hline 944650 \\ 944582 \\ \hline \end{array}$	113	731444 731746	504	268254	41 40
74	1		.	114	·	$\frac{504}{504}$		
21	9.676562	390	9.944514	114	9.732048	504	10.267952	39
22	676796 677039	390	944446	114 114	732351	503	$267649 \\ 267347$	38 37
23 24	677264	$\begin{array}{c} 390 \\ 389 \end{array}$	$\begin{array}{c} 944377 \\ 944309 \end{array}$	114	732653 732955	503 503	267045	36
25	677498	389	944241	114	733257	503	266743	35
26	677731	389	944172	114	733558	503	266442	34
27	677964	388	944104	114	733860	502	266140	33
28	678197	388	944036	114	734162	502	265838	32
29	678430	388	943967	114	734463	502	265537	31
30	678663	388	943899	114	734764	502	265236	$\overline{30}$
$\overline{31}$	9 678895	387	9.943830	114	9.735066	502	10.264931	29
32	679128	387	943761	114	735367	502	264633	28
33	679360	387	943693	115	735668	501	264332	27
34	679592	387	943624	115	735969	501	$264031 \ 263731$	26 25
35 36	$679824 \\ 680056$	$\begin{array}{c} 386 \\ 386 \end{array}$	$   \begin{array}{r}     943555 \\     943486   \end{array} $	115 115	736269 736570	501 501	263430	24
37	680288	386	943417	115	736871	501	263129	23
38	680519	385	943348	115	737171	500	262829	22
39	680750	385	943279	115	737471	500	262529	21
40	680982	385	943210	115	737771	500	262229	20
41	9.681213	385	9.943141	115	$\overline{9.738071}$	500	10.261929	19
42	681443	384	943072	115	738371	500	261629	18
43	681674	384	943003	115	738671	499	261329	17
44	681905	384	942934	115	738971	499	261029	16
45	682135	384	942864	115	739271	499	260729	15
46	682365	383	942795	116	739570	499	260430	14
47	682595	383	942726	116	739870	499	260130	13
48 49	$\begin{array}{c c} 682825 \\ 683055 \end{array}$	383 383	$\begin{array}{c} 942656 \\ 942587 \end{array}$	116 116	740169 $740468$	499   498	$259831 \ 259532$	12 11
50	683284	382	942587 $942517$	116	740468	498 $498$	259233	10
$\frac{50}{51}$	$\frac{033204}{9.683514}$	-	$\frac{942317}{9.942448}$	-			$\frac{253233}{10.258934}$	$-\frac{1}{9}$
52	683743	382 382	9.942448	116 116	$\begin{array}{c c} 9.741066 \\ 741365 \end{array}$	498 498	258635	8
53	683972	$\frac{382}{382}$	942308	116	741363	498	258336	7
54	684201	381	942239	116	741962	497	258038	6
55	684430	381	942169	116	742261	497	257739	5
56	684658	381	942099	116	742559	497	257441	4
57	684887	380	942029	116	742858	497	257142	3
58	685115	380	941959	116	743156	497	256844	2
59	685343	380		117	743454	497	256546	1
60	685571	380	9418191	117	743752	496	256248	0
	Cosine	25	Sine	1	Cotang.	I	Tang.	M.
Name of Street,	THE RESERVE OF THE PERSON NAMED IN	-	THE PERSON NAMED IN COLUMN	-	The state of the s	-	-	The same of

4 M	Sine	D.	Cosine	D.	Tang.	( D.	Cotang.	1
		<u>1 380</u>	19.941819	<u>'</u>		496	10.256248	1 60
1	685799	379	941749	117	744050	496	255950	59
2 3		379	941679	117	744348	496	255652	
4		379	941609 $941539$	$\begin{vmatrix} 117 \\ 117 \end{vmatrix}$	744645 744943	$\begin{array}{c} 496 \\ 496 \end{array}$	$oxed{255355} 255057$	57 56
5	686709	378	941469	117	745240	496	254760	55
7		$\begin{array}{c} 378 \\ 378 \end{array}$	$941398 \\ 941328$	117	745538	495	254462	54
8		378	941328 $941258$	$\begin{array}{c} 117 \\ 117 \end{array}$	745835 $746132$	$\begin{array}{c} 495 \\ 495 \end{array}$	254165 $253868$	53 52
9	687616	377	941187	117	746429	495	253571	51
$\frac{10}{10}$	$\frac{687843}{687843}$	377	941117	117	746726	495	253274	50
11 12	9.688069	377 377	$\begin{array}{r} 9.941046 \\ 940975 \end{array}$	118 118	9.747023 $747319$	$\begin{array}{c} 494 \\ 494 \end{array}$	10.252977	49 48
13	688521	376	940905		747616	494	$252681 \\ 252384$	47
14	688747	376	940834	118	747913	494	252087	46
15 16	688972	$\begin{array}{c} 376 \\ 376 \end{array}$	$\begin{vmatrix} 940763 \\ 940693 \end{vmatrix}$	118 118	748209 $748505$	$\begin{array}{c} 494 \\ 493 \end{array}$	$251791 \ 251495$	45
17	689423	375	940622	118	748801	$\begin{array}{c} 493 \\ 493 \end{array}$	251495 251199	43
18	689648	375	940551	118	749097	493	250903	4.2
$\begin{array}{c c} 19 \\ 20 \end{array}$	689873	375 375	$940480 \\ 940409$	118 118	749393 $749689$	$\begin{array}{c} 493 \\ 493 \end{array}$	$250607 \\ 250311$	41 40
$\frac{20}{21}$	$\frac{030038}{9.690323}$	$\frac{373}{374}$	$\frac{940409}{9.940338}$	$\frac{118}{118}$	$\frac{749669}{9.749985}$	$\frac{493}{493}$	$\frac{250311}{10.250015}$	$\frac{40}{39}$
22	690548	374	940267	118	750281	$\begin{array}{c} 493 \\ 492 \end{array}$	249719	38
23	690772	374	940196	118	750576	492	249424	37
24 25	690996 691220	$\begin{array}{c} 374 \\ 373 \end{array}$	$   \begin{array}{r}     940125 \\     940054   \end{array} $	119 119	750872 751167	$\begin{array}{c} 492 \\ 492 \end{array}$	$egin{array}{c} 249128 \ 248833 \ \end{array}$	36 35
26	691444	373	939982	119	751462	492	248538	34
27	691668	373	939911	119	751757	492	248243	33
$\begin{array}{c} 28 \\ 29 \end{array}$	691892 692115	$\begin{array}{c} 373 \\ 372 \end{array}$	$939840 \\ 939768$	119 119	$\begin{array}{c} 752052 \\ 752347 \end{array}$	$\begin{array}{c} 491 \\ 491 \end{array}$	$egin{array}{c} 247948 \ 247653 \end{array}$	32 31
30	692339	$37\tilde{2}$	939697	113	752642	491	247053 $247358$	30
$\overline{31}$	9.692562	372	9.939625	119	$\overline{9.752937}$	491	$\overline{10.247063}$	$\overline{29}$
32 33	692785	371	939554	119	753231	491	246769	28
34	$\begin{bmatrix} 693008 \\ 693231 \end{bmatrix}$	$\begin{array}{c} 371 \\ 371 \end{array}$	$egin{array}{c} 939482 \ 939410 \ \end{array}$	119 119	$\begin{array}{c} 753526 \\ 753820 \end{array}$	$\begin{array}{c} 491 \\ 490 \end{array}$	$egin{array}{c} 246474 \ 246180 \ \end{array}$	27 26
35	693453	371	939339	119	754115	490	245885	25
36 37	693676	370	939267	120	754409	490	245591	24
38	$\begin{array}{ c c c c c } \hline 693898 \\ 694120 \\ \hline \end{array}$	$\begin{array}{c} 370 \\ 370 \end{array}$	$939195 \\ 939123$	$\frac{120}{120}$	754703 754997	$\begin{array}{c} 490 \\ 490 \end{array}$	$245297 \ 245003$	23 22
39	694342	370	939052	120	755291	490	244709	21
$\frac{40}{13}$	694564	369	-939980	$\frac{120}{}$	755585	489	244415	$\frac{20}{}$
$\frac{\overline{41}}{42}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{c} 369 \\ 369 \end{array}$	9.938908	120	9.755878	489	10.244122	19
43		369 369	$\begin{array}{c} 938836 \\ 938763 \end{array}$	$\frac{120}{120}$	756172 756465	489 489	$oxed{243828} \ 243535$	18 17
44	695450	368	938691	120	756759	489	243241	16
45 46	695671 695892	$\begin{array}{c} 368 \\ 368 \end{array}$	938619	120	757052	489	242948	15
47	696113	368 3€8	$\begin{array}{c} 938547 \\ 938475 \end{array}$	$\frac{120}{120}$	$757345 \ 757638$	488 488	$242655 \\ 242362$	13
48	696334	367	938402	121	757931	488	242069	12
4.9 50	696554 696775	$\begin{array}{c} 367 \\ 367 \end{array}$	938330	121	758224	488	241776	11
$\frac{30}{51}$	$\frac{696775}{9.696995}$	$\frac{367}{367}$	$\frac{938258}{9.938185}$	$\frac{121}{121}$	$\frac{758517}{9.758810}$	$\frac{488}{488}$	$\frac{241483}{10.241190}$	$\frac{10}{9}$
52	697215	366		121	759102	$\frac{488}{487}$	240898	8
53	697435	366	938040	121	759395	487	240605	7
54 55	697654	$\begin{array}{c} 366 \\ 366 \end{array}$	937967	121	759687	487	240313	6 5
56	698094	365	$937895 \\ 937822$	121 121	759979 760272	$\begin{array}{c} 487 \\ 487 \end{array}$	$240021 \ 239728$	4
57	698313	365	937749	121	760564	487	239436	3
58 59	698532 698751	365 365	937676	121	760856	486	239144	2
60	698970	364	$\begin{array}{c} 937604 \\ 937531 \end{array}$	$\frac{121}{121}$	761148 761439	$\begin{array}{c c} 486 \\ 486 \end{array}$	238852 $238561$	1.0
-	Cosine		Sine		Cotang.		Tang.	M.
_			Sino		Cottang.		Tung.	-

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	-
0	9.698970	364	9.937531	121	9.761439	486	10.238561	60
1	699189	364	937458	$\tilde{1}\tilde{2}\tilde{2}$	761731	486	238269	59
2	699407	364	937385		762023	486	237977	58
3	699626	364	937312		762314	486	237686	57
4	699844	363	937238	122	762606	485	237394	56.
5	700062	363	937165	122	762897	485	237103	55
6	700280	363	937092	122	763188	485	236812	54
7	700498	363	937019	122	763479	485	236521	53
8	700716	363	936946	122	763770	485	236230	52
9	700933	362	936872		764061	485	235939	51
10	701151	362	936799	$\frac{122}{}$	-764352	484	235648	50
11	9.701368	362	9.936725	122	9.764643	484	10.235357	49
12	701585	362	936652	123	764933	484	235067	48
13	$701802 \\ 702019$	361	936578	123	765224	484	234776	47
14 15	702019	361	936505	123	765514	484	234486	46
16	702452	361 $361$	$936431 \\ 936357$	$\begin{array}{c} 123 \\ 123 \end{array}$	765805 $766095$	484 484	234195	45
17	702669	360	936284		766385	483	233905	44
18	702885	360	936210	123	766675	$\begin{array}{c c} 463 \\ 483 \end{array}$	233615 $233325$	43
19	703101	360	936136	123	766965	483	233035	42 41
20	703317	360	936062	123	767255	483	232745	41 40
$\frac{21}{21}$	$\overline{9.703533}$	359	9.935988	$\frac{120}{123}$	$\frac{767505}{9.767545}$	483		
$\frac{21}{22}$	703749	359	935914		767834		10.232455	39
23	703964	359	935840	123	768124	482	$232166 \\ 231876$	38 37
24	704179	359	935766		768413		$\frac{231570}{231587}$	36
25	704395	359	935692	124	768703		$\frac{231367}{231297}$	35
26	704610	358	935618	124	768992		231008	34
27	704825	358	935543	124	769281	482	230719	33
28	705040	358	935469	124	769570	482	230430	32
29	705254	358	935395	124	769860	481	230140	31
30	705469	357	935320	124	770148	481	229852	30
$\overline{31}$	9.705683	357	9.935246	124	9.770437	481	10.229563	$\overline{29}$
32	705898	357	935171	124	770726	481	229274	28
33	706112	357	935097	124	771015	481	228985	27
34	706326	356	935022	124	771303		228697	26
35	706539	356	934948	124		481	228408	25
36	706753	356	934873		771880	4.80	228120	24
37	706967	356	934798	125	772168		227832	23
38	707180	355	934723		772457		227543	22
39	707393 707606	355	934649		772745		227255	21
$\frac{40}{11}$	1	355	$\frac{934574}{2}$		773033		-226967	20
41	9.707819	355	9.934499	125	9.773321	480	10.226679	19
42	708032	354	934424		773608		226392	18
43	708245 708458	354	934349	125			226104	17
44 45	708458 $708670$		934274				225816	16
46	708882		$oxed{934199} 934123$		774471 774759	479	225529	15
47	709094		934048			$\begin{array}{ c c c }\hline 479\\ 479\end{array}$	$egin{array}{c} 225241 \ 224954 \ \end{array}$	14
48	709306	353	933973				$224954 \\ 224667$	13 12
49	709518	353	933898				224379	11
50	709730	353	933822	126	775908	478	224092	10
$\overline{51}$	9 709941	352	9.933747	·			$\frac{224002}{10.223805}$	$\frac{10}{9}$
52	710153	352	933671	126			223518	8
53	710364	352	933596				223231 223231	7
54	710575	352	933520		777055		222945	6
55	710786	351	933445		777342		222658	5
56	710997	351	933369		777628		222372	4
57	711208	351	933293	126	777915		222085	3
58	711419		933217		778201	477	221799	2
59	711629	350	933141	126			221512	1
60	711839	350	933066	126	778774	477	221226	0
	Cosine		Sine		Cotang.		{ Tang.	M.
-			1		- (3	1	1	

	G: 1		0 .	-	1 03 1	7		
M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	$oxed{9} egin{array}{c} 711839 \ 712050 \ \end{array}$	350	$oxed{9.933066} \ oxed{932990}$	$\frac{126}{127}$	$9.778774 \\ 779060$	477 477	$\begin{bmatrix} 10.221226 \\ 220940 \end{bmatrix}$	60 59
$\begin{vmatrix} 1\\2 \end{vmatrix}$	712050 $712260$	$\begin{array}{c} 350 \\ 350 \end{array}$	932990 $932914$	$\frac{127}{127}$	779346	176	220940 220654	58
3	712469	349	932838	127	779632	476	$\frac{220034}{220368}$	57
4	712679	349	932762	$\tilde{1}\tilde{2}7$	779918	476	220082	56
5	712889	349	932685	127	780203	476	219797	55
6	713098	349	932609	127	780489	476	219511	54
7	713308	349	932533	127	780775	476	219225	53
8	713517	348	932457	127	781060	476	218940	52
9	$713726 \ 713935$	$\begin{array}{c} 348 \\ 348 \end{array}$	$932380 \ 932304$	$\frac{127}{127}$	781346 $781631$	475	$218654 \\ 218369$	51 50
						475		
11 12	$\begin{vmatrix} 9.714144 \\ 714352 \end{vmatrix}$	$\begin{array}{c} 348 \\ 347 \end{array}$	9.932228 $932151$	$\begin{array}{c} 127 \\ 127 \end{array}$	$9.781916 \\ 782201$	475 475	$10.218084 \ 217799$	49 48
13	714552	$\begin{bmatrix} 347 \\ 347 \end{bmatrix}$	932131	128	782486	475	$\frac{217533}{217514}$	47
14	714769	347	931998	128	782771	475	217229	46
15	714978	347	931921	$\tilde{1}\tilde{2}8$	783056	475	216944	45
16	715186	347	931845	128	783341	475	216659	44
17	715394	346	931768	128	783626	474	216374	43
18	715602	346	931691	128	783910	474	216090	42
19	715809	346	931614	128	784195	474	215805	41 40
$\frac{20}{27}$	$\frac{716017}{0.0016024}$	346	$\frac{931537}{2001400}$	$\frac{128}{1000}$	784479	474	$\frac{215521}{100000000000000000000000000000000000$	
21 22	$9.716224 \\ 716432$	345	9.931460	128 128	9.784764		$\begin{array}{r} 10.215236 \\ 214952 \end{array}$	39 38
23	716432 $716639$	$\begin{array}{c} 345 \\ 345 \end{array}$	$931383 \\ 931306$	$\frac{128}{128}$	785048 785332	474 473	214668	37
24	716846	345	931229	129	785616	473	214384	36
25	717053	345	931152	129	785900	473	214100	35
26	717259	344	931075	129	786184		213816	34
27	717466	344	930998	129	786468		213532	33
28	717673	344	930921	129	786752	473	213248	32
29	717879	344	930843	129	787036		212964	31
$\frac{30}{30}$	718085	343	930766	129	787319	472	$\frac{212681}{2120000000000000000000000000000000000$	$\frac{30}{30}$
31	9.718291	343	9.930688	129	9.787603	472	10.212397	29
32	718497 718703	343	$930611 \\ 930533$	129	787886 788170		212114 $211830$	28 27
33 34	718909	$\begin{array}{c c} 343 \\ 343 \end{array}$	930456	$\begin{array}{c} 129 \\ 129 \end{array}$	788453	472 472	211547	26
35	719114	342	930378	ž	788736		211264	25
36	719320	342	930300	130	789019		210981	24
37	719525	342	930223	130	789302		210698	
38	719730	342	930145	130			210415	
39	719935	341	930067	130	789868		210132	
40	$\frac{720140}{}$	341	929989	$\frac{130}{130}$		471	209849	
41	9.720345	341	9.929911	130	9.790433	471	10.209567	
42	720549	341	929833		790716		209284	18
43 44	720754 720958	$\begin{array}{c c} 340 \\ 340 \end{array}$	$\begin{array}{c} 929755 \\ 929677 \end{array}$	$\begin{array}{ c c }\hline 130\\130\end{array}$	790999 $791281$	471	$209001 \\ 208719$	
44	720938	340	929577	$130 \\ 130$			208437	15
46	721366	340	929521	130	791846	470	208154	14
47	721570	340	929442	130	792128		207872	
48	721774	339	929364	131	792410	470	207590	12
49	721978	339	929286	131	792692		207308	11
50	722181	339	929207	131	792974	·	207026	10
$\overline{51}$	$9.72\overline{2385}$	339	9.929129	131	9.793256	470	10.206744	9
52	722588	339	929050	131	793538	469	206462	8
53	722791	338	928972	131	793819	469	206181	6
54 55	722994 723197	$\begin{array}{c} 338 \\ 338 \end{array}$	$\begin{array}{c} 928893 \\ 928815 \end{array}$	131 131	794101 $794383$	$\begin{array}{c} 469 \\ 469 \end{array}$	$\begin{vmatrix} 205899 \\ 205617 \end{vmatrix}$	5
56	723197	338	928736		794664		205336	4
57	723603	337	928657	131	794945		205055	3
58	723805	337	928578	131	795227		204773	2
59	724007	337	928499	131	795508	468	204492	1
60	724210	337	928420	131	795789	468	204211	0
	Cosine		Sine		Cotang.	1	Tang.	M.
1	-							-

		e inegr			DI OF LC	,		-
M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.724210	337	9.928420	132		468	10.204211	60
1	724412	337	928342	$\frac{132}{132}$	796070 796351	468 468	$\begin{array}{c} \cdot & 203930 \\ 203649 \end{array}$	59 58
2	724614	$\begin{array}{c} 336 \\ 336 \end{array}$	928263 $928183$		796632	468	203368	57
$\begin{bmatrix} 3 \\ 4 \end{bmatrix}$	724816 $725017$	336	928104	132	796913	468	203087	56
5	725219	336	928025	132	797194	468	202806	55
6	$7\widetilde{2}\widetilde{5}\widetilde{4}\widetilde{2}\widetilde{0}$	335	927946	132	797475	468	202525	54
7	725622	335	927867	132	797755	468	202245	53
8	725823	335	927787	132	798036	467	201964	52
9	726024	335	927708	132	798316	467	$201684 \\ 201404$	51 50
10	-726225	335	927629	132	798596	467		
11	9.726426	334	9.927549	132	9.798877	467	10.201123 $200843$	49 48
12	726626	$\begin{array}{c c} 334 \\ \hline 334 \end{array}$	$927470 \ 927390$	133 133	799157 $799437$	$\begin{array}{c} 467 \\ 467 \end{array}$	200563	47
13	726827 $727027$	$\frac{534}{334}$	927390 $927310$	133	799717	467	200283	46
14	727228	334	927231	133	799997	466	200003	45
16	$7\overline{2}7\overline{4}28$	333	927151	133	800277	466	199723	44
17	727628	333	927071	133	800557	466	199443	43
18	727828	333	926991	133	800836	466	199164	42
19	728027	333	926911	133	801116	466	$198884 \\ 198604$	41 40
20	728227	333	926831	$\frac{133}{2}$	801396	466		
21	9.728427	332	9.926751	133	9.801675	466	10.198325 $198045$	39 38
22	728626	332	926671	133 133	$801955 \\ 802234$	466 465	197766	37
23	728825 $729024$	$\begin{array}{c} 332 \\ 332 \end{array}$	$\begin{array}{c} 926591 \\ 926511 \end{array}$	134	802513	465	197487	36
24 25	729024 $729223$	331	926431	134	802792	465	197208	35
26	729422	331	926351	134	803072	465	196928	34
27	729621	331	926270	134	803351	465	196649	33
28	729820	331	926190	134	803630	465	196370	32
29	730018	330	926110	134	803908	465	196092 $195813$	$\frac{31}{30}$
30	730216	330	$\frac{926029}{}$	$\frac{134}{134}$	804187	465		
31	9.730415	330	9.925949	134	9.804466	464	$10.195534 \\ 195255$	29 28
32	730613	330	$\begin{array}{c} 925868 \\ 925788 \end{array}$	$\begin{array}{c} 134 \\ 134 \end{array}$	$804745 \\ 805023$	$\begin{array}{c} 464 \\ 464 \end{array}$	193253 $194977$	27
33	730811 731009	$\begin{array}{c} 330 \\ 329 \end{array}$	925707		805302	464	194698	26
35	731206	329	925626		805580	464	194420	25
36	731404	329	925545		805859	464	194141	24
37	731602	329	925465		806137	464	193863	23
38	731799	329	925384	135	806415	463	193585	22
39	731996	328	925303		$806693 \\ 806971$	$\begin{array}{c} 463 \\ 463 \end{array}$	193307 $193029$	$\begin{vmatrix} 21\\20 \end{vmatrix}$
$\frac{40}{1}$	$\frac{732193}{20000}$	$\frac{328}{200}$	$\frac{925222}{0.005141}$					$\frac{20}{19}$
41	9.732390	$\frac{328}{298}$	9.925141 $925060$	135 135	$9.807249 \\ 807527$	$\begin{array}{c} 463 \\ 463 \end{array}$	$10.192751\\192473$	18
42 43	732587 732784	$\begin{array}{c} 328 \\ 328 \end{array}$	$925000 \\ 924979$	135	807805	463	192195	17
44	732980	327	924897	135	808083	463	191917	16
45	733177	327	924816	135	808361	463	191639	15
46	733373	327	924735	136	808638	462	191362	14
47	733569	327	924654		808916	462	191084	
48	733765	327	924572		809193	462	$\begin{array}{c} 190807 \\ 190529 \end{array}$	12
49	733961	$\begin{array}{c} 326 \\ 326 \end{array}$	$\begin{array}{c} 924491 \\ 924409 \end{array}$	$\begin{array}{c} 136 \\ 136 \end{array}$	$809471 \\ 809748$	$\begin{array}{c} 462 \\ 462 \end{array}$	190529 $190252$	10
$\frac{50}{51}$	734157			-	$\frac{809748}{9.810025}$	$\frac{462}{462}$	$\frac{130232}{10.189975}$	$\frac{10}{9}$
51	9.734353 $734549$	$\begin{array}{c} 326 \\ 326 \end{array}$	9.924328 $924246$	136 136	9.810025 $810302$	$\begin{array}{c} 462 \\ 462 \end{array}$	189698	8
52 53	734549	$\begin{array}{c} 320 \\ 325 \end{array}$	924240 $924164$		810580	462	189420	8
54	734939	325	924083		810857	462	189143	6
55	735135	325	924001	136	811134	461	188866	5
56	735330	325	923919	136	811410	461	188590	4
57	735525	325	923837	136	811687	461	188313	3
58	735719	324	923755	137	$811964 \\ 812241$	$\begin{array}{c} 461 \\ 461 \end{array}$	188036 $187759$	2
59	735914 736109	$\begin{array}{c c} 324 \\ 324 \end{array}$	$\begin{array}{r} 923673 \\ 923591 \end{array}$	$\begin{array}{c} 137 \\ 137 \end{array}$	$812241 \\ 812517$		187789	
60		1 1)24		191		- TO (		
	Cosine		Sine		Cotang.		Tang.	M.

57 Degrees.

Tar.	G:	l p		l D	l m	l D		
M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	$\begin{vmatrix} 9.736109 \\ 736303 \end{vmatrix}$	$\begin{array}{c c} 324 \\ 324 \end{array}$	$\begin{array}{r} 9.923591 \\ 923509 \end{array}$	137   137		461 461	10.187482	
2	736498	324	923427	137		$\begin{array}{c} 401 \\ 461 \end{array}$	186930	59 58
$\tilde{3}$	736692	323	923345	137	813347	460	186653	57
4	736886	323	923263	137	813623	460	186377	56
5	737080	323	923181	137	813899	460	186101	55
6 7	737274 $737467$	$\begin{array}{c} 323 \\ 323 \end{array}$	923098 923016	137 137	814175 814452	$\begin{array}{c} 460 \\ 460 \end{array}$	185825 185548	54 53
8	737661	322	922933	137	814728	460	185272	52
9	737855	322	922851	137	815004	460	184996	51
10	738048	322	922768	138	815279	460	184721	50
11	9.738241	322	9.922686	138	9.815555	459	10.184445	49
12 13	738434	322	922603	138	815831	459	184169	48
14	738627 738820	$\begin{array}{c} 321 \\ 321 \end{array}$	$\begin{array}{c} 922520 \\ 922438 \end{array}$	138 138	$816107 \\ 816382$	$\begin{array}{c} 459 \\ 459 \end{array}$	183893 183618	47
15	739013	321	922355	138	816658	459	183342	45
16	739206	321	922272	138	816933	459	183067	44
17	739398	321	922189	138	817209	459	182791	43
18	739590 739783	$\begin{array}{c} 320 \\ 320 \end{array}$	$\begin{array}{c} 922106 \\ 922023 \end{array}$	138 138	817484 817759	$\begin{array}{c} 459 \\ 459 \end{array}$	$182516 \\ 182241$	42 41
20	739975	$\begin{array}{c} 320 \\ 329 \end{array}$	$\begin{vmatrix} 322023 \\ 921940 \end{vmatrix}$	138	818035	458	181965	40
$\overline{21}$	$9.74\overline{0167}$	320	$\frac{9.921857}{1}$	$\frac{139}{139}$	$\frac{318330}{9.818310}$	$\frac{150}{458}$	10.181690	$\frac{2}{39}$
22	740359	320	921774	139	818585	458	181415	38
23	740550	319	921691	139	818860	458	181140	37
24 25	740742	319	921607	139	819135	458	180865	36 35
26	740934 741125	$\begin{array}{c} 319 \\ 319 \end{array}$	$921524 \\ 921441$	$\frac{139}{139}$	819410 819684	458 458	$180590 \\ 180316$	34
27	741316	319	921357	139	819959	458	180041	33
28	741508	318	921274	139	820234	458	179766	32
29	741699	318	921190	139	820508	457	179492	31
$\frac{30^{4}}{21}$	741889	318	921107	$\frac{139}{190}$	820783	457	179217	$\frac{30}{20}$
$\begin{array}{c} 31 \\ 32 \end{array}$	$oxed{9.742080}{742271}$	$\begin{array}{c} 318 \\ 318 \end{array}$	$\begin{array}{c} 9.921023 \\ 920939 \end{array}$	$\frac{139}{140}$	$9.821057 \\ 821332$	$\begin{array}{c} 457 \\ 457 \end{array}$	10.178943	29 28
33	742462	317	920856	140	821606	457	178394	27
34	742652	317	920772	140	821880	457	178120	26
35	742842	317	920688	140	822154	457	177846	25
$\begin{array}{c} 36 \\ 37 \end{array}$	$\begin{array}{c c} 743033 \\ 743223 \end{array}$	317	$\begin{array}{c} 920604 \\ 920520 \end{array}$	140 140	822429 $822705$	$\begin{array}{c} 457 \\ 457 \end{array}$	177571 $177297$	24 23
38	743413	$\begin{array}{c} 317 \\ 316 \end{array}$	920436	140	822977	456	177023	22
39	743602	\$16	920352		823250	456	176750	21
$     \begin{array}{r}       36 \\       37 \\       38 \\       39 \\       \hline       40 \\       \hline       41     \end{array} $	743792	316	920268		823524	456	176476	20
41	9.743982	316	9.920184	$\overline{140}$	9.823798	456	10.176202	19
42 43	744171	316	920099	140	824072	456	175928	18 17
44	744361 744550	$\begin{array}{c} 315 \\ 315 \end{array}$	$egin{array}{c} 920015 \ 919931 \ \end{array}$	140	$824345 \\ 824619$	$\begin{array}{c} 456 \\ 456 \end{array}$	$175655 \\ 175381$	16
45	744739	315	919846	141	824893	456	175107	15
46	744928	315	919762	141	825166	456	174834	14
47	745117	315	919677	141	£25439	455	174561	13
48 49	745306 745494	314	919593 $919508$	141 141	825713 $825986$	455 455	174287 $174014$	12 11
50	745494	314	919424		826259	455	173741	10
$\overline{51}$	$\frac{710000}{9.745871}$	314	9.919339	$\frac{1}{141}$	$\frac{3.826532}{9.826532}$	$-\frac{1}{455}$	10.173468	$\frac{-9}{9}$
52	746059	314	919254	141	826805	455	173195	8
53	746248	313	919169	141	827078	455	172922	7
54. 55	746436	313	919085	141	827351	455	$\frac{172649}{172376}$	5
56	746624 746812	313 313	$9190000 \\ 918915$	141 142	$\frac{827624}{827897}$	455 ° 454	172370 $172103$	4
57	746999	313	918830	142	828170	454	171830	3
58	747187	312	918745	142	823442	454	171558	2
59 60	747374	312	918659	142	828715	454	171285	10
1001	747562	312	918574	142	828987	454	171013	
	Cosine		Sine		Cotang.		Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.747562	312	*		9.828987		10.17f043	60
1	747749	312	918489	142	829260	454	170740	60 59
$\hat{2}$	747936	312	918404	142	829532	454	170468	58
3	748123	311	918318	142	829805	454	170195	57
4	748310	311	918233	142	830077	454	169923	56
5	748497	311	918147	142	830349	453	169651	55
6	748683	311	918062	142	830621	453	169379	54
7	748870	311	917976	143	830893	453	169107	53
8	749056	310	917891	143	831165	453	168835	52
9 10	749243 749429	$\frac{310}{310}$	917805 $917719$	143	831437	453	168563	$\frac{51}{50}$
1				$\frac{143}{143}$	831709	453	168291	$\frac{50}{}$
11	9.749615	310	9.917634	143	9.831981	453	10.168019	49
12 13	$749801 \\ 749987$	$\begin{array}{c} 310 \\ 309 \end{array}$	$917548 \\ 917462$	$\frac{143}{143}$	832253	453	167747	48
14	750172	309	917376	143	832525 $832796$	$\begin{array}{c} 453 \\ 453 \end{array}$	$167475 \ 167204$	47
15	750358	309	917290	143	833068	$\begin{array}{c} 455 \\ 452 \end{array}$	167204	46 45
16	750543	309	917204	143	833339	452	166561	44
17	750729	309	917118	144	833611	452	166389	43
18	750914	308	917032	144	833882	452	166118	42
19	751099	308	916946	144	834154	452	165846	41
20	751284	308	916859	144	834425	452	165575	40
$\overline{21}$	9.751469	308	9.916773	144	9.834696	452	10.165304	$\overline{39}$
22	751654	308	916687	144	834967	452	165033	38
23	751839	308	916600	144	835238	452	164762	37
24	752023	307	916514	144	835509	452	164491	36
25	752208	307	916427	144	835780	451	164220	35
26 27	752392 752576	$\begin{array}{c} 307 \\ 307 \end{array}$	$916341 \\ 916254$	144	836051	451	163949	34
28	752760	307	$916354 \\ 916167$	144 145	836322 $836593$	451	163678	33
29	752944	306	916081	145	836864	451 451	$163407 \\ 163136$	32
30	753128	306	915994	145	837134	451	162866	30
$\frac{33}{31}$	$\frac{75313}{9.753312}$	$\frac{306}{306}$	$\frac{9.915907}{9.915907}$	$\frac{1}{145}$	$\frac{037131}{9.837405}$	$\frac{451}{451}$	$\frac{102500}{10.162595}$	$\frac{30}{29}$
$\frac{31}{32}$	753495	306	915820	145	837675	451	162325	28
33	753679	306	915733	145	837946	451	162054	27
34	753862	305	915646	145	838216	451	161784	26
35	754046	305	915559	145	838487	450	161513	25
36	754229	305	915472	145	838757	450	161243	24
37	754412	305	915385	145	839027	450	160973	23
38	754595	305	915297	145	839297	450	160703	22
$\begin{bmatrix} 39 \\ 40 \end{bmatrix}$	754778 754960	304	915210	145	839568 $839838$	450	160432	21
		304	$\frac{915123}{2005005}$	$\frac{146}{146}$		450	160162	$\frac{20}{10}$
41	9.755143	$\begin{array}{c} 304 \\ 304 \end{array}$	9.915035	146	9.840108	450	10.159892	19
42 43	755326 755508	$\begin{array}{c} 304 \\ 304 \end{array}$	$egin{array}{c} 914948 \ 914860 \ \end{array}$	$\frac{146}{146}$	$840378 \ 840647$	$\begin{array}{c} 450 \\ 450 \end{array}$	159622	18 17
44	755690	304	914300	146	840917	$\begin{array}{c} 450 \\ 449 \end{array}$	159353 $159083$	16
45	755872	303	914685	145	841187	449	158813	15
46	756054	303	914598	146	841457	449	158543	14
47	756236	303	914510	146	841726	449	158274	13
48	756418	303	914422	146	841996	449	158004	12
49	756600	303	914334	146	842266	449	157734	11
$\frac{50}{}$	756782	302	914246	147	842535	449	157465	10
$\overline{51}$	9.756963	302	9.914158	147	9.842805	449	10.157195	3
52	757144	302	914070	147	843074	449	156926	8
53	757326	302	913982	147	843343	449	156657	7
54	757507	302	913894	147	843612	449	156388	6
55 56	757688	301	913806	147	843882	448	156118	5
57	757869 758050	$\begin{array}{c} 301 \\ 301 \end{array}$	913718   913630	$\frac{147}{147}$	$844151 \\ 844420$	448 448	155849	4 3
58	758230	301	913530	147	844420	448	$155580 \ 155311$	2
59	758411	301	913453	147	844958	448	155042	1
60	758591	301	913365	147	845227	448	154773	Ö
	Cosine		Sine	1	Cotang.		Tang.	M.
	Cosme	}	Sinc	-	Cottang.		rang.	17.5

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.758591	301	9.913365	147	9.845227	448	10.154773	60
$\begin{array}{c c} 1 \\ 2 \end{array}$	758772 $758952$	$\frac{300}{300}$	913276 $913187$	147	$845496 \\ 845764$	448 448	$154504 \\ 154236$	59 58
$\tilde{3}$	759132	300	913699	148	846033	448	153967	57
4	759312	300	913010	148	846302	448	153698	56
5	759492	300	912922	148	$egin{array}{c} 846570 \ 846839 \ \hline \end{array}$	447	153430	55
6 7	759672 $759852$	$\begin{array}{c} 299 \\ 299 \end{array}$	912833 $912744$	148 148	847107	447 447	$153161 \ 152893$	54 53
8	760031	299	912655	148	847376	447	152624	52
9	760211	299	912566	148	847644	447	152356	51
10	760390	299	$\frac{912477}{2}$		847913	447	152087	50
11 12	9.760569 $760748$	298 298	$9.912388 \\ 912299$	148 149	$9.848181 \\ 848449$	447 447	10.151819	49
13	760927	298	912299 $912210$	149	848717	447	$151551 \ 151283$	48 47
14	761106	298	912121	149	848986	447	151014	46
15	761285	298	912031	149	849254	447	150746	45
16 17	761464 $761642$	298 297	$911942 \\ 911853$	149 149	$849522 \\ 849790$	$\begin{array}{r} 447 \\ 446 \end{array}$	150478 $150210$	44 43
18	761821	297	911763	149	850058	446	149942	42
19	761999	297	911674	149	850325	446	149675	41
$\frac{20}{}$	762177	297	-911584	$\frac{149}{}$	850593	446	149407	40
21	9.762356	297	9.911495	149	9.850861	446	10.149139	39
22 23	$762534 \ 762712$	$\begin{array}{c} 296 \\ 296 \end{array}$	$911405 \\ 911315$	149 150	$851129 \ 851396$	$\begin{array}{c} 446 \\ 446 \end{array}$	148871 148604	38
24	762889	296	911226	150	851664	446	148336	36
25	763067	296	911136	150	851931	446	148069	35
26	763245	296	911046	150	852199	446	147801	34
27 28	$763422 \\ 763600$	$\begin{array}{c} 296 \\ 295 \end{array}$	$910956 \\ 910866$	150 150	$oxed{852466} 852733$	446 445	$147534 \ 147267$	33 32
$\begin{vmatrix} 20 \\ 29 \end{vmatrix}$	763777	295	910776	150	853001	445	146999	31
30	763954	295	910686	150		445	146732	30
$\overline{31}$	9.764131	295	9.910596	150	9.853535	445	10.146465	$\overline{29}$
32	764308	295	910506	150	853802	445	146198	28
33 34	764485 764662	$\begin{array}{c} 294 \\ 294 \end{array}$	910415 $910325$	$  150 \\   151  $	854069 854 <b>3</b> 36	445 445	$145931 \\ 145664$	27 26
35	764838	294	910235		854603	445	145397	25
36	765015	294	910144	151	854870	445	145130	24
37 38	765191 765367	$\begin{array}{c} 294 \\ 294 \end{array}$	910054 $909963$	151 151	855137 $855404$	$\begin{array}{c} 445 \\ 445 \end{array}$	$144863 \\ 144596$	23 22
39	765544	293	909873		855671	444	144329	21
40	765720	293	909782		855938	444	144062	20
$\overline{41}$	9.765896	293	9.909691	$\overline{151}$	9.856204	444	$\overline{10.143796}$	$\overline{19}$
42	766072	293	909601	151	856471	444	143529	18
43 44	$766247 \\ 766423$	$\begin{array}{c} 293 \\ 293 \end{array}$	$\begin{vmatrix} 909510 \\ 909419 \end{vmatrix}$	151 151	856737 $857004$	444 444	$\begin{array}{c c} & 143263 \\ & 142996 \end{array}$	17 16
45	766598	292	909328	152	857270	444	142730	15
46	766774	292	909237	152	857537	444	142463	14
47	766949	292	909146			444 444	142197 $141931$	13 12
48 49	767124 $767300$	$\begin{array}{c c} 292 \\ 292 \end{array}$	$\begin{vmatrix} 909055 \\ 908964 \end{vmatrix}$			444	141951	11
50	767475	291	908873			443	141398	10
$\frac{1}{51}$	9.767649	291	9.908781	$\overline{152}$	9.858868	443	10.141132	9
52	767824	291	908690	152	859134	443	140866	8
53	767999	291	908599			443 443	140600 140334	7
54 55	$768173 \\ 768348$	291 290	908507 $908416$		859932	443	140068	6 5
56	768522	290	908324		860198	443	139802	4
57	768697	290	908233			443	139536	3
58 59	768871 769045	290	908141	153 153		443	$\begin{array}{ c c c c c }\hline & 139270 \\ & 139005 \\ \hline \end{array}$	2
60	769045		908049				138739	
	Cosine	700		1	Cotang.		Tang.	M.
	Cosine		Sine		Cotang.		Tang.	11

				(OOS.) A	,	LE OF E	1		-
:	M.		D.	Cosine	D.	Tang.	D.	Cotang.	
ı	0	$\begin{bmatrix} 9.769219 \\ 769393 \end{bmatrix}$		9.907958			443	10.138739	
Н	2	769566	289	907866	153 153			$\begin{array}{ c c c c }\hline & 138473 \\ & 138208 \\ \hline \end{array}$	59 58
1	3	769740	289	907682	153			137942	57
t	4	769913	289	907590	153	862323	442	137677	56
	5	770087	289	907498	153		442	137411	55
П	67	770260 770433	288 288	$907406 \\ 907314$	$\begin{array}{ c c }\hline 153\\154\end{array}$	862854 863119	442	137146	54
ı	8	770606	288	907222	154		$\begin{array}{c c} 442 \\ 442 \end{array}$	136881 136615	53 52
ı	9	770779	288	907129	154	863650	442	136350	51
	10	770952	288	907037	154	863915	442	136985	50
	11	9.771125	288	9 906945	154		442	10.135820	49
	12 13	771298	287	906852	154		442	135555	
	14	771470 771643	$\begin{array}{c} 287 \\ 287 \end{array}$	906760 906667	$\frac{154}{154}$	$864710 \\ 864975$	442	135290	47
	15	771815	287	906575	154	865240	441 441	$oxed{135025} 134760$	46 45
	16	771987	287	906482	154	865505	441	134495	44
	17	772159	287	906389	155	865770	441	134230	43
	18 19	772331	286	906296	155	866035	441	133965	42
	20	772503 772675	$\begin{array}{c} 286 \\ 286 \end{array}$	$906204 \\ 906111$	155 155	$866300 \\ 866564$	441	133700	41
	21	$\frac{2019}{9.772847}$	$\frac{286}{286}$	$\frac{300111}{9.906018}$	$\frac{155}{155}$	$\frac{866364}{9.866829}$	441	$\frac{133436}{10129171}$	$\frac{40}{30}$
	22	773018	$\frac{280}{286}$	9.995018	155	9.866829 $867094$	441 441	10.133171 $132906$	39 38
2	23	773190	286	905832	155	867358	441	132642	37
	4	773361	285	305739	155	867623	441	132377	36
	25   26	773533	285	905645	155	867887	441	132113	35
	7	773704 773875	$\begin{array}{c} 285 \\ 285 \end{array}$	905552 $905459$	155 155	$868152 \\ 868416$	440 440	$131848 \\ 131584$	34
	8	774046	285	905366	156	868680	440	131384 $131320$	33 32
	29	774217	285	905272	156	868945	440	131055	31
	0	774388	284	905179	156	869209	440	130791	30
	1	9.774558	284	9.905085	156	9.869473	440	10.130527	$\overline{29}$
	3	774729 774899	284	904992	156	869737	440	130263	28
	4	775070	284 284	$904898 \\ 904804$	156 156	870001 870265	$\begin{array}{c} 440 \\ 440 \end{array}$	$\frac{129999}{129735}$	27 26
3	5	775240	284	904711	156	870529	440	$\frac{129755}{129471}$	25
	C	775410	283	904617	156	870793	44()	129207	24
	7 8	775580	283	904523	156	871057	440	128943	23
	9	775750 775920	$\begin{array}{c c} 283 \\ 283 \end{array}$	904429 904335	157 157	871321 871585	$\begin{array}{c c} 440 \\ 440 \end{array}$	128679	22
	ŏ	776090	283	904241	$\frac{157}{157}$	871849	439	$\begin{array}{c} 128415 \\ 128151 \end{array}$	21 20
4	1	9.776259	283	9.904147	157	$\frac{3.1013}{9.872112}$	$\frac{-439}{439}$	$\frac{123131}{10.127888}$	$\frac{20}{19}$
4	2	776429	282	904053	157	872376	439	127624	18
	$\frac{3}{4}$	776598	282	903959	157	872640	439	127360	17
	5	$\frac{776768}{776937}$	282 282	903864	157	872903	439	127097	16
	6	777106	282	$   \begin{array}{c c}     903770 \\     903676   \end{array} $	157 157	873167 873430	$\begin{array}{c c} 439 \\ 439 \end{array}$	$\frac{126833}{126570}$	15 14
4	7	777275	281	903581	157	873694	$\begin{array}{c} 439 \\ 439 \end{array}$	126306	13
	8	777444	281	903487	157	873957	439	126043	12
	$\begin{vmatrix} 9 \\ 0 \end{vmatrix}$	777613	281	903392	158	874220	439	125780	11
	$\frac{0}{1}$	777781	$\frac{281}{201}$	903298	158	874484	439	125516	10
	$\begin{vmatrix} 1 \\ 2 \end{vmatrix}$	9.777950 778119	281 281	$\begin{array}{c} 9.903203 \\ 903108 \end{array}$	158	$\frac{9.874747}{875010}$	439	10.125253	9
5	3	778287	$\frac{281}{280}$	903108	158 158	875010	$\begin{array}{c c} 439 \\ 438 \end{array}$	$\frac{124990}{124727}$	8
5	4	778455	280	902919	158	875536	438	124464	6
	5	778624	280	902824	158	875800	438	124200	5
	6	778792	280	902729	158	876063	438	123937	4
	8	$\begin{array}{c c}     778960 \\     779128 \end{array}$	$\begin{array}{c} 280 \\ 280 \end{array}$	902634 902539	158 159	876326 876589	438 438	123674	3
5	9	779295	279	902539	159	876851	438	$\frac{123411}{123149}$	$\frac{2}{1}$
	0	779463	279	902349	159	877114	438	122886	0
	Ī	Cosine	1	Sine 1		Cotang.		Tang.	<u>M</u> .
-						Course.		Tung.	111.

No.   Sine   D.   Cosine   D.   Tang.   D.   Cotang.							2		
1         779631         279         992253         159         877377         438         122623         58           3         779968         279         992063         159         877600         438         122097         57           4         780133         279         991872         159         878185         56         5780300         278         991872         159         878591         438         121305         56           7         780634         278         991655         159         878953         437         120784         52           8         780901         278         991490         159         8789478         437         120784         52           9         780908         278         991490         159         879478         437         120525         51           10         781134         278         991394         160         879478         437         120525         51           11         9.781468         277         991106         160         880628         437         119735         48           12         781468         277         990141         160         881052         437	М.	Sinc	D. j	Cosine	D.	Tang.	D.	Cotang.	
2	0	9.7794631	279		159	9.877114	438	10.122886	60
3         779966         279         902063         159         877903         438         122097         57           5         780300         278         901977         159         878165         438         121835         56           7         780634         278         901671         159         878953         437         121047         53           6         780801         278         901585         159         878953         437         120784         52           9         780968         278         901400         159         879478         437         120525         51           10         781134         278         901394         160         879741         437         120259         50           11         9.781301         277         90106         60         889625         437         119735         48           13         781662         277         901010         160         880625         437         119735         48           14         781800         277         901011         160         881052         437         118494         43           15         781666         277         9		779631	279				438		
4         780133         279         901967         159         878128         438         121572         55           6         780467         278         901871         159         878128         438         121303         54           7         780634         278         901595         159         8789216         437         120474         52           9         780968         278         901490         159         879478         437         120522         51           10         781144         278         901394         160         879741         437         120522         51           11         9.781301         277         9.901202         160         880265         437         119732         47           12         781468         277         901010         160         880625         437         119410         46           15         781806         277         901011         160         880703         437         118948         45           16         782132         277         900818         167         881314         437         118644         43           17         782928         276	2		279			877640	438		
56         780300         278         901872         159         878428         438         121572         54           7         780634         273         901681         159         878953         437         121947         53           8         780801         278         901490         159         879478         437         120784         52           10         781134         278         901490         159         879478         437         120252         51           11         9.781301         277         9.901298         160         880603         437         119735         48           13         781684         277         901061         60         880528         437         119472         47           14         781800         277         901010         160         880528         437         119472         47           15         781666         277         900818         163         881344         437         118648         44           16         782329         276         900262         160         881539         437         118161         42           19         782298         276									
66         7804634         278         9016181         159         8789691         438         121047         53           8         780801         278         901631         159         878953         437         120784         52           9         780968         278         901490         159         879478         437         120522         51           10         781344         278         901394         160         879474         437         120522         51           11         9.781301         277         901010         160         880525         437         110,119997         49           12         781468         277         901010         160         880528         437         119472         47           14         781800         277         900814         160         881052         437         1184194         43           15         781966         277         900818         163         881314         437         118424         43           16         782238         276         900529         160         882101         437         118424         43           19         783630         276									
7         780634         278         901681         159         879633         437         121047         53           9         780968         278         901595         159         879478         437         120522         51           10         781134         278         901394         160         379741         437         120522         51           11         9.781301         277         901010         160         880265         437         10.119997         49           12         781664         277         901010         160         880528         437         119472         47           14         781966         277         901010         160         881052         437         119472         47           15         781966         277         900181         160         881052         437         118464         437           16         782132         277         900818         160         881576         437         118424         43           17         782293         276         909529         160         881539         437         118161         42           18         782796         278									
6         780801         278         901585         159         879216         437         120784         52           10         781134         278         901490         159         879478         437         120522         51           11         9,781301         277         901202         160         880265         437         119735         48           13         781634         277         901010         160         880528         437         119170         47           14         781800         277         901010         160         880528         437         119472         47           16         782132         277         909141         160         881052         437         118948         45           16         782132         277         909481         160         881576         437         118686         44           17         782293         276         990529         160         881534         437         11864         42           19         782931         276         990233         161         882363         436         10.117373         39           21         783653         275								121309	
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16         782132         277         900818         160         881574         437         118668         44           17         782298         276         900026         160         881576         437         118161         42           19         782600         276         900529         160         882101         437         111861         42           20         782796         276         900433         161         882363         436         10.117375         39           21         9.782961         276         9.90433         161         882363         436         10.117375         39           22         783127         276         9.90249         161         882887         436         10.117375         39           24         783458         2.75         900047         161         883410         436         116529         36           25         783623         275         899551         161         883492         436         116328         35           26         783788         275         899561         161         884457         436         115543         32           29         784232         274									
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22         783127         276         990240         161         882887         436         117113         38           23         783292         275         900144         161         883148         436         116520         36           24         783458         275         990047         161         883672         436         116520         36           25         783623         275         899854         161         883934         436         116066         38           26         783788         275         899854         161         883934         436         115606         33           28         784113         275         899660         161         884457         436         115543         32           29         784282         274         899660         162         884980         436         115203         30           30         784447         274         899167         162         884924         436         115020         30           31         9.784612         274         899170         162         885524         436         114475         29           32         784776         274	ž								
23         783292         275         900144         161         883148         436         116852         37           24         783458         275         900047         161         883410         436         116392         35           25         783623         275         899851         161         883672         436         116328         35           26         783788         275         899854         161         884196         436         115606         34           27         733955         275         899601         161         884457         436         115543         32           28         784118         275         899601         161         884457         436         115543         32           29         784282         274         899564         162         884980         436         115281         31           30         784447         274         899273         162         885523         436         114497         28           31         784612         274         899176         162         885765         436         114497         28           32         7847676         274									
24         783458         275         900047         161         883410         436         116590         36           25         783623         275         899854         161         883672         436         116328         35           26         783788         275         899854         161         883934         436         116066         34           27         783953         275         899660         161         884196         436         115804         33           28         784118         275         899660         161         884457         436         115543         32           30         784447         274         899661         162         884980         436         115281         31           31         9.784612         274         899467         162         884980         436         115281         31           32         784776         274         899176         162         885503         436         114497         28           33         784941         274         899176         162         885765         436         114235         47           34         785105         273									
25         783623         275         899951         161         883672         436         116328         35           26         783788         275         899854         161         883934         436         116066         34           27         783955         275         899757         161         884196         436         115804         33           28         784118         275         899660         161         884457         436         115543         32           29         784282         274         899467         162         884980         436         115281         31           30         784447         274         9.899370         162         9.885242         436         116497         29           32         784761         274         899078         162         885505         436         114497         29           33         784941         274         899078         162         886026         436         113974         26           34         785105         274         899078         162         886026         436         113974         26           35         785269         273									
26         783788         275         899851         161         883934         436         116066         34           27         783955         275         899757         161         884196         436         115804         33           28         784118         275         899660         161         884457         436         115804         33           30         784447         274         899467         162         884980         436         115020         30           31         9.784612         274         899273         162         885503         436         114097         23           32         784776         274         899273         162         885503         436         114497         23           33         784941         274         899078         162         885028         436         113974         26           34         785105         274         899078         162         886288         436         113712         25           35         785269         273         893831         162         886288         436         113712         25           36         7852697         273	_			-					
27         783955         275         899757         161         884196         436         115804         33           28         784113         275         899660         161         884457         436         115543         32           29         784282         274         899564         161         884719         436         115528         1           30         784447         274         899467         162         884980         436         115020         30           31         9.784612         274         899176         162         885503         436         114497         28           32         78476         274         899176         162         885503         436         114235         27           34         785105         274         899078         162         886026         436         113712         25           35         785433         273         893811         162         886549         435         113451         24           37         785597         273         898699         162         886549         435         113451         24           37         785925         273									
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33         784941         274         899176         162         885765         436         114235         27           34         785105         274         899078         162         886026         436         113974         26           35         785269         273         893831         162         886288         436         113712         25           36         785433         273         898787         162         886849         435         113451         24           37         785597         273         898699         162         887072         435         112928         22           39         785925         273         898592         162         887333         435         112667         21           40         786089         273         898299         163         887594         435         112406         20           41         9.786252         272         9.898397         163         888116         435         1118451         19           42         786416         272         898202         163         888316         435         1118481         10.10112145         19           43         786769									
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1         789504         269         896433         165         893331         434         106669         58           2         789827         269         896236         165         893331         434         106699         58           4         789882         269         88638         165         893511         434         106149         56           5         790149         269         895089         165         894111         434         105629         54           7         790471         268         8959599         165         894871         434         105629         54           8         790632         268         895641         165         894692         433         105108         25           9         707073         268         895411         165         894692         433         104688         160           10         790954         268         895451         165         895412         433         104488         51           11         7917155         267         895441         166         896192         433         104668         48           13         791466         267         8	M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
2         789665         289         896335         165         893331         434         106669         58           3         789887         269         896137         165         893511         434         106149         56           5         7790149         268         895939         165         894471         434         105689         55           6         790310         268         895940         165         894824         134         105629         54           7         790471         268         895641         165         895152         433         105108         52           9         70973         268         895641         165         895152         433         10488         51           10         790954         268         895542         165         895142         433         10488         51           11         9.791715         267         895431         166         895932         433         104688         48           12         791757         267         895444         166         896492         433         103348         46           15         791917         267         89	0		269	9.896532					
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4         789988         269         896137         165         893851         434         1056889         56         790310         268         895939         165         894111         434         1055889         55           7         790471         268         895939         165         894371         434         105568         53           8         790632         268         89541         165         894892         433         105168         52           9         790793         268         895541         165         895152         433         104588         50           10         790954         268         895542         165         895412         433         104588         50           11         9.79115         268         9.89543         166         895932         433         104068         48           12         79175         267         895445         166         895422         433         103388         47           14         79197         267         894945         166         896712         433         103384         46           15         79177         267         894465         166	2								
5         790149         269         898038         165         894371         434         105589         55           6         790471         268         895939         165         894371         434         105629         54           7         790471         268         895840         165         894892         433         105368         53           8         790632         268         895641         165         895152         433         10468         51           10         790954         268         895542         166         895152         433         10468         85           11         9.791115         267         895343         166         895932         433         10468         48           13         791486         267         895445         166         896452         433         103688         46           14         791596         267         895456         166         896452         433         103288         45           16         79197         267         894846         166         896741         433         103294           17         792077         267         894846 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>									
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7         790471         268         895741         165         894862         433         105368         53           8         790632         268         895741         165         894892         433         105108         52           10         790954         268         895542         165         895152         433         104684         51           11         791115         268         9.895431         166         9.89542         433         104088         85           12         791275         267         895244         166         896932         433         104088         85           13         791436         267         895445         166         896452         433         103808         47           14         791596         267         894446         166         8969712         433         102289         41           16         791917         267         894846         166         897231         433         102509         42           17         79237         266         894466         166         897341         433         102509         42           20         792876         266									
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28         793832         265         893745         167         900086         432         099914         32           30         794150         264         893544         167         900605         432         099395         30           31         9.794308         264         9.893444         168         9.900864         432         099395         30           32         794467         264         893343         168         901124         432         098876         28           33         794626         264         893412         168         901642         432         098576         28           34         794784         264         893041         168         901642         432         098358         26         35         794942         264         893041         168         901901         432         098999         25         36         795101         264         892839         168         902419         432         097621         22         37         795259         263         892283         168         902479         432         097321         22         39         795757         263         892253         168         90238 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>33</td></t<>									33
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	•	D.	<u>'                                      </u>	D.	Tang.	D.	Cotang.	
0	$\begin{vmatrix} 9.798872 \\ 799028 \end{vmatrix}$	$\begin{array}{c} 260 \\ 260 \end{array}$	$oxed{9.890503}{890400}$	$\begin{array}{c c} 170 \\ 171 \end{array}$	$9.908369 \\ 908628$	$\begin{array}{c} 430 \\ 430 \end{array}$	[10.091631]	60 59
$\frac{1}{2}$	799184	260 260	890298	$171 \\ 171$	908886	$\begin{array}{c} 430 \\ 430 \end{array}$	$091372 \\ 091114$	58 58
$\tilde{3}$	799339	259	890195	171	909144	430	090856	57
4	799495	259	890093	171	909402	430	090598	56
5	799651	259	889990	171	909660	430	090340	55
6	799806	259	889888	171	909918	430	090082	54
7	799962	259	889785	171	910177	430	089823	53
8	800117	259	889682	171	$910435 \\ 910693$	430	089565	52
9	$\begin{vmatrix} 800272 \\ 800427 \end{vmatrix}$	258 258	889579 $889477$	171 171	910093 $910951$	$\begin{array}{c c} 430 \\ 430 \end{array}$	$089307 \\ 089049$	51 50
	$\frac{800427}{9.800582}$			$\frac{171}{172}$	$\frac{910331}{9.911209}$		10.088791	$\frac{30}{49}$
11 12	800382	$\begin{array}{c} 258 \\ 258 \end{array}$	$9.889374 \\ 889271$	$\frac{172}{172}$	9.911209 $911467$	$\begin{array}{c} 430 \\ 430 \end{array}$	088533	49
13	800892	$\frac{258}{258}$	889168	172	911724	430	088276	47
14	801047	258	889064	$17\overline{2}$	911982	430	088018	46
15	801201	258	888961	172	912240	430	087760	45
16	801356	257	888858	172	912498	430	087502	44
17	801511	257	888755	172	912756	430	087244	43
18	801665	257	888651	172	913014	429	086986	42
$\begin{vmatrix} 19\\20 \end{vmatrix}$	$801819 \\ 801973$	$\begin{array}{c} 257 \\ 257 \end{array}$	888548 888444	$\frac{172}{173}$	913271 $913529$	$\begin{array}{c} 429 \\ 429 \end{array}$	$086729 \ 086471$	41 40
$\begin{bmatrix} 21 \\ 22 \end{bmatrix}$	$\begin{array}{c} 9.802128 \\ 802282 \end{array}$	$\begin{array}{c} 257 \\ 256 \end{array}$	$9.888341 \\ 888237$	$\begin{array}{c} 173 \\ 173 \end{array}$	9.913787 $914044$	$\begin{array}{c} 429 \\ 429 \end{array}$	$\begin{array}{c} 10.086213 \\ 085956 \end{array}$	39 38
23	802436	$\begin{array}{c} 256 \\ 256 \end{array}$	888134	$173 \\ 173$	914302	$\begin{array}{c} 429 \\ 429 \end{array}$	085698	37
24	802589	$\frac{250}{256}$	888030	$\frac{1}{173}$	914560	429	085440	36
25	802743	256	887926	173	914817	429	085183	35
26	802897	256	887822	173	915075	429	084925	34
27	803050	256	887718	173	915332	429	084668	33
28	803204	256	887614	173	915590	429	084410	32
29	803357	255	887510	173	915847	429	084153	31
$\frac{30}{21}$	803511	$\frac{255}{255}$	887406	174	916104	429	083896	$\frac{30}{20}$
31	9.803664	255	9.887302	174	9.916362	429	10.083638	29
32 33	$803817 \ 803970$	$\begin{array}{c} 255 \\ 255 \end{array}$	$887198 \\ 887093$	174 174	$916619 \\ 916877$	$\begin{array}{c} 429 \\ 429 \end{array}$	$083381 \\ 083123$	28 27
34	804123	$\frac{255}{255}$	886989	174	917134	$\begin{array}{c c} 429 \\ 429 \end{array}$	082866	26
35	804276	254	886885		917391	$4\overline{29}$	082609	25
36	804428	254	886780	174	917648	429	082352	24
3.7	804581	254	886676	174	917905	429	082095	23
38	804734	254	886571	174	918163	428	081837	22
39	804886	254	886466	174	918420	428	081580	21
$\frac{40}{41}$	$\frac{805039}{205101}$	254	886362	$\frac{175}{186}$	$\frac{918677}{0.018004}$	428	$\frac{081323}{10.0000}$	$\frac{20}{10}$
41	9.805191	254	9.886257	175	9.918934	428	10.081066	19 18
42 43	$805343 \ 805495$	$\begin{array}{c} 253 \\ 253 \end{array}$	$886152 \\ 886047$	175 175	$   \begin{array}{r}     919191 \\     919448   \end{array} $	$\begin{array}{c} 428 \\ 428 \end{array}$	$080809 \ 080552$	17
43	$\begin{array}{c} 805495 \\ 805647 \end{array}$	$\begin{array}{c} 253 \\ 253 \end{array}$	885942	175	919705	428	080295	16
45	805799	$\frac{2.53}{253}$	885837	175	919962	428	080038	15
46	805951	$\frac{253}{253}$	885732	175	920219	428	079781	14
47	806103	253	885627	175	920476	428	079524	13
48	806254	253	885522	175	920733	428	079267	12
49	806406	252	885416	175	920990	428	079010	11
$\frac{50}{50}$	806557	$\frac{252}{}$	885311	176	$\frac{921247}{2001500}$	$-\frac{428}{428}$	078753	$\frac{10}{0}$
51	9.806709	252	9.885205	176	9.921503	428	10.078497	9
52 53	806860	252	885100	$\begin{array}{c} 176 \\ 176 \end{array}$	$\begin{array}{c} 921760 \\ 922017 \end{array}$	$\begin{array}{c} 428 \\ 428 \end{array}$	$078240 \\ 077983$	8 7
54	$oxed{807011}{807163}$	$\begin{array}{c} 252 \\ 252 \end{array}$	884994 884889		922017 $922274$	428	$077985 \\ 077726$	6
55	807314	$\frac{252}{252}$	884783	176	922530	428	077470	5
56	807465	251	884677	176	922787	428	077213	4
57	807615	251	884572	176	923044	428	076956	3
58	807766	251	884466	176	923300	428	076700	2
59	807917	251	884360	176	923557	427	076443	1
60	808067	251	884254	177		427	076187	0
	Cosine		Sine		Cotang.		Tang.	M.
-	The state of the last				rees			

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.808067	251	9.884254		9.923813	427	10.076187	60
1	808218	251	884148		924070	427	075930	59
2 3	808368	251	884042	177	924327	427	$075673 \\ 075417$	58 57
	808519	250	883936	177	924583	427 427	075160	56
4	808669	250	$883829 \\ 883723$	$\frac{177}{177}$	924840 $925096$	427	074904	55
5	808819	250	883617	177	925352	427	074648	54
6	808969 809119	$\begin{array}{c c} 250 \\ 250 \end{array}$	883510	177	925609	427	074391	53
8	809269	250	883404	177	925865	$\frac{127}{427}$	074135	52
9	809419	249	883297	178	926122	427	073878	51
10	809569	249	883191	178	926378	427	073622	50
11	9.809718	249	9.883084	178	$9.92\overline{6634}$	427	10.073366	$\overline{49}$
12	809868	$\tilde{2}\tilde{4}\tilde{9}$	882977	178	926890	427	073110	48
13	810017	249	882871	178	927147	427	072853	47
14	810167	249	882764	178	927403	427	072597	46
15	810316	248	882657	178	927659	427	072341	45
16	810465	248	882550	178	927915	427	072085	44
17	810614	248	882443		928171	427	071829	43 42
18	810763	248	882336	179	928427	427	$\begin{bmatrix} 071573 \\ 071317 \end{bmatrix}$	41
19	810912	248	882229	179	928683	$\begin{array}{c} 427 \\ 427 \end{array}$	071060	
$\frac{20}{20}$	811061	248	882121	$\frac{179}{150}$	$\frac{928940}{200000000000000000000000000000000000$			$\frac{1}{39}$
21	9.811210	248	9.882014	179	9.929196	$\begin{array}{c} 427 \\ 427 \end{array}$	$\begin{array}{c} 10.070804 \\ 070548 \end{array}$	38
22	811358	247	881907	179 179	$\begin{array}{c} 929452 \\ 929708 \end{array}$	427	070292	37
23	811507	247	881799 881692		929708 $929964$	426	070036	36
24 25	811655 811804	$\begin{array}{c} 247 \\ 247 \end{array}$	881584	179	930220	426	069780	35
26	811952	247	881477	179	930475	426	069525	34
27	812100	$\tilde{2}47$	881369	179	930731	426	069269	33
28	812248	247	881261	180	930987	426	069013	32
29	812396	246	881153		931243	426	068757	31
30	812544	246	881046	180	931499	426	068501	30
$\overline{31}$	9.812692	246	9.880938	180	9.931755	426	10.068245	29
32	812840	$2\overline{4}6$	880830	180	932010	426	067990	
33	812988	246	880722		932266	426	067734	27
34	813135	246	880613		932522	426	067478	26
35	813283	246	880505		932778	426	067222	25 24
36	813430	245	880397		933033 $933289$		$066967 \\ 066711$	23
37	813578	245	880289 880180		933545		066455	
38	813725 813872	$\begin{array}{c} 245 \\ 245 \end{array}$	880072		933800		066200	1
40	814019	245	879963		934056		065944	20
$\frac{1}{41}$	$\frac{814013}{9.814166}$	$\frac{245}{245}$	$\frac{019355}{9.879855}$		$\frac{0.934311}{9.934311}$	$\frac{1}{426}$	10.065689	19
41	9.814100		879746		934567		065433	
43	814460	i	879637				065177	18
44	814607		879529				064922	16
45	814753		879420	181	935333	426	064667	15
46	814900	244	879311	181			064411	14
47	815046	244	879202				064156	13
48	815193		879093				063900	12
49	815339		878984				063645 063390	
50	815485	·	878875					10
51		243	9.878766				10.063134	
52			878656				$\begin{array}{c c} 062879 \\ 062624 \end{array}$	
53			878547				062368	
54			878438		-		062113	
55 56			878328			1	061858	4
57			878109				061602	3
58			877999				061347	2
59			877890				061092	1
60			877780				060837	
1-	l Cosine	1	Sine	1	Cotang.	1	Tang.	M.
1	Cosmic		Dine	1	Course.		1	-

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.816943	242	9.877780	183		425	10.060837	60
1	817088	242	$877670 \ 877560$	183 183	$939418 \\ 939673$	425	060582	59
2 3	$817233 \\ 817379$	$\begin{array}{c c} 242 \\ 242 \end{array}$	877450	183	939928	$\begin{array}{c} 425 \\ 425 \end{array}$	$060327 \ 060072$	58 57
4	817524	241	877340	183	940183	$\begin{array}{c} 425 \\ 425 \end{array}$	059817	56
5	817668	241	877230	184	940438	425	059562	55
6	817813	241	877120	184	940694	425	059306	54
7	817958	241	877010	184	940949	425	059051	53
8	818103	241	876899	184	941204	425	058796	52
9	818247	241	876789	184	941458	425	058542	51
10	818392	241	876678	184	941714	425	058286	50
$\overline{11}$	9.818536	240	9.876568	184	9.941968	425	$\overline{10.058032}$	$\overline{49}$
12	818681	240	876457	184	942223	425	057777	4.8
13	818825	240	876347	184	942478	425	057522	47
14	818969	240	876236	185	942733	425	057267	46
15	819113	240	876125	185	942988	425	057012	45
16	819257	240	876014	185	943243	425	056757	44
17	819401	240	$875904 \\ 875793$	185 185	$943498 \\ 943752$	425	$056502 \\ 056248$	43
18	819545 $819689$	$\begin{array}{c} 239 \\ 239 \end{array}$	875682	$\frac{185}{185}$	943732 $944007$	$\begin{array}{c} 425 \\ 425 \end{array}$	055993	42 41
$\begin{vmatrix} 19 \\ 20 \end{vmatrix}$	$819089 \\ 819832$	239 239	875571	185	944007 $944262$	$\begin{array}{c} 425 \\ 425 \end{array}$	055738	40
					$\frac{344202}{9.944517}$			39
21	$\begin{array}{c} 9.819976 \\ 820120 \end{array}$	$\begin{array}{c} 239 \\ 239 \end{array}$	$9.875459 \\ 875348$	185 185	9.944517	$\begin{array}{c} 425 \\ 424 \end{array}$	$\begin{array}{c} 10.055483 \\ 055229 \end{array}$	38
22 23	820120 $820263$	239	875237	$\frac{185}{185}$	945026	424	053225	37
24	820406	$\frac{239}{239}$	875126	186	945281	424	054719	36
25	820550	238	875014	186	945535	424	054465	35
$\begin{vmatrix} 26 \\ 26 \end{vmatrix}$	820693	$\mathbf{\tilde{238}}$	874903	186	945790	424	054210	34
27	820836	238	874791	186	946045	424	053955	33
28	820979	238	874680	186	946299	424	053701	32
29	821122	238	874568	186	946554	424	053446	31
30	821265	238	874456	186	946808	424	053192	30
$ \overline{31} $	9.821407	238	9.874344	186	9.947063	424	10.052937	29
32	821550	238	874232	187	947318	424	052682	28
33	821693	237	874121	187	947572	424	052428	27
34	821835		874009	187	947826	424	052174	26
35	821977	237	873896	187	948081	424	051919	25
36	822120	237	873784 $873672$	187 187	948336 $948590$	$\begin{array}{c} 424 \\ 424 \end{array}$	$051664 \\ 051410$	24 23
$\begin{bmatrix} 37 \\ 38 \end{bmatrix}$	$822262 \\ 822404$	$\begin{array}{c} 237 \\ 237 \end{array}$	873560		948844	424	051410	
39	822546	$\frac{237}{237}$	873448	187	949099	424	050901	21
40	822688	236	873335	187	949353	424	050647	20
$\frac{40}{41}$	$\frac{622830}{9.822830}$	$\frac{236}{236}$	$9.87\overline{3223}$	$\frac{13}{187}$	$\frac{9.949607}{9.949607}$	424	$\frac{10.050393}{10.050393}$	$\frac{1}{19}$
$\begin{vmatrix} 41\\42 \end{vmatrix}$	822972	236	873110	188	949862	424	050138	18
43	823114	236	872998	188	950116	424	049884	17
44	823255	236	872885	188	950370	424	049630	16
45	823397	236	872772	188	950625	424	049375	15
46	823539	236	872659	188	950879	424	049121	14
47	823680	235	872547	188	951133	424	048867	13
48	823821	235	872434	188	951388	424	048612	12
49	823963		872321	188	951642	424	048358	11
50	824104		872208	188	$\frac{951896}{2000000000000000000000000000000000000$	424	048104	$\frac{10}{0}$
51	9.824245	235	9.872095	189	9.952150	424	10.047850	9
52	824386		871981	189	952405	$\begin{array}{c} 424 \\ 424 \end{array}$	$047595 \\ 047341$	8 7
53	824527	235	871868	189 189	952659 $952913$	$\begin{array}{c} 424 \\ 424 \end{array}$	047341	6
54 55	824668 824808		871755 871641	189	952915 953167	$\begin{array}{c} 424 \\ 423 \end{array}$	$047087 \\ 046833$	5
56	824808		871528		953421	423	046579	4
57	825090		871414	189	953675	423	046325	3
58	825230		871301	189	953929	423	046071	2
59	825371	234	871187	189	954183	423	045817	1
60	825511		871073		954437	423	045563	0
-	Cosine	1	Sine		Cotang.		Teng.	M.
	Cosme		~IIIC		4000005		- c8	

1		Dogi			III OF IIC		mile	
M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.825511	234	9.871073		9.954437	423	10.045563	
1	825651	233	$870960 \\ 870846$	190	954691	423	045309	59
3	$\begin{array}{c c} 825791 \\ 825931 \end{array}$	$\begin{array}{c} 233 \\ 233 \end{array}$	870732	190	954945 $955200$	$\begin{array}{c} 423 \\ 423 \end{array}$	$045055 \\ 044800$	58 57
4	826071	$\frac{233}{233}$	870618	190	955454	423	044546	56
5	826211	233	870504		955707	423	044293	55
6	826351	233	870390	190	955961	$\tilde{4}23$	044039	54
7	826491	233	870276	190	956215	423	043785	53
8	826631	233	870161	190	956469	423	043531	52
9	826770	232	870047	191	956723	423	043277	51
10	$\frac{826910}{600000000000000000000000000000000000$	232	869933	191	$\frac{956977}{2}$	423	043023	$\frac{50}{}$
11	9.827049	232	9.869818	191	9.957231	423	10.042769	49
12 13	$oxed{827189}{827328}$	232 232	$869704 \\ 869589$	191 191	957485 957739	$\begin{array}{c} 423 \\ 423 \end{array}$	$042515 \ 042261$	48
14	827467	$\frac{232}{232}$	869474	191	957993	$\begin{array}{c} 423 \\ 423 \end{array}$	$042201 \\ 042007$	47 46
15	827606	232	869360	191	958246	423	041754	45
16	827745	232	869245	191	958500	423	041500	44
17	827884	231	869130	191	958754	423	041246	43
18	828923	231	869015	192	959008	423	040992	42
19	828162	231	868900	192	959262	423	040738	41
$\frac{20}{}$	828301	231	868785	192	959516	423	040484	40
21	9.828439	231	9.868670	192	9.959769	423	10.040231	39
22	828578	231	868555	192	960023	423	039977	38
23 24	828716 828855	$\begin{array}{c} 231 \\ 230 \end{array}$	868440 868324	192	$960277 \\ 960531$	$\begin{array}{c} 423 \\ 423 \end{array}$	$039723 \\ 039469$	37
25	828993	$\frac{230}{230}$	868209	$\frac{192}{192}$	960331	$\begin{array}{c} 423 \\ 423 \end{array}$	039469	36 35
26	829131	$\frac{230}{230}$	868093	192	961038	423	038962	34
27	829269	230	867978	193	961291	$4\overline{23}$	038709	33
28	829407	230	867862	193	961545	423	038455	32
29	829545	230	867747	193	961799	423	038201	31
30	829683	230	867631	193	962052	423	037948	30
31	9.829821	229	9.867515	193	9.962306	423	10.037694	29
32	829959	229	867399	193	962560	423	037440	28
33 34	$egin{array}{ccc} 830097 \ 830234 \ \end{array}$	229	867283	193	962813	423	037187	27
35	830372	$\begin{array}{c} 229 \\ 229 \end{array}$	$867167 \\ 867051$	193 193	$963067 \\ 963320$	$\begin{array}{c} 423 \\ 423 \end{array}$	$036933 \\ 036680$	26 25
36	830509	229	866935		963574	423	036426	24
37	830646	229	866819		963827	$4\overline{23}$	036173	23
38	830784	229	866703	194	964081	423	035919	22
39	830921	228	866586		964335	423	035665	21
40	831058	228	866470	194	964588	422	035412	20
41	9.831195	228	9.866353	194	9.964842	422	10.035158	19
42	831332	228	866237	194	965095	422	034905	18
43	831469	228	866120	194	965349	422	034651	17
44 45	$831606 \\ 831742$	228	$866004 \\ 865887$	195	$965602 \\ 965855$	$\begin{array}{c} 422 \\ 422 \end{array}$	$034398 \ 034145$	16
46	831742	$\begin{array}{c} 228 \\ 228 \end{array}$	865770	$\begin{array}{c} 195 \\ 195 \end{array}$	966109	$\begin{array}{c} 422 \\ 422 \end{array}$	$\begin{array}{c} 034145 \\ 033891 \end{array}$	15 14
47	832015	227	865653	195	966362	$\begin{array}{c} 422 \\ 422 \end{array}$	033638	13
48	832152	227	865536	195	966616	422	033384	12
49	832288	227	865419	195	966869	422	033131	11
50	832425	227	865302	195	967123	422	032877	10
51	9.832561	227	9.865185	$\overline{195}$	9.967376	422	10.032624	9
52	832697	227	865068	195	967629	422	032371	8 7
53	832833	227	864950		967883	422	032117	
54 55	832969 833105	226	864833		968136	422	031864	6
56	833241	$\begin{array}{c} 226 \\ 226 \end{array}$	$864716 \\ 864598$	$\begin{array}{c} 196 \\ 196 \end{array}$	$968389 \\ 968643$	$\begin{array}{c} 422 \\ 422 \end{array}$	$031611 \\ 031357$	5 4
57	833377	$\begin{array}{c} 220 \\ 226 \end{array}$	864481	196	968896	422	031104	3
58	833512	226	864363	196	969149	422	030851	2
59	833648	226	864245	196	969403	422	030597	1
60	833783	226	864127	196	969656	422	030344	0
	Cosine		Sine		Cotang.		Tang.	M.

$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	Cotang.  030344  030091  029838  029584  029078  028825  028571  028318  028065  027559	60 59 58 57 56 55 54 53 52 51
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	030091 029838 029584 029331 029078 028825 028571 028318 028065 027812	59 58 57 56 55 54 53 52
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	029838 029584 029331 029078 028825 028571 028318 028065 027812	59 58 57 56 55 54 53 52
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	029584 029331 029078 028825 028571 028318 028065 027812	57 56 55 54 53 52
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	029331 029078 028825 028571 028318 028065 027812	56 55 54 53 52
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	029078 028825 028571 028318 028065 027812	55 54 53 52
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 028825 \\ 028571 \\ 028318 \\ 028065 \\ 027812 \end{array}$	54 53 52
$egin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{c} 028571 \\ 028318 \\ 028065 \\ 027812 \end{array}$	53 52
8 834865 225 863183 197 971682 422	$\begin{array}{c} 028318 \\ 028065 \\ 027812 \end{array}$	52
	027812	
9   834999   224   863064   197   971935   422		
10   835134   224   862946   198   972188   422	097550	50
	021009	$\overline{49}$
12 835403 224 862709 198 972694 422	027306	48
13 835538 224 862590 198 972948 422	027052	47
$egin{array}{ c c c c c c c c c c c c c c c c c c c$	$026799 \\ 026546$	46 45
$egin{array}{ c c c c c c c c c c c c c c c c c c c$	026293	44
$\begin{bmatrix} 17 & 836075 & 223 & 862115 & 198 & 973960 & 422 \end{bmatrix}$	0.26040	43
18   836209   223   861996   198   974213   422	025787	42
19 836343 223 861877 198 974466 422	025534	41
$oxed{20} oxed{836477} oxed{223} oxed{861758} oxed{199} oxed{974719} oxed{422}$	025281	40
	025027	$\overline{39}$
$oxed{22} oxed{836745} oxed{223} oxed{861519} oxed{199} oxed{975226} oxed{422}$	024774	38
23 836878 223 861400 199 975479 422	024521	37
$egin{bmatrix} 24 & 837012 & 222 & 861280 & 199 & 975732 & 422 \ 25 & 837146 & 222 & 861161 & 199 & 975985 & 422 \end{bmatrix}$	$024268 \\ 024015$	36
$egin{bmatrix} 25 & 837146 & 222 & 861161 & 199 & 975985 & 422 \ 26 & 837279 & 222 & 861041 & 199 & 976238 & 422 \ \end{bmatrix}$	024015	35 34
$\begin{bmatrix} 26 \\ 27 \end{bmatrix} = \begin{bmatrix} 837279 \\ 837412 \end{bmatrix} = \begin{bmatrix} 222 \\ 222 \end{bmatrix} = \begin{bmatrix} 860922 \\ 199 \end{bmatrix} = \begin{bmatrix} 976491 \\ 976491 \end{bmatrix} = \begin{bmatrix} 422 \\ 422 \end{bmatrix}$	023509	33
28 837546 222 860802 199 976744 422	023256	32
29 837679 222 860682 200 976997 422	023003	31
$oxed{30} oxed{837812} oxed{222} oxed{860562} oxed{200} oxed{977250} oxed{422}$	022750	30
	.022497	29
$oxed{32} oxed{838078} oxed{221} oxed{860322} oxed{200} oxed{977756} oxed{422}$	022244	28
33   838211   221   860202   200   978009   422	021991	27
34 838344 221 860082 200 978262 422	021738	
$egin{array}{ c c c c c c c c c c c c c c c c c c c$	$021485 \\ 021232$	$\begin{bmatrix} 25 \\ 24 \end{bmatrix}$
$egin{array}{ c c c c c c c c c c c c c c c c c c c$	$021232 \\ 020979$	23
$\begin{bmatrix} 37 \\ 38 \end{bmatrix}  \begin{array}{c ccccccccccccccccccccccccccccccccccc$	020726	
39 839007 221 859480 201 979527 422	020473	
40 839140 220 859360 201 979780 422	020220	
	019967	$\overline{19}$
42 839404 220 859119 201 980286 422	019714	18
43 839536 220 858998 201 980538 422	019462	
44 839668 220 858877 201 980791 421	019209	16
45 839800 220 858756 202 981044 421	$018956 \\ 018703$	
$egin{array}{ c c c c c c c c c c c c c c c c c c c$	$018703 \\ 018450$	
47	018430 $018197$	
48	017944	
50 840459 219 858151 202 982309 421	017691	
	.017438	9
52 840722 219 857908 202 982814 421	017186	8
53 840854 219 857786 202 983067 421	016933	
54 840985 219 857665 203 983320 421	016680	
55 841116 218 857543 203 983573 421	016427	5
$egin{array}{ c c c c c c c c c c c c c c c c c c c$	$016174 \\ 015921$	4
57         841378         218         857300         203         984079         421           58         841509         218         857178         203         984331         421	015921 $015669$	
58   841509   218   857178   203   364531   421	015416	
60 841771 218 856934 203 984837 421	015163	
	Tang.	M.
Cosine   Sine   Cotang.	1 ang.	111.

	Sine	D.	Cosine	D.	Tang. 6.	Ď.	Cotang.	
0	19.841771	218	9.856934		9.984837	421	10.0151631	- CI
1	841902	$\frac{218}{218}$	856812		985090	421	014910	60 59
2	842033	218	856690	204	985343	421	014657	58
. 3	842163	217	856568		985596	421	014404	57
4 5	$842294 \\ 842424$	217 217	$856446 \\ 856323$	$\begin{array}{c} 204 \\ 204 \end{array}$	$985848 \ 986101$	$\begin{array}{c} 421 \\ 421 \end{array}$	$014152 \\ 013899$	56 55
6	842555	217	856201	$\frac{204}{204}$	986354	421	013646	54
7	842685	217	856078	204	986607	421	013393	53
8	842815	217	855956		986860	421	013140	52
9 10	$842946 \\ 843076$	$\begin{array}{c} 217 \\ 217 \end{array}$	855833 855711	$\begin{array}{c} 204 \\ 205 \end{array}$	987112 $987365$	421 421	$012888 \\ 012635$	51
$\frac{10}{11}$	$\frac{343070}{9.843206}$	$\frac{217}{216}$	$\frac{055711}{9.855588}$	$\frac{205}{205}$	$\frac{387303}{9.987618}$	421	$\frac{012033}{10.012382}$	$\frac{50}{49}$
12	843336	$\frac{210}{216}$	855465		987871	421	012129	49
13	843466	216	855342	205	988123	421	011877	47
14	843595	216	855219		988376	421	011624	46
15 16	843725 843855	$\begin{array}{c} 216 \\ 216 \end{array}$	$855096 \\ 854973$	$\begin{bmatrix} 205 \\ 205 \end{bmatrix}$	988629 988882	$\frac{421}{421}$	$egin{array}{c} 011371 \ 011118 \ \end{array}$	45
17	843984	216	854850		989134	421	010866	44 43
18	844114	215	854727		989387	421	010613	
19	844243	215	854603		989640	421	010360	41
20	844372	215	854480	1.1	989893	421	010107	40
21	$9.844502 \\ 844631$	215 215	9.854356 854233		9.990145	421	10.009855	39
22 23	844760	215	854109		$990398 \\ 990651$	$\frac{421}{421}$	009602 009349	38 37
24	844889	215	853986		990903	421	009097	36
25	845018	215	853862			421	008844	35
26	845147	215	853738 853614		$991409 \\ 991662$	421	008591	34
27 28	$oxed{845276}{845405}$	$\begin{array}{c c} 214 \\ 214 \end{array}$	853490	$\begin{array}{c c} 207 \\ 207 \end{array}$	991002	$\begin{array}{c} 421 \\ 421 \end{array}$	008338 008086	$\begin{array}{c c} 33 \\ 32 \end{array}$
29	845533	214	853366		992167	421	007833	
30	845662	214	853242	207	992420	421	007580	
31	9.845790	214	9.853118	207	9.992672	421	10.007328	29
32	845919	214	852994		992925	421	007075	
$\begin{bmatrix} 33 \\ 34 \end{bmatrix}$	846047 846175	$\begin{array}{c c} 214 \\ 214 \end{array}$	$\begin{array}{r} 852869 \\ 852745 \end{array}$	$\begin{bmatrix} 207 \\ 207 \end{bmatrix}$	993178 $993430$	421 421	$006822 \\ 006570$	27 26
35	846304	214	852620		993683	$\tilde{421}$	006317	
36	846432	213	852496		993936	421	006064	
37 38	846560 846688	$\begin{array}{c} 213 \\ 213 \end{array}$	852371 $852247$	203 208	994189 $994441$	421 42i	005811	23
39	846816	$\frac{213}{213}$	852122	208	994694	421	$005559 \\ 005306$	
40	846944	213	851997	208	994947	421	005053	
$\overline{41}$	9.847071	213	9.851872	208	9.995199	421	10.004801	19
42	847199	213	851747		995452	421	004548	
43 44	847327 $847454$	$\begin{array}{c} 213 \\ 212 \end{array}$	$851622 \\ 851497$		995705 995957	$\begin{array}{ c c }\hline 421\\ 421\end{array}$	004295	
45	847582	212	851372		996210	421	$\begin{bmatrix} & 004043 \\ & 003790 \end{bmatrix}$	16
46	847709	212	851246	209	996463	421	003537	
47	847836	212	851121	209	996715	421	003285	
48 49	847964 $848091$	212 212	850996 850870		$996968 \\ 997221$	421 421	$\begin{array}{ c c c c c c }\hline 003032\\ 002779\\ \hline \end{array}$	
50	848218	212	850745		997473	421	002527	10
$\frac{3}{51}$	$\frac{1}{9.848345}$	$\frac{212}{212}$	9.850619		9.997726	$\frac{1}{421}$	10.002274	9
52	848472	211	850493	210	997979	421	002021	8
53	848599	211	850368			421	001769	7
54 55	848726 848852	211 211	850242 850116		$\begin{array}{c} 998484 \\ 998737 \end{array}$	$\begin{array}{c} 421 \\ 421 \end{array}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	
56	848979	211	849990		998989	421	001203	4
57	849106	211	849864	210	999242	421	000758	3
58 59	849232 849359	211	849738		999495	421	000505	
60	849485	211	849611 849485	$\begin{array}{ c c } 210 \\ 210 \end{array}$	$999748 \\ 10.000000$	421 421	$000253 \\ 000000$	
	Cosine		Sine	72.0	Cotang.	1	Tang.	M.
-		4 14	N. Control				z. ung.	173 ·
•			4.	Deg	rees.			

## A TRAVERSE TABLE

SHOWING THE DIFFERENCE OF

## LATITUDE AND DEPARTURE

FOR DISTANCES BETWEEN 1 AND 100, AND FOR ANGLES TO QUARTER DEGREES BETWEEN 1° AND 90°.

1	A Print Agency		1				-
Distance.	₹ I	Deg.	1/2 I	Deg.	$\frac{3}{4}$ D	eg.	Distance.
ınce	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ınce
	1.00	0.00	1.00	0.01	1.00	0.01	
1 2 3 4 5 6 7 8	$\begin{bmatrix} 2.00 \\ 3.00 \end{bmatrix}$	$\begin{bmatrix} 0.01 \\ 0.01 \end{bmatrix}$	$oxed{2.00 \ 3.00}$	$\begin{bmatrix} 0.02 \\ 0.03 \end{bmatrix}$	$\begin{bmatrix} 2.00 \\ 3.00 \end{bmatrix}$	$\begin{bmatrix} 0.03 \\ 0.04 \end{bmatrix}$	1 2 3 4 5
4 5	$\frac{4.00}{5.00}$	$\begin{bmatrix} 0.02 \\ 0.02 \end{bmatrix}$	$\left egin{array}{c} 4.00 \ 5.00 \end{array} ight $	$\begin{bmatrix} 0.03 \\ 0.04 \end{bmatrix}$	$\begin{bmatrix} 4.00 \\ 5.00 \end{bmatrix}$	$\begin{bmatrix} 0.05 \\ 0.07 \end{bmatrix}$	4
6	6.00	0.03	6.00	0.05	6.00	0.08	6
8	$\begin{bmatrix} 7.00 \\ 8.00 \end{bmatrix}$	$\begin{bmatrix}0.03\\0.03\end{bmatrix}$	$\begin{bmatrix} 7.00 \\ 8.00 \end{bmatrix}$	$\begin{bmatrix} 0.06 \\ 0.07 \end{bmatrix}$	$\begin{bmatrix} 7.00 \\ 8.00 \end{bmatrix}$	$\begin{array}{c c} 0.09 \\ 0.10 \end{array}$	7 8 1
$\begin{vmatrix} 9 \\ 10 \end{vmatrix}$	$\begin{array}{c} 9.00 \\ 10.00 \end{array}$	$\begin{array}{c} 0.04 \\ 0.04 \end{array}$	$\begin{bmatrix} 9.00 \\ 10.00 \end{bmatrix}$	$\begin{bmatrix} 0.08 \\ 0.09 \end{bmatrix}$	9.00	$\begin{bmatrix} 0.12 \\ 0.13 \end{bmatrix}$	9
11	$\frac{10.00}{11.00}$	$\frac{0.04}{0.05}$	$\frac{10.00}{11.00}$	$\frac{0.03}{0.10}$	$\frac{10.00}{11.00}$	$\frac{0.13}{0.14}$	11
12 13	$\begin{array}{c c} 12.00 \\ 13.00 \end{array}$	$\begin{array}{c} 0.05 \\ 0.06 \end{array}$	$\begin{array}{c c} 12.00 \\ 13.00 \end{array}$	$\begin{bmatrix} 0.10 \\ 0.11 \end{bmatrix}$	$oxed{12.00}{13.00}$	$\begin{bmatrix} 0.16 \\ 0.17 \end{bmatrix}$	12 13
14	14.00	0.06	14.00	0.12	14.00	0.18	14
15 16	$\begin{array}{c c} 15.00 \\ 16.00 \end{array}$	$\begin{bmatrix} 0.07 \\ 0.07 \end{bmatrix}$	$\begin{array}{c c} 15.00 \\ 16.00 \end{array}$	$\begin{bmatrix}0.13\\0.14\end{bmatrix}$	$\begin{bmatrix} 15.00 \\ 16.00 \end{bmatrix}$	$\begin{bmatrix}0.20\\0.21\end{bmatrix}$	15 16
17 18	17.00	$\begin{bmatrix} 0.07 \\ 0.08 \end{bmatrix}$	17.00	0.15	17.00	0.22	17
19	$\begin{array}{c c} 18.00 \\ 19.00 \end{array}$	0.08	$\begin{bmatrix} 18.00 \\ 19.00 \end{bmatrix}$	$\begin{bmatrix}0.16\\0.17\end{bmatrix}$	$\begin{array}{ c c }\hline 18.00\\ 19.00\end{array}$	$\begin{bmatrix}0.24\\0.25\end{bmatrix}$	18 19
$\left  \begin{array}{c} 20 \\ \hline 21 \end{array} \right $	$\frac{20.00}{21.00}$	$\frac{0.09}{0.09}$	$\frac{20.00}{21.00}$	$\frac{0.17}{0.19}$	$\frac{20.00}{21.00}$	$\frac{0.26}{0.07}$	20
22	22.00	0.10	22.00	$\begin{bmatrix} 0.18 \\ 0.19 \end{bmatrix}$	$\begin{bmatrix} 21.00 \\ 22.00 \end{bmatrix}$	$\begin{bmatrix} 0.27 \\ 0.29 \end{bmatrix}$	$\begin{array}{c} 21 \\ 22 \end{array}$
23 24	$\begin{bmatrix} 23.00 \\ 24.00 \end{bmatrix}$	$\begin{bmatrix} 0.10 \\ 0.10 \end{bmatrix}$	$\begin{bmatrix} 23.00 \\ 24.00 \end{bmatrix}$	$\begin{array}{c} 0.20 \\ 0.21 \end{array}$	$23.00 \\ 24.00$	$\begin{array}{c} \textbf{0.30} \\ \textbf{0.31} \end{array}$	$\begin{array}{c c} 23 \\ 24 \end{array}$
25	25.00	0.11	25.00	0.22	25.00	0.33	25
26 27	$\begin{bmatrix} 26.00 \\ 27.00 \end{bmatrix}$	$\begin{bmatrix} 0.11 \\ 0.12 \end{bmatrix}$	$\left[egin{array}{c} 26.00 \ 27.00 \end{array} ight]$	$\begin{bmatrix}0.23\\0.24\end{bmatrix}$	$\begin{array}{ c c c }\hline 26.00 \\ 27.00 \\ \end{array}$	$\begin{array}{c} \textbf{0.34} \\ \textbf{0.35} \end{array}$	$\begin{array}{c c} 26 \\ 27 \end{array}$
28 29	$\begin{array}{c c} 28.00 \\ 29.00 \end{array}$	$\begin{array}{c c} 0.12 \\ 0.13 \end{array}$	$\begin{array}{ c c } 28.00 \\ 29.00 \end{array}$	$\begin{bmatrix}0.24\\0.25\end{bmatrix}$	$\begin{array}{ c c } 28.00 \\ 29.00 \end{array}$	$\begin{array}{c} \textbf{0.37} \\ \textbf{0.38} \end{array}$	28 29
30	30.00	0.13	30.00	0.26	30.00	0.39	30
$\begin{bmatrix} 31 \\ 32 \end{bmatrix}$	$\frac{31.00}{32.00}$	$\begin{bmatrix} 0.14 \\ 0.14 \end{bmatrix}$	$\begin{vmatrix} 31.00 \\ 32.00 \end{vmatrix}$	$\begin{bmatrix}0.27\\0.28\end{bmatrix}$	$\frac{31.00}{32.00}$	$\begin{smallmatrix}0.41\\0.42\end{smallmatrix}$	$\begin{array}{c c} 31 \\ 32 \end{array}$
33	33.00	0.14	33.00	0.29	33,00	0.43	33
$\begin{array}{c c} 34 \\ 35 \end{array}$	$\begin{array}{c} 34.00 \\ 35.00 \end{array}$	$\begin{array}{c c} 0.15 \\ 0.15 \end{array}$	$oxed{34.00\ 35.00}$	$\begin{bmatrix}0.30\\0.31\end{bmatrix}$	$\begin{vmatrix} 34.00 \\ 35.00 \end{vmatrix}$	$\begin{array}{c} 0.45 \\ 0.46 \end{array}$	$\begin{array}{c c} 34 \\ 35 \end{array}$
$\begin{array}{c c} 36 \\ 37 \end{array}$	$\frac{36.00}{37.00}$	$\begin{bmatrix} 0.16 \\ 0.16 \end{bmatrix}$	$\begin{bmatrix} 36.00 \\ 37.00 \end{bmatrix}$	$\begin{bmatrix}0.31\\0.32\end{bmatrix}$	36.00 37.00	$\begin{array}{c} 0.47 \\ 0.48 \end{array}$	36 37
38	38.00	0.17	38.00	0.33	38.00	0.50	38
39 40	$\begin{array}{c} 39.00 \\ 40.00 \end{array}$	$\left \begin{array}{c}0.17\\0.17\end{array}\right $	$\begin{bmatrix} 39.00 \\ 40.00 \end{bmatrix}$	$\begin{bmatrix}0.34\\0.35\end{bmatrix}$	39.00 40.00	$\begin{array}{c} 0.51 \\ 0.52 \end{array}$	$\begin{array}{c c} 39 \\ 40 \end{array}$
41	41.00	0.18	41.00	0.36	41.00	0.54	41
42 43	$\begin{array}{c} 42.00 \\ 43.00 \end{array}$	$\begin{array}{c c} 0.18 \\ 0.19 \end{array}$	$\begin{array}{ c c c }\hline 42.00\\ 43.00 \end{array}$	0.37 0.38	$\begin{array}{c c} 42.00 \\ 43.00 \end{array}$	$\begin{array}{c} 0.55 \\ 0.56 \end{array}$	42 43
44 45	44.00 45.00	$\begin{array}{c} 0.19 \\ 0.20 \end{array}$	44.00 45.00	$\begin{array}{c} \textbf{0.38} \\ \textbf{0.39} \end{array}$	44.00 45.00	0.58	44 45
46	46.00	0.20	46.00	0.40	46.00	0.60	46
47 48	$\begin{vmatrix} 47.00 \\ 48.00 \end{vmatrix}$	$\begin{array}{c c} 0.21 \\ 0.21 \end{array}$	$   \begin{array}{c} 47.00 \\ 48.00 \end{array}  $	$\begin{bmatrix} 0.41 \\ 0.42 \end{bmatrix}$	47.00 48.00	$\begin{array}{c} 0.62 \\ 0.63 \end{array}$	47
49 50	49.00 50.00	$\begin{array}{c c} 0.21 \\ 0.22 \end{array}$	49.00 50.00	$\begin{array}{c} 0.43 \\ 0.44 \end{array}$	49.00 50.00	0.64 0.65	49 50
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
Distance.	203	Deg.	201	Deg.	901	Deg.	Distance.
	004	. Dog.	03-2	Deg.	004	Deg.	H

Dist	1 1	Deg.	1 1	Deg.	24	Deg.	Dist
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75	51.00 52.00 53.00 54.00 55.00 56.00 57.00 58.00 60.00 61.00 62.00 63.00 64.00 65.00 66.00 67.00 68.00 69.00 70.00 71.00 72.00 73.00 74.00 75.00	0.22 0.23 0.23 0.24 0.24 0.24 0.25 0.26 0.26 0.27 0.27 0.27 0.28 0.29 0.30 0.30 0.31 0.31 0.32 0.32 0.32 0.33	51.00 52.00 53.00 54.00 55.00 56.00 57.00 58.00 60.00 61.00 62.09 63.00 64.00 65.00 66.00 67.00 68.00 69.00 70.00 71.00 72.00 73.00 74.00 75.00	$\begin{array}{ c c c c c }\hline 0.45\\ \hline 0.45\\ 0.45\\ 0.45\\ 0.46\\ 0.47\\ 0.48\\ 0.49\\ 0.50\\ 0.51\\ 0.52\\ \hline 0.53\\ 0.54\\ 0.55\\ 0.56\\ 0.57\\ 0.58\\ 0.58\\ 0.59\\ 0.60\\ 0.61\\ \hline 0.62\\ 0.63\\ 0.64\\ 0.65\\ 0.65\\ 0.65\\ \end{array}$	51.00 52.00 53.00 54.00 55.00 56.00 57.99 58.99 60.99 61.99 62.99 63.99 64.99 65.99 66.99 67.99 68.99 67.99 70.99 71.99 72.99 73.99 74.99	0.67 0.68 0.69 0.71 0.72 0.73 0.75 0.76 0.77 0.79 0.80 0.81 0.82 0.84 0.85 0.86 0.88 0.89 0.90 0.92 0.93 0.93 0.95 0.97 0.98	51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75
76 77 78 79 80 81 82 83 84 85 86 87 88 99 91 92 93 94 95 96 97 98 99 100 100 100 100 100 100 100 100 100	76.00 76.00 77.00 78.00 79.00 80.00 81.00 82.00 83.00 84.00 85.00 86.00 87.00 90.00 91.00 92.00 93.00 94.00 95.00 96.00 97.00 98.00 99.00 100.00 Dep.	0.33 0.34 0.34 0.34 0.35 0.35 0.36 0.37 0.38 0.38 0.38 0.39 0.40 0.40 0.41 0.41 0.41 0.41 0.42 0.42 0.42 0.42 0.43 0.43 0.43 0.44 Lat.	76.00 77.00 78.00 79.00 80.00 81.00 82.00 83.00 84.00 85.00 86.00 87.00 88.00 90.00 91.00 92.00 93.00 94.00 95.00 96.00 97.00 98.00 99.00 100.00 Dep.	0.66 0.67 0.68 0.69 0.70 0.71 0.72 0.72 0.73 0.74 0.75 0.76 0.77 0.78 0.79 0.80 0.81 0.82 0.83 0.84 0.85 0.86 0.87 Lat.	75.99 76.99 77.99 78.99 79.99 80.99 81.99 82.99 83.99 84.99 85.99 86.99 87.99 90.99 91.99 91.99 92.99 93.99 94.99 95.99 96.99 97.99 98.99	0.99 1.01 1.02 1.03 1.05 1.06 1.07 1.09 1.10 1.11 1.13 1.14 1.15 1.16 1.18 1.19 1.20 1.22 1.23 1.24 1.26 1.27 1.28 1.30 1.31 Lat.	76778 79 80 812 834 85 87 88 99 91 22 334 95 6 97 89 90 10 33 94 95 6 97 80 90 10 33 94 95 6 97 80 90 10 33 94 95 6 97 80 90 10 33 94 95 6 97 80 90 10 33 94 95 6 97 80 90 10 33 94 95 6 97 80 90 10 33 95 6 97 80 90 10 33 95 6 97 80 90 10 30 90 10 10 10 10 10 10 10 10 10 10 10 10 10
Dista	893	Deg.	89½ I	eg.	89 <del>1</del> I	Deg.	Dist

_									-
Distance.	1 D	eg.	1¼ I	eg.	1½ I	Deg.	1 <del>3</del> I	Deg.	Distance.
nee.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
$\frac{1}{2}$	$1.00 \\ 2.00$	$\begin{array}{ c c }\hline 0.02\\0.03\\ \end{array}$	$\begin{array}{ c c } \hline 1.00 \\ 2.00 \\ \hline \end{array}$	$\begin{array}{c c} \hline 0.02 \\ 0.04 \\ \end{array}$	$\begin{array}{ c c }\hline 1.00 \\ 2.00 \\ \hline \end{array}$	0.03	$\begin{array}{ c c }\hline 1.00 \\ 2.00 \\ \hline \end{array}$	$\begin{bmatrix} 0.03 \\ 0.06 \end{bmatrix}$	1 2
3	$\begin{vmatrix} 3.00 \\ 4.00 \end{vmatrix}$	$\begin{bmatrix} 0.05 \\ 0.07 \end{bmatrix}$	$\begin{vmatrix} 3.00 \\ 4.00 \end{vmatrix}$	0.07	3.00	0.08	3.00	0.09	3
5	5.00	0.09	5.00	$\begin{array}{c} 0.09 \\ 0.11 \end{array}$	$\begin{vmatrix} 4.00 \\ 5.00 \end{vmatrix}$	$\begin{array}{c c} 0.10 \\ 0.13 \end{array}$	$\begin{array}{c c} 4.00 \\ 5.00 \end{array}$	$0.12 \\ 0.15$	5
6 7	$\begin{array}{ c c }\hline 6.00\\ 7.00\\ \end{array}$	$\begin{bmatrix} 0.10 \\ 0.12 \end{bmatrix}$	$oxed{0.00}{7.00}$	$0.13 \\ 0.15$	$\begin{array}{ c c }\hline 6.00\\ 7.00\end{array}$	$\begin{array}{c} 0.16 \\ 0.18 \end{array}$	$\begin{array}{c c} 6.00 \\ 7.00 \end{array}$	$\begin{bmatrix} 0.18 \\ 0.21 \end{bmatrix}$	6,
8 9	$\begin{array}{ c c } 8.00 \\ 9.00 \end{array}$	$\begin{array}{c} 0.14 \\ 0.16 \end{array}$	$\begin{array}{ c c } 8.00 \\ 9.00 \end{array}$	$\begin{array}{c} 0.17 \\ 0.20 \end{array}$	$\begin{vmatrix} 8.00 \\ 9.00 \end{vmatrix}$	$\begin{bmatrix} 0.21 \\ 0.24 \end{bmatrix}$	$8.00 \\ 9.00$	$\begin{bmatrix} 0.25 \\ 0.28 \end{bmatrix}$	8
10	10.00	0.17	10.00	d.22	10.00	0.26	10.00	0.31	10
11 12	$\begin{vmatrix} 11.00 \\ 12.00 \end{vmatrix}$	$\begin{array}{c} 0.19 \\ 0.21 \end{array}$	$\begin{bmatrix} 11.00 \\ 12.00 \end{bmatrix}$	$\begin{array}{c} 0.24 \\ 0.26 \end{array}$	$\begin{vmatrix} 11.00 \\ 12.00 \end{vmatrix}$	$\begin{bmatrix} 0.28 \\ 0.31 \end{bmatrix}$	$10.99 \\ 11.99$	$\begin{bmatrix} 0.34 \\ 0.37 \end{bmatrix}$	11 12
13 14	$\begin{vmatrix} 13.00 \\ 14.00 \end{vmatrix}$	$\begin{bmatrix}0.23\\0.24\end{bmatrix}$	$  13.00 \\ 14.00  $	$\begin{array}{c} 0.28 \\ 0.31 \end{array}$	$\begin{vmatrix} 13.00 \\ 14.00 \end{vmatrix}$	$\begin{bmatrix}0.34\\0.37\end{bmatrix}$	$\begin{vmatrix} 12.99 \\ 13.99 \end{vmatrix}$	$\begin{bmatrix}0.40\\0.43\end{bmatrix}$	13 14
15	15.00	0.26	15.00	0.33	14.99	0.39	14.99	0.46	15
16 17	$  \begin{array}{c} 16.00 \\ 17.00 \end{array}  $	$\begin{array}{c} 0.28 \\ 0.30 \end{array}$	$\begin{array}{ c c }\hline 16.00\\ 17.00\\ \end{array}$	$\begin{array}{c} 0.35 \\ 0.37 \end{array}$	$ \begin{array}{c} 15.99 \\ 16.99 \end{array} $	$\begin{bmatrix} 0.42 \\ 0.45 \end{bmatrix}$	$\begin{array}{ c c }\hline 15.99\\ 16.99\end{array}$	$\begin{bmatrix} 0.49 \\ 0.52 \end{bmatrix}$	16 17
18 19	$\begin{vmatrix} 18.00 \\ 19.00 \end{vmatrix}$	$\begin{array}{c} 0.31 \\ 0.33 \end{array}$	$\begin{array}{ c c }\hline 18.00\\ 19.00\\ \end{array}$	$\begin{array}{c} 0.39 \\ 0.41 \end{array}$	$  \begin{array}{c} 17.99 \\ 18.99 \end{array}  $	$\begin{bmatrix} 0.47 \\ 0.50 \end{bmatrix}$	17.99   18.99	$\begin{bmatrix} 0.55 \\ 0.58 \end{bmatrix}$	18 19
20	20.00	0.35	20.00	0.44	19.99	0.52	19.99	0.61	20
21 22	$\begin{vmatrix} 21.00 \\ 22.00 \end{vmatrix}$	$\begin{bmatrix} 0.37 \\ 0.38 \end{bmatrix}$	$\begin{vmatrix} 21.00 \\ 21.99 \end{vmatrix}$	$\begin{array}{c} 0.46 \\ 0.48 \end{array}$	$\begin{vmatrix} 20.99 \\ 21.99 \end{vmatrix}$	$\begin{array}{c c} 0.55 \\ 0.58 \end{array}$	$\begin{vmatrix} 20.99 \\ 21.99 \end{vmatrix}$	$\begin{bmatrix} 0.64 \\ 0.67 \end{bmatrix}$	21 22
23 24	$\begin{vmatrix} 23.00 \\ 24.00 \end{vmatrix}$	$egin{array}{c} 0.40 \ 0.42 \ \end{array}$	$ \begin{array}{c} 22.99 \\ 23.99 \end{array} $	$\begin{array}{c} 0.50 \\ 0.52 \end{array}$	$\begin{vmatrix} 22.99 \\ 23.99 \end{vmatrix}$	$\begin{bmatrix} 0.60 \\ 0.63 \end{bmatrix}$	$22.99 \\ 23.99$	$\begin{bmatrix}0.70\\0.73\end{bmatrix}$	23 24
25	$\begin{vmatrix} 25.00 \\ 26.00 \end{vmatrix}$	$\begin{array}{c} 0.44 \\ 0.45 \end{array}$	$\begin{vmatrix} 24.99 \\ 25.99 \end{vmatrix}$	0.55	24.99	0.65	24.99	0.76	25
26 27	27.00	0.47	26.99	$\begin{bmatrix} 0.57 \\ 0.59 \end{bmatrix}$	$ \begin{array}{c} 25.99 \\ 26.99 \end{array} $	$0.68 \\ 0.71$	$\begin{vmatrix} 25.99 \\ 26.99 \end{vmatrix}$	$\begin{bmatrix} 0.79 \\ 0.83 \end{bmatrix}$	26 27
28 29	$\begin{vmatrix} 28.00 \\ 29.00 \end{vmatrix}$	$\begin{array}{c} 0.49 \\ 0.51 \end{array}$	$\begin{bmatrix} 27.99 \\ 28.99 \end{bmatrix}$	$\begin{array}{c} 0.61 \\ 0.63 \end{array}$	$\begin{vmatrix} 27.99 \\ 28.99 \end{vmatrix}$	$\begin{bmatrix} 0.73 \\ 0.76 \end{bmatrix}$	27.99 $28.99$	$\begin{array}{c} 0.86 \\ 0.89 \end{array}$	28 29
30.	$\frac{30.00}{31.00}$	$\frac{0.52}{0.54}$	$\frac{29.99}{30.99}$	0.65	29.99	0.79	29.99	0.92	30
$\begin{array}{c} 31 \\ 32 \end{array}$	32.00	0.56	31.99	$\begin{bmatrix} 0.68 \\ 0.70 \end{bmatrix}$	$30.99 \\ 31.99$	$\begin{array}{ c c } 0.81 \\ 0.84 \end{array}$	30.99   31.99	$\begin{bmatrix} 0.95 \\ 0.98 \end{bmatrix}$	$\begin{bmatrix} 31 \\ 32 \end{bmatrix}$
33 34	$\begin{vmatrix} 32.99 \\ 33.99 \end{vmatrix}$	$\begin{array}{c} 0.58 \\ 0.59 \end{array}$	$ \frac{32.99}{33.99} $	$\begin{bmatrix}0.72\\0.74\end{bmatrix}$	$\begin{vmatrix} 32.99 \\ 33.99 \end{vmatrix}$	$\begin{array}{ c c }\hline 0.86\\ 0.89\end{array}$	$\begin{vmatrix} 32.98 \\ 33.98 \end{vmatrix}$	$\begin{vmatrix} 1.01 \\ 1.04 \end{vmatrix}$	33 34
35, 36	34.99	$\begin{array}{c} 0.61 \\ 0.63 \end{array}$	$34.99 \\ 35.99$	$\begin{array}{c} 0.76 \\ 0.79 \end{array}$	34.99 35.99	$\begin{array}{c} 0.92 \\ 0.94 \end{array}$	34.98 35.98	1.07	35 36
37	36.99	0.65	36.99	0.81	36.99	0.97	36.98	1.13	37
38 39	37.99 38:99	$\begin{array}{c} 0.66 \\ 0.68 \end{array}$	$\begin{vmatrix} 37.99 \\ 38.99 \end{vmatrix}$	$\begin{array}{c} \textbf{0.83} \\ \textbf{0.85} \end{array}$	37.99 38.99	$\begin{array}{c c} 0.99 \\ 1.02 \end{array}$	$  37.98 \\ 38.98 $	1.16	$\begin{array}{c} 38 \\ 39 \end{array}$
$\frac{40}{41}$	$\frac{39.99}{40.99}$	$\begin{array}{ c c }\hline 0.70 \\ \hline 0.72 \\ \hline \end{array}$	$\frac{39.99}{40.99}$	$\frac{0.87}{0.89}$	$\frac{39.99}{40.99}$	$\begin{array}{ c c }\hline 1.05\\\hline 1.07\end{array}$	$\frac{39.98}{40.98}$	$\frac{1.22}{1.05}$	40
42	41.99	0.73	41.99	0.92	41.99	1.10	41.98	$1.25 \\ 1.28$	41 42
43 44	$\begin{vmatrix} 42.99 \\ 43.99 \end{vmatrix}$	$\begin{bmatrix} 0.75 \\ 0.77 \end{bmatrix}$	$ 42.99 \\ 43.99$	$\begin{bmatrix} 0.94 \\ 0.96 \end{bmatrix}$	$ \begin{array}{c} 42.99 \\ 43.99 \end{array} $	1.13	$ \begin{array}{c} 42.98 \\ 43.98 \end{array} $	1.31	43 44
45 46	44.99 45.99	$\begin{array}{c c} 0.79 \\ 0.80 \end{array}$	44.99 45.99	$\begin{array}{c} 0.98 \\ 1.00 \end{array}$	44.99 45.99	$\begin{vmatrix} 1.18 \\ 1.20 \end{vmatrix}$	44.98 45.98	1.37	45
47, 48	$\begin{vmatrix} 46.99 \\ 47.99 \end{vmatrix}$	$0.82 \\ 0.84$	$46.99 \\ 47.99$	1.03	46.99	1.23	46.98	1.44	47
49	48.99	0.86	48.99	1.07	47.98 48.98	1.26	47.98 48.98	$\begin{vmatrix} 1.47 \\ 1.50 \end{vmatrix}$	48 49
50 °	149.99 Don	0.87	49.99 Dep	$\frac{1.09}{1.01}$	$\frac{49.98}{D_{cor}}$	1.31	49.98	1.53	$\frac{50}{6}$
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep. Lat.		Distance.
Dist	89	Deg.	883	Deg.	881	Deg.	881 Deg.		Dist
	1.				2		W	0	

				-	i				
Dista	1 D	eg.	1½ I	Deg.	$1\frac{1}{2}$ ]	Deg.	1¾ I	Deg.	Dista
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
Distance   552 554 556 5789   612 63 64 656 67	Lat.  50.99 51.99 52.99 53.99 54.99 55.99 56.99 60.99 61.99 63.99 64.99 65.99 66.99 67.99 68.99 70.99 71.99 72.99 73.99 74.99 75.99 76.99 76.99 76.99 78.99 78.99 78.99 88.99 88.99 88.99 88.99	Dep.    0.89   0.91   0.92   0.94   0.96   0.98   0.99   1.01   1.03   1.05   1.10   1.12   1.13   1.15   1.17   1.19   1.20   1.22   1.24   1.26   1.27   1.29   1.31   1.33   1.34   1.36   1.38   1.40   1.41   1.43   1.45   1.47   1.48   1.48   1.47   1.48   1.48   1.47   1.48   1.48   1.47   1.48   1.48   1.47   1.48   1.48   1.47   1.48   1.48   1.47   1.48   1.48   1.47   1.48   1.48   1.47   1.48   1.48   1.47   1.48   1.48   1.47   1.48   1.48   1.47   1.48   1	Lat.  50.99 51.99 52.99 53.99 54.99 55.99 56.99 59.99 60.99 61.99 62.99 63.98 64.98 65.98 66.98 67.98 68.98 70.98 71.98 72.98 73.98 74.98 75.98 76.98 76.98 76.98 76.98 76.98 78.98 78.98 78.98 78.98 78.98 78.98 78.98 78.98 78.98 78.98 78.98 78.98 78.98 78.98	Dep.  1.11 1.13 1.16 1.18 1.20 1.22 1.24 1.27 1.29 1.31 1.33 1.35 1.37 1.40 1.42 1.44 1.46 1.48 1.51 1.53 1.55 1.57 1.59 1.61 1.64 1.68 1.70 1.72 1.75 1.77 1.79 1.81 1.83 1.85					Distance. 5123545567896 612366667899 71273475677890 8123845
86 87 88 89 90	85.99 86.99 87.99 88.99 89.99	1.50 1.52 1.54 1.55 1.57	85.98 86.98 87.98 88.98 89.98	1.88 1.90 1.92 1.94 1.96	85.97 86.97 87.97 88.97 89.97	2.25 2.28 2.30 2.33 2.36	85.96 86.96 87.96 88.96 89.96	2.63 2.66 2.69 2.72 2.75	86 87 88 89 90
91 92 93 94 95 96 97 98 99 100	90.99 91.99 92.99 93.99 94.99 95.99 96.99 97.99 98.98	1.59 1.61 1.62 1.64 1.66 1.68 1.69 1.71 1.73	90.98 91.98 92.98 93.98 94.98 95.98 96.98 97.98 98.98	1.99 2.01 2.03 2.05 2.07 2.09 2.12 2.14 2.16 2.18	90.97 91.97 92.97 93.97 94.97 95.97 96.97 97.97 98.97 99.97	2.38 2.41 2.43 2.46 2.49 2.51 2.54 2.57 2.59 2.62	90.96 91.96 92.96 93.96 94.96 95.96 96.95 97.95 98.95	2.78 2.81 2.84 2.87 2.90 2.94 2.96 2.99 3.02 3.05	91 92 93 94 95 96 97 98 99 100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep. Lat.		Distance.
A	89 1	89 Deg: $88\frac{3}{4}$ Deg. $88\frac{1}{2}$ Deg. $88\frac{1}{4}$ Deg.						D	
	TO TO								

D:	2 D	eg.	2 <del>1</del> I	eg.	$2\frac{1}{2}$ I	Deg.	$2\frac{3}{4}$ I	Deg.	Dis
istance	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
$\frac{}{1}$	$\begin{array}{ c c }\hline 1.00 \\ 2.00 \\ \end{array}$	$\begin{bmatrix} 0.03 \\ 0.07 \end{bmatrix}$	$\begin{array}{c} \hline 1.00 \\ 2.00 \end{array}$	0.04	$\begin{array}{c} 1.00 \\ 2.00 \end{array}$	$\begin{bmatrix} 0.04 \\ 0.09 \end{bmatrix}$	$\begin{array}{c} 1.00 \\ 2.00 \end{array}$	$\begin{array}{c c} \hline 0.05 \\ 0.10 \\ \hline \end{array}$	
9 4 5	$egin{array}{c c} 3.00 \\ 4.00 \\ 5.00 \\ \hline \end{array}$	$\begin{bmatrix} 0.10 \\ 0.14 \\ 0.17 \end{bmatrix}$	$egin{array}{c} 3.00 \ 4.00 \ 5.00 \ \end{array}$	$egin{array}{c} 0.12 \ 0.16 \ 0.20 \ \end{array}$	$egin{array}{c} 3.00 \ 4.00 \ 5.00 \ \end{array}$	$egin{array}{c c} 0.13 \\ 0.17 \\ 0.22 \\ \end{array}$	$ \begin{array}{c c} 3.00 \\ 4.00 \\ 4.99 \end{array} $	$0.14 \\ 0.19 \\ 0.24$	1 2 3 4 5
6 7	$\begin{bmatrix} 6.00 \\ 7.00 \end{bmatrix}$	$\begin{array}{c} 0.21 \\ 0.24 \end{array}$	$\begin{array}{c c} 6.00 \\ 6.99 \end{array}$	$\begin{bmatrix}0.24\\0.27\end{bmatrix}$	5.99 6.99	$\begin{bmatrix} 0.26 \\ 0.31 \end{bmatrix}$	$\begin{bmatrix} 5.99 \\ 6.99 \end{bmatrix}$	$\begin{bmatrix}0.29\\0.34\end{bmatrix}$	7
8 9 10	7.99 8.99 9.99	$egin{array}{c} 0.28 \ 0.31 \ 0.35 \ \end{array}$	$7.99 \\ 8.99 \\ 9.99$	$0.31 \\ 0.35 \\ 0.39$	7.99 8.99 9.99	$0.35 \\ 0.39 \\ 0.44$	7.99 8.99 9.99	$\begin{bmatrix} 0.38 \\ 0.43 \\ 0.48 \end{bmatrix}$	8 9 10
$\frac{10}{11}$ 12	10.99 $11.99$	$\begin{array}{c} \hline 0.38 \\ 0.42 \end{array}$	10.99 11.99	$\begin{array}{c} 0.43 \\ 0.47 \end{array}$	10.99	$\begin{array}{c c} \hline 0.48 \\ 0.52 \end{array}$	10.99	0.53   0.58	11 12
13 14 15	12.99 13.99 14.99	$egin{array}{c c} 0.45 \\ 0.49 \\ 0.52 \\ \end{array}$	$12.99 \\ 13.99 \\ 14.99$	$0.51 \\ 0.55 \\ 0.59$	$12.99 \\ 13.99 \\ 14.99$	$0.57 \\ 0.61 \\ 0.65$	$egin{array}{c} 12.99 \ 13.98 \ 14.98 \ \end{array}$	$egin{array}{c} 0.62 \ 0.67 \ 0.72 \ \end{array}$	13 14 15
16 17	15.99 16.99	$0.52 \\ 0.56 \\ 0.59$	15.99 16.99	$\begin{array}{c} 0.63 \\ 0.67 \end{array}$	$15.99 \\ 16.98$	$\begin{array}{c} 0.70 \\ 0.74 \end{array}$	15.98 16.98	$\begin{array}{c} 0.77 \\ 0.82 \end{array}$	$\begin{array}{c} 16 \\ 17 \end{array}$
18 19 20	$   \begin{vmatrix}     17.99 \\     18.99 \\     19.99   \end{vmatrix} $	$\begin{bmatrix} 0.63 \\ 0.66 \\ 0.70 \end{bmatrix}$	17.99   18.99   19.98	$0.71 \\ 0.75 \\ 0.79$	$oxed{17.98} \ 18.98 \ 19.98$	$egin{array}{c} 0.79 \ 0.83 \ 0.87 \ \end{array}$	17.98 18.98 19.98	$0.86 \\ 0.91 \\ 0.96$	18 19 20
$\begin{array}{c} 20 \\ \hline 21 \\ 22 \end{array}$	20.99 $21.99$	$ \begin{array}{c c} 0.73 \\ 0.77 \end{array} $	20.98 $21.98$	$\begin{array}{c} \hline 0.82 \\ 0.86 \end{array}$	20.98 $21.98$	$\begin{array}{c} \hline 0.92 \\ -0.96 \\ \hline \end{array}$	$20.98 \\ 21.97$	1.01	21 22
23 24	$\begin{vmatrix} 22.99 \\ 23.99 \end{vmatrix}$	$\begin{array}{c} 0.80 \\ 0.84 \end{array}$	$\begin{vmatrix} 22.98 \\ 23.98 \\ 24.98 \end{vmatrix}$	$0.90 \\ 0.94 \\ 0.98$	22.98 23.98 24.98	$egin{array}{c} 1.00 \\ 1.05 \\ 1.09 \\ \end{array}$	$\begin{vmatrix} 22.97 \\ 23.97 \\ 24.97 \end{vmatrix}$	$egin{array}{c} 1.10 \ 1.15 \ 1.20 \ \end{array}$	23 24 25
25 26 27	24.98 25.98 26.98	$\begin{bmatrix} 0.87 \\ 0.91 \\ 0.94 \end{bmatrix}$	25.98 26.98	$\begin{bmatrix} 1.02 \\ 1.06 \end{bmatrix}$	25.98 26.97	$1.13 \\ 1.18$	25.97 $26.97$	$1.25 \\ 1.30$	26 27
28 29 30	$\begin{bmatrix} 27.98 \\ 28.98 \\ 29.98 \end{bmatrix}$	$ \begin{array}{c c} 0.98 \\ 1.01 \\ 1.05 \end{array} $	$\begin{vmatrix} 27.98 \\ 28.98 \\ 29.98 \end{vmatrix}$	1.10 1.14 1.18	$\begin{vmatrix} 27.97 \\ 28.97 \\ 29.97 \end{vmatrix}$	$egin{array}{c} 1.22 \\ 1.26 \\ 1.31 \\ \end{array}$	$\begin{vmatrix} 27.97 \\ 28.97 \\ 29.97 \end{vmatrix}$	1.34 1.39 1.44	28 29 30
$\begin{array}{c} 31 \\ 32 \end{array}$	$30.98 \\ 31.98$	$1.08 \\ 1.12$	$30.98 \\ 31.98$	$\begin{array}{ c c }\hline 1.22\\ 1.26\\ \end{array}$	30.97 $31.97$	$\frac{1.35}{1.40}$	30.96 31.96	1.49 $1.54$	31 32
33 34 35	$\begin{vmatrix} 32.98 \\ 33.98 \\ 34.98 \end{vmatrix}$	$\begin{array}{ c c }\hline 1.15 \\ 1.19 \\ 1.22 \\ \end{array}$	$\begin{vmatrix} 32.97 \\ 33.97 \\ 34.97 \end{vmatrix}$	$\begin{array}{ c c } 1.30 \\ 1.33 \\ 1.37 \end{array}$	$\begin{vmatrix} 32.97 \\ 33.97 \\ 34.97 \end{vmatrix}$	1.44 1.48 1.53	32.96 33.96 34.96	$\begin{array}{ c c } 1.58 \\ 1.63 \\ 1.68 \end{array}$	33 34 35
36 37	$\begin{vmatrix} 35.98 \\ 36.98 \end{vmatrix}$	1.26 $1.29$	35.97 36.97	$1.41 \\ 1.45$	35.97 36.96	1.57 1.61 1.66	35.96 36.96 37.96	$ \begin{array}{c c} 1.73 \\ 1.78 \\ 1.82 \end{array} $	36 37 38
38 39 40	37.98 38.98 39.98	1.33 1.36 1.40	$\begin{vmatrix} 37.97 \\ 38.97 \\ 39.97 \end{vmatrix}$	$\begin{array}{ c c } 1.49 \\ 1.53 \\ 1.57 \end{array}$	37.96 38.96 39.96	1.70	38.96 39.95	1.87	39 40
41 42	$ 40.98 \\ 41.97$	$1.43 \\ 1.47$	40.97	1.61 1.65	40.96	1.77	40.95	1.97	41 42
43 44 45	43.97	$ \begin{array}{ c c } 1.50 \\ 1.54 \\ 1.57 \end{array} $	$\begin{vmatrix} 42.97 \\ 43.97 \\ 44.97 \end{vmatrix}$	$ \begin{array}{c c} 1.69 \\ 1.73 \\ 1.77 \end{array} $	$\begin{array}{ c c c c }\hline 42.96 \\ 43.96 \\ 44.96 \\\hline \end{array}$	1.88 1.92 1.96	$  \begin{array}{c} 42.95 \\ 43.95 \\ 44.95 \end{array}  $	$\begin{array}{ c c c } 2.06 \\ 2.11 \\ 2.16 \end{array}$	43 44 45
46 47	$\begin{vmatrix} 45.97 \\ 46.97 \end{vmatrix}$	1.61	45.96 46.96	1.81 1.85 1.88	45.96 46.96 47.95	$\begin{array}{ c c } 2.01 \\ 2.05 \\ 2.09 \end{array}$	45.95 46.95 47.95	$\begin{array}{ c c } 2.21 \\ 2.25 \\ 2.30 \end{array}$	46 47 48
48 49 50	48.97	1.68 1.71 1.74	$  47.96 \\ 48.96 \\ 49.96 $	1.92 1.96	48.95 49.95	2.14 2.18	48.94 49.94	2.35 2.40	49 50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
Dista	88	Deg.	873	Deg.	$87\frac{1}{2}$	Deg.	871	Deg.	Dist
11.5			**		11		11		

Dist	2 1	eg.	21/4	Deg.	$2\frac{1}{2}$	Deg.	23/4	Deg.	Dist
ınce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ance.
Distance.   512 53 54 556 57 88 59 60   61 62 63 64 65 66 67 68 69 70   712 73 74 75 76 77 89   812 83 84 85 88 89 90   912 93 94 95 96 97	50.97 51.97 52.97 53.97 54.97 55.97 56.97 57.96 59.96 60.96 61.96 62.96 63.96 64.96 65.96 66.96 67.96 69.96 70.96 71.96 72.96 73.95 74.95 75.95 76.95 77.95 78.95 78.95 80.95 81.95 82.95 83.95 84.95 85.95 86.95 87	Dep.  1.78 1.81 1.85 1.88 1.92 1.95 1.99 2.02 2.06 2.09 2.13 2.16 2.20 2.23 2.27 2.30 2.34 2.41 2.48 2.51 2.55 2.58 2.62 2.65 2.72 2.76 2.79 2.83 2.97 2.83 2.97 3.00 3.04 3.07 3.11 3.14 3.18 3.21 3.25 3.39	Lat.    50.96     51.96     52.96     53.96     54.96     55.96     56.96     57.96     58.95     60.95     61.95     62.95     63.95     64.95     63.95     63.95     64.95     65.95     67.95     68.95     69.95     70.95     71.94     72.94     73.94     74.94     75.94     76.94     77.94     76.94     77.94     78.94     77.94     78.94     78.94     79.94     80.94     81.94     82.94     83.94     83.93     85.93     86.93     87.93     93.93     93.93     93.93     94.93     95.93     96.93     96.93	Dep.  2.00 2.04 2.08 2.12 2.16 2.20 2.24 2.28 2.36 2.39 2.43 2.47 2.51 2.55 2.59 2.63 2.67 2.71 2.75 2.79 2.83 2.87 2.91 2.94 2.98 3.02 3.06 3.14 3.18 3.22 3.26 3.30 3.34 3.38 3.42 3.45 3.49 3.53 3.77 3.61 3.65 3.69 3.73 3.77 3.81	50.95 51.95 52.95 53.95 54.95 55.95 56.95 57.94 58.94 60.94 61.94 62.94 63.94 64.94 65.94 66.94 67.94 68.93 70.93 71.93 72.93 73.93 74.93 75.93 76.93 77.93 78.92 79.92 80.92 81.92 82.92 83.92 84.92 85.92 85.92 86.92 87.92 88.92 89.91 90.91 91.91 92.91 93.91 96.91	2.22 2.27 2.31 2.36 2.40 2.44 2.49 2.53 2.57 2.62 2.75 2.88 2.92 2.97 3.01 3.14 3.18 3.23 3.27 3.31 3.40 3.45 3.49 3.58 3.62 3.75 3.75 3.62 3.75 3.75 3.75 3.75 3.75 3.75 3.75 3.75	50.94 51.94 52.94 53.94 54.94 55.94 56.93 57.93 58.93 60.93 61.93 62.93 63.93 64.93 65.92 66.92 67.92 68.92 69.92 70.92 71.92 72.92 73.91 74.91 75.91 76.91 77.91 78.91 79.91 80.91 81.91 82.90 83.90 84.90 85.90 86.90 87.90 88.90 89.90 90.90 91.89 93.89 94.89 95.89 96.89	2.45 2.50 2.54 2.64 2.69 2.73 2.78 2.88 2.93 2.97 3.02 3.07 3.12 3.26 3.31 3.36 3.41 3.45 3.50 3.55 3.60 3.74 3.79 3.84 3.93 3.93 3.93 3.93 3.93 3.93 3.93 3.9	Distance. 5123345567890 6123666667890 717237457677898 823845688899 9123945697
98 99 100	$\begin{vmatrix} 97.94 \\ 98.94 \\ 99.94 \end{vmatrix}$	$     \begin{array}{c c}       3.42 \\       3.46 \\       3.49     \end{array} $	97.92 98.92 99.92	3.85 3.89 3.93	97.91 98.91 99.91	4.27 4.32 4.36	97.89 98.89 99.88	$ \begin{array}{r} 4.70 \\ 4.75 \\ 4.80 \end{array} $	98 99 100
Distance.	Dep.	Lai.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
Dista	88 D	eg.	87 <u>3</u> I	Deg.	87 <u>1</u> ]	Deg.	871 1	Deg.	Dista

	1				1		Ji		
Dist	3 I	Deg.	31 3	Deg.	$3\frac{1}{2}$	Deg.	33	Deg.	Dist
Distance	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance. 1-23
1	1.00	0.05	1.00	0.06	1.00	0.06	1.00	0.06	1
$\begin{vmatrix} 2\\3 \end{vmatrix}$	$\begin{vmatrix} 2.00 \\ 3.00 \end{vmatrix}$	$0.10 \\ 0.16$	$\begin{array}{ c c c c } 2.00 \\ 3.00 \end{array}$	$0.11 \\ 0.17$	$\begin{bmatrix} 2.00 \\ 2.99 \end{bmatrix}$	$\begin{array}{ c c }\hline 0.12\\ 0.18\end{array}$	$2.00 \\ 2.99$	$\begin{array}{c c} 0.13 \\ 0.20 \end{array}$	$\frac{2}{3}$
5	3.99	$0.21 \\ 0.26$	$\frac{3.99}{4.99}$	$\begin{array}{c} 0.23 \\ 0.28 \end{array}$	$\begin{bmatrix} 3.99 \\ 4.99 \end{bmatrix}$	$0.24 \\ 0.31$	3.99 4.99	$0.26 \\ 0.33$	4 5
6 7	5.99	0.31	5.99	0.34	5.99	0.37	5.99	0.39	6
8	6.99	$\begin{bmatrix} 0.37 \\ 0.42 \end{bmatrix}$	6.99	$\begin{array}{c} 0.40 \\ 0.45 \end{array}$	6.99	$\begin{vmatrix} 0.43 \\ 0.49 \end{vmatrix}$	6.99 7.98	$\begin{array}{c} 0.46 \\ 0.52 \end{array}$	7 8
9 10	8.99	$\begin{array}{c c} 0.47 \\ 0.52 \end{array}$	$8.99 \\ 9.98$	$\begin{array}{c} 0.51 \\ 0.57 \end{array}$	8.98 9.98	$0.55 \\ 0.61$	8.98 9.98	0.59	$\frac{9}{10}$
11	10.98	0.58	10.98	0.62	10.98	0.67	10.98	0.72	11
12 13	$  11.98 \\ 12.98 $	$\begin{array}{c} 0.63 \\ 0.68 \end{array}$	$  \begin{array}{c} 11.98 \\ 12.98 \end{array}  $	$\begin{array}{c} \textbf{0.68} \\ \textbf{0.73} \end{array}$	11.98 12.98	$\begin{bmatrix} 0.73 \\ 0.79 \end{bmatrix}$	11.97 $12.97$	$\begin{array}{c} 0.78 \\ 0.85 \end{array}$	12 13
14 15	$13.98 \\ 14.98$	$\begin{bmatrix} 0.73 \\ 0.79 \end{bmatrix}$	$\begin{bmatrix} 13.98 \\ 14.98 \end{bmatrix}$	$\begin{array}{c} 0.79 \\ 0.85 \end{array}$	$13.97 \\ 14.97$	$\begin{array}{c} 0.85 \\ 0.92 \end{array}$	$13.97 \\ 14.97$	$\begin{array}{c} 0.92 \\ 0.98 \end{array}$	14 15
16 17	15.98 16.98	$\begin{bmatrix} 0.84 \\ 0.89 \end{bmatrix}$	15.97	0.91	15.97	0.98	15.97	1.05	16
18	17.98	0.94	16.97 $17.97$	$\begin{array}{c} 0.96 \\ 1.02 \end{array}$	$  16.97 \\ 17.97 $	$1.04 \\ 1.10$	$16.96 \\ 17.96$	$\frac{1.11}{1.18}$	17 18
19 20	$18.98 \\ 19.97$	$\begin{array}{c} \textbf{0.99} \\ \textbf{1.05} \end{array}$	$18.97 \\ 19.97$	$\frac{1.08}{1.13}$	$18.96 \\ 19.96$	$\begin{array}{c c} 1.16 \\ 1.22 \end{array}$	18.96   19.96	$\frac{1.24}{1.31}$	19 20
21 22	20.97	1.10	20.97	1.19	20.96	1.28	20.96	1.37	21
23	$\begin{vmatrix} 21.97 \\ 22.97 \end{vmatrix}$	$\begin{array}{c} 1.15 \\ 1.20 \end{array}$	$\begin{vmatrix} 21.96 \\ 22.96 \end{vmatrix}$	$\begin{array}{c} 1.25 \\ 1.30 \end{array}$	$\begin{vmatrix} 21.96 \\ 22.96 \end{vmatrix}$	$\begin{array}{c c} 1.34 \\ 1.40 \end{array}$	$\begin{bmatrix} 21.95 \\ 22.95 \end{bmatrix}$	$\begin{array}{c} 1.44 \\ 1.50 \end{array}$	22 23
24 25	$\begin{bmatrix} 23.97 \\ 24.97 \end{bmatrix}$	$\begin{array}{c} 1.26 \\ 1.31 \end{array}$	$\begin{bmatrix} 23.96 \\ 24.96 \end{bmatrix}$	$\begin{array}{c} 1.36 \\ 1.42 \end{array}$	$\begin{bmatrix} 23.96 \\ 24.95 \end{bmatrix}$	$\begin{array}{c} 1.47 \\ 1.53 \end{array}$	$\begin{vmatrix} 23.95 \\ 24.95 \end{vmatrix}$	$\begin{array}{c} 1.57 \\ 1.64 \end{array}$	24 25
26 27	$\begin{bmatrix} 25.96 \\ 26.96 \end{bmatrix}$	$\begin{array}{c c} 1.36 \\ 1.41 \end{array}$	25.96 26.96	$\frac{1.47}{1.53}$	$\begin{vmatrix} 25.95 \\ 26.95 \end{vmatrix}$	$\begin{array}{c} 1.59 \\ 1.65 \end{array}$	25.94 26.94	1.70	26 27
28	27.96	1.47	27.95	1.59	27.95	1.71	27.94	$\begin{bmatrix} 1.77 \\ 1.83 \end{bmatrix}$	28
29	$\begin{bmatrix} 28.96 \\ 29.96 \end{bmatrix}$	$\begin{bmatrix} 1.52 \\ 1.57 \end{bmatrix}$	28.95 29.95	$\begin{array}{c} 1.64 \\ 1.70 \end{array}$	$\begin{vmatrix} 28.95 \\ 29.94 \end{vmatrix}$	$\begin{array}{c} 1.77 \\ 1.83 \end{array}$	$\begin{vmatrix} 28.94 \\ 29.94 \end{vmatrix}$	$\begin{array}{c} 1.90 \\ 1.96 \end{array}$	29 30
$\frac{\overline{31}}{32}$	$30.96 \\ 31.96$	$\begin{array}{c} 1.62 \\ 1.67 \end{array}$	30.95 31.95	1.76 1.81	$30.94 \\ 31.94$	1.89 1.95	30.93 31.93	2.03	31
33	32.95	1.73	32.95	1.87	32.94	2.01	32.93	$\begin{bmatrix} 2.09 \\ 2.16 \end{bmatrix}$	32 33
34 35	$33.95 \\ 34.95$	$\begin{bmatrix} 1.78 \\ 1.83 \end{bmatrix}$	$\begin{bmatrix} 33.95 \\ 34.94 \end{bmatrix}$	$\begin{array}{c c} 1.93 \\ 1.98 \end{array}$	$\begin{vmatrix} 33.94 \\ 34.93 \end{vmatrix}$	$2.08 \\ 2.14$	$\begin{vmatrix} 33.93 \\ 34.92 \end{vmatrix}$	$\begin{bmatrix} 2.22 \\ 2.29 \end{bmatrix}$	34   35
36 37	35.95 36.95	$\begin{array}{c} 1.88 \\ 1.94 \end{array}$	$35.94 \\ 36.94$	$\begin{bmatrix} 2.04 \\ 2.10 \end{bmatrix}$	35.93 36.93	$\begin{array}{c c} 2.20 \\ 2.26 \end{array}$	$\begin{vmatrix} 35.92 \\ 36.92 \end{vmatrix}$	$\begin{bmatrix}2.35\\2.42\end{bmatrix}$	36 37
38	37.95	1.99	37.94	2.15	37.93	2.32	37.92	2.49	38
39 40	$\begin{array}{c} 38.95 \\ 39.95 \end{array}$	$\begin{bmatrix} 2.04 \\ 2.09 \end{bmatrix}$	$\frac{38.94}{39.94}$	$\begin{bmatrix} 2.21 \\ 2.27 \end{bmatrix}$	$\begin{vmatrix} 38.93 \\ 39.93 \end{vmatrix}$	$2.38 \\ 2.44$	$\begin{bmatrix} 38.92 \\ 39.91 \end{bmatrix}$	$\begin{bmatrix} 2.55 \\ 2.62 \end{bmatrix}$	39 40
$\begin{vmatrix} 41\\42 \end{vmatrix}$	40.94	$2.15 \\ 2.20$	40.93 41.93	$\begin{array}{ c c }\hline 2.32\\ 2.38\\ \end{array}$	$40.92 \\ 41.92$	$2.50 \\ 2.56$	40.91	2.68	41
43	42.94	2.25	42.93	2.44	42.92	2.63	41.91  42.91	$\begin{bmatrix} 2.75 \\ 2.81 \end{bmatrix}$	42 43
44 45	$\frac{43.94}{44.94}$	$\begin{bmatrix} 2.30 \\ 2.36 \end{bmatrix}$	$\begin{vmatrix} 43.93 \\ 44.93 \end{vmatrix}$	$2.49 \\ 2.55$	$\begin{bmatrix} 43.92 \\ 44.92 \end{bmatrix}$	$\begin{bmatrix} 2.69 \\ 2.75 \end{bmatrix}$	$\frac{43.91}{44.90}$	2.88   2.94	44 45
46 47	45.94 46.94	$\begin{bmatrix} 2.41 \\ 2.46 \end{bmatrix}$	$\begin{array}{c c} 45.93 \\ 46.92 \end{array}$	$\begin{array}{c c} 2.61 \\ 2.66 \end{array}$	45.91  46.91	2.81 2.87	$\begin{array}{c c} 45.90 \\ 46.90 \end{array}$	$\frac{3.01}{3.07}$	46 47
48	47.93 48.93	$2.51 \\ 2.56$	$   \begin{vmatrix}     47.92 \\     48.92   \end{vmatrix} $	2.72	47.91	2.93	47.90	3.14	48
50	49.93	$\frac{2.60}{2.62}$	49.92	$\begin{bmatrix} 2.78 \\ 2.83 \end{bmatrix}$	$\begin{array}{c} 48.91 \\ 49.91 \end{array}$	$\begin{bmatrix} 2.99 \\ 3.05 \end{bmatrix}$	$\frac{48.90}{49.89}$	$\begin{bmatrix} 3.20 \\ 3.27 \end{bmatrix}$	49 50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	.nce
Dist	87 D	eg.	863 1	Deg.	$86\frac{1}{2}$ ]	Deg.	86 <del>1</del> I	Deg.	Distance.

Distance.	3 I	eg.	31 ]	Deg.	3 <u>1</u> ]	Deg.	. 33 ]	Deg.	Dist
ince.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 70 71 72 73 74 75 76 77	Lat.  50.93 51.93 52.93 53.93 54.92 55.92 56.92 57.92 59.92 60.92 61.92 62.91 63.91 64.91 65.91 66.91 67.91 68.91 69.90 70.90 71.90 72.90 73.90 74.90 75.90 76.89	Dep.  2.67 2.72 2.77 2.83 2.88 2.98 3.04 3.09 3.14 3.19 3.24 3.30 3.35 3.40 3.45 3.51 3.66 3.72 3.77 3.82 3.87 3.98 4.03	50.92 51.92 52.91 53.91 54.91 55.91 56.91 57.91 59.90 60.90 61.90 62.90 63.90 64.90 65.89 66.89 67.89 68.89 70.89 71.88 72.88 73.88 74.88 75.88 76.88	Dep.  2.89 2.95 3.00 3.06 3.12 3.17 3.23 3.29 3.34 3.40 3.46 3.51 3.57 3.63 3.69 3.74 3.80 3.86 3.91 3.97 4.03 4.08 4.14 4.20 4.25 4.31 4.37	Lat.  50.90 51.90 52.90 53.90 54.90 55.90 56.89 57.89 59.89 60.89 61.88 62.88 63.88 64.88 65.88 67.87 68.87 69.87 70.87 71.87 72.86 73.86 74.86 75.86 76.86	Dep.  3.11 3.17 3.24 3.30 3.36 3.42 3.48 3.54 3.60 3.66 3.72 3.79 3.85 3.91 3.97 4.03 4.09 4.15 4.21 4.27 4.33 4.40 4.46 4.52 4.58 4.64 4.70	Lat.  50.89 51.89 52.89 53.88 54.88 55.88 56.88 56.88 57.88 60.87 61.87 62.87 63.86 64.86 65.86 66.86 67.85 70.85 71.85 72.84 73.84 75.84 76.84	Dep.  3.34 3.40 3.47 3.53 3.60 3.66 3.73 3.79 3.86 3.92 3.99 4.05 4.12 4.19 4.25 4.32 4.38 4.45 4.51 4.58 4.64 4.71 4.77 4.84 4.91 4.97 5.04	100-   511 523 545 556 578 560   61 623 645 667 669 70 71 72 74 75 77 77
78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94	77.89 78.89 79.89 80.89 81.89 82.89 83.88 84.88 85.88 86.88 87.88 88.88 90.88 91.87 92.87 93.87	4.08 4.13 4.19 4.24 4.29 4.34 4.40 4.45 4.50 4.55 4.61 4.66 4.71 4.76 4.81 4.87 4.92	77.87 78.87 79.87 80.87 81.87 82.87 83.86 84.86 85.86 86.86 87.86 88.86 89.86 90.85 91.85 92.85 93.85	4.42 4.48 4.54 4.59 4.65 4.71 4.76 4.82 4.88 4.93 4.99 5.05 5.10 5.16 5.22 5.27 5.33	77.85 78.85 79.85 80.85 81.85 82.85 83.84 84.84 85.84 86.84 87.84 88.83 89.83 90.83 91.83 92.83 93.82	4.76 4.82 4.88 4.94 5.01 5.07 5.13 5.19 5.25 5.31 5.37 5.43 5.49 5.62 5.68 5.74	77.83 78.83 79.83 80.83 81.82 82.82 83.82 84.82 85.82 86.81 87.81 88.81 90.81 91.80 92.80 93.80	5.10 5.17 5.23 5.30 5.36 5.43 5.49 5.56 5.62 5.69 5.76 5.82 5.89 5.95 6.02 6.08 6.15	78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94
Distance.   00   00   00   00   00   00   00	94.87 95.87 96.87 97.87 98.86 99.86 Dep.	4.97 5.02 5.08 5.13 5.18 5.23 Lat.	94.85 95.85 96.84 97.84 98.84 99.84 Dep.	5.39 5.44 5.50 5.56 5.61 5.67 Lat.	$\begin{array}{c} 94.82 \\ 95.82 \\ 96.82 \\ 97.82 \\ 98.82 \\ \hline 99.81 \\ \hline \hline \\ \hline $	5.80 5.86 5.92 5.98 6.04 6.10 Lat.	94.80 95.79 96.79 97.79 98.79 99.79 Dep.	6.21 6.28 6.34 6.41 6.47 6.54 Lat.	Distance. 066 846 966 846

70		1		1		li		1		
1	Distance.	4 I	Deg.	41	Deg.	$4\frac{1}{2}$ ]	Deg.	43/4	Deg.	Distance.   12
l	nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
I	$\frac{1}{2}$	$\begin{bmatrix} 1.00 \\ 2.00 \end{bmatrix}$	$\begin{array}{c} 0.07 \\ 0.14 \end{array}$	$\frac{1.00}{1.99}$	$\begin{array}{c} 0.07 \\ 0.15 \end{array}$	$\begin{array}{ c c }\hline 1.00\\ 1.99\\ \end{array}$	$\begin{array}{c} \hline 0.08 \\ 0.16 \end{array}$	$\frac{1.00}{1.99}$	$\begin{array}{c} 0.08 \\ 0.17 \end{array}$	1
ı	2 3 4	$\begin{bmatrix} 2.99 \\ 3.99 \end{bmatrix}$	$\begin{array}{c} 0.21 \\ 0.28 \end{array}$	2.99 3.99	$\begin{bmatrix} 0.22 \\ 0.30 \end{bmatrix}$	2.99	0.24	2.99	0.25	3
I	5	4.99	0.35	4.99	0.37	$\begin{vmatrix} 3.99 \\ 4.98 \end{vmatrix}$	0.31	3.98 4.98	$\begin{array}{c} 0.33 \\ 0.41 \end{array}$	4 5
ı	7	$\begin{bmatrix} 5.99 \\ 6.98 \end{bmatrix}$	$\begin{bmatrix} 0.42 \\ 0.49 \end{bmatrix}$	$\begin{bmatrix} 5.98 \\ 6.98 \end{bmatrix}$	$\begin{bmatrix} 0.44 \\ 0.52 \end{bmatrix}$	$\begin{bmatrix} 5.98 \\ 6.98 \end{bmatrix}$	$\begin{bmatrix} 0.47 \\ 0.55 \end{bmatrix}$	$\begin{bmatrix} 5.98 \\ 6.97 \end{bmatrix}$	$\begin{array}{c} 0.50 \\ 0.58 \end{array}$	6
	8 9	$\begin{bmatrix} 7.98 \\ 8.98 \end{bmatrix}$	$\begin{array}{c} 0.56 \\ 0.63 \end{array}$	$\begin{bmatrix} 7.98 \\ 8.98 \end{bmatrix}$	$\begin{bmatrix} 0.59 \\ 0.67 \end{bmatrix}$	$\begin{bmatrix} 7.98 \\ 8.97 \end{bmatrix}$	$\begin{array}{c c} 0.63 \\ 0.71 \end{array}$	$\begin{array}{ c c } 7.97 \\ 8.97 \end{array}$	$\begin{array}{c} 0.66 \\ 0.75 \end{array}$	8 9
	$\frac{10}{11}$	$\frac{9.98}{10.97}$	$\frac{0.70}{0.77}$	$\left \frac{9.97}{10.97}\right $	$\frac{0.74}{0.82}$	$\left \frac{9.97}{10.97}\right $	$\frac{0.78}{0.86}$	$\begin{array}{ c c }\hline 9.97 \\\hline 10.96 \\\hline \end{array}$	0.83	_10
I	12 13	$11.97 \\ 12.97$	$0.84 \\ 0.91$	$\begin{vmatrix} 11.97 \\ 12.96 \end{vmatrix}$	0.89	11.96	0.94	11.96	$\begin{array}{c} 0.91 \\ 0.99 \\ \end{array}$	11 12
l	14	13.97	0.98	13.96	$\begin{array}{c} 0.96 \\ 1.64 \end{array}$	$\begin{vmatrix} 12.96 \\ 13.96 \end{vmatrix}$	1.02	12.96 13.95	$\begin{array}{c} 1.08 \\ 1.16 \end{array}$	13 14
1	15 16	14.96 15.96	$\begin{vmatrix} 1.05 \\ 1.12 \end{vmatrix}$	$\begin{array}{ c c }\hline 14.96\\ 15.96\\ \end{array}$	$\begin{array}{c} 1.11 \\ 1.19 \end{array}$	$\begin{array}{c c} 14.95 \\ 15.95 \end{array}$	$1.18 \\ 1.26$	14.95 15.95	$\begin{array}{c} 1.24 \\ 1.32 \end{array}$	15 16
	17 18	$\begin{array}{c} 16.96 \\ 17.96 \end{array}$	$\begin{array}{c} 1.19 \\ 1.26 \end{array}$	16.95   17.95	$\begin{array}{c} 1.26 \\ 1.33 \end{array}$	$\begin{array}{c c} 16.95 \\ 17.94 \end{array}$	$1.33 \\ 1.41$	$16.94 \\ 17.94$	$\frac{1.41}{1.49}$	17 18
ı	$\begin{vmatrix} 19 \\ 20 \end{vmatrix}$	$\begin{array}{c c} 18.95 \\ 19.95 \end{array}$	$\begin{array}{c c} 1.33 \\ 1.40 \end{array}$	$18.95 \\ 19.95$	$\begin{array}{c} 1.40 \\ 1.48 \end{array}$	$\begin{array}{c c} 18.94 \\ 19.94 \end{array}$	$\begin{bmatrix} 1.49 \\ 1.57 \end{bmatrix}$	$   \begin{array}{c c}     18.93 \\     19.93   \end{array} $	$\begin{array}{c} 1.57 \\ 1.66 \end{array}$	19 20
١	21	20.95	1.46	$\overline{20.94}$	1.56	20.94	1.65	20.93	$\frac{-1.74}{}$	$\overline{21}$
	22 23	$\begin{vmatrix} 21.95 \\ 22.94 \\ \end{vmatrix}$	1.53	$\begin{vmatrix} 21.94 \\ 22.94 \end{vmatrix}$	$\begin{array}{c} 1.63 \\ 1.70 \end{array}$	$egin{array}{c c} 21.93 \ 22.93 \ \end{array}$	$\begin{bmatrix} 1.73 \\ 1.80 \end{bmatrix}$	$\begin{bmatrix} 21.92 \\ 22.92 \end{bmatrix}$	$\begin{array}{c} 1.82 \\ 1.90 \end{array}$	22 23
I	24 25	$\begin{bmatrix} 23.94 \\ 24.94 \end{bmatrix}$	$\begin{array}{c} 1.67 \\ 1.74 \end{array}$	$oxed{23.93}{24.93}$	$\begin{array}{c c} 1.78 \\ 1.85 \end{array}$	$\begin{bmatrix} 23.93 \\ 24.92 \end{bmatrix}$	$\begin{array}{c c} 1.88 \\ 1.96 \end{array}$	$\begin{vmatrix} 23.92 \\ 24.91 \end{vmatrix}$	$\begin{array}{c} 1.99 \\ 2.07 \end{array}$	24 25
l	$\begin{bmatrix} 26 \\ 27 \end{bmatrix}$	$\begin{bmatrix} 25.94 \\ 26.93 \end{bmatrix}$	1.81	$\left  egin{array}{c} 25.93 \ 26.93 \ \end{array} \right $	$\begin{bmatrix} 1.93 \\ 2.00 \end{bmatrix}$	$\begin{bmatrix} 25.92 \\ 26.92 \end{bmatrix}$	$2.04 \\ 2.12$	$25.91 \\ 26.91$	$2.15 \\ 2.24$	$\begin{array}{c} 26 \\ 27 \end{array}$
l	28 29	$\begin{vmatrix} 27.93 \\ 28.93 \end{vmatrix}$	$\begin{bmatrix} 1.95 \\ 2.02 \end{bmatrix}$	$\begin{bmatrix} 27.92 \\ 28.92 \end{bmatrix}$	$2.08 \\ 2.15$	$\begin{bmatrix} 27.91 \\ 28.91 \end{bmatrix}$	$\begin{bmatrix} 2.20 \\ 2.28 \end{bmatrix}$	$\begin{vmatrix} 27.90 \\ 28.90 \end{vmatrix}$	2.32	28
١	30	29.93	2.09	29.92	2.22	29.91	2.35	29.90	$\begin{array}{c} 2.40 \\ 2.48 \end{array}$	29 30
I	31 32	$\begin{bmatrix} 30.92 \\ 31.92 \end{bmatrix}$	$\begin{bmatrix} 2.16 \\ 2.23 \end{bmatrix}$	$\begin{vmatrix} 30.91 \\ 31.91 \end{vmatrix}$	$\begin{bmatrix} 2.30 \\ 2.37 \end{bmatrix}$	$\begin{bmatrix} 30.90 \\ 31.90 \end{bmatrix}$	$2.43 \\ 2.51$	30.89 31.89	$\frac{2.57}{2.65}$	$\begin{array}{c c} \hline 31 \\ 32 \end{array}$
ı	33 34	$\begin{bmatrix} 32.92 \\ 33.92 \end{bmatrix}$	$\begin{bmatrix} 2.30 \\ 2.37 \end{bmatrix}$	$\begin{vmatrix} 32.91 \\ 33.91 \end{vmatrix}$	$\begin{array}{c c} 2.45 \\ 2.52 \end{array}$	$\begin{bmatrix} 32.90 \\ 33.90 \end{bmatrix}$	$2.59 \\ 2.67$	$\begin{vmatrix} 32.89 \\ 33.88 \end{vmatrix}$	$\begin{array}{c} 2.73 \\ 2.82 \end{array}$	33 34
to.	35 36	$\frac{34.91}{35.91}$	$2.44 \\ 2.51$	$\begin{vmatrix} 34.90 \\ 35.90 \end{vmatrix}$	$2.59 \\ 2.67$	34.89 35.89	$\frac{2.75}{2.82}$	34.88 35.88	2.90	35
	37 38	$   \begin{array}{c c}     36.91 \\     37.91   \end{array} $	$2.58 \\ 2.65$	$\begin{vmatrix} 36.90 \\ 37.90 \end{vmatrix}$	2.74	36.89	2.90	36.87	$\begin{array}{c} 2.98 \\ 3.06 \end{array}$	36 37
	39	38.90	2.72	38.89	2.82	37.88 38.88	2.98 3.06	$\begin{vmatrix} 37.87 \\ 38.87 \end{vmatrix}$	$\frac{3.15}{3.23}$	38 39
	$\frac{40}{41}$	$\begin{array}{c c} 39.90 \\ \hline 40.90 \end{array}$	$\frac{2.79}{2.86}$	$\left \frac{39.89}{40.89}\right $	$\begin{array}{ c c }\hline 2.96 \\ \hline 3.04 \\ \hline \end{array}$	$\begin{array}{ c c }\hline 39.88 \\ \hline 40.87 \\ \hline \end{array}$	$\frac{3.14}{3.22}$	$\frac{39.86}{40.86}$	$\frac{3.31}{3.40}$	$\left  \frac{40}{41} \right $
۱	42 43	$\begin{array}{c c} 41.90 \\ 42.90 \end{array}$	$\begin{bmatrix} 2.93 \\ 3.00 \end{bmatrix}$	$ \begin{array}{c} 41.88 \\ 42.88 \end{array} $	$\begin{vmatrix} 3.11 \\ 3.19 \end{vmatrix}$	41.87  42.87	$\frac{3.30}{3.37}$	$\begin{vmatrix} 41.86 \\ 42.85 \end{vmatrix}$	$\frac{3.48}{3.56}$	42
ı	44 45	43.89 44.89	$\frac{3.07}{3.14}$	43.88	3.26	43.86	3.45	43.85	3.64	43 44
-	46 47	45.89	3.21	45.87	$\begin{bmatrix} 3.33 \\ 3.41 \\ 9.49 \end{bmatrix}$	44.86	3.53	44.85	3.73 3.81	45 46
	48	46.89  47.88	3.28 3.35	46.87 $47.87$	3.48	$ \begin{array}{c} 46.86 \\ 47.85 \end{array} $	$\begin{bmatrix} 3.69 \\ 3.77 \end{bmatrix}$	46.84  $ 47.84 $	$\frac{3.89}{3.97}$	47 48
	49 50	48.88	$\begin{bmatrix} 3.42 \\ 3.49 \end{bmatrix}$	48.87 49.86	$\begin{bmatrix} 3.63 \\ 3.71 \end{bmatrix}$	48.85	$\begin{vmatrix} 3.84 \\ 3.92 \end{vmatrix}$	48.83	4.06	49 50
	nce.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
	Distance.	86 ]	Deg.	853	Deg.	85 <u>1</u>	Deg.	851/4	Deg.	Distance.
1								100		

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Distance.	4 I	Deg.	44	Deg.	4½ I	Deg.	43	Deg.	Distance.
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ince.
51 52	50.88 51.87	3.56 3.63	50.86 51.86	$\frac{3.78}{3.85}$	$\overline{\frac{50.84}{51.84}}$	4.00 4.08	$\begin{array}{ c c c }\hline 50.82\\51.82\\ \end{array}$	$4.22 \\ 4.31$	51 52
53 54	52.87 53.87	$\begin{vmatrix} 3.70 \\ 3.77 \end{vmatrix}$	52.85 53.85	3.93 4.00	52.84 53.83	$\begin{vmatrix} 4.16 \\ 4.24 \end{vmatrix}$	52.82 53.81	$\begin{vmatrix} 4.39 \\ 4.47 \end{vmatrix}$	53 54
55 56	54.87 55.86	$\frac{3.84}{3.91}$	54.85 55.85	4.08 4.15	54.83 55.83	$\begin{array}{c c} 4.32 \\ 4.39 \\ \end{array}$	54.81 55.81	4.55	55 56
57 58	56.86 57.86	3.98 4.05	56.84 57.84	$4.22 \\ 4.30$	56.82 57.82	4.47 4.55	56.80 57.80	$\begin{array}{ c c } \hline 4.72 \\ 4.80 \\ \hline \end{array}$	57 58
59 60	58.86 59.85	$\begin{array}{ c c } \hline 4.12 \\ 4.19 \\ \hline \end{array}$	58.84 59.84	4.37 $4.45$	58.82 59.82	$4.63 \\ 4.71$	58.80 59.79	4.89 $4.97$	59 60
$\begin{array}{ c c }\hline 61\\ 62\\ \end{array}$	60.85 61.85	$\frac{4.26}{4.32}$	$\frac{60.83}{61.83}$	4.52	60.81	4.79	60.79 $61.79$	$\frac{5.05}{5.13}$	$\begin{array}{ c c }\hline 61 \\ 62 \\ \hline \end{array}$
63 64	62.85	4.39	62.83 $63.82$	4.59 $4.67$ $4.74$	$61.81 \\ 62.81 \\ 63.80$	4.86	62.78 $63.78$	5.22 5.30	63
65 66	64.84	4.53 4.60	64.82	4.82	64.80 65.80	5.02 5.10 5.18	64.78 $65.77$	5.38 5.47	65 66
67 68	66.84 67.83	$\frac{4.67}{4.74}$	66.82	4.97 5.04	66.79 $67.79$	5.26 5.34	66.77 $67.77$	5.55 5.63	67 68
69 70	68.83	4.81 4.88	68.81	5.11 5.19	$\begin{vmatrix} 68.79 \\ 69.78 \end{vmatrix}$	5.41 5.49	68.76 69.76	5.71 5.80	69 70
$\frac{71}{72}$	70.83	4.95	70.80	$\frac{-5.26}{}$	70.78	5.57	70.76	5.88	$\overline{71}$
73 74	$egin{array}{c} 71.82 \\ 72.82 \\ 73.82 \\ \hline \end{array}$	$\begin{array}{c} 5.02 \\ 5.09 \\ 5.16 \end{array}$	71.80 $72.80$	5.34 5.41	71.78 $72.77$	5.65	71.75	5.96	72 73
75 76	74.82	5.16 $5.23$	73.80 $74.79$	5.48	73.77 $74.77$	5.81 5.88	73.75	6.13	74 75
77 78	75.81	5.30 5.37	75.79	5.63	75.77	$\begin{array}{c} 5.96 \\ 6.04 \\ 6.10 \end{array}$	75.74	6.29 $6.38$	76
79 80	$egin{array}{c c} 77.81 \\ 78.81 \\ 79.81 \\ \hline \end{array}$	5.44	77.79	5.78 5.85	77.76	$\begin{array}{c} 6.12 \\ 6.20 \\ 6.20 \end{array}$	77.73	6.46	78 79
81	80.80	$\frac{5.58}{5.65}$	$\frac{79.78}{80.78}$	$\frac{5.93}{6.00}$	$\begin{array}{ c c }\hline 79.75 \\ \hline 80.75 \\ \hline \end{array}$	$\frac{6.28}{6.36}$	$\frac{79.73}{80.72}$	$\frac{6.62}{6.71}$	$\begin{array}{ c c } \hline 80 \\ \hline 81 \\ \end{array}$
82 83	$\begin{vmatrix} 81.80 \\ 82.80 \end{vmatrix}$	5.72 5.79	81.78	$\begin{array}{c} 6.08 \\ 6.15 \end{array}$	81.75 82.74	$\begin{array}{c c} 6.43 \\ 6.51 \end{array}$	$\begin{vmatrix} 81.72 \\ 82.71 \end{vmatrix}$	$\begin{array}{c} 6.79 \\ 6.87 \end{array}$	82 83
84 85	$\begin{vmatrix} 83.80 \\ 84.79 \end{vmatrix}$	$\begin{array}{c} 5.86 \\ 5.93 \end{array}$	83.77	$\begin{array}{c} 6.23 \\ 6.30 \end{array}$	$\begin{bmatrix} 83.74 \\ 84.74 \end{bmatrix}$	$\begin{array}{c} 6.59 \\ 6.67 \end{array}$	$\begin{vmatrix} 83.71 \\ 84.71 \end{vmatrix}$	6.96 7.04	84 85
86 87	85.79   86.79	$\begin{array}{c} 6.00 \\ 6.07 \end{array}$	85.76	$\begin{array}{c} 6.37 \\ 6.45 \end{array}$	$\begin{bmatrix} 85.73 \\ 86.73 \end{bmatrix}$	$\begin{array}{c} 6.75 \\ 6.83 \end{array}$	85.70	$7.12 \\ 7.20$	86
88	87.79	6.14 $6.21$	87.76	$\begin{array}{c} 6.52 \\ 6.60 \\ 6.67 \end{array}$	87.73	$\begin{array}{c c} 6.90 \\ 6.98 \\ \hline \end{array}$	87.70	7.29 $7.37$	88 89
$\frac{90}{91}$	$\left \frac{89.78}{90.78}\right $	$\frac{6.28}{6.35}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\frac{6.67}{6.74}$	$\left \frac{89.72}{90.72}\right $	$\frac{7.06}{7.14}$	$\begin{array}{ c c }\hline 89.69 \\ \hline 90.69 \\ \hline \end{array}$	$\frac{7.45}{7.54}$	$\frac{90}{91}$
92 93	$oxed{91.78} \ oxed{92.77}$	$\begin{array}{c} 6.42 \\ 6.49 \end{array}$	$\begin{bmatrix} 91.75 \\ 92.74 \end{bmatrix}$	$\begin{array}{c} 6.82 \\ 6.89 \end{array}$	$\begin{bmatrix} 91.72 \\ 92.71 \end{bmatrix}$	$\begin{bmatrix} 7.22 \\ 7.30 \end{bmatrix}$	$91.68 \\ 92.68$	$\begin{array}{c} 7.62 \\ 7.70 \end{array}$	92 93
94 95	$\begin{bmatrix} 93.77 \\ 94.77 \end{bmatrix}$	6.56	$\left  \begin{array}{c} 93.74 \\ 94.74 \end{array} \right $	6.97 $7.04$	$\begin{vmatrix} 93.71 \\ 94.71 \end{vmatrix}$	$\begin{array}{c c} 7.38 \\ 7.45 \end{array}$	$\begin{bmatrix} 93.68 \\ 94.67 \end{bmatrix}$	7.78	94 95
96 97	$\begin{bmatrix} 95.77 \\ 96.76 \end{bmatrix}$	$\begin{bmatrix} 6.70 \\ 6.77 \end{bmatrix}$	$\begin{bmatrix} 95.74 \\ 96.73 \end{bmatrix}$	7.11	$\begin{array}{c c} 95.70 \\ 96.70 \\ \end{array}$	7.53   7.61	$95.67 \\ 96.67$	$\begin{array}{c} 7.95 \\ 8.03 \end{array}$	96 97
98 99	97.76	6.84	$\begin{bmatrix} 97.73 \\ 98.73 \end{bmatrix}$	7.26 $7.34$	$\left  egin{array}{c} 97.70 \ 98.69 \ \end{array} \right $	7.69	97.66  $ 98.66 $	$\begin{array}{c} 8.12 \\ 8.20 \\ \end{array}$	98
$\frac{100}{6}$	$\frac{99.76}{\text{Dep.}}$	6.98 Lat.	$ \frac{  99.73  }{  Dep.  } \frac{  7.41  }{  Lat.  } $		99.69 Don	7.85 Lat.	99.66 Dep.	8.28 Lat.	100
Distance.	Dep.	Liat.	Dep.		Dep.		Dep.	1146.	Distance.
Dis	86 I	eg.	$85\frac{3}{4} \text{ Deg.}$ $85\frac{1}{2} \text{ Deg.}$ $85\frac{1}{4} \text{ Deg.}$		Deg.	Dis			

	1		1		n		#	400000 and	
Distance.	5 I	eg.	51/4	Deg.	51/2	Deg.	53	Deg.	Distance.
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
$\frac{1}{2}$	$1.00 \\ 1.99$	$0.09 \\ 0.17$	$1.00 \\ 1.99$	0.09	$\frac{1.00}{1.99}$	$\begin{array}{ c c }\hline 0.10\\ 0.19\\ \end{array}$	0.99	$0.10 \\ 0.20$	1
2 3 4 5	2.99	$0.26 \\ 0.35$	2.99 3.98	0.27	2.99	0.29	2.98	0.30	2 3
5	4.98	0.44	4.98	$\begin{array}{c c} 0.37 \\ 0.46 \end{array}$	$\begin{vmatrix} 3.98 \\ 4.98 \end{vmatrix}$	$\begin{array}{ c c } \textbf{0.38} \\ \textbf{0.48} \end{array}$	$\frac{3.98}{4.97}$	$\begin{array}{c c} 0.40 \\ \hline 0.50 \end{array}$	4 5
6 7	5.98	$\begin{array}{c} 0.52 \\ 0.61 \end{array}$	$\begin{bmatrix} 5.97 \\ 6.97 \end{bmatrix}$	$\begin{array}{c} 0.55 \\ 0.64 \end{array}$	5.97	$\begin{array}{c} 0.58 \\ 0.67 \end{array}$	5.97 6.96	$\begin{array}{c} 0.60 \\ 0.70 \end{array}$	6 7
8 9	7.97 8.97	$\left \begin{array}{c} 0.70 \\ 0.78 \end{array}\right $	$\begin{array}{ c c }\hline 7.97\\ 8.96\end{array}$	$\begin{array}{c} 0.73 \\ 0.82 \end{array}$	7.96 8 96	$\begin{array}{c} 0.76 \\ 0.86 \end{array}$	$7.96 \\ 8.95$	$0.80 \\ 0.90$	8
10	9.96	0.87	9.96	0.92	9.95	0.96	9.95	1.00	10
11 12	10.96 $11.95$	$\begin{array}{c} 0.96 \\ 1.05 \end{array}$	$10.95 \\ 11.95$	$\begin{array}{c} 1.01 \\ 1.10 \end{array}$	$10.95 \\ 11.94$	$\begin{array}{c c} 1.05 \\ 1.15 \end{array}$	10.94   11.94	$\begin{array}{c} 1.10 \\ 1.20 \end{array}$	11 12
13 14	$12.95 \\ 13.95$	$\begin{bmatrix} 1.13 \\ 1.22 \end{bmatrix}$	$  \begin{array}{c} 12.95 \\ 13.94 \end{array}  $	$\begin{array}{c} 1.19 \\ 1.28 \end{array}$	$\begin{vmatrix} 12.94 \\ 13.94 \end{vmatrix}$	$\begin{array}{c} 1.25 \\ 1.34 \end{array}$	$\begin{vmatrix} 12.93 \\ 13.93 \end{vmatrix}$	$\begin{array}{c} 1.30 \\ 1.40 \end{array}$	13 14
15 16	14.94 15.94	1.31 1.39	$14.94 \\ 15.93$	1.37	14.93	1.44	14.92	1.50	15
17	16.94	1.48	16.93	$\begin{array}{c} 1.46 \\ 1.56 \end{array}$	15.93 $16.92$	$\begin{array}{c} 1.53 \\ 1.63 \end{array}$	$\begin{array}{c c} 15.92 \\ 16.91 \end{array}$	$\begin{array}{c} 1.60 \\ 1.70 \end{array}$	16 17
18 19	17.93   18.93	$\begin{array}{c} 1.57 \\ 1.66 \end{array}$	$\begin{bmatrix} 17.92 \\ 18.92 \end{bmatrix}$	$\begin{array}{c} 1.65 \\ 1.74 \end{array}$	17.92   18.91	$\begin{array}{c c} 1.73 \\ 1.82 \end{array}$	17.91   18.90	$\begin{array}{c} 1.80 \\ 1.90 \end{array}$	18 19
$\frac{20}{21}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\frac{1.74}{1.83}$	$\frac{19.92}{20.91}$	$\frac{1.83}{1.92}$	$\frac{19.91}{20.90}$	1.92	19.90	2.00	20
22	21.92	1.92	21.91	2.01	21.90	$\begin{bmatrix} 2.01 \\ 2.11 \end{bmatrix}$	$\begin{vmatrix} 20.89 \\ 21.89 \end{vmatrix}$	$\begin{bmatrix} 2.10 \\ 2.20 \end{bmatrix}$	21 22
23 24	$\begin{bmatrix} 22.91 \\ 23.91 \end{bmatrix}$	$\begin{bmatrix} 2.00 \\ 2.09 \end{bmatrix}$	$\left  egin{array}{c} 22.90 \ 23.90 \ \end{array}  ight $	$\begin{bmatrix} 2.10 \\ 2.20 \end{bmatrix}$	$\begin{bmatrix} 22.89 \\ 23.89 \end{bmatrix}$	$\begin{bmatrix} 2.20 \\ 2.30 \end{bmatrix}$	$\begin{bmatrix} 22.88 \\ 23.88 \end{bmatrix}$	$\begin{bmatrix} 2.30 \\ 2.40 \end{bmatrix}$	23 24
25 26	$\begin{bmatrix} 24.90 \\ 25.90 \end{bmatrix}$	$\begin{bmatrix} 2.18 \\ 2.27 \end{bmatrix}$	$\begin{array}{ c c } 24.90 \\ 25.89 \end{array}$	$\begin{array}{c} 2.29 \\ 2.38 \end{array}$	$\begin{vmatrix} 24.88 \\ 25.88 \end{vmatrix}$	$\begin{array}{c c} 2.40 \\ 2.49 \end{array}$	24.87 25.87	$2.50 \\ 2.60$	25 26
27 28	$\begin{bmatrix} 26.90 \\ 27.89 \end{bmatrix}$	$\begin{bmatrix} 2.35 \\ 2.44 \end{bmatrix}$	$\begin{vmatrix} 26.89 \\ 27.88 \end{vmatrix}$	$2.47 \\ 2.56$	$\begin{vmatrix} 26.88 \\ 27.87 \end{vmatrix}$	$\begin{bmatrix} 2.59 \\ 2.68 \end{bmatrix}$	26.86	2.71	27
29	28.89	2.53	28.88	2.65	28.87	2.78	$\begin{bmatrix} 27.86 \\ 28.85 \end{bmatrix}$	$\begin{bmatrix} 2.81 \\ 2.91 \end{bmatrix}$	28 29
$\frac{30}{31}$	$\left \frac{29.89}{30.88}\right $	$\frac{2.61}{2.70}$	$\frac{29.87}{30.87}$	$\begin{array}{c c} 2.75 \\ \hline 2.84 \end{array}$	$\begin{array}{ c c }\hline 29.86 \\ \hline 30.86 \\ \hline \end{array}$	$\frac{2.88}{2.97}$	$\frac{29.85}{30.84}$	$\frac{3.01}{3.11}$	$\frac{30}{31}$
32 33	$\begin{vmatrix} 31.88 \\ 32.87 \end{vmatrix}$	$\frac{2.79}{2.88}$	$\begin{vmatrix} 31.87 \\ 32.86 \end{vmatrix}$	$\begin{bmatrix} 2.93 \\ 3.02 \end{bmatrix}$	$\frac{31.85}{32.85}$	$\frac{3.07}{3.16}$	$\begin{vmatrix} 31.84 \\ 32.83 \end{vmatrix}$	3.21	32
34	33.87 34.87	2.96 3.05	$\begin{vmatrix} 33.86 \\ 34.85 \end{vmatrix}$	3.11	33.84	3.26	33.83	$\begin{bmatrix} 3.31 \\ 3.41 \end{bmatrix}$	33
35 36	35.86	3.14	35.85	$\begin{bmatrix} 3.20 \\ 3.29 \end{bmatrix}$	$\frac{34.84}{35.83}$	$\begin{array}{c} 3.35 \\ 3.45 \end{array}$	$\left  egin{array}{c} 34.82 \ 35.82 \end{array} \right $	$\begin{bmatrix} 3.51 \\ 3.61 \end{bmatrix}$	35 36
37 38	$oxed{36.86} \ 37.86$	$\begin{array}{c} 3.22 \\ 3.31 \end{array}$	$  \frac{36.84}{37.84}  $	$\begin{bmatrix} 3.39 \\ 3.48 \end{bmatrix}$	$\begin{vmatrix} 36.83 \\ 37.83 \end{vmatrix}$	$\begin{array}{c c} 3.55 \\ 3.64 \end{array}$	$\begin{vmatrix} 36.81 \\ 37.81 \end{vmatrix}$	$\begin{bmatrix} 3.71 \\ 3.81 \end{bmatrix}$	37 38
39 40	$\begin{vmatrix} 38.85 \\ 39.85 \end{vmatrix}$	$\begin{array}{c} 3.40 \\ 3.49 \end{array}$	$\begin{vmatrix} 38.84 \\ 39.83 \end{vmatrix}$	$\begin{bmatrix} 3.57 \\ 3.66 \end{bmatrix}$	$\frac{38.82}{39.82}$	$\begin{bmatrix} 3.74 \\ 3.83 \end{bmatrix}$	$\frac{38.80}{39.80}$	$\frac{3.91}{4.01}$	39 40
41	40.84	3.57	40.83	3.75	40.81	3.93	40.79	4.11	41
42 43	41.84  42.84	$\begin{bmatrix} 3.66 \\ 3.75 \end{bmatrix}$	$ \begin{array}{c} 41.82 \\ 42.82 \\ \end{array} $	$\begin{bmatrix} 3.84 \\ 3.93 \end{bmatrix}$	$\begin{vmatrix} 41.81 \\ 42.80 \end{vmatrix}$	$oxed{4.03}{4.12}$	$\begin{vmatrix} 41.79 \\ 42.78 \end{vmatrix}$	$\frac{4.21}{4.31}$	42 43
44 45	$\begin{vmatrix} 43.83 \\ 44.83 \end{vmatrix}$	$\begin{bmatrix} 3.83 \\ 3.92 \end{bmatrix}$	$\begin{array}{ c c c }\hline 43.82 \\ 44.81 \\\hline\end{array}$	$\begin{array}{c c} 4.03 \\ 4.12 \end{array}$	43.80 44.79	4.22 4.31	$\begin{vmatrix} 43.78 \\ 44.77 \end{vmatrix}$	4.41 4.51	44 45
46	45.82  46.82	4.01 4.10	45.81  46.80	$\begin{array}{c} 4.21 \\ 4.30 \end{array}$	45.79 46.78	4.41 4.50	45.77	4.61	46
48	47.82 48.81	4.18 4.27	47.80	4.39	47.78	4.60	$\begin{vmatrix} 46.76 \\ 47.76 \end{vmatrix}$	4.71 4.81	47 48
49 50	49.81	4.27	$     \begin{array}{r}       48.79 \\       49.79     \end{array} $	4.48	48.77	$\begin{array}{c} 4.70 \\ 4.79 \end{array}$	$\begin{vmatrix} 48.75 \\ 49.75 \end{vmatrix}$	$\frac{4.91}{5.01}$	49 50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
Dist	85 ]	Deg.	843	Deg.	$84\frac{1}{2}$	Deg.	841	Deg.	Distance.
-			H						

Dis	5 I	eg.	51 ]	Deg.	512	Deg.	$5\frac{3}{4}$	Deg.	Dis
tance	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	tance
Distance   123345567890   12344567890   12344568888886	Lat.    50.81     51.80     52.80     53.79     54.79     55.79     56.78     59.77     60.77     61.76     62.76     63.76     64.75     65.75     66.75     67.74     69.73     70.73     71.73     72.72     73.72     74.71     75.71     76.71     77.70     79.70     80.69     81.69     82.68     83.68     84.68     85.67	Dep.  4.44 4.53 4.62 4.71 4.79 4.88 4.97 5.06 5.14 5.23 5.40 5.49 5.58 5.67 5.75 5.84 5.93 6.01 6.10 6.19 6.28 6.36 6.45 6.62 6.71 6.80 6.89 6.97 7.06 7.15 7.23 7.41 7.50	Lat.  50.79 51.78 52.78 53.77 54.77 55.77 56.76 57.76 58.75 60.74 61.74 62.74 63.73 64.73 64.73 65.72 66.72 67.71 70.70 71.70 72.69 73.69 74.69 75.68 76.68 77.67 79.66 80.66 81.66 82.65 83.65 84.64 85.64	Dep.  4.67 4.76 4.85 4.94 5.03 5.12 5.22 5.31 5.40 5.58 5.67 5.86 5.95 6.04 6.13 6.22 6.31 6.41 6.50 6.95 7.05 7.14 7.23 7.32 7.69 7.69 7.78 7.87	Lat.    50.77     51.76     52.76     53.75     54.75     55.74     56.74     57.73     59.72     60.72     61.71     62.71     63.71     64.70     65.70     66.69     67.69     67.69     68.68     69.68     70.67     72.66     73.66     74.65     75.65     76.65     76.65     77.64     79.63     80.63     81.62     82.62     83.61     85.60	Dep.  4.89 4.98 5.08 5.18 5.27 5.37 5.46 5.56 5.65 5.75  5.85 6.04 6.13 6.23 6.33 6.42 6.52 6.61 6.71  6.81 6.90 7.00 7.09 7.19 7.28 7.38 7.48 7.57 7.67  7.76 7.86 7.96 8.05 8.15 8.24	Lat.  50.74 51.74 52.73 53.73 54.72 55.72 56.71 57.71 58.70 60.69 61.69 62.68 63.68 64.67 65.67 66.66 67.66 68.65 69.65 70.64 71.64 72.63 73.63 74.62 75.62 76.61 77.61 78.60 79.60 80.59 81.59 82.58 83.58 84.57 85.57	Dep.  5.11 5.21 5.31 5.41 5.51 5.61 5.71 5.81 6.01 6.11 6.21 6.31 6.41 6.51 6.61 6.71 7.01 7.11 7.21 7.31 7.41 7.51 7.61 7.71 7.81 7.91 8.02 8.12 8.32 8.42 8.52 8.62	Distance. 51 523 545 56 66 67 68 69 70 71 72 73 74 75 76 77 89 81 82 83 85 86
87 88 89	86.67 87.67 88.66	7.58 7.67 7.76	86.64 87.63 88.63	7.96 8.05 8.14	86.60 87.59 88.59	8.34 8.43 8.53	86.56 87.56 88.55	8.72 8.82 8.92	87 88 89
90 91 92 93 94 95 96 97 98 99 100	89.66 90.65 91.65 92.65 93.64 94.64 95.63 96.63 97.63 98.62 99.62	7.84 7.93 8.02 8.11 8.19 8.28 8.37 8.45 8.63 8.72	89.62 90.62 91.61 92.61 93.61 94.60 95.60 96.59 97.59 98.59 99.58	8.24 8.33 8.42 9.51 9.60 9.69 8.78 8.88 8.97 9.06 9.15	89.59 90.58 91.58 92.57 93.57 94.56 95.56 96.55 97.55 98.54 99.54	8.63 8.72 8.82 8.91 9.01 9.11 9.20 9.30 9.39 9.49 9.58	89.55 90.54 91.54 92.53 93.53 94.52 96.51 97.51 98.50 99.50	$\begin{array}{r} 9.02 \\ \hline 9.12 \\ 9.22 \\ 9.32 \\ 9.42 \\ 9.52 \\ 9.62 \\ 9.62 \\ 9.72 \\ 9.82 \\ 9.92 \\ 10.02 \\ \end{array}$	90 91 92 93 94 95 96 97 98 99 100
Distance.	85 I	Lat.	Dep.	Lat. Deg.	Dep.   84½	Lat. Deg.	Dep.	Lat. Deg.	Distance.

Dis	6 D	eg.	6½ I	eg.	$6\frac{1}{2}$ I	eg.	63 I	Deg.	Dist
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
1 2 3 4 5 6 7 8 9 10	0.99 1.99 2.98 3.98 4.97 5.97 6.96 7.96 8.95 9.95	0.10 0.21 0.31 0.41 0.52 0.63 0.73 0.84 0.94 1.05	0.99 1.99 2.98 3.98 4.97 5.96 6.96 7.95 8.95 9.94	0.11 0.22 0.33 0.44 0.54 0.65 0.76 0.87 0.98 1.09	0.99 1.99 2.98 3.97 4.97 5.96 6.96 7.95 8.94 9.94	0.11 0.23 0.34 0.45 0.57 0.68 0.79 0.91 1.02 1.13	0.99 1.99 2.98 3.97 4.97 5.96 6.95 7.94 8.94 9.93	$\begin{array}{c} -0.12 \\ 0.24 \\ 0.35 \\ 0.47 \\ 0.59 \\ 0.71 \\ 0.82 \\ 0.94 \\ 1.06 \\ 1.18 \end{array}$	1 2 3 4 5 6 7 8 9 10
11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	10.94 11.93 12.93 13.92 14.92 15.91 16.91 17.90 18.90 19.89 20.88 21.88 22.87 23.87 24.86 25.86 26.85 27.85 28.84 29.84	1.15 1.25 1.36 1.46 1.57 1.67 1.78 1.88 1.99 2.09 2.20 2.30 2.40 2.51 2.61 2.72 2.82 2.93 3.03 3.14	10.93 11.93 12.92 13.92 14.91 15.90 16.90 17.89 18.89 19.88 20.88 21.87 22.86 23.86 24.85 25.85 26.84 27.83 28.83 29.82	1.20 1.31 1.42 1.52 1.63 1.74 1.85 1.96 2.07 2.18 2.29 2.40 2.50 2.61 2.72 2.83 2.94 3.05 3.16 3.27	10.93 11.92 12.92 13.91 14.90 15.90 16.89 17.88 18.83 19.87 20.87 21.86 22.85 23.85 24.84 25.83 26.83 27.82 28.81 29.81	1.25 1.36 1.47 1.59 1.70 1.81 1.92 2.04 2.15 2.26 2.38 2.49 2.60 2.72 2.83 2.94 3.06 3.17 3.28 3.40	10.92 11.92 12.91 13.90 14.90 15.89 16.88 17.88 18.87 19.86 20.85 21.85 22.84 23.83 24.83 25.82 26.81 27.81 28.80 29.79	1.29 1.41 1.53 1.65 1.76 1.88 2.00 2.12 2.23 2.35 2.47 2.59 2.70 2.82 2.94 3.06 3.17 3.29 3.41 3.53	11 12 13 14 15 16 17 18 19 20 21 22 23 24 26 27 29 30
31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49	30.83 31.82 32.82 33.81 34.81 35.80 36.80 37.79 38.79 39.78 40.78 41.77 42.76 44.75 45.75 46.74 47.74	3.24 3.34 3.45 3.55 3.66 3.76 3.87 4.08 4.18 4.29 4.39 4.49 4.60 4.70 4.81 4.91 5.02 5.12	30.82 31.81 32.80 33.80 34.79 35.79 36.78 37.77 39.76 40.76 41.75 42.74 43.74 44.73 45.73 46.72 47.71 48.71	3.37 3.48 3.59 3.70 3.81 3.92 4.03 4.14 4.25 4.35 4.46 4.57 4.68 4.79 4.90 5.01 5.12 5.23 5.34	$     \begin{array}{r}       30.80 \\       31.79 \\       32.79 \\       33.78 \\       34.78 \\       35.77 \\       36.76 \\       37.76 \\       38.75 \\       39.74 \\       \hline       40.74 \\       41.73 \\       42.72 \\       44.71 \\       45.70 \\       46.70 \\       47.69 \\       48.69 \\    \end{array} $	3.51 3.62 3.74 3.85 3.96 4.08 4.19 4.30 4.41 4.53 4.64 4.76 4.87 4.87 4.98 5.09 5.21 5.32 5.43 5.55	30.79 31.78 32.77 33.76 34.76 35.75 36.75 37.74 38.73 39.72 40.72 41.71 42.70 43.68 46.67 47.67 48.66	3.64 3.76 3.88 4.00 4.11 4.23 4.35 4.47 4.58 4.70 4.82 4.94 5.05 5.17 5.29 5.41 5.52 5.64 5.76	31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49
Distance.	49.73	5.23 Lat. Deg.	19.70 Dep.	Lat. Deg.	49.68 Dep.	Lat. Deg.	149.65 Dep.	Lat. Deg.	Distance.

	Distance.		6 Deg. 64 Deg.				1	1 03 T	1	
-					Jeg.	$0_{\overline{2}}$ 1	Deg	04 1	Deg.	Dist
-		Lat.	Dep.	Lat.	Dep.	Lat.	Dep	Lat.	Dep.	Distance.
	51 52 53 54	50.72 51.72 52.71 53.70	5.33 5.44 5.54 5.64	50.70 51.69 52.68 53.68	5.55 5.66 5.77 5.88	50.67 51.67 52.66 53.65	5.77 $5.89$ $6.00$ $6.11$	50.65 51.64 52.63 53.63	5.99 6.11 6.23 6.35	51 52 53 54
	55   56   57   58   59	54.70 55.69 56.69 57.68 58.68	5.75 5.85 5.96 6.06 6.17	54.67 55.67 56.66 57.66 58.65	$5.99 \\ 6.10 \\ 6.21 \\ 6.31 \\ 6.42$	54.65 55.64 56.63 57.63 58.62	6.23 $6.34$ $6.45$ $6.57$ $6.68$	54.62 55.61 56.60 57.60 58.59	$     \begin{array}{c}       6.46 \\       6.58 \\       6.70 \\       6.82 \\       6.93     \end{array} $	55 56 57 58 59
	$\frac{60}{61}$	$\frac{59.67}{60.67}$	$\frac{6.27}{6.38}$	$\frac{59.64}{60.64}$	$\begin{array}{c c} 6.53 \\ \hline 6.64 \end{array}$	$\frac{59.61}{60.61}$	$\frac{6.79}{6.91}$	$\frac{59.58}{60.58}$	$\frac{7.05}{7.17}$	$\frac{60}{61}$
	62 63 64 65	61.66 62.65 63.65 64.64	6.48 $6.59$ $6.69$ $6.79$	$\begin{vmatrix} 61.63 \\ 62.63 \\ 63.62 \end{vmatrix}$	6.75 6.86 6.97 7.08	$egin{array}{c c} 61.60 \\ 62.60 \\ 63.59 \\ \hline \end{array}$	$egin{array}{c c} 7.02 \ 7.13 \ 7.25 \ \end{array}$	61.57 $62.56$ $63.56$ $64.55$	7.29 $7.40$ $7.52$ $7.64$	62 63 64 65
The second secon	66 67 68	65.64 66.63 67.63	$ \begin{array}{c c} 6.90 \\ 7.00 \\ 7.11 \end{array} $	$egin{array}{c} 64.61 \\ 65.61 \\ 66.60 \\ 67.60 \\ \end{array}$	7.19 7.29 7.40	$\begin{array}{c} 64.58 \\ 65.58 \\ 66.57 \\ 67.56 \end{array}$	7.36 $7.47$ $7.58$ $7.70$	65.54 66.54 67.53	7.76 7.88 7.99	66 67 68
1_	69 70	$\begin{array}{c c} 68.62 \\ 69.62 \end{array}$	$\frac{7.21}{7.32}$	68.59	$\frac{7.51}{7.62}$	68.56	$7.81 \\ 7.92$	$68.52 \\ 69.51$	8.11	69 70
	71 72 73 74	70.61 71.61 72.60 73.59	7.42 7.53 7.63 7.74	$egin{array}{c c} 70.58 \ 71.57 \ 72.57 \ 73.56 \ \hline \end{array}$	7.73 7.84 7.95 8.06	70.54 $71.54$ $72.53$ $73.52$	8.04 8.15 8.26 8.38	70.51 $71.50$ $72.49$ $73.49$	8.35 $8.46$ $8.58$ $8.70$	71 72 73 74
	75 76 77	74.59 75.58 76.58	7.84 $7.94$ $8.05$	74.55 75.55 76.54	8.17 8.27 8.38	74.52 75.51 76.51	$8.49 \\ 8.60 \\ 8.72$	74.48 75.47 76.47	8.82 8.93 9.05	75 76 77
1	78 79 80	77.57 $78.57$ $79.56$	$8.15 \\ 8.26 \\ 8.36$	77.54 $78.53$ $79.53$	$8.49 \\ 8.60 \\ 8.71$	77.50 78.49 79.49	$8.83 \\ 8.94 \\ 9.06$	77.46 78.45 79.45	$9.17 \\ 9.29 \\ 9.40$	78 79 80
	81 82 83	80.56 81.55 82.55	8.47 8.57 8.68	$   \begin{array}{c c}     80.52 \\     81.51 \\     82.51   \end{array} $	8.82 8.93 9.04	80.48 81.47 82.47	9.17 $9.28$ $9.40$	80.44 81.43 82.42	9.52 $9.64$ $9.76$	81 82 83
	84 85 86	83.54 84.53 85.53 86.52	$8.78 \\ 8.88 \\ 8.99 \\ 9.09$	83.50 84.50 85.49	9.14 $9.25$ $9.36$	83.46 84.45 85.45	9.51 $9.62$ $9.74$	$\begin{vmatrix} 83.42 \\ 84.41 \\ 85.40 \\ 86.40 \end{vmatrix}$	$egin{array}{c} 9.87 \ 9.99 \ 10.11 \ 10.23 \ \end{array}$	84 85 86 87
	87 88 89 90	87.52 88.51 89.51	$   \begin{array}{c}     9.09 \\     9.20 \\     9.30 \\     9.41   \end{array} $	$egin{array}{c} 86.48 \ 87.48 \ 88.47 \ 89.47 \ \end{array}$	9.47 9.58 9.69 9.80	86.44 87.43 88.43 89.42	$9.85 \\ 9.96 \\ 10.08 \\ 10.19$	87.39 88.38 89.38	$     \begin{array}{c c}       10.23 \\       10.34 \\       10.46 \\       10.58     \end{array} $	88 89 90
-	$\begin{vmatrix} \overline{91} \\ 92 \end{vmatrix}$	90.50 $91.50$	$9.51 \\ 9.62$	$90.46 \\ 91.45$	$\begin{array}{c} 9.91 \\ 10.02 \end{array}$	$90.42 \\ 91.41$	$\overline{\begin{smallmatrix} 10.30 \\ 10.41 \end{smallmatrix}}$	90.37 $91.36$	$ \begin{array}{ c c c c c } \hline 10.70 \\ 10.81 \\ 10.93 \end{array} $	$\begin{array}{c c} \hline 91 \\ 92 \\ \hline \end{array}$
	93 94 95	92.49 93.49 94.48	9.72 $9.83$ $9.93$	92.45 93.44 94.44	10.12 $10.23$ $10.34$	$\begin{vmatrix} 92.40 \\ 93.40 \\ 94.39 \\ 05.90 \end{vmatrix}$	$ \begin{array}{c c} 10.53 \\ 10.64 \\ 10.75 \\ \end{array} $	92.36 93.35 94.34	$11.05 \\ 11.17$	93 94 95
	96 97 98	95.47 $96.47$ $97.46$	$ \begin{array}{c} 10.03 \\ 10.14 \\ 10.24 \end{array} $	$\begin{vmatrix} 95.43 \\ 96.42 \\ 97.42 \end{vmatrix}$	10.45 $10.56$ $10.67$	$\begin{vmatrix} 95.38 \\ 96.38 \\ 97.37 \end{vmatrix}$	$ \begin{array}{c c} 10.87 \\ 10.98 \\ 11.09 \end{array} $	$\begin{vmatrix} 95.33 \\ 96.33 \\ 97.32 \end{vmatrix}$	$ \begin{array}{c cccc} 11.28 \\ 11.40 \\ 11.52 \end{array} $	96 97 98
1	$\frac{99}{00}$	$98.46 \\ 99.45$	$\begin{array}{ c c }\hline 10.35 \\ \hline 10.45 \\ \hline \end{array}$	98.41 $99.41$	$\frac{10.78}{10.89}$	$\begin{array}{ c c }\hline 98.36\\ 99.36\\ \hline\end{array}$	$\frac{11.21}{11.32}$	98.31 $99.31$	$\begin{vmatrix} 11.64 \\ 11.75 \end{vmatrix}$	$\begin{array}{c c} 99 \\ 100 \\ \hline \vdots \end{array}$
	Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	Dist	84 I	Deg.	833	Deg.	83½	Deg.	831	Deg.	Dist

Distance	7 D	eg.	74 [	Deg.	71/2	Deg.	73	Deg.	Dist
ince.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
1 2 3 4 5 6 7 8 9	1.99 2.98 3.97 4.96 5.96 6.95 7.94 8.93	0.12 0.24 0.37 0.49 0.61 0.73 0.85 0.97 1.10 1.22	0.99 1.98 2.98 3.97 4.96 5.95 6.94 7.94 8.93 9.92	0.13 0.25 0.38 0.50 0.63 0.76 0.88 1.01 1.14 1.26	0.99 1.98 2.97 3.97 4.96 5.95 6.94 7.93 8.92 9.91	0.13 0.26 0.39 0.52 0.65 0.78 0.91 1.04 1.17 1.31	0.99 1.98 2.97 3.96 4.95 5.95 6.94 7.93 8.92 9.91	0.13 0.27 0.40 0.54 0.67 0.81 0.94 1.08 1.21 1.35	1 2 3 4 5 6 7 , 8 9 10
11 12 13 14 15 16 17 18 19	10.92 11.91 12.90 13.90 14.89 15.88 16.87 17.87 18.86	1.34 1.46 1.58 1.71 1.83 1.95 2.07 2.19 2.32	10.91 11.90 12.90 13.89 14.88 15.87 16.86 17.86 18.85	1.39 1.51 1.64 1.77 1.89 2.02 2.15 2.27 2.40	10.91 11.90 12.89 13.88 14.87 15.86 16.85 17.85 18.84	1.44 1.57 1.70 1.83 1.96 2.09 2.22 2.35 2.48	10.90 11.89 12.88 13.87 14.86 15.85 16.84 17.84 18.83	1.48 1.62 1.75 1.89 2.02 2.16 2.29 2.43 2.56	11 12 13 14 15 16 17 18 19
20 21 22 23 24 25 26 27 28 29 30	20.84 21.84 22.83 23.82 24.81 25.81 26.80 27.79 28.78	2.44 2.56 2.68 2.80 2.92 3.05 3.17 3.29 3.41 3.53 3.66	$\begin{array}{ c c c }\hline 19.84\\\hline 20.83\\21.82\\22.82\\23.81\\24.80\\25.79\\26.78\\27.78\\28.77\\29.76\\\hline\end{array}$	2.52 2.65 2.78 2.90 3.03 3.15 3.28 3.41 3.53 3.66 3.79	19.83 20.82 21.81 22.80 23.79 24.79 25.78 26.77 27.76 28.75 29.74	2.61 2.74 2.87 3.00 3.13 3.26 3.39 3.52 3.65 3.79 3.92	20.81 21.80 22.79 23.78 24.77 25.76 26.75 27.74 28.74 29.73	2.70 2.83 2.97 3.10 3.24 3.37 3.51 3.64 3.78 3.91 4.05	20 21 22 23 24 25 26 27 28 29
31 32 33 34 35 36 37 38 39 40	30.77 31.76 32.75 33.75 34.74 35.73 36.72 37.72 38.71	3.78 3.90 4.02 4.14 4.27 4.39 4.51 4.63 4.75 4.87	30.75 31.74 32.74 33.73 34.72 35.71 36.70 37.70 38.69 39.68	3.91 4.04 4.16 4.29 4.42 4.54 4.67 4.80 4.92 5.05	30.73 31.73 32.72 33.71 34.70 35.69 36.68 37.67 38.67 39.66	4.05 4.18 4.31 4.44 4.57 4.70 4.83 4.96 5.09 5.22	30.72 31.71 32.70 33.69 34.68 35.67 36.66 37.65 38.64 39.63	4.18 4.32 4.45 4.58 4.72 4.85 4.99 5.12 5.26 5.39	
41 42 43 44 45 46 47 48 49 50	40.70 41.69 42.68 43.67 44.67 45.66 46.65 47.64 48.63	5.00 5.12 5.24 5.36 5.48 5.61 5.73 5.85 5.97 6.09	40.67 41.66 42.66 43.65 44.64 45.63 46.62 47.62 48.61 49.60	5.17 5.30 5.43 5.55 5.68 5.81 5.93 6.06 6.18 6.31	40.65 41.64 42.63 43.62 44.62 45.61 46.60 47.59 48.58 49.57	5.35 5.48 5.61 5.74 5.87 6.00 6.13 6.27 6.40 6.53	40.63 41.62 42.61 43.60 44.59 45.58 46.57 47.56 48.55 49.54	5.53 5.66 5.80 5.93 6.0° 6.20 6.34 6.47 6.61 6.74	41 42 43 445 47 48 49 50
Distance.	Dep. 83 1	Lat. Deg.	Dep. 823					Dep.   Lat.	

Distance.	7 D	eg.	71 ]	Deg.	$7\frac{1}{2}$ ]	Deg.	74 ]	Deg.	Distance.
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ince.
51 52 53 54 55 56 57 58 59	50.62 51.61 52.60 53.60 54.59 55.58 56.58 57.57 58.56	6.22 6.34 6.46 6.58 6.70 6.82 6.95 7.07 7.19	50.59 51.58 52.58 53.57 54.56 55.55 56.54 57.54 58.53	6.44 6.56 6.69 6.81 6.94 7.07 7.19 7.32 7.45	50.56 51.56 52.55 53.54 54.53 55.52 56.51 57.50 58.50	6.66 6.79 6.92 7.05 7.18 7.31 7.44 7.57 7.70	50.53 51.53 52.52 53.51 54.50 55.49 56.48 57.47 58.46	6.88 7.01 7.15 7.28 7.42 7.55 7.69 7.82 7.96	51 52 53 54 55 56 57 58 59
60 61 62 63 64 65 66 67 68 69	$\begin{array}{c} 59.55 \\ \hline 60.55 \\ 61.54 \\ 62.53 \\ 63.52 \\ 64.52 \\ 65.51 \\ 66.50 \\ 67.49 \\ 68.49 \\ \end{array}$	7.31 7.43 7.56 7.68 7.80 7.92 8.04 8.17 8.29 8.41	$\begin{array}{c} 59.52 \\ \hline 60.51 \\ 61.50 \\ 62.50 \\ 63.49 \\ 64.48 \\ 65.47 \\ 66.46 \\ 67.46 \\ 68.45 \\ \end{array}$	7.57 7.70 7.82 7.95 8.08 8.20 8.33 8.46 8.58 8.71	59.49 60.48 61.47 62.46 63.45 64.44 65.44 66.43 67.42 68.41	7.83 7.96 8.09 8.22 8.35 8.48 8.61 8.75 8.88 9.01	59.45 60.44 61.43 62.42 63.42 64.41 65.40 66.39 67.38 68.37	8.09 8.23 8.36 8.50 8.63 8.77 8.90 9.04 9.17 9.30	60 61 62 63 64 65 66 67 68 69
$   \begin{array}{r}     70 \\     \hline     71 \\     72 \\     73 \\     74 \\     75 \\     76 \\     77 \\     78 \\     79 \\     80 \\   \end{array} $	$\begin{array}{r} 69.48 \\ \hline 70.47 \\ 71.46 \\ 72.46 \\ 73.45 \\ 74.44 \\ 75.43 \\ 76.43 \\ 77.42 \\ 78.41 \\ 79.40 \\ \end{array}$	8.53 8.65 8.77 8.90 9.02 9.14 9.26 9.38 9.51 9.63 9.75	69.44 70.43 71.42 72.42 73.41 74.40 75.39 76.38 77.38 78.37 79.36	8.83 8.96 9.09 9.21 9.34 9.46 9.59 9.72 9.84 9.97 10.10	69.40 70.39 71.38 72.38 73.37 74.36 75.35 76.34 77.33 78.32 79.32	$\begin{array}{r} 9.14 \\ \hline 9.27 \\ 9.40 \\ 9.53 \\ 9.66 \\ 9.79 \\ 9.92 \\ 10.05 \\ 10.18 \\ 10.31 \\ 10.44 \\ \end{array}$	69.36 70.35 71.34 72.33 73.32 74.31 75.31 76.30 77.29 78.28 79.27	$\begin{array}{r} 9.44 \\ \hline 9.57 \\ 9.71 \\ 9.84 \\ 9.98 \\ 10.11 \\ 10.25 \\ 10.38 \\ 10.52 \\ 10.65 \\ 10.79 \\ \end{array}$	70 71 72 73 74 75 76 77 78 79 80
81 82 83 84 85 86 87 88 89 90	80.40 81.39 82.38 83.37 84.37 85.36 86.35 87.34 88.34 89.33	9.87 9.99 10.12 10.24 10.36 10.48 10.60 10.72 10.85 10.97	80.35 81.34 82.34 83.33 84.32 85.31 86.30 87.30 88.29 89.28	10.22 10.35 10.47 10.60 10.73 10.85 10.98 11.11 11.23 11.36	80.31 81.30 82.29 83.28 84.27 85.26 86.26 87.25 88.24 89.23	10.57 10.70 10.83 10.96 11.09 11.23 11.36 11.49 11.62 11.75	80.26 81.25 82.24 83.23 84.22 85.21 86.21 87.20 88.19 89.18	$\begin{array}{ c c c c c c }\hline 10.92\\ 11.06\\ 11.19\\ 11.33\\ 11.46\\ 11.60\\ 11.73\\ 11.87\\ 12.00\\ 12.14\\ \end{array}$	81 82 83 84 85 86 87 88 89 90
91 92 93 94 95 96 97 98 99 100	90.32 91.31 92.31 93.30 94.29 95.28 96.28 97.27 98.26 99.25	11.09 11.21 11.33 11.46 11.58 11.70 11.82 11.94 12.07 12.19	90.27 91.26 92.26 93.25 94.24 95.23 96.22 97.22 98.21 99.20	11.48 11.61 11.74 11.86 11.99 12.12 12.24 12.37 12.49 12.62	90.22 91.21 92.20 93.20 94.19 95.18 96.17 97.16 98.15 99.14	11.88 12.04 12.14 12.27 12.40 12.53 12.66 12.79 12.92 13.05	90.17 91.16 92.15 93.14 94.13 95.12 96.11 97.10 98.10 99.09	12.27 12.41 12.54 12.68 12.81 12.95 13.08 13.22 13.35 13.49	91 92 93 94 95 96 97 98 99 100
Distance.			Dep. 823	Lat. Deg.	Dep.   Lat.		Dep. Lat. 821 Deg.		Distance.

-									
Dist	8 :	Deg.	31/4	Deg.	81/2	Deg.	83/4	Deg.	Dist
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance. 1
1 2 3 4 5 6 7 8 9	0.99 1.98 2.97 3.96 4.95 5.94 6.93 7.92 8.91	$ \begin{vmatrix} 0.14 \\ 0.28 \\ 0.42 \\ 0.56 \\ 0.70 \\ 0.84 \\ 0.97 \\ 1.11 \\ 1.25 \\ \end{vmatrix} $	0.99 1.98 2.97 3.96 4.95 5.94 6.93 7.92 8.91	$ \begin{vmatrix} 0.14 \\ 0.29 \\ 0.43 \\ 0.57 \\ 0.72 \\ 0.86 \\ 1.00 \\ 1.15 \\ 1.29 \\ \end{vmatrix} $	0.99 1.98 2.97 3.96 4.95 5.93 6.92 7.91 8.90	$ \begin{vmatrix} 0.15 \\ 0.30 \\ 0.44 \\ 0.59 \\ 0.74 \\ 0.89 \\ 1.03 \\ 1.18 \\ 1.33 \\ \end{vmatrix} $	0.99 1.98 2.97 3.95 4.94 5.93 6.92 7.91 8.90	0.15 0.30 0.46 0.61 0.76 0.91 1.06 1.22 1.37	2 3 4 5 6 7 8 9
$ \begin{array}{c c} 10 \\ 11 \\ 12 \\ 13 \\ 14 \\ 15 \\ 16 \\ 17 \\ 18 \\ 19 \\ 20 \\ \hline 21 \\ 22 \end{array} $	$ \begin{vmatrix} 9.90 \\ 10.89 \\ 11.88 \\ 12.87 \\ 13.86 \\ 14.85 \\ 15.84 \\ 16.83 \\ 17.82 \\ 18.82 \\ 19.81 \\ \hline 20.80 \\ 21.79 $	1.39 1.53 1.67 1.81 1.95 2.09 2.23 2.37 2.51 2.64 2.78 2.92 3.06	$ \begin{vmatrix} 9.90 \\ 10.89 \\ 11.88 \\ 12.87 \\ 13.86 \\ 14.85 \\ 15.84 \\ 16.83 \\ 17.81 \\ 18.80 \\ 19.79 \\ \hline 20.78 \\ 21.77 \\ \end{vmatrix} $	$\begin{array}{ c c c }\hline 1.43\\\hline 1.58\\1.72\\1.87\\2.01\\2.15\\2.30\\2.44\\2.58\\2.73\\2.87\\\hline 3.01\\3.16\\\hline\end{array}$	$\begin{array}{ c c c c c }\hline 9.89 \\\hline 10.88 \\\hline 11.87 \\\hline 12.86 \\\hline 13.85 \\\hline 14.84 \\\hline 15.82 \\\hline 16.81 \\\hline 17.80 \\\hline 19.78 \\\hline 20.77 \\\hline 21.76 \\\hline \end{array}$	$\begin{array}{ c c c }\hline 1.48\\\hline 1.63\\\hline 1.77\\\hline 1.92\\\hline 2.07\\\hline 2.22\\\hline 2.36\\\hline 2.51\\\hline 2.66\\\hline 2.81\\\hline 2.96\\\hline \hline 3.10\\\hline 3.25\\\hline \end{array}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{ c c c }\hline 1.52\\\hline 1.67\\1.83\\1.98\\2.13\\2.28\\2.43\\2.59\\2.74\\2.89\\3.04\\\hline 3.19\\3.35\\\hline\end{array}$	$\begin{array}{ c c c }\hline 10\\\hline 11\\\hline 12\\\hline 13\\\hline 14\\\hline 15\\\hline 16\\\hline 17\\\hline 18\\\hline 19\\\hline 20\\\hline \hline 21\\\hline 22\\\hline \end{array}$
$ \begin{array}{c c} 23 \\ 24 \\ 25 \\ 26 \\ 27 \\ 28 \\ 29 \\ 30 \\ \hline 31 \\ \end{array} $	$ \begin{array}{r} 22.78 \\ 23.77 \\ 24.76 \\ 25.75 \\ 26.74 \\ 27.73 \\ 28.72 \\ 29.71 \\ \hline 30.70 \end{array} $	3.20 3.34 3.48 3.62 3.76 3.90 4.04 4.18	$\begin{array}{c} 22.76 \\ 23.75 \\ 24.74 \\ 25.73 \\ 26.72 \\ 27.71 \\ 28.70 \\ 29.69 \\ \hline 30.68 \end{array}$	$   \begin{array}{r}     3.30 \\     3.44 \\     3.59 \\     3.73 \\     3.87 \\     4.02 \\     4.16 \\     4.30 \\    \hline     4.45 \\   \end{array} $	$\begin{array}{c} 22.75 \\ 23.74 \\ 24.73 \\ 25.71 \\ 26.70 \\ 27.69 \\ 28.68 \\ 29.67 \\ \hline 30.66 \end{array}$	$   \begin{array}{r}     3.40 \\     3.55 \\     3.70 \\     3.84 \\     3.99 \\     4.14 \\     4.29 \\     4.43 \\    \hline     4.58 \\   \end{array} $	$\begin{array}{r} 22.73 \\ 23.72 \\ 24.71 \\ 25.70 \\ 26.69 \\ 27.67 \\ 28.66 \\ 29.65 \\ \hline 30.64 \\ \end{array}$	3.50 $3.65$ $3.80$ $3.96$ $4.11$ $4.26$ $4.41$ $4.56$ $4.72$	23 24 25 26 27 28 29 30 31
$ \begin{array}{c} 32 \\ 33 \\ 34 \\ 35 \\ 36 \\ 37 \\ 38 \\ 39 \\ 40 \\ \hline 41 \end{array} $	31.69 32.68 33.67 34.66 35.65 36.64 37.63 38.62 39.61	4.45 4.59 4.73 4.87 5.01 5.15 5.29 5.43 5.57	31.67 32.66 33.65 34.64 35.63 36.62 37.61 38.60 39.59	4.59 4.74 4.88 5.02 5.17 5.31 5.45 5.60 5.74	31.65 32.64 33.63 34.62 35.60 36.59 37.58 38.57 39.56	4.73 4.88 5.03 5.17 5.32 5.47 5.62 5.76 5.91	31.63 32.62 33.60 34.59 35.58 36.57 37.56 38.55 39.53	4.87 5.02 5.17 5.32 5.48 5.63 5.78 5.93 6.08	32 33 34 35 36 37 38 39 40
41 42 43 44 45 46 47 48 49 50	40.60 41.59 42.58 43.57 44.56 45.55 46.54 47.53 48.52 49.51	5.71 5.85 5.98 6.12 6.26 6.40 6.54 6.68 6.82 6.96	40.58 41.57 42.56 43.54 44.53 45.52 46.51 47.50 48.49 49.48	5.88 6.03 6.17 6.31 6.46 6.60 6.74 6.89 7.03 7.17	40.55 41.54 42.53 43.52 44.51 45.49 46.48 47.47 48.46 49.45	6.06 6.21 6.36 6.50 6.65 6.80 6.95 7.09 7.24 7.39	40.52 41.51 42.50 43.49 44.48 45.46 46.45 47.44 48.43 49.42	6.24 6.39 6.54 6.69 6.85 7.00 7.15 7.30 7.45 7.61	41 42 43 44 45 46 47 48 49 50
Distance.	22 I	Lat. Deg.	Dep.   813 I	Lat. Deg.	81½	Lat. Deg.	Dep.	Lat. Deg.	Distance.

Dista	8 I	eg.	81	Deg.	$8\frac{1}{2}$ I	eg,	8 <del>3</del> ]	Deg.	Dist
unce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ance
Distance:   512354556   57856   61626364   656667   67777   67778   812384   85878   8888   8	50.50 51.49 52.48 53.47 54.46 55.46 56.45 57.44 58.43 59.42 60.41 61.40 62.39 63.38 64.37 65.36 66.35 67.34 68.33 69.32 70.31 71.30 72.29 73.28 74.27 75.26 76.25 77.24 78.23 79.22 80.21 81.20 82.19 83.18 84.17 85.16 86.15	Dep.  7.10 7.24 7.38 7.52 7.65 7.79 7.93 8.07 8.21 8.35  8.49 8.63 8.77 8.91 9.05 9.19 9.32 9.46 9.60 9.74  9.88 10.02 10.16 10.30 10.44 10.58 10.72 10.86 10.99 11.13  11.27 11.41 11.55 11.69 11.83 11.97 12.11 12.25	50.47         51.46         52.45         53.44         54.43         55.42         56.41         57.40         58.39         59.38         60.37         61.36         62.35         63.34         64.33         65.32         66.31         67.30         68.29         69.28         70.27         71.25         72.24         73.23         74.22         75.21         76.20         77.19         78.18         79.17         80.16         81.15         82.14         83.13         84.12         85.11         86.10	7.32 7.46 7.61 7.75 7.89 8.04 8.18 8.32 8.47 8.61 8.75 8.90 9.04 9.18 9.33 9.47 9.61 9.76 9.90 10.04 10.19 10.33 10.47 10.62 10.76 10.91 11.05 11.19 11.34 11.48 11.62 11.77 11.91 12.05 12.20 12.34 12.48	50.44           51.43           52.42           53.41           54.40           55.38           56.37           57.36           58.35           59.34           60.33           61.32           62.31           63.30           64.29           65.28           67.25           68.24           69.23           70.22           71.21           72.20           73.19           74.18           75.17           76.15           77.14           78.13           79.12           80.11           81.10           82.09           83.08           84.07           85.06           86.04	7.54 7.69 7.83 7.98 8.13 8.28 8.43 8.57 8.72 8.87 9.02 9.16 9.31 9.46 9.61 9.76 9.90 10.05 10.20 10.35 10.49 10.64 10.79 11.23 11.38 11.53 11.68 11.53 11.68 11.97 12.12 12.27 12.42 12.56 12.71 12.86	Lat.  50.41 51.39 52.38 53.37 54.36 55.35 56.34 57.32 58.31 59.30 60.29 61.28 62.27 63.26 64.24 65.23 66.22 67.21 68.20 69.19 70.17 71.16 72.15 73.14 74.13 75.12 76.10 77.09 78.08 79.07 80.06 81.05 82.03 83.02 84.01 85.00 85.99 86.98	Dep.  7.76 7.91 8.06 8.21 8.37 8.52 8.67 8.82 8.98 9.13  9.28 9.43 9.58 9.74 9.89 10.04 10.19 10.34 10.50 10.65 10.80 10.95 11.10 11.26 11.41 11.56 11.71 11.87 12.02 12.17 12.32 12.47 12.63 13.08 13.23 13.39	istance.   512   553   556   578   560   612   625   636   645   656   657   6
$     \begin{array}{c c}       88 \\       89 \\       \hline       90 \\       \hline       31     \end{array} $	$ \begin{vmatrix} 87.14 \\ 88.13 \\ 89.12 \\ \hline 90.11 \end{vmatrix} $	$ \begin{array}{r} 12.25 \\ 12.39 \\ 12.53 \\ \hline 12.66 \end{array} $	$ \begin{array}{r} 87.09 \\ 88.08 \\ 89.07 \\ \hline 90.06 \end{array} $	$ \begin{array}{r} 12.63 \\ 12.77 \\ 12.91 \\ \hline 13.06 \end{array} $	$ \begin{array}{r} 87,03 \\ 88.02 \\ 89.01 \\ \hline 90.00 \end{array} $	$ \begin{array}{r} 13.01 \\ 13.16 \\ 13.30 \\ \hline 13.45 \end{array} $	$   \begin{array}{r}     86.98 \\     87.96 \\     \hline     88.95 \\     \hline     89.94   \end{array} $	$ \begin{array}{r} 13.39 \\ 13.54 \\ 13.69 \\ \hline 13.84 \end{array} $	$   \begin{array}{r}     88 \\     89 \\     \hline     90 \\     \hline     91   \end{array} $
92 93 94 95 96 97 98 99 100	91.10 92.09 93.09 94.08 95.07 96.06 97.05 98.04 99.03	12.80 12.94 13.08 13.22 13.36 13.50 13.64 13.78 13.92	$ 91.05 \\ 92.04 \\ 93.03 \\ 94.02 \\ 95.01 \\ 96.00 \\ 96.99 \\ 97.98 \\ 98.97 $	13.20 13.34 13.49 13.63 13.78 13.92 14.06 14.21 14.35	90.99 91.98 92.97 93.96 94.95 95.93 96.92 97.91 98.90	13.60 13.75 13.89 14.04 14.19 14.34 14.49 14.63 14.78	90.93 91.92 92.91 93.89 94.88 95.87 96.86 97.85 98.84	14.00 14.15 14.30 14.45 14.60 14.76 14.91 15.06 15.21	92 93 94 95 96 97 98 99 100
Distance.	Dep. 32 1			Deg.	Dep.   Lat.		Dep. Lat. 814 Deg.		Distance.

			01.1	9 <sub>4</sub> Deg.		D		D ,	
Distance.	91	eg.	94 1	Jeg.	9½	Deg.	94	Deg.]	Distance
nce.	Lat.	Dep.	Lat,	Dep.	Lat.	Dep.	Lat.	Dep.	ince.
1 2 3 4 5 6 7 8 9 10	1.98 2.96 3.95 4.94 5.93 6.91 7.90 8.89	0.16 0.31 0.47 0.63 0.78 0.94 1.10 1.25 1.41 1.56	0.99 1.97 2.96 3.95 4.93 5.92 6.91 7.90 8.88 9.87	0.16 0.32 0.48 0.64 0.80 0.96 1.13 1.29 1.45	0.99 1.97 2.96 3.95 4.93 5.92 6.90 7.89 8.88 9.86	0.17 0.33 0.50 0.66 0.83 0.99 1.16 1.32 1.49 1.65	0.99 1.97 2.96 3.94 4.93 5.91 6.90 7.88 8.87 9.86	$egin{array}{c} 0.17 \\ 0.34 \\ 0.51 \\ 0.68 \\ 0.85 \\ 1.02 \\ 1.19 \\ 1.35 \\ 1.52 \\ 1.69 \\ \hline \end{array}$	1 2 3 4 5 6 7 8 9
11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 27 28 29 30 31 32 33 34 40 41 42 43 44 45 46 47 48 49 50 50 50 50 50 50 50 50 50 50 50 50 50	11.85 12.84 13.83 14.82 15.80 16.79 17.78 18.77 19.75 20.74 21.73 22.72 23.70 24.69 25.68 26.67 27.66 29.63 30.62 31.61 32.59 33.58 34.57 35.56 36.54 37.53 38.52 39.51 40.50 41.48 42.47 43.46 44.45 45.43 46.42 47.41 48.40 49.38	1.72 1.88 2.03 2.19 2.35 2.50 2.66 2.82 2.97 3.13 3.29 3.44 3.60 3.75 3.91 4.07 4.22 4.38 4.54 4.69 4.85 5.01 5.16 5.32 5.94 6.10 6.26 6.41 6.57 6.73 6.88 7.04 7.20 7.35 7.51 7.67 7.82	10.86 11.84 12.83 13.82 14.80 15.79 16.78 17.77 18.75 19.74 20.73 21.71 22.70 23.69 24.67 25.66 26.65 27.64 28.62 29.61 30.60 31.58 32.57 33.56 34.54 35.53 36.52 37.51 38.49 39.48 40.47 41.45 42.44 43.43 44.41 45.40 46.39 47.38 49.35	1.77 1.93 2.09 2.25 2.41 2.57 2.73 2.89 3.05 3.21 3.38 3.54 3.70 3.86 4.02 4.18 4.34 4.50 4.66 4.82 4.98 5.14 5.30 5.47 5.63 5.79 5.95 6.11 6.27 6.43 6.59 6.75 6.91 7.07 7.23 7.39 7.55 7.72 7.88 8.04	10.85 11.84 12.82 13.81 14.79 15.78 16.77 17.75 18.74 19.73 20.71 21.70 22.68 23.67 24.66 25.64 26.63 27.62 28.60 29.59 30.57 31.56 32.55 33.53 34.52 35.51 36.49 37.48 38.47 39.45 40.44 41.42 42.41 43.40 44.38 45.37 46.34 48.33 49.32 D.71	1.82 1.98 2.15 2.31 2.48 2.64 2.81 2.97 3.14 3.30 3.47 3.63 3.80 3.96 4.13 4.29 4.46 4.62 4.79 4.95 5.12 5.28 5.45 5.61 5.78 5.97 6.92 7.10 7.26 7.26 7.26 7.26 7.26 7.26 7.26 7.26	10.84 11.83 12.81 13.80 14.78 15.77 16.75 17.74 18.73 19.71 20.70 21.68 22.67 23.65 24.64 25.62 26.61 27.60 28.58 29.57 30.55 31.54 32.52 33.51 34.49 35.48 36.47 37.45 38.44 39.42 40.41 41.39 42.38 43.36 44.35 45.34 46.32 47.31 48.29 49.28	1.86 2.03 2.20 2.37 2.54 2.71 2.88 3.05 3.22 3.39 3.56 3.73 3.90 4.06 4.23 4.40 4.57 4.74 4.91 5.08 5.25 5.42 5.76 5.93 6.10 6.27 6.44 6.60 6.77 6.94 7.11 7.28 7.62 7.79 7.96 8.13 8.30 8.47	11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 44 45 46 47 48 49 50 40 40 40 40 40 40 40 40 40 40 40 40 40
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance,
Dis	81 I	Deg.	80¾ I	Deg.	801/2	Deg.	804 1	Deg.	Dis

Dis	9 1	Deg.	91/2	Deg.	$9\frac{1}{2}$	Deg.	93 ]	Deg.	Dia
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
51 52 53 54 55 56 57 58 59 60	50.37 51.36 52.35 53.34 54.32 55.31 56.30 57.29 58.27 59.26	7.98 8.13 8.29 8.45 8.60 8.76 8.92 9.07 9.23 9.39	50.34 51.32 52.31 53.30 54.28 55.27 56.26 57.25 58.23 59.22	8.20 8.36 8.52 8.68 8.84 9.00 9.16 9.32 9.48 9.64	50.30 51.29 52.27 53.26 54.25 55.23 56.22 57.20 58.19	8.42 8.58 8.75 8.91 9.08 9.24 9.41 9.57 9.74 9.90	50.26 51.25 52.23 53.22 54.21 55.19 56.18 57.16 58.15 59.13	8.64 8.81 8.98 9.14 9.31 9.48 9.65 9.82 9.99 10.16	51 52 53 54 55 56 57 58 59 60
61 62 63 64 65 66 67 68 69 70	60.25 61.24 62.22 63.21 64.20 65.19 66.18 67.16 68.15 69.14	9.54 9.70 9.86 10.01 10.17 10.32 10.48 10.64 10.79 10.95	60.21 61.19 62.18 63.17 64.15 65.14 66.13 67.12 68.10 69.09	9.81 9.97 10.13 10.29 10.45 10.61 10.77 10.93 11.09 11.25	59.18 60.16 61.15 62.14 63.12 64.11 65.09 66.08 67.07 68.05 69.04	9.90 10.07 10.23 10.40 10.56 10.73 10.89 11.06 11.22 11.39 11.55	60.12 61.10 62.09 63.08 64.06 65.05 66.03 67.02 68.00 68.99	10.16 10.33 10.50 10.67 10.84 11.01 11.18 11.35 11.52 11.69 11.85	61 62 63 64 65 66 67 68 69 70
71 72 73 74 75 76 77 78 79 80	70.13 71.11 72.10 73.09 74.08 75.06 76.05 77.04 78.03 79.02	11.11 11.26 11.42 11.58 11.73 11.89 12.05 12.20 12.36 12.51	70.08 71.06 72.05 73.04 74.02 75.01 76.00 76.99 77.97 78.96	11.41 11.57 11.73 11.89 12.06 12.22 12.38 12.54 12.70 12.86	70.03 71.01 72.00 72.99 73.97 74.96 75.94 76.93 77.92 78.90	11.72 11.88 12.05 12.21 12.38 12.54 12.71 12.87 13.04 13.20	69.97 70.96 71.95 72.93 73.92 74.90 75.89 76.87 77.86 78.84	12.02 12.19 12.36 12.53 12.70 12.87 13.04 13.21 13.38 13.55	71 72 73 74 75 76 77 78 79 80
81 82 83 84 85 86 87 88 89 90	80.00 80.99 81.98 82.97 83.95 84.94 85.93 86.92 87.90 88.89	12.67 12.83 12.98 13.14 13.30 13.45 13.61 13.77 13.92 14.08	79.95 80.93 81.92 82.91 83.89 84.88 85.87 86.86 87.84 88.83	13.02 13.18 13.34 13.50 13.66 13.82 13.98 14.15 14.31 14.47	79.89 80.88 81.86 82.85 83.83 84.82 85.81 86.79 87.78 88.77	13.37 13.53 13.70 13.86 14.03 14.19 14.36 14.52 14.69 14.85	79.83 80.82 81.80 82.79 83.77 84.76 85.74 86.73 87.71 88.70	13.72 13.89 14.06 14.23 14.39 14.56 14.73 14.90 15.07 15.24	81 82 83 84 85 86 87 88 89 90
91 92 93 94 95 96 97 98 99 100	89.88 90.87 91.86 92.84 93.83 94.82 95.81 96.79 97.78 98.77	14.24 14.39 14.55 14.70 14.86 15.02 15.17 15.33 15.49 15.64	89.82 90.80 91.79 92.78 93.76 94.75 95.74 96.73 97.71 98.70	14.63 14.79 14.95 15.11 15.27 15.43 15.59 15.75 15.91 16.07	89.75 90.74 91.72 92.71 93.70 94.68 95.67 96.66 97.64 98.63	15.02 15.18 15.35 15.51 15.68 15.84 16.01 16.17 16.34 16.50	89.69 90.67 91.66 92.64 93.63 94.61 95.60 96.58 97.57 98.56	15.41 15.58 15.75 15.92 16.09 16.26 16.43 16.60 16.77 16.93	91 92 93 94 95 96 97 98 99 100
Distance.	81 I	Lat. Deg.	Dep.   80 <sup>3</sup> / <sub>4</sub> 1	Lat.	80½	Lat. Deg.	80½	Lat. Deg.	Distance.

10000000		1		H						
	Distance	10	Deg.	101	Deg.	$10\frac{1}{2}$	Deg.	103	Deg.	Distance.
	nce	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce
1 1 1 1 1 1 1 1 1 1 2 2 2 2 2	123456789011234567890112	0.98 1.97 2.95 3.94 4.92 5.91 6.89 7.88 8.86 9.85 10.83 11.82 12.80 13.79 14.77 15.76 16.74 17.73 18.71 19.70 20.68 21.67		$\begin{array}{ c c c c c }\hline 0.98 \\ 1.97 \\ 2.95 \\ 3.94 \\ 4.92 \\ 5.90 \\ 6.89 \\ 7.87 \\ 8.86 \\ 9.84 \\\hline \hline 10.82 \\ 11.81 \\ 12.79 \\ 13.78 \\ 14.76 \\ 15.74 \\ 16.73 \\ 17.71 \\ 18.70 \\ 19.68 \\\hline 20.66 \\ 21.65 \\\hline \end{array}$	0.18 0.36 0.53 0.71 0.89 1.07 1.25 1.42 1.60 1.78 1.96 2.14 2.31 2.49 2.67 2.85 3.03 3.20 3.38 3.56 3.74 3.91	0.98 1.97 2.95 3.93 4.92 5.90 6.88 7.87 8.85 9.83 10.82 11.80 12.78 13.77 14.75 15.73 16.72 17.70 18.68 19.67 20.65 21.63	0.18 0.36 0.55 0.73 0.91 1.09 1.28 1.46 1.64 1.82 2.00 2.19 2.37 2.55 2.73 2.92 3.10 3.28 3.46 3.64 3.83 4.01	0.98 1.96 2.95 3.93 4.91 5.89 6.88 7.86 8.84 9.82 10.81 11.79 12.77 13.75 14.74 15.72 16.70 17.68 18.67 19.65 20.63 21.61	0.19 0.37 0.56 0.75 0.93 1.12 1.31 1.49 1.68 1.87 2.05 2.24 2.42 2.61 2.80 2.98 3.17 3.36 3.54 3.73 3.92 4.10	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22
2: 2: 2: 2: 2: 2: 2: 2: 3:	4   5   6   7   8   9   1	22.65 23.64 24.62 25.61 26.59 27.57 28.56 29.54	3.99 4.17 4.34 4.51 4.69 4.86 5.04 5.21	22.63 23.62 24.60 25.59 26.57 27.55 28.54 29.52	4.09 4.27 4.45 4.63 4.80 4.98 5.16 5.34	22.61 23.60 24.58 25.56 26.55 27.53 28.51 29.50	4.19 4.37 4.56 4.74 4.92 5.10 5.28 5.47	22.60 23.58 24.56 25.54 26.53 27.51 28.49 29.47	4.29 4.48 4.66 4.85 5.04 5.22 5.41 5.60	23 24 25 26 27 28 29 30
35 35 34 35 36 37 38 39 40	2   3   4   5   5   7   8   9   9	30.53 31.51 32.50 33.48 34.47 35.45 36.44 37.42 38.41 39.39	5.38 5.56 5.73 5.90 6.08 6.25 6.42 6.60 6.77 6.95	30.51 31.49 32.47 33.46 34.44 35.43 36.41 37.39 38.38 39.36	5.52 5.69 5.87 6.05 6.23 6.41 6.58 6.76 6.94 7.12	30.48 31.46 32.45 33.43 34.41 35.40 36.38 37.36 38.35 39.33	5.65 5.83 6.01 6.20 6.38 6.56 6.74 6.92 7.11 7.29	30.46 31.44 32.42 33.40 34.39 35.37 36.35 37.33 38.32 39.30	5.78 5.97 6.16 6.34 6.53 6.71 6.90 7.09 7.27 7.46	31 32 33 34 35 36 37 38 39 40
4: 4: 4: 4: 4: 4: 4: 4: 4: 5:	2 3 4 5 5 7 8 9 0	40.38 41.36 42.35 43.33 44.32 45.30 46.29 47.27 48.26 49.24	7.12 7.29 7.47 7.64 7.81 7.99 8.16 8.34 8.51 8.68	40.35 41.33 42.31 43.30 44.28 45.27 46.25 47.23 48.22 49.20	7.30 7.47 7.65 7.83 8.01 8.19 8.36 8.54 8.72 8.90	40.31 41.30 42.28 43.26 44.25 45.23 46.21 47.20 48.18 49.16	7.47 7.65 7.84 8.02 8.20 8.38 8.57 8.75 8.93 9.11	40.28 41.26 42.25 43.23 44.21 45.19 46.18 47.16 48.14 49.12	7.65 7.83 8.02 8.21 8.39 8.58 8.77 8.95 9.14 9.33	41 42 43 44 45 46 47 48 49 50
. Distance.		80 I	Lat.	Dep.   79 <sup>3</sup> / <sub>4</sub> ]	Lat. Deg.	Dep. 79½	Lat. Deg.	79½ ]	Lat.	Distance.

	20 P S S S S S S S S S S S S S S S S S S		j	10½ Deg.				}	
Dis	10 1	Deg.	101	Deg.	$10\frac{1}{2}$	Deg.	$10\frac{3}{4}$ ]	Deg.	Dis
Distance.	Tot	Don	Lat.	Don	T ( ]	D.,	Tat	Don	Distance. 5
51	Lat.	Dep.		Dep.	Lat.	Dep.	Lat.	Dep.	-57 H
52	$50.23 \\ 51.21$	$\begin{array}{c c} 8.86 \\ 9.03 \end{array}$	$50.19 \\ 51.17$	$9.08 \mid 9.25 \mid$	$50.15 \\ 51.13$	$\begin{array}{c c} 9.29 \\ 9.48 \end{array}$	50.10   51.09	$\begin{array}{c c} 9.51 \\ 9.70 \end{array}$	52
53 54	52.19 53.18	$egin{array}{c} 9.20 \ 9.38 \ \end{array}$	52.15   53.14	$\begin{array}{c c} 9.43 \\ 9.61 \end{array}$	$52.11 \\ 53.10$	$9.66 \\ 9.84$	$\begin{array}{c c} 52.07 \\ 53.05 \end{array}$	$9.89 \mid 10.07 \mid$	53 54
55 56	54.16 55.15	$9.55 \\ 9.72$	54.12 55.11	9.79	54.08	10.02	$54.03 \\ 55.02$	$ \begin{array}{c c} 10.26 \\ 10.45 \end{array} $	55 56
57	56.13	9.90	56.09	$\begin{vmatrix} 9.96 \\ 10.14 \end{vmatrix}$	55.06 56.05	$10.21 \\ 10.39$	56.00	10.63	57
58 59	57.12   58.10	10.07 $10.25$	$\begin{bmatrix} 57.07 \\ 58.06 \end{bmatrix}$	10.32 $10.50$	57.03 58.01	$10.57 \\ 10.75$	$56.98 \\ 57.96$	10.82   11.00	58 59
$\frac{69}{61}$	$\frac{59.09}{60.07}$	$\frac{10.42}{10.50}$	59.04	10.68	59.00	10.93	$\frac{58.95}{50.03}$	$\frac{11.19}{11.29}$	$\frac{60}{61}$
61 62	61.06	$\begin{bmatrix} 10.59 \\ 10.77 \end{bmatrix}$	$\begin{bmatrix} 60.03 \\ 61.01 \end{bmatrix}$	$10.85 \\ 11.03$	$59.98 \\ 60.96$	$ \begin{array}{c c} 11.12 \\ 11.30 \end{array} $	$59.93 \\ 60.91$	$11.38 \\ 11.56$	62
$\begin{array}{c} 63 \\ 64 \end{array}$	$62.04 \\ 63.03$	10.94   11.11	$ \begin{array}{c} 61.99 \\ 62.98 \end{array} $	$ \begin{array}{c c} 11.21 \\ 11.39 \end{array} $	$\begin{vmatrix} 61.95 \\ 62.93 \end{vmatrix}$	11.48 11.66	$\begin{bmatrix} 61.89 \\ 62.88 \end{bmatrix}$	$\begin{array}{c c} 11.75 \\ 11.94 \end{array}$	63 64
65 66	$64.01 \\ 65.00$	$ \begin{array}{c c} 11.29 \\ 11.46 \end{array} $	63.96 64.95	11.57	$63.91 \\ 64.89$	11.85 12.03	63.86	$   \begin{array}{c c}     12.12 \\     12.31   \end{array} $	65 66
67	65.98	11.63	65.93	11.92	65.88	12.21	65.82	12.50	67
68 69	$\begin{array}{c} 66.97 \\ 67.95 \end{array}$	$  11.81 \\ 11.98  $	$\left  \begin{array}{c} 66.91 \\ 67.90 \end{array} \right $	12.10   12.28	66.86  67.84	$12.39 \\ 12.57$	$  66.81 \\ 67.79 $	$  12.68 \\ 12.87  $	68 69
70	$\frac{68.94}{60.00}$	12.16	68.88	$\frac{12.46}{19.69}$	68.83	12.76	68.77	$\frac{13.06}{13.24}$	$\left  \frac{70}{71} \right $
71 72	$69.92 \\ 70.91$	$12.33 \\ 12.50$	69.87   70.85	$12.63 \\ 12.81$	$\begin{bmatrix} 69.81 \\ 70.79 \end{bmatrix}$	$\begin{array}{c} 12.94 \\ 13.12 \end{array}$	$\begin{vmatrix} 69.75 \\ 70.74 \end{vmatrix}$	13.43	72
73 74	71.89 72.88	12.68   12.85	$71.83 \\ 72.82$	$\frac{12.99}{13.17}$	$ 71.78  \\ 72.76$	$\begin{array}{ c c }\hline 13.30\\ 13.49\\ \hline\end{array}$	$\begin{vmatrix} 71.72 \\ 72.70 \end{vmatrix}$	$13.62 \\ 13.80$	73 74
75 76	73.86 74.85	$\begin{vmatrix} 13.02 \\ 13.20 \end{vmatrix}$	$\begin{vmatrix} 73.80 \\ 74.79 \end{vmatrix}$	$13.35 \\ 13.52$	$73.74 \\ 74.73$	13.67	73.68  $ 74.67 $	13.99 14.18	75 76
77	75.83	13.37	75.77	13.70	75.71	14.03	75.65	14.36	77
78 79	$  76.82 \\ 77.80 $	$\begin{vmatrix} 13.54 \\ 13.72 \end{vmatrix}$	76.76	$13.88 \\ 14.06$	76.69	$  14.21 \\ 14.40  $	76.63	14.55 $  14.74$	78 79
$\frac{80}{81}$	$\frac{78.78}{79.77}$	$\frac{13.89}{14.07}$	$\frac{78.72}{79.71}$	$\frac{14.24}{14.41}$	$\frac{78.66}{79.64}$	$\frac{14.58}{14.76}$	$\frac{78.60}{79.58}$	$\frac{14.92}{15.11}$	$\frac{80}{81}$
82	80.75	14.24	80.69	14.59	80.63	14.94	80.56	15.29	82
83 84	81.74 82.72	14.41 14.59	81.68	14.77 14.95	81.61 82.59	15.13 15.31	$\begin{vmatrix} 81.54 \\ 82.53 \end{vmatrix}$	15.48 15.67	83
85 86	$\begin{vmatrix} 83.71 \\ 84.69 \end{vmatrix}$	$14.76 \\ 14.93$	83.64	$\begin{vmatrix} 15.13 \\ 15.30 \end{vmatrix}$	83.58 84.56	15.49 15.67	83.51 84.49	15.85 16.04	85
87	85.68 86.66	15.11 15.28	85.61	15.48 15.66	85.54	15.85 16.04	85.47 85.46	$\begin{vmatrix} 16.23 \\ 16.41 \end{vmatrix}$	87
88 89	87.65	15.45	87.58	15.84	86.53 87.51	16.22	87.44	16.60	89
$\frac{90}{91}$	$\frac{88.63}{89.62}$	$\frac{15.63}{15.80}$	$\frac{88.56}{89.55}$	$\begin{array}{ c c }\hline 16.01\\\hline 16.19\end{array}$	$\frac{88.49}{89.48}$	$\frac{16.40}{16.58}$	$\frac{88.42}{89.40}$	$\frac{16.79}{16.97}$	$\frac{90}{91}$
92	90.60	15.98	90.53	16.37	90.46	16.77	90.39	17.16	92
93 94	91.59  $ 92.57 $	$\begin{vmatrix} 16.15 \\ 16.32 \end{vmatrix}$	$\begin{vmatrix} 91.52 \\ 92.50 \end{vmatrix}$	16.55 $16.73$	91.44  $  92.43 $	$  16.95 \\ 17.13  $	$\begin{vmatrix} 91.37 \\ 92.35 \\ 200.000 \end{vmatrix}$	$  17.35 \\ 17.53 $	93
95 96	93.56 94.54	16.50 16.67	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$  16.90 \\ 17.08 $	93.41 94.39	17.31 17.49	93.33  $  94.32 $	17.72   17.91	95 96
97	95.53	16.84 17.02	95.45 96.44	17.26 17.44	95.38	17.68	95.30 96.28	18.09	97 98
98 99	$\begin{vmatrix} 96.51 \\ 97.50 \\ \end{vmatrix}$	17.19	97.42	17.62	$\begin{vmatrix} 96.36 \\ 97.34 \\ \end{vmatrix}$	17.86 18.04	97.26	18.47	99
$\frac{100}{3}$	98.48 Dep.	17.36 Lat.	$\frac{98.40}{\text{Dep.}}$	17.79 Lat.	$\frac{98.33}{\text{Dep.}}$	$\frac{18.22}{\text{Lat.}}$	$\frac{98.25}{\text{Dep.}}$	18.65 Lat.	$\frac{100}{6}$
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Бер.	1.00.	Distance.
Dis	80	Deg.	793	Deg.	$79\frac{1}{2}$	Deg.	794	Deg.	Dis
-	1	8 194 Deg.							2/3/min (17)

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Distance	11 ]	Deg.	1114	Deg.	11½	Deg.	113	Deg.	Distance.
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce
1 2 3 4 5 6 7 8 9 10	3.93		0.98 1.96 2.94 3.92 4.90 5.88 6.87 7.85 8.83 9.81	0.20 0.39 0.59 0.78 0.98 1.17 1.37 1.56 1.76	0.98 1.96 2.94 3.92 4.90 5.88 6.86 7.84 8.82 9.80	0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.59 1.79	0.98 1.96 2.94 3.92 4.90 5.87 6.85 7.83 8.81 9.79	0.20 0.41 0.61 0.82 1.02 1.22 1.43 1.63 1.83 2.04	1 2 3 4 5 6 7 8 9
11 12 13 14 15 16 17 18 19 20	10.80 11.78 12.76 13.74 14.72 15.71 16.69 17.67 18.65 19.63	2.10 2.29 2.48 2.67 2.86 3.05 3.24 3.43 3.63 3.82	10.79 11.77 12.75 13.73 14.71 15.69 16.67 17.65 18.63 19.62	2.15 2.34 2.54 2.73 2.93 3.12 3.32 3.51 3.71 3.90	10.78 11.76 12.74 13.72 14.70 15.68 16.66 17.64 18.62 19.60	2.19 2.39 2.59 2.79 2.99 3.19 3.39 3.59 3.79	$ \begin{array}{r}     \hline       10.77 \\       11.75 \\       12.73 \\       13.71 \\       14.69 \\       15.66 \\       16.64 \\       17.62 \\       18.60 \\       19.58 \end{array} $	2.24 2.44 2.65 2.85 3.06 3.26 3.46 3.66 3.87 4.07	11 12 13 14 15 16 17 18 19 20
21 22 23 24 25 26 27 28 29 30	20.61 21.60 22.58 23.56 24.54 25.52 26.50 27.49 28.47 29.45	4.01 4.20 4.39 4.58 4.77 4.96 5.15 5.34 5.53 5.72	20.60 21.58 22.56 23.54 24.52 25.50 26.48 27.46 28.44 29.42	4.10 4.29 4.49 4.68 4.88 5.07 5.27 5.46 5.66 5.85	20.58 21.56 22.54 23.52 24.50 25.48 26.46 27.44 28.42 29.40	4.19 4.39 4.59 4.78 4.98 5.18 5.38 5.58 5.58 5.78 5.98	20.56 21.54 22.52 23.50 24.48 25.46 26.43 27.41 28.39 29.37	4.28 4.48 4.68 4.89 5.09 5.30 5.50 5.70 5.91 6.11	21 22 23 24 25 26 27 28 29 30
31 32 33 34 35 36 37 38 39 40	30.43 31.41 32.39 33.38 34.36 35.34 36.32 37.30 38.28 39.27	5.92 6.11 6.30 6.49 6.68 6.87 7.06 7.25 7.44 7.63	30.40 31.39 32.37 33.35 34.33 35.31 36.29 37.27 38.25 39.23	6.05 6.24 6.44 6.63 6.83 7.02 7.22 7.41 7.61 7.80	30.38 31.36 32.34 33.32 34.30 35.28 36.26 37.24 38.22 39.20	6.18 6.38 6.58 6.78 6.98 7.18 7.38 7.58 7.78 7.78	30.35 31.33 32.31 33.29 34.27 35.25 36.22 37.20 38.18 39.16	6.31 6.52 6.72 6.92 7.13 7.33 7.53 7.74 7.94 8.15	31 32 33 34 35 36 37 38 39 40
41 42 43 44 45 46 47 48 49 50	40.25 41.23 42.21 43.19 44.17 45.15 46.14 47.12 48.10 49.08	7.82 8.01 8.20 8.40 8.59 8.78 8.97 9.16 9.35 9.54	40.21 41.19 42.17 43.15 44.14 45.12 46.10 47.08 48.06 49.04	8.00 8.19 8.39 8.58 8.78 8.97 9.17 9.36 9.56 9.75	40.18 41.16 42.14 43.12 44.10 45.08 46.06 47.04 48.02 49.00	8.17 8.37 8.57 8.57 8.97 9.17 9.37 9.57 9.77	$\begin{array}{c} 30.10 \\ \hline 40.14 \\ 41.12 \\ 42.10 \\ 43.08 \\ 44.06 \\ 45.04 \\ 46.02 \\ 46.99 \\ 47.97 \\ 48.95 \\ \end{array}$	8.35 8.55 8.76 8.96 9.16 9.37 9.57 9.78 9.98 10.18	41 42 43 44 45 46 47 48 49 50
Distance.	79 I	Lat.	78 <sup>3</sup> / <sub>4</sub> I	Lat.	78½ 1	Lat.	Dep.   78½ I	Lat.	Distance.
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Distance	11	Deg.	.114	Deg.	11,	L Deg.	113	Deg.	Dista
nce	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
51 52 53 54 55 56 60 61 62 63 64 65 66 67 70 71 72 73 74 75 77 80 81 82	50.06 51.04 52.03 53.01 53.99 54.97 55.95 56.93 57.92 58.90 59.88 60.86 61.84 62.82 63.81 64.79 65.77 66.75 67.73 68.71 69.70 70.68 71.66 72.64 73.62 74.60 75.59 76.57 77.55 78.53 79.51 80.49	9.73 9.92 10.11 10.30 10.49 10.69 11.26 11.45 11.64 11.83 12.02 12.21 12.40 12.59 12.78 13.36 13.55 13.74 13.93 14.12 14.31 14.69 14.88 15.07 15.26 15.46 15.65	50.02 51.00 51.98 52.96 53.94 54.92 55.90 56.89 57.87 58.85 59.83 60.81 61.79 62.77 63.75 64.73 65.71 66.69 67.67 68.66 69.64 70.62 71.60 72.58 73.56 74.54 75.52 76.50 77.48 78.46 79.44 80.42	9.95 10.14 10.34 10.53 10.73 10.93 11.12 11.32 11.51 11.71 11.90 12.10 12.29 12.49 12.68 12.88 13.07 13.27 13.46 13.66 13.85 14.05 14.24 14.44 14.63 14.83 15.02 15.21 15.61 15.80 16.00	$49.98$ $50.96$ $51.94$ $52.92$ $53.90$ $54.88$ $55.86$ $56.84$ $57.82$ $58.80$ $\overline{59.78}$ $60.76$ $61.74$ $62.72$ $63.70$ $64.68$ $65.66$ $66.63$ $67.61$ $69.57$ $70.55$ $71.53$ $72.51$ $73.49$ $74.47$ $75.45$ $76.43$ $77.41$ $78.39$ $\overline{79.37}$ $80.35$	10.17 10.37 10.57 10.97 10.97 11.16 11.36 11.56 11.76 11.96 12.16 12.36 12.56 12.56 13.56 13.56 13.56 13.56 13.56 13.56 13.56 13.55 14.55 14.55 14.75 15.55 15.55 15.95 16.15	$\begin{array}{c} 49.93 \\ 50.91 \\ 51.89 \\ 52.87 \\ 53.85 \\ 54.83 \\ 55.81 \\ 56.78 \\ 57.76 \\ 58.74 \\ \hline 59.72 \\ 60.70 \\ 61.68 \\ 62.66 \\ 63.64 \\ 64.62 \\ 65.60 \\ 66.58 \\ 67.55 \\ 68.53 \\ \hline 69.51 \\ 70.49 \\ 71.47 \\ 72.45 \\ 73.43 \\ 74.41 \\ 75.39 \\ 76.37 \\ 77.34 \\ 78.32 \\ \hline 79.30 \\ 80.28 \\ \hline \end{array}$	10.39 10.59 10.79 11.00 11.20 11.40 11.61 12.01 12.22 12.42 12.63 13.03 13.24 13.44 13.64 13.64 13.85 14.05 14.25 14.46 14.66 14.87 15.07 15.27 15.48 15.68 16.09 16.29 16.49 16.70	52 53 54 55
83 84 85	$   \begin{array}{r}     81.48 \\     82.46 \\     83.44   \end{array} $	15.84 $16.03$ $16.22$	$\begin{vmatrix} 81.41 \\ 82.39 \\ 83.37 \end{vmatrix}$	16.19 16.39 16.58	81.33 82.31 83.29	$\begin{vmatrix} 16.55 \\ 16.75 \\ 16.95 \end{vmatrix}$	81.26 82.24 83.22	$\begin{vmatrix} 16.90 \\ 17.11 \\ 17.31 \end{vmatrix}$	84 85
86 87 88	$egin{array}{c} 84.42 \ 85.40 \ 86.38 \ \hline \end{array}$	$egin{array}{c c} 16.41 & \\ 16.60 & \\ 16.79 & \\ \end{array}$	$\begin{vmatrix} 84.35 \\ 85.33 \\ 86.31 \end{vmatrix}$	16.78 $16.97$ $17.17$	$\begin{vmatrix} 84.27 \\ 85.25 \\ 86.23 \end{vmatrix}$	17.15 17.35 17.54	84.20 85.18 86.16	17.51 $17.72$ $17.92$	86 87 88
89 90	87.36 88.35	16.79 16.98 17.17	87.29 88.27	17.36 17.56	87.21 88.19	$\begin{vmatrix} 17.34 \\ 17.74 \\ 17.94 \end{vmatrix}$	87.14 88.11	18.12 18.33	89 90
91 92 93 94 95 96 97 98 99 100	89.33 90.31 91.29 92.27 93.25 94.24 95.22 96.20 97.18 98.16	17.36 17.55 17.75 17.94 18.13 18.32 18.51 18.70 18.89 19.03	89.25 90.23 91.21 92.19 93.17 94.16 95.14 96.12 97.10 98.08	17.75 17.95 18.14 18.34 18.53 18.73 18.92 19.12 19.31 19.51	89.17 90.15 91.13 92.11 93.09 94.07 95.05 96.03 97.01 97.99	18.14 18.34 18.54 18.74 18.94 19.14 19.34 19.54 19.74 19.94	89.09 90.07 91.05 92.03 93.01 93.99 94.97 95.95 96.93 97.90	18.53 18.74 18.94 19.14 19.35 19.55 19.75 19.96 20.16 20.36	91 92 93 94 95 96 97 98 99
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
Dis	79 D	eg.	783	Deg.	$78\frac{1}{2}$ ]	Deg.	784	Deg.	Dis

r		1		II.		ll:		11		-
	Distance.	12	Deg.	124	Deg.	1.2½	Deg.	123	Deg.	Distance.
1		Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce
	1 2 3 4 5 6 7 8 9	0.98 1.96 2.93 3.91 4.89 5.87 6.85 7.83 8.80 9.78		0.98 1.95 2.93 3.91 4.89 5.86 6.84 7.82 8.80 9.77	$\begin{array}{c} 0.21 \\ 0.42 \\ 0.64 \\ 0.85 \\ 1.06 \\ 1.27 \\ 1.49 \\ 1.70 \\ 1.91 \\ 2.12 \end{array}$	0.98 1.95 2.93 3.91 4.88 5.86 6.83 7.81 8.79 9.76	0.22 0.43 0.65 0.87 1.08 1.30 1.52 1.73 1.95 2.16	0.98 1.95 2.93 3.90 4.88 5.85 6.83 7.80 8.78 9.75	0.22 0.44 0.66 0.88 1.10 1.32 1.54 1.77 1.99 2.21	1 2 3 4 5 6 7 8 9
	11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 40 41 42 43 44 44 45 46 46 47 48 48 48 49 49 49 49 49 49 49 49 49 49 49 49 49	10.76 11.74 12.72 13.69 14.67 15.65 16.63 17.61 18.58 19.56 20.54 21.52 22.50 23.48 24.45 25.43 26.41 27.39 28.37 29.34 30.32 31.30 32.28 33.26 34.24 35.21 36.19 37.17 38.15 39.13 40.10 41.08 42.06 43.04 44.99 45.97 46.95 47.93 48.91	2.29 2.49 2.70 2.91 3.12 3.33 3.53 3.74 3.95 4.16 4.37 4.57 4.78 4.99 5.20 5.41 5.61 5.82 6.03 6.24 6.45 6.65 6.65 6.65 7.07 7.28 7.48 7.69 7.90 8.11 8.32 8.52 8.52 8.73 8.94 9.15 9.36 9.15 9.15 9.15 9.15 9.15 9.15 9.15 9.15	10.75 11.73 12.70 13.68 14.66 15.64 16.61 17.59 18.57 19.54 20.52 21.50 22.48 23.45 24.43 25.41 26.39 27.36 28.34 29.32 30.29 31.27 32.25 33.23 34.20 32.28	2.33 2.55 2.76 2.97 3.18 3.39 3.61 3.82 4.03 4.24 4.46 4.67 4.88 5.30 5.52 5.73 5.94 6.15 6.37 6.58 6.79 7.00 7.21 7.43 7.64 7.85 8.27 8.27 8.27 8.27 8.27 8.27 8.27 8.27	10.74 11.72 12.69 13.67 14.64 15.62 16.60 17.57 18.55 19.53 20.50 21.48 22.45 23.43 24.41 25.38 26.36 27.34 28.31 29.29 30.27 31.24 32.22 33.19 34.17 35.15 36.12 37.10 38.08 39.05 40.03 41.98 42.96 43.93 44.91 45.89 46.86 47.84	2.38 2.60 2.81 3.03 3.25 3.46 3.68 3.90 4.11 4.33 4.55 4.76 4.98 5.19 5.41 5.63 5.84 6.06 6.28 6.49 6.71 6.93 7.14 7.36 7.58 7.79 8.01 8.22 8.44 8.66 8.87 9.31 9.52 9.74 9.95 10.39 10.61	10.73 11.70 12.68 13.65 14.63 15.61 16.58 17.56 18.53 19.51 20.48 21.46 22.43 23.41 24.38 25.36 26.33 27.31 28.28 29.26 30.24 31.21 32.19 33.16 34.14 35.11 36.09 37.06 38.04 39.01 39.99 40.96 41.94 42.92 43.89 44.87 45.84 46.82 47.79	2.43 2.65 2.87 3.09 3.31 3.53 3.75 3.97 4.19 4.41 4.63 4.86 5.08 5.30 5.52 5.74 5.96 6.18 6.40 6.62 6.84 7.28 7.50 7.72 7.95 8.17 8.39 8.61 8.83 9.27 9.49 9.71 9.27 9.27 9.27 9.27 9.27 9.27 9.27 9.27	11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 27 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 49 49 49 49 49 49 49 49 49 49 49 49
		Dep.	Lat.	Dep.	10.61 Lat.	48.81 Dep.	10.82    Lat.	48.77 Dep.	11.03 Lat.	<u>50</u>
L	Distance.		Deg.	773		77½		774 1		Distance.

Dis	12	Deg.	121/4	Deg.	121/2	Deg.	123	Deg.	Dis
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
51 52 53 54 55	49.89 50.86 51.84 52.82 53.80	$ \begin{array}{ c c c c }\hline 10.60\\10.81\\11.02\\11.23\\11.44\\\hline \end{array} $	49.84 50.82 51.79 52.77	10.82 11.03 11.25 11.46	$ \begin{array}{r} 49.79 \\ 50.77 \\ 51.74 \\ 52.72 \\ 53.70 \\ 54.70 \\ 55.72 \\ 55.70 $	11.04 11.25 11.47 11.69	$ \begin{array}{r} 49.74 \\ 50.72 \\ 51.69 \\ 52.67 \\ 53.64 \end{array} $	11.26 11.48 11.70 11.02	51 52 53 54
56 57 58 59	54.78 55.75 56.73 57.71	$ \begin{array}{c c} 11.64 \\ 11.85 \\ 12.06 \\ 12.27 \end{array} $	53.75 54.72 55.70 56.68 57.66	$\begin{array}{c} 11.67 \\ 11.88 \\ 12.09 \\ 12.31 \\ 12.52 \\ \end{array}$	53.70 54.67 55.65 56.63 57.60	$ \begin{array}{c cccc} 11.90 \\ 12.12 \\ 12.34 \\ 12.55 \\ 12.77 \end{array} $	53.64 54.62 55.59 56.57 57.55	$ \begin{array}{ c c c c } \hline 12.14 \\ 12.36 \\ 12.58 \\ 12.80 \\ 13.02 \\ \hline \end{array} $	55 56 57 58 59
$ \begin{array}{c c} 60 \\ 61 \\ 62 \\ 63 \\ 64 \end{array} $	$ \begin{array}{r} 58.69 \\ \hline 59.67 \\ 60.65 \\ 61.62 \\ 62.60 \end{array} $	$\begin{array}{ c c c }\hline 12.47\\\hline 12.68\\\hline 12.89\\\hline 13.10\\\hline 13.31\\\hline \end{array}$	$ \begin{array}{ c c c c } \hline 58.63 \\ 59.61 \\ 60.59 \\ 61.57 \\ 62.54 \end{array} $	$\begin{array}{r} 12.73 \\ \hline 12.94 \\ 13.16 \\ 13.37 \\ 13.58 \\ \end{array}$	$ \begin{array}{r} 58.58 \\ \hline 59.55 \\ 60.53 \\ 61.51 \\ 62.48 \end{array} $	$ \begin{array}{r} 12.99 \\ \hline 13.20 \\ 13.42 \\ 13.64 \\ 13.85 \end{array} $	$\begin{array}{ c c c c }\hline 58.52\\\hline 59.50\\60.47\\61.45\\62.42\\\hline \end{array}$	$ \begin{array}{ c c c c c } \hline 13.24 \\ \hline 13.46 \\ 13.68 \\ 13.90 \\ 14.12 \end{array} $	$ \begin{array}{ c c } \hline 60 \\ \hline 61 \\ 62 \\ 63 \\ 64 \\ \end{array} $
65 66 67 68 69	63.58 64.56 65.54 66.51 67.49	13.51 13.72 13.93 14.14 14.35	63.52 64.50 65.47 66.45 67.43	13.79 14.00 14.22 14.43 14.64	63.46 64.44 65.41 66.39 67.36	$ \begin{array}{c c} 14.07 \\ 14.29 \\ 14.50 \\ 14.72 \\ 14.93 \end{array} $	$\begin{bmatrix} 63.40 \\ 64.37 \\ 65.35 \\ 66.32 \\ 67.30 \end{bmatrix}$	$ \begin{array}{c cccc} 14.35 \\ 14.57 \\ 14.79 \\ 15.01 \\ 15.23 \end{array} $	65 66 67 68 69
$ \begin{array}{ c c c } \hline 70 \\ \hline 71 \\ 72 \\ 73 \end{array} $	$ \begin{array}{r r}                                    $	$\begin{array}{r} 14.55 \\ \hline 14.76 \\ 14.97 \\ 15.18 \\ \end{array}$	$ \begin{array}{r}                                     $	$ \begin{array}{r} 14.85 \\ \hline 15.06 \\ 15.28 \\ 15.49 \end{array} $	$ \begin{array}{r}     68.34 \\     \hline     69.32 \\     70.29 \\     71.27 \end{array} $	15.15 15.37 15.58 15.80	$ \begin{array}{r}     68.27 \\     \hline     69.25 \\     70.22 \\     71.20 \end{array} $	$ \begin{array}{r} 15.45 \\ \hline 15.67 \\ 15.89 \\ 16 11 \end{array} $	
74 75 76 77	$\begin{vmatrix} 72.38 \\ 73.36 \\ 74.34 \\ 75.32 \end{vmatrix}$	15.39 15.59 15.80 16.01	$\begin{array}{c c} 72.32 \\ 73.29 \\ 74.27 \\ 75.25 \end{array}$	15.70 15.91 16.13 16.34	$\begin{bmatrix} 72.25 \\ 73.22 \\ 74.20 \\ 75.17 \end{bmatrix}$	$   \begin{array}{c c}     16.02 \\     16.23 \\     16.45 \\     16.67   \end{array} $	$egin{array}{c} 72.18 \\ 73.15 \\ 74.13 \\ 75.10 \\ \end{array}$	16.33 16.55 16.77 16.99	74 75 76 77
78 79 80 81	$ \begin{vmatrix} 76.30 \\ 77.27 \\ 78.25 \\ \hline 79.23 \end{vmatrix} $	$ \begin{array}{ c c c } \hline 16.22 \\ 16.43 \\ \hline 16.63 \\ \hline \hline 16.84 \end{array} $	$ \begin{array}{r} 76.22 \\ 77.20 \\ 78.18 \\ \hline 79.16 \end{array} $	$ \begin{array}{c} 16.55 \\ 16.76 \\ 16.97 \\ \hline 17.19 \end{array} $	$ \begin{array}{c c} 76.15 \\ 77.13 \\ 78.10 \\ \hline 79.08 \end{array} $	$ \begin{array}{c c} 16.88 \\ 17.10 \\ 17.32 \\ \hline 17.53 \end{array} $	$   \begin{array}{r}     76.08 \\     77.05 \\     78.03 \\     \hline     79.00   \end{array} $	$ \begin{array}{r} 17.21 \\ 17.44 \\ 17.66 \\ \hline 17.88 \end{array} $	78 79 80 81
82 83 84 85	30.21 81.19 82.16 83.14	17.05 $17.26$ $17.46$ $17.67$	80.13 81.11 82.09 83.06	17.40 $17.61$ $17.82$ $18.04$	$\begin{vmatrix} 80.06 \\ 81.03 \\ 82.01 \\ 82.99 \\ 80.06 \end{vmatrix}$	17.75 17.96 18.18 18.40	79.98 80.95 81.93 82.90	18.10 $18.32$ $18.54$ $18.76$	82 83 84 85
86 87 88 89 90	84.12 85.10 86.08 87.06 88.03	17.88 $18.09$ $18.30$ $18.50$ $18.71$	$\begin{vmatrix} 84.04 \\ 85.02 \\ 86.00 \\ 86.97 \\ 87.95 \end{vmatrix}$	18.25 $18.46$ $18.67$ $18.88$ $19.10$	$\begin{vmatrix} 83.96 \\ 84.94 \\ 85.91 \\ 86.89 \\ 87.87 \end{vmatrix}$	18.61 $18.83$ $19.05$ $19.26$ $19.48$	83.88 84.85 85.83 86.81 87.78	18.98 19.20 19.42 19.64 19.86	86 87 88 89 90
91 92 93 94	89.01 89.99 90.97 91.95	18.92 19.13 19.34 19.54	88.93 89.91 90.88 91.86	19.31 19.52 19.73 19.94	88.84 89.82 90.80 91.77	$   \begin{array}{r}     \hline             19.70 \\             19.91 \\             20.13 \\             20.35   \end{array} $	88.76 89.73 90.71 91.68	20.08 20.30 20.52 20.75	91 92 93 94
95 96 97 98	92.92 93.90 94.88 95.86 96.84	19.75 19.96 20.17 20.38 20.58	92.84 93.81 94.79 95.77 96.75	$\begin{array}{c} 20.16 \\ 20.37 \\ 20.58 \\ 20.79 \end{array}$	$egin{array}{c} 92.75 \\ 93.72 \\ 94.70 \\ 95.68 \\ 96.65 \\ \hline \end{array}$	20.56 20.78 20.99 21.21 21.43	92.66 93.63 94.61 95.58 96.56	20.97 21.19 21.41 21.63 21.85	95 96 97 98 99
$\begin{array}{ c c }\hline 99\\\hline 100\\\hline \vdots\\\hline \end{array}$	$\frac{97.81}{\text{Dep.}}$	20.79 Lat.	$\frac{97.73}{97.72}$ Dep.	21.01 21.22 Lat.	97.63 Dep.	21.43 21.64 Lat.	$\frac{97.53}{\text{Dep.}}$	22.07 Lat.	100
Distance.		Deg.	773	Deg	77½	Deg.	771	Deg.	Distance.

Distance.	13	Deg.	134	Deg.	131	Deg.	133	Deg.	Dist
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
$ \begin{array}{ c c c } \hline 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 10 \\ \end{array} $	0.97	0.23	0.97	0.23	0.97	0.23	0.97	0.24	1
	1.95	0.45	1.95	0.46	1.95	0.47	1.94	0.48	2
	2.92	0.67	2.92	0.69	2.92	0.70	2.91	0.71	3
	3.90	0.90	3.89	0.92	3.89	0.93	3.89	0.95	4
	4.87	1.12	4.87	1.15	4.86	1.17	4.86	1.19	5
	5.85	1.35	5.84	1.38	5.83	1.40	5.83	1.43	6
	6.82	1.57	6.81	1.60	6.81	1.63	6.80	1.66	7
	7.80	1.80	7.79	1.83	7.78	1.87	7.77	1.90	8
	8.77	2.02	8.76	2.06	8.75	2.10	8.74	2.14	9
	9.74	2.25	9.73	2.29	9.72	2.33	9.71	2.38	10
11 12 13 14 15 16 17 18 19 20	10.72 11.69 12.67 13.64 14.62 15.59 16.57 17.54 18.51 19.49	2.47 2.70 2.92 3.15 3.37 3.60 3.82 4.05 4.27 4.50	10.71 11.68 12.65 13.63 14.60 15.57 16.55 17.52 18.49 19.47	2.52 2.75 2.98 3.21 3.44 3.67 3.90 4.13 4.35 4.58	10.70 11.67 12.64 13.61 14.59 15.56 16.53 17.50 18.48 19.45	2.57 2.80 3.03 3.27 3.50 3.74 3.97 4.20 4.44 4.67	10.68 11.66 12.63 13.60 14.57 15.54 16.51 17.48 18.46 19.43	2.61 2.85 3.09 3.33 3.57 3.80 4.04 4.28 4.52 4.75	11 12 13 14 15 16 17 18 19
21	20.46	4.72	20.44	4.81	20.42	4.90	20.40	4.99	21
22	21.44	4.95	21.41	5.04	21.39	5.14	21.37	5.23	22
23	22.41	5.17	22.39	5.27	22.36	5.37	22.34	5.47	23
24	23.38	5.40	23.36	5.50	23.34	5.60	23.31	5.70	24
25	24.36	5.62	24.33	5.73	24.31	5.84	24.28	5.94	25
26	25.33	5.85	25.31	5.96	25.28	6.07	25.25	6.18	26
27	26.31	6.07	26.28	6.19	26.25	6.30	26.23	6.42	27
28	27.28	6.30	27.25	6.42	27.23	6.54	27.20	6.66	28
29	28.26	6.52	28.23	6.65	28.20	6.77	28.17	6.89	29
30	29.23	6.75	29.20	6.88	29.17	7.00	29.14	7.13	30
31	30.21	6.97	30.17	7.11	30.14	7.24	30.11	7.37	31
32	31.18	7.20	31.15	7.33	31.12	7.47	31.08	7.61	32
33	32.15	7.42	32.12	7.56	32.09	7.70	32.05	7.84	33
34	33.13	7.65	33.09	7.79	33.06	7.94	33.03	8.08	34
35	34.10	7.87	34.07	8.02	34.03	8.17	34.00	8.32	35
36	35.08	8.10	35.04	8.25	35.01	8.40	34.97	8.56	36
37	36.05	8.32	36.02	8.48	35.98	8.64	35.94	8.79	37
38	37.03	8.55	36.99	8.71	36.95	8.87	36.91	9.03	38
39	38.00	8.77	37.96	8.94	37.92	9.10	37.88	9.27	39
40	38.97	9.00	38.94	9.17	38.89	9.34	38.85	9.51	40
41	39.95	9.22	39.91	9.40	39.87	9.57	39.83	9.75	41
42	40.92	9.45	40.88	9.63	40.84	9.80	40.80	9.98	42
43	41.90	9.67	41.86	9.86	41.81	10.04	41.77	10.22	43
44	42.87	9.90	42.83	19.08	42.78	10.27	42.74	10.46	44
45	43.85	10.12	43.80	10.31	43.76	10.51	43.71	10.70	45
46	44.82	10.35	44.78	10.54	44.73	10.74	44.68	10.93	46
47	45.80	10.57	45.75	10.77	45.70	10.97	45.65	11.17	47
48	46.77	10.80	46.72	11.00	46.67	11.21	46.62	11.41	48
49	47.74	11.02	47.70	11.23	47.65	11.41	47.60	11.65	49
50	48.72	11.25	48.67	11.46	48.62	11.67	48.57	11.88	50
Distance.	77 I	Lat. Deg.	76 <sup>3</sup> / <sub>4</sub> 1	Deg.	76½	Lat. Deg.	Dep.   76¼ ]	Deg.	Distance.

		12 Dag			11		11		1
Distance.	13	Deg.	134	Deg.	13½	Deg.	133	Deg.	Dist
ince.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
51 52	49.69 50.67		$\begin{array}{ c c c }\hline 49.64\\50.62\\ \hline\end{array}$	$11.69 \\ 11.92$	49.59 50.56	$11.91 \\ 12.14$	$   \overline{49.54} \\ 50.51$	$\begin{vmatrix} 12.12 \\ 12.36 \end{vmatrix}$	51 52
53 54	$\begin{vmatrix} 51.64 \\ 52.62 \end{vmatrix}$	$\begin{vmatrix} 11.92 \\ 12.15 \end{vmatrix}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{vmatrix} 12.15 \\ 12.38 \end{vmatrix}$	51.54 52.51	$\begin{vmatrix} 12.37 \\ 12.61 \end{vmatrix}$	51.48 52.45	$  12.60 \\ 12.84$	53 54
55 56	$\begin{vmatrix} 53.59 \\ 54.56 \end{vmatrix}$	$\begin{vmatrix} 12.37 \\ 12.60 \end{vmatrix}$	53.54	$\begin{vmatrix} 12.61 \\ 12.84 \end{vmatrix}$	53.48 54.45	$\begin{vmatrix} 12.84 \\ 13.07 \end{vmatrix}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{vmatrix} 13.07 \\ 13.31 \end{vmatrix}$	55 56
57 58	55.54	$\begin{vmatrix} 12.82 \\ 13.05 \end{vmatrix}$	55.48	$\begin{vmatrix} 13.06 \\ 13.29 \end{vmatrix}$	55.43 56.40	13.31	55.37 56.34	$\begin{vmatrix} 13.55 \\ 13.79 \end{vmatrix}$	57 58
59 60	$\begin{bmatrix} 57.49 \\ 58.46 \end{bmatrix}$	$\begin{array}{ c c }\hline 13.27\\13.50\\\hline \end{array}$	$\begin{array}{ c c c }\hline 57.43\\ 58.40\\ \hline \end{array}$	$\begin{vmatrix} 13.52 \\ 13.75 \end{vmatrix}$	$\begin{array}{ c c c c }\hline 57.37\\ 58.34\\ \hline\end{array}$	$\begin{array}{ c c }\hline 13.77\\14.01\\\hline \end{array}$	57.31 58.28	$\begin{array}{ c c }\hline 14.02\\14.26\\\hline\end{array}$	59 60
61 62	59.44	13.72 13.95	59.38	$\begin{vmatrix} 13.98 \\ 14.21 \end{vmatrix}$	$\begin{vmatrix} 59.31 \\ 60.29 \end{vmatrix}$	14.24 14.47	$\begin{bmatrix} 59.25 \\ 60.22 \end{bmatrix}$	14.50 14.74	61 62
63	$\begin{vmatrix} 61.39 \\ 62.36 \\ 63.36 \end{vmatrix}$	14.17	$\begin{vmatrix} 61.32 \\ 62.30 \\ 62.30 \end{vmatrix}$	14.44	$\begin{vmatrix} 61.26 \\ 62.23 \\ 22.23 \\ 32.23 \\ 33.23 \\ 34$	14.71	$\begin{vmatrix} 61.19 \\ 62.17 \end{vmatrix}$	$  14.97 \\ 15.21$	63 64
65	63.33	14.62	63.27	$\begin{vmatrix} 14.90 \\ 15.13 \end{vmatrix}$	$\begin{vmatrix} 63.20 \\ 64.18 \end{vmatrix}$	15.17	63.14	15.45	65
67 68 69	$   \begin{vmatrix}     65.28 \\     66.26 \\     67.23   \end{vmatrix} $	15.07	$\begin{vmatrix} 65.22 \\ 66.19 \\ 67.16 \end{vmatrix}$	15.36 15.59	65.15	15.64	65.08	15.93	68
70	68.21	15.52 $15.75$	$\frac{67.16}{68.14}$	$15.81 \\ 16.04$	$\begin{vmatrix} 67.09 \\ 68.07 \end{vmatrix}$	16.11 $16.34$	67.02 $67.99$	16.40 $16.64$	69 70
71 72 72	69.18	15.97 $16.20$	69.11	16.27 16.50	69.04	16.57 16.81	68.97	16.88	71 72
73 74 75	$\begin{vmatrix} 71.13 \\ 72.10 \\ 73.08 \end{vmatrix}$	$oxed{16.42} \ 16.65 \ 16.87$	71.06  $ 72.03 $ $ 73.00 $	16.73 16.96 17.19	$  70.98  \\ 71.96 \\ 72.93$	17.04 $17.28$ $17.50$	70.91 71.88 72.85	17.35 17.59 17.83	73 74 75
76 77	74.05	17.10 17.32	73.98 $74.95$	17.19 $17.42$ $17.65$	73.90	17.74 $17.98$	73.82	18.06 18.30	76 77
78 79	76.00 76.98	17.55 17.77	75.92 76.90	17.88 18.11	75.84 76.82	18.21	$75.76 \\ 76.74$	18.54 18.78	78 79
$\frac{80}{81}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\frac{18.00}{18.22}$	$\frac{77.87}{78.84}$	$\frac{18.34}{18.57}$	$\frac{77.79}{78.76}$	$\frac{18.68}{18.91}$	$\frac{77.71}{78.68}$	$\frac{19.01}{19.25}$	$\frac{80}{81}$
82 83	79.90	18.45	79.82	18.79 $19.02$	79.73 80.71	19.14 19.38	$\begin{vmatrix} 79.65 \\ 80.62 \end{vmatrix}$	19.49 $19.73$	82 83
84 85	81.85 82.82	$\begin{vmatrix} 18.90 \\ 19.12 \end{vmatrix}$	$\begin{vmatrix} 81.76 \\ 82.74 \end{vmatrix}$	19.25	81.68 82.65	19.61 19.84	81.59 82.56	$   \begin{array}{c}     19.97 \\     20.20   \end{array} $	84 85
86 87	83.80	$   \begin{array}{c c}     19.35 \\     19.57   \end{array} $	83.71	19.71 19.94	83.62 84.60	$\begin{bmatrix} 20.08 \\ 20.31 \end{bmatrix}$	83.54 84.51	$20.44 \\ 20.68$	86 87
88 89	$\begin{vmatrix} 85.74 \\ 86.72 \end{vmatrix}$	$\begin{bmatrix} 19.80 \\ 20.02 \end{bmatrix}$	85.66 86.63	$\begin{bmatrix} 20.17 \\ 20.40 \end{bmatrix}$	85.57 86.54	$\begin{array}{c} 20.54 \\ 20.78 \end{array}$	85.48 86.45	$\frac{20.92}{21.15}$	88 89
$\frac{90}{91}$	$\frac{87.69}{88.67}$	$\frac{20.25}{20.47}$	87.60	$\frac{20.63}{20.86}$	$\frac{87.51}{88.49}$	$\frac{21.01}{21.24}$	$\frac{87.42}{88.39}$	$\frac{21.39}{21.63}$	$\frac{90}{91}$
92 93	89.64 90.62	$\begin{bmatrix} 20.70 \\ 20.92 \end{bmatrix}$	$\begin{vmatrix} 89.55 \\ 90.52 \end{vmatrix}$	$\begin{bmatrix} 21.09 \\ 21.32 \end{bmatrix}$	$\begin{vmatrix} 89.46 \\ 90.43 \end{vmatrix}$	$\begin{bmatrix} 21.48 \\ 21.71 \end{bmatrix}$	89.36 90.33	$\frac{21.87}{22.10}$	92 93
94 95	$91.59 \\ 92.57$	$\begin{vmatrix} 21.15 \\ 21.37 \end{vmatrix}$	$\begin{bmatrix} 91.50 \\ 92.47 \end{bmatrix}$	$\frac{21.54}{21.77}$	$\begin{array}{ c c }\hline 91.40\\92.38\\\hline\end{array}$	21.94 22.18	$\begin{bmatrix} 91.31 \\ 92.28 \end{bmatrix}$	$\frac{22.34}{22.58}$	94 95
96 97	$93.54 \\ 94.51$	$21.60 \\ 21.82$	$\begin{vmatrix} 93.44 \\ 94.42 \end{vmatrix}$	$\begin{array}{c} 22.00 \\ 22.23 \end{array}$	$\begin{vmatrix} 93.35 \\ 94.32 \end{vmatrix}$	22.41 22.64	$\begin{bmatrix} 93.25 \\ 94.22 \end{bmatrix}$	22.82 23.06	96 97
98	95.49	22.27	$ \begin{array}{c} 95.39 \\ 96.36 \\ 07.24 \\ \end{array} $	$22.46 \\ 22.69$	$\begin{vmatrix} 95.29 \\ 96.26 \\ 07.24 \end{vmatrix}$	22.88 23.11	95.19  $ 96.16 $	23.29	98
$\frac{100}{3}$	$\frac{97.44}{\text{Dep.}}$	22.50 Lat.	97.34 22.92 Dep. Lat.		$\frac{97.24}{\text{Dep.}}$	23.34 Lat.	$\frac{97.13}{\text{Dep.}}$	23.77 Lat.	ce.
Distance.						•			Distance.
D	77]	Deg.	763	Deg.	$76\frac{1}{2}$	Deg.	764 ]	Deg.	D

			1				1		
Distance.	14	Deg.	141	Deg.	$14\frac{1}{2}$	Deg.	143	Deg.	Distance.
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ınce
$\frac{1}{2}$	$0.97 \\ 1.94$	$\begin{array}{ c c }\hline 0.24\\ 0.48\\ \end{array}$	$0.97 \\ 1.94$	$0.25 \\ 0.49$	$\begin{array}{r} \hline 0.97 \\ 1.94 \end{array}$	$\begin{array}{c} 0.25 \\ 0.50 \end{array}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{ c c }\hline 0.25 \\ 0.51 \\ \hline \end{array}$	1
$\begin{bmatrix} 2\\3\\4 \end{bmatrix}$	2.91 3.88	$\begin{bmatrix} 0.73 \\ 0.97 \end{bmatrix}$	$\frac{2.91}{3.88}$	$0.74 \\ 0.98$	$\begin{bmatrix} 2.90 \\ 3.87 \end{bmatrix}$	0.75	2.90	$0.76 \\ 1.02$	2 3 4 5
5 6	4.85 5.82	$1.21 \\ 1.45$	4.85 5.82	1.23 $1.48$	4.84 5.81	$1.25 \\ 1.50$	4.84 5.80	1.27 $1.53$	5
8	$\begin{vmatrix} 6.79 \\ 7.76 \end{vmatrix}$	1.69 1.94	6.78 7.75	$1.72 \\ 1.97$	6.78	$\begin{bmatrix} 1.75 \\ 2.00 \end{bmatrix}$	6.77	1.78 $2.04$	6 7
9 10	$\begin{bmatrix} 8.73 \\ 9.70 \end{bmatrix}$	$2.18 \\ 2.42$	8.72 9.69	$2.22 \\ 2.46$	8.71 9.68	$2.25 \\ 2.50$	8.70	2.29 2.55	$\begin{bmatrix} 8 \\ 9 \\ 10 \end{bmatrix}$
11 12	$  10.67 \\   11.64  $	$2.66 \\ 2.90$	10.66 11.63	$2.71 \\ 2.95$	10.65 $11.62$	$\begin{array}{ c c }\hline 2.75\\ 3.00\\ \end{array}$	$\begin{array}{ c c c }\hline 10.64\\11.60\end{array}$	$\begin{array}{c} -2.80 \\ 3.06 \end{array}$	$\frac{11}{12}$
13	$\begin{vmatrix} 12.61 \\ 13.58 \end{vmatrix}$	$\begin{array}{ c c }\hline 3.15\\ 3.39\\ \end{array}$	$\begin{vmatrix} 12.60 \\ 13.57 \end{vmatrix}$	$\frac{3.20}{3.45}$	12.59 13.55	$\frac{3.25}{3.51}$	12.57 13.54	3.31 3.56	13 14
15 16	14.55   15.52	$\begin{vmatrix} 3.63 \\ 3.87 \end{vmatrix}$	14.54 15.51	$\frac{3.69}{3.94}$	$14.52 \\ 15.49$	$\frac{3.76}{4.01}$	14.51 15.47	$\frac{3.82}{4.07}$	15 16
17 18	16.50 17.47	4.11 4.35	16.48 17.45	$4.18 \\ 4.43$	$16.46 \\ 17.43$	$\begin{array}{c} 4.26 \\ 4.51 \end{array}$	16.44 17.41	4.33	17 18
19 20	$\begin{vmatrix} 18.44 \\ 19.41 \end{vmatrix}$	$\frac{4.60}{4.84}$	18.42 19.38	$4.68 \\ 4.92$	$18.39 \\ 19.36$	$\begin{array}{c c} 4.76 \\ 5.01 \end{array}$	18.37 19.34	4.84 5.09	19 20
21 22	$20.38 \\ 21.35$	$\frac{5.08}{5.32}$	$\begin{array}{ c c c } \hline 20.35 \\ 21.32 \\ \hline \end{array}$	$\begin{array}{r} 5.17 \\ 5.42 \end{array}$	$20.33 \\ 21.30$	$\frac{5.26}{5.51}$	$     \begin{array}{ c c c c c c c c c c c c c c c c c c c$	5.35	21
23 24	$\begin{vmatrix} 22.32 \\ 23.99 \end{vmatrix}$	5.56 5.81	$22.29 \\ 23.26$	5.66	$   \begin{bmatrix}     22.27 \\     23.24   \end{bmatrix} $	$\begin{bmatrix} 5.76 \\ 6.01 \end{bmatrix}$	$\begin{bmatrix} 21.28 \\ 22.24 \\ 23.21 \end{bmatrix}$	5.60 5.86 6.11	22 23
25 26	$\begin{vmatrix} 24.26 \\ 25.23 \end{vmatrix}$	$\begin{array}{c} 6.05 \\ 6.29 \end{array}$	$\begin{vmatrix} 24.23 \\ 25.20 \end{vmatrix}$	6.15	24.20 $25.17$	$\begin{array}{c} 6.26 \\ 6.51 \end{array}$	24.18 25.14	$6.37 \\ 6.62$	24 25
27 28	$\begin{vmatrix} 26.20 \\ 27.17 \end{vmatrix}$	$6.53 \\ 6.77$	$\begin{vmatrix} 26.17 \\ 27.14 \end{vmatrix}$	6.65	$ \begin{array}{c c} 26.14 \\ 27.11 \end{array} $	6.76 $7.01$	$\begin{bmatrix} 25.14 \\ 26.11 \\ 27.08 \end{bmatrix}$	6.87 $7.13$	26 27 28
$\begin{array}{ c c }\hline 29\\ 30\\ \hline \end{array}$	$   \begin{array}{r}     28.14 \\     29.11   \end{array} $	$7.02 \\ 7.26$	$\begin{vmatrix} 28.11 \\ 29.08 \end{vmatrix}$	7.14 7.38	28.08 29.04	$7.26 \\ 7.51$	$\begin{bmatrix} 27.08 \\ 28.04 \\ 29.01 \end{bmatrix}$	7.38 $7.64$	29 30
31 32	30.08	$7.50 \\ 7.74$	$30.05 \\ 31.02$	7.63 7.88	$\frac{30.01}{30.98}$	$\frac{7.76}{8.01}$	$\frac{29.98}{30.95}$	7.89	$\overline{31}$
33 34	$\begin{bmatrix} 32.02 \\ 32.99 \end{bmatrix}$	$7.98 \\ 8.23$	$\begin{vmatrix} 31.98 \\ 32.95 \end{vmatrix}$	$8.12 \\ 8.37$	$\begin{vmatrix} 31.95 \\ 32.92 \end{vmatrix}$	8.26 8.51	31.91 $32.88$	$8.15 \\ 8.40 \\ 8.66$	32 33
35 36	$33.96 \\ 34.93$	8.47	$\begin{vmatrix} 33.92 \\ 34.89 \end{vmatrix}$	8.62 8.86	33.89 34.85	8.76 9.01	33.85 34.81	8.91 9.17	34 35
37 38	$35.90 \\ 36.87$	$\begin{array}{c} 8.95 \\ 9.19 \end{array}$	35.86 36.83	$9.11 \\ 9.35$	$\begin{vmatrix} 35.82 \\ 36.79 \end{vmatrix}$	$9.26 \\ 9.51$	35.78 36.75	$9.42 \\ 9.67$	36 37
$\begin{bmatrix} 39 \\ 40 \end{bmatrix}$	37.84 38.81	$\begin{array}{c} 9.44 \\ 9.68 \end{array}$	$37.80 \\ 38.77$	9.60 9.85	$\begin{vmatrix} 37.76 \\ 38.73 \end{vmatrix}$	$9.76 \\ 10.02$	37.71 38.68	9.93	38
41 42	$39.78 \\ 40.75$	$\frac{9.92}{10.16}$	$\frac{39.74}{40.71}$	$\frac{10.09}{10.34}$	39.69 $40.66$	$\overline{10.27}$	39.65	10.44	$\frac{40}{41}$
43	$\begin{vmatrix} 41.72 \\ 42.69 \end{vmatrix}$	$     \begin{array}{c c}       10.40 \\       10.64     \end{array} $	$41.68 \\ 42.65$	$\begin{vmatrix} 10.54 \\ 10.58 \\ 10.83 \end{vmatrix}$	$\begin{vmatrix} 40.66 \\ 41.63 \\ 42.60 \end{vmatrix}$	10.52 $10.77$	$\begin{vmatrix} 40.62 \\ 41.58 \\ 49.55 \end{vmatrix}$	10.69 $10.95$	42 43
45 46	43.66	10.89	43.62 44.58	11.08 $11.32$	$\begin{vmatrix} 42.60 \\ 43.57 \\ 44.53 \end{vmatrix}$	$egin{array}{c} 11.02 \ 11.27 \ 11.52 \ \end{array}$	42.55	11.20 $11.46$	44 45
47 48	$\frac{45.60}{46.57}$	11.37 11.61	45.55 46.52	11.57 $11.82$	45.50 46.47	$\begin{vmatrix} 11.32 \\ 11.77 \\ 12.02 \end{vmatrix}$	44.48	11.71	46 47
49 50	47.54 48.51	11.85 $12.10$	47.49 48.46	12.06 $12.31$	47.44 48.41	12.02 $12.27$ $12.52$	$\begin{array}{c} 46.42 \\ 47.39 \\ 48.35 \end{array}$	$egin{array}{c} 12.22 \ 12.48 \ 12.73 \ \end{array}$	48 49 50
Distance.	Dep.	Lat.	Dep. Lat.		Dep.	Lat.	Dep.	Lat.	
Dist	76 I	Deg.	753 ]	Deg.	$75\frac{1}{2}$	Deg.	751	Deg.	Distance.
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Distance.	14	Deg.	141	Deg.	$14\frac{1}{2}$	Deg.	143	Deg.	Distance.
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
51 52 53 54 55 56 57 59 60 61 62 63 64 65 66 67 77 77 77 77 77 77 77 77 77 77 77	49.49         50.46         51.43         52.40         33.37         54.34         55.31         56.28         57.25         58.22         59.19         60.16         61.13         62.10         63.07         64.04         65.92         68.89         69.86         70.83         71.80         72.77         73.74         74.71         75.68         76.65         77.62         78.59         79.56         80.53         81.50         82.48         83.30         89.27         90.24         91.21         92.18         93.15         94.12         95.09         96.06         97.03	12.34         12.58         12.58         13.06         13.31         13.55         13.79         14.03         14.52         14.76         15.00         15.24         15.48         15.72         16.45         16.69         16.93         17.18         17.66         17.90         18.14         18.39         18.63         18.87         19.35         19.60         19.84         20.08         20.32         20.56         20.56         21.29         21.53         21.77         22.26         23.47         23.71         23.95         24.19	49.43         50.40         51.37         52.34         53.31         54.28         55.25         56.22         57.18         59.12         60.09         61.06         62.03         63.97         64.94         65.91         66.88         67.85         68.82         69.78         70.75         72.69         73.66         74.63         75.60         76.57         77.54         78.51         79.48         80.45         81.42         82.38         83.35         84.32         85.29         86.26         87.23         89.17         90.14         91.11         92.92	12.55 12.80 13.05 13.29 13.54 13.78 14.03 14.28 14.52 14.77 15.02 15.26 15.5! 15.75 16.00 16.25 16.49 16.74 16.98 17.23 17.48 17.72 18.22 18.46 18.71 18.95 19.94 20.18 20.43 20.68 20.92 21.17 21.66 21.91 22.15 22.40 22.65 23.89 23.88 24.62	49.38         50.34         51.31         52.28         53.25         54.22         55.18         56.15         57.12         58.09         59.06         60.03         60.99         61.96         62.93         63.90         64.87         65.83         67.77         68.74         69.71         70.67         71.64         72.61         73.58         74.55         75.52         76.48         77.45         78.42         79.39         80.36         81.32         82.29         83.26         84.23         85.20         86.17         87.13         88.10         89.07         91.91         94.88         95.85         96.81	12.77 13.02 13.27 13.52 13.77 14.02 14.27 14.52 14.77 15.02 15.27 15.52 15.77 16.02 16.27 16.53 17.78 17.28 17.53 17.78 18.03 17.28 17.53 17.78 18.03 19.28 19.53 19.53 19.28 20.53 20.78 21.28 21.53 21.78 22.28 21.78 22.28 22.28 22.53 22.28 23.54 24.79 24.54 24.79 24.54 24.79 25.04	49.32         50.29         51.25         52.22         53.19         54.15         55.12         56.09         57.06         58.99         59.96         60.92         61.89         62.86         63.83         64.79         65.76         69.63         71.56         72.53         73.50         74.46         75.43         76.40         77.36         81.23         82.20         83.17         84.13         85.10         86.07         87.03         88.00         88.97         89.94         90.90         91.87         95.74         96.70	12.98         13.24         13.49         13.75         14.00         14.51         14.77         15.02         15.28         15.53         15.53         15.79         16.04         16.29         16.55         17.31         17.57         17.82         18.08         18.33         18.59         18.60         19.86         20.11         20.62         20.88         21.13         21.64         22.15         22.41         23.68         23.17         23.68         23.17         23.68         23.17         23.44         24.95         25.21         25.46         25.21         25.46	51 52 53 54 55 56 57 58 59 61 62 63 64 65 66 67 68 69 71 72 73 74 75 76 77 78 78 80 81 82 83 84 85 86 87 88 88 89 90 90 90 90 90 90 90 90 90 9
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
Dis.	76 1	Deg.	753	Deg.	75½	Deg.	754	Deg.	Dis

-							2		
Distance	15 I	Deg.	154	Deg.	15½	Deg.	15¾	Deg.	Distance.
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
1 2 3 4 5 6 7 8 9 10	0.97 1.93 2.90 3.86 4.83 5.80 6.76 7.73 8.69 9.66	0.26 0.52 0.78 1.04 1.29 1.55 1.81 2.07 2.33 2.59	0.96 1.93 2.89 3.86 4.82 5.79 6.75 7.72 8.68 9.65	0.26 0.53 0.79 1.05 1.32 1.58 1.84 2.10 2.37 2.63	0.96 1.93 2.89 3.85 4.82 5.78 6.75 7.71 8.67 9.64	0.27 0.53 0.80 1.07 1.34 1.60 1.87 2.14 2.41 2.67	0.96 1.92 2.89 3.85 4.81 5.77 6.74 7.70 8.66 9.62	0.27 0.54 0.81 1.09 1.36 1.63 1.90 2.17 2.44 2.71	1 2 3 4 5 6 7 8 9
11 12 13 14 15 16 17 18 19 20	10.63 11.59 12.56 13.52 14.49 15.45 16.42 17.39 18.35 19.32	2.85 3.11 3.36 3.62 3.88 4.14 4.40 4.66 4.92 5.18	10.61 11.58 12.54 13.51 14.47 15.44 16.40 17.37 18.33 19.30	2.89 3.16 3.42 3.68 3.95 4.21 4.47 4.73 5.00 5.26	10.60 11.56 12.53 13.49 14.45 15.42 16.38 17.35 18.31 19.27	2.94 3.21 3.47 3.74 4.01 4.28 4.54 4.51 5.08 5.34	10.59 11.55 12.51 13.47 14.44 15.40 16.36 17.32 18.29 19.25	2.99 3.26 3.53 3.80 4.07 4.34 4.61 4.89 5.16 5.43	11 12 13 14 15 16 17 18 19 20
21 22 23 24 25 26 27 28 29 30	20.28 21.25 22.22 23.18 24.15 25.11 26.08 27.05 28.01 28.98	5.44 5.69 5.95 6.21 6.47 6.73 6.99 7.25 7.51 7.76	20.26 21.23 22.19 23.15 24.12 25.08 26.05 27.01 27.98 28.94	5.52 5.79 6.05 6.31 6.58 6.84 7.10 7.36 7.63 7.89	$ \begin{array}{r}     \hline                                $	5.61 5.88 6.15 6.41 6.68 6.95 7.22 7.48 7.75 8.02	20.21 21.17 22.14 23.10 24.06 25.02 25.99 26.95 27.91 28.87	5.70 5.97 6.24 6.51 6.79 7.06 7.33 7.60 7.87 8.14	21 22 23 24 25 26 27 28 29 30
31 32 33 34 35 36 37 38 39 40	29.94 30.91 31.88 32.84 33.81 34.77 35.74 36.71 37.67 38.64	8.02 8.28 8.54 8.80 9.06 9.32 9.58 9.84 10.09 10.35	29.91 30.87 31.84 32.80 33.77 34.73 35.70 36.66 37.63 38.59	8.15 8.42 8.68 8.94 9.21 9.47 9.73 10.00 10.26 10.52	29.87 30.84 31.80 32.76 33.73 34.69 35.65 36.62 37.58 38.55	8.28 8.55 8.82 9.09 9.35 9.62 9.89 10.16 10.42 10.69	29.84 30.80 31.76 32.72 33.69 34.65 35.61 36.57 37.54 38.50	8.41 8.69 8.96 9.23 9.50 9.77 10.04 10.31 10.59 10.86	31 32 33 34 35 36 37 38 39 40
41 42 43 44 45 46 47 48 49 50	39.60 40.57 41.53 42.50 43.47 44.43 45.40 46.36 47.33 48.30	10.61 10.87 11.13 11.39 11.65 11.91 12.16 12.42 12.68 12.94	39.56 40.52 41.49 42.45 43.42 44.38 45.35 46.31 47.27 48.24	10.78 11.05 11.31 11.57 11.84 12.10 12.36 12.63 12.89 13.15	39.51 40.47 41.44 42.40 43.36 44.33 45.29 46.25 47.22 48.18	10.96 11.22 11.49 11.76 12.03 12.29 12.56 12.83 13.09 13.36	39.46 40.42 41.39 42.35 43.31 44.27 45.24 46.20 47.16 48.12	11.13 11.40 11.67 11.94 12.21 12.49 12.76 13.03 13.30 13.57	41 42 43 44 45 46 47 48 49 50
Distance.	Dep. 75 1	Lat.	Lat. Dep. Lat.		74½	Lat. Deg.	Dep. 741	Lat. Deg.	Distance.

D	15	Deg.	15}	Deg.	151	Deg.	153	Deg.	ם
Distance. 15									Distance.
ce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51 52	$\begin{vmatrix} 49.26 \\ 50.23 \end{vmatrix}$	$\begin{array}{ c c } 13.20 \\ 13.46 \end{array}$	$\begin{array}{ c c }\hline 49.20\\ 50.17\end{array}$	$\begin{array}{ c c }\hline 13.41\\ 13.68\\ \hline\end{array}$	$\begin{vmatrix} 49.15 \\ 50.11 \end{vmatrix}$	$\begin{bmatrix} 13.63 \\ 13.90 \end{bmatrix}$	49.09 50.05	13.84	51 52
53 54	$\begin{bmatrix} 51.19 \\ 52.16 \end{bmatrix}$	$\begin{vmatrix} 13.72 \\ 13.98 \end{vmatrix}$	$51.13 \\ 52.10$	$\begin{array}{c} 13.94 \\ 14.20 \end{array}$	$\begin{bmatrix} 51.07 \\ 52.04 \end{bmatrix}$	$14.16 \\ 14.43$	51.01 51.97	$14.39 \\ 14.66$	53 54
55	53.13	14.24	53.06	14.47	53.00	14.70	52.94	14.93	55
56 57	$\begin{bmatrix} 54.09 \\ 55.06 \end{bmatrix}$	14.49   14.75	$\begin{bmatrix} 54.03 \\ 54.99 \end{bmatrix}$	$\begin{bmatrix} 14.73 \\ 14.99 \end{bmatrix}$	$53.96 \\ 54.93$	$14.97 \\ 15.23$	$53.90 \\ 54.86$	$\begin{array}{c} 15.20 \\ 15.47 \end{array}$	56 57
58 59	$  56.02   \\ 56.99  $	$\begin{array}{c c} 15.01 \\ 15.27 \end{array}$	$\begin{bmatrix} 55.96 \\ 56.92 \end{bmatrix}$	$\begin{array}{c c} 15.26 \\ 15.52 \end{array}$	55.89 56.85	$\begin{array}{c c} 15.50 \\ 15.77 \end{array}$	55.82 56.78	$\begin{array}{ c c }\hline 15.74\\ 16.01\end{array}$	58 59
60	$\frac{57.96}{59.00}$	15.53	57.89	15.78	57.82	16.03	57.75	16.29	$\frac{60}{61}$
61 62	58.92 59.89	$15.79 \\ 16.05$	58.85  $ 59.82 $	$16.04 \\ 16.31$	58.78 59.75	$\begin{array}{c c} 16.30 \\ 16.57 \end{array}$	58.71 59.67	$16.56 \\ 16.83$	62
63 64	$60.85 \\ 61.82$	$\begin{array}{c c} 16.31 \\ 16.56 \end{array}$	$\begin{bmatrix} 60.78 \\ 61.75 \end{bmatrix}$	$\begin{bmatrix} 16.57 \\ 16.83 \end{bmatrix}$	$\begin{vmatrix} 60.71 \\ 61.67 \end{vmatrix}$	$16.84 \\ 17.10$	60.63	$  \begin{array}{c} 17.10 \\ 17.37 \end{array}  $	63 64
65 66	$\begin{vmatrix} 62.79 \\ 63.75 \end{vmatrix}$	$16.82 \\ 17.08$	$\begin{vmatrix} 62.71 \\ 63.68 \end{vmatrix}$	$17.10 \\ 17.35$	$\begin{bmatrix} 62.64 \\ 63.60 \end{bmatrix}$	$\begin{array}{c} 17.37 \\ 17.64 \end{array}$	$62.56 \\ 63.52$	$17.64 \\ 17.92$	65 66
67	64.72	17.34	64.64	17.62	64.56	17.90	64.48	18.19	67
68 69	$\begin{array}{c} 65.68 \\ 66.65 \end{array}$	$17.60 \\ 17.86$	65.61	17.89 18.15	$\begin{vmatrix} 65.53 \\ 66.49 \end{vmatrix}$	18.17   18.44	65.45	$\begin{array}{c} 18.46 \\ 18.73 \end{array}$	68 69
$\frac{70}{71}$	$\frac{67.61}{68.58}$	$\frac{18.12}{18.38}$	$\frac{67.54}{68.50}$	$\frac{18.41}{18.68}$	$\frac{67.45}{68.42}$	$\frac{18.71}{18.97}$	$\begin{array}{ c c }\hline 67.37 \\ \hline 68.33\end{array}$	$\frac{19.00}{19.27}$	$\frac{70}{71}$
72	69.55	18.63	69.46	18.94	69.38	19.24	69.30	19.54	72 73
73 74	70.51 $71.48$	$18.89 \\ 19.15$	70.43  $ 71.39 $	$\begin{array}{c c} 19.20 \\ 19.46 \end{array}$	$\begin{bmatrix} 70.35 \\ 71.31 \end{bmatrix}$	$19.51 \\ 19.78$	70.26 $  71.22$	$\begin{bmatrix} 19.82 \\ 20.09 \end{bmatrix}$	74
75 76	$72.44 \\ 73.41$	$\begin{bmatrix} 19.41 \\ 19.67 \end{bmatrix}$	$\begin{bmatrix} 72.36 \\ 73.32 \end{bmatrix}$	$\begin{array}{c c} 19.73 \\ 19.99 \end{array}$	$72.27 \\ 73.24$	$\begin{bmatrix} 20.04 \\ 20.31 \end{bmatrix}$	$\begin{vmatrix} 72.18 \\ 73.15 \end{vmatrix}$	$\begin{bmatrix} 20.36 \\ 20.63 \end{bmatrix}$	75 76
77	$74.38 \\ 75.34$	$19.93 \\ 20.19$	$74.29 \\ 75.25$	$\begin{array}{c} 20.25 \\ 20.52 \end{array}$	$\begin{vmatrix} 74.20 \\ 75.16 \end{vmatrix}$	$20.58 \\ 20.84$	$74.11 \\ 75.07$	$\left  egin{array}{c} 20.90 \ 21.17 \end{array} \right $	77 78
79 80	$76.31 \\ 77.27$	$\begin{bmatrix} 20.45 \\ 20.71 \end{bmatrix}$	76.22	$\begin{bmatrix} 20.78 \\ 21.04 \end{bmatrix}$	76.13	21.11	$76.03 \\ 77.00$	$21.44 \\ 21.72$	79 80
81	$\overline{78.24}$	$\frac{20.11}{20.96}$	$\frac{77.18}{78.15}$	$\frac{21.04}{21.31}$	$\frac{77.09}{78.05}$	$\begin{array}{ c c }\hline 21.38 \\ \hline 21.65 \\ \hline \end{array}$	77.96	$\overline{21.99}$	81
82 83	$\begin{vmatrix} 79.21 \\ 80.17 \end{vmatrix}$	$     \begin{array}{c c}       21.22 \\       21.48     \end{array} $	$\begin{vmatrix} 79.11 \\ 80.08 \end{vmatrix}$	$21.57 \\ 21.83$	$79.02 \\ 79.98$	$\begin{bmatrix} 21.91 \\ 22.18 \end{bmatrix}$	$  \begin{array}{c} 78.92 \\ 79.88 \end{array}  $	$22.26 \\ 22.53$	82 83
84	$   \begin{array}{c c}     81.14 \\     82.10   \end{array} $	$\begin{bmatrix} 21.74 \\ 22.00 \end{bmatrix}$	$\begin{vmatrix} 81.04 \\ 82.01 \end{vmatrix}$	$22.09 \\ 22.36$	80.94	22.45	80.85	$\begin{bmatrix} 22.80 \\ 23.07 \end{bmatrix}$	84. 85
85 86	83.07	22.26	82.97	22.62	$\begin{vmatrix} 81.91 \\ 82.87 \end{vmatrix}$	$\begin{bmatrix} 22.72 \\ 22.98 \end{bmatrix}$	82.77	23.34	86
87 88	$\begin{array}{ c c }\hline 84.04\\ 85.00\\ \hline\end{array}$	$\begin{bmatrix} 22.52 \\ 22.78 \end{bmatrix}$	$\begin{vmatrix} 83.94 \\ 84.90 \end{vmatrix}$	$22.88 \\ 23.15$	83.84	$23.25 \\ 23.52$	$\begin{vmatrix} 83.73 \\ 84.70 \end{vmatrix}$	$oxed{23.62}{23.89}$	87 88
89 90	85.97 86.93	$\begin{vmatrix} 23.03 \\ 23.29 \end{vmatrix}$	85.87 86.83	$23.41 \\ 23.67$	85.76 86.73	$\begin{bmatrix} 23.78 \\ 24.05 \end{bmatrix}$	85.66	$\begin{bmatrix} 24.16 \\ 24.43 \end{bmatrix}$	89 90
91	87.90	$\overline{23.55}$	87.80	$\overline{23.94}$	87.69	$\overline{24.32}$	87.58	$24.70 \\ 24.97$	91
92 93	88.87	$\begin{vmatrix} 23.81 \\ 24.07 \end{vmatrix}$	$\begin{vmatrix} 88.76 \\ 89.73 \end{vmatrix}$	$\begin{vmatrix} 24.20 \\ 24.46 \end{vmatrix}$	88.65 89.62	$\begin{vmatrix} 24.59 \\ 24.85 \end{vmatrix}$	88.55 89.51	25.24	92 93
94 95	90.80  $ 91.76 $	$\begin{bmatrix} 24.33 \\ 24.59 \end{bmatrix}$	90.69  $ 91.65 $	$24.72 \\ 24.99$	90.58 $91.54$	$\begin{vmatrix} 25.12 \\ 25.39 \end{vmatrix}$	$  90.47 \\ 91.43  $	$\left  \begin{array}{c} 25.52 \\ 25.79 \end{array} \right $	94 95
96 97	$92.73 \\ 93.69$	24.85 25.11	92.62	$25.25 \\ 25.51$	$92.51 \\ 93.47$	25.65 25.92	$92.40 \\ 93.36$	$\begin{bmatrix} 26.06 \\ 26.33 \end{bmatrix}$	96 97
98	94.66	25.36	94.55	25.78	94.44	26.19	94.32 95.28	26.60 $26.87$	98 99
100	95.63	$25.62 \ 25.88$	$95.51 \\ 96.48$	$\begin{array}{ c c c }\hline 26.04 \\ 26.30 \\ \hline \end{array}$	$\begin{array}{c} 95.40 \\ 96.36 \end{array}$	$\begin{bmatrix} 26.46 \\ 26.72 \end{bmatrix}$	$\frac{95.28}{96.25}$	$\frac{20.87}{27.14}$	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
Dista	75 ]	Deg.	743	Deg.	74 <del>1</del>	Deg.	744	Deg.	Dist
-									

-	ע	16	Deg.	16}	Deg.	161	Deg.	163	Deg.	
	Distance.							104	Deg.	Distance.
		Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
	1 2	$\begin{array}{ c c } 0.96 \\ 1.92 \\ \end{array}$	$0.28 \\ 0.55$	$\begin{array}{ c c }\hline 0.96\\ 1.92\\ \end{array}$	$\begin{array}{c} 0.28 \\ 0.56 \end{array}$	$\begin{array}{c} 0.96 \\ 1.92 \end{array}$	$\begin{array}{c} 0.28 \\ 0.57 \end{array}$	$\begin{array}{c c} 0.96 \\ 1.92 \end{array}$	$\begin{array}{c} 0.29 \\ 0.58 \end{array}$	$\frac{1}{2}$
	3 4	2.88 3.85	0.83 $1.10$	2.88 3.84	$0.84 \\ 1.12$	$2.88 \\ 3.84$	$0.85 \\ 1.14$	$\begin{bmatrix} 2.87 \\ 3.83 \end{bmatrix}$	$0.86 \\ 1.15$	$\frac{3}{4}$
	5 6	4.81 5.77	1.38 $1.65$	4.80 5.76	$\begin{array}{c} 1.40 \\ 1.68 \end{array}$	4.79 5.75	$\begin{bmatrix} 1.42 \\ 1.70 \end{bmatrix}$	$\begin{array}{ c c }\hline 4.79\\ 5.75\\ \end{array}$	$\begin{array}{c} 1.44 \\ 1.73 \end{array}$	5 6
	8	6.73	$\begin{bmatrix} 1.93 \\ 2.21 \end{bmatrix}$	6.72 7.68	$\begin{array}{c} 1.96 \\ 2.24 \end{array}$	$6.71 \\ 7.67$	$egin{array}{c} 1.99 \ 2.27 \ \end{array}$	$\begin{array}{ c c } 6.70 \\ 7.66 \end{array}$	$\begin{array}{c} 2.02 \\ 2.31 \end{array}$	7 8
Contract of the Contract of th	$\begin{array}{c} 9 \\ 10 \end{array}$	$\begin{array}{ c c } 8.65 \\ 9.61 \\ \hline \end{array}$	$\begin{bmatrix} 2.48 \\ 2.76 \end{bmatrix}$	$\begin{array}{ c c } 8.64 \\ 9.60 \end{array}$	$\begin{bmatrix} 2.52 \\ 2.80 \end{bmatrix}$	$\begin{array}{c} 8.63 \\ 9.59 \end{array}$	$\begin{bmatrix} 2.56 \\ 2.84 \end{bmatrix}$	$\begin{array}{ c c }\hline 8.62\\ 9.58\\ \hline\end{array}$	$2.59 \\ 2.88$	9 10
The second second	11 12	10.57 $11.54$	$\begin{array}{ c c }\hline 3.03\\ 3.31\end{array}$	$10.56 \\ 11.52$	$\begin{array}{c} 3.08 \\ 3.36 \end{array}$	10.55	$\frac{3.12}{3.41}$	$10.53 \\ 11.49$	$\begin{array}{c} 3.17 \\ 3.46 \end{array}$	11 12
1	13 14	$\begin{vmatrix} 12.50 \\ 13.46 \end{vmatrix}$	$\begin{vmatrix} 3.58 \\ 3.86 \end{vmatrix}$	$\begin{vmatrix} 12.48 \\ 13.44 \end{vmatrix}$	$\begin{array}{c} 3.64 \\ 3.92 \end{array}$	$\begin{array}{ c c }\hline 12.46\\13.42\end{array}$	$\begin{bmatrix} 3.69 \\ 3.98 \end{bmatrix}$	$\begin{array}{ c c }\hline 12.45\\ 13.41\end{array}$	$\begin{array}{c} 3.75 \\ 4.03 \end{array}$	13 14
	15 16	$\begin{vmatrix} 14.42 \\ 15.38 \end{vmatrix}$	$ \begin{array}{c} 4.13 \\ 4.41 \\  \end{array}$	$\begin{vmatrix} 14.40 \\ 15.36 \end{vmatrix}$	4.20 4.48	$\begin{vmatrix} 14.38 \\ 15.34 \end{vmatrix}$	$\begin{array}{ c c }\hline 4.26 \\ 4.54 \end{array}$	$\begin{array}{ c c }\hline 14.36\\15.32\\\hline\end{array}$	$\begin{array}{c} 4.32 \\ 4.61 \end{array}$	15 16
	17 18	16.34 $17.30$	$\begin{vmatrix} 4.69 \\ 4.96 \end{vmatrix}$	$\begin{bmatrix} 16.32 \\ 17.28 \end{bmatrix}$	$\begin{array}{c} 4.76 \\ 5.04 \end{array}$	$16.30 \\ 17.26$	$\begin{array}{ c c } 4.83 \\ 5.11 \end{array}$	$16.28 \\ 17.24$	$\frac{4.90}{5.19}$	17 i8
	19 20	$18.26 \\ 19.23$	$\begin{bmatrix} 5.24 \\ 5.51 \end{bmatrix}$	$\begin{array}{ c c }\hline 18.24\\ 19.20\\ \hline\end{array}$	$\begin{bmatrix} 5.32 \\ 5.60 \end{bmatrix}$	18.22 $19.18$	$\begin{array}{ c c }\hline 5.40\\ 5.68\\ \end{array}$	$  18.19 \\ 19.15  $	$\begin{array}{c} 5.48 \\ 5.76 \end{array}$	19 20
	$\begin{array}{c} 21 \\ 22 \end{array}$	20.19 $21.15$	$\begin{bmatrix} 5.79 \\ 6.06 \end{bmatrix}$	$\begin{vmatrix} 20.16 \\ 21.12 \end{vmatrix}$	$\begin{array}{c} 5.88 \\ 6.16 \end{array}$	$20.14 \\ 21.09$	$\begin{array}{c} 5.96 \\ 6.25 \end{array}$	$\begin{array}{ c c c }\hline 20.11\\21.07\\ \end{array}$	$\begin{array}{c} 6.05 \\ 6.34 \end{array}$	$\frac{21}{22}$
	$\begin{bmatrix} 23 \\ 24 \end{bmatrix}$	$22.11 \\ 23.07$	$\begin{bmatrix} 6.34 \\ 6.62 \end{bmatrix}$	$\begin{bmatrix} 22.08 \\ 23.04 \end{bmatrix}$	$\begin{array}{c} 6.44 \\ 6.72 \end{array}$	$\begin{vmatrix} 22.05 \\ 23.01 \end{vmatrix}$	$\begin{array}{c} 6.53 \\ 6.82 \end{array}$	$\begin{vmatrix} 22.02 \\ 22.98 \end{vmatrix}$	$\begin{array}{c} 6.63 \\ 6.92 \end{array}$	23 24
J. 1900 J. A	25 26	$24.03 \\ 24.99$	$\begin{bmatrix} 6.89 \\ 7.17 \end{bmatrix}$	$\begin{bmatrix} 24.00 \\ 24.96 \end{bmatrix}$	$\begin{array}{c} 7.00 \\ 7.28 \end{array}$	$\begin{bmatrix} 23.97 \\ 24.93 \end{bmatrix}$	$7.10 \\ 7.38$	$23.94 \\ 24.90$	7.20 $7.49$	25 26
1	27 28	$25.95 \\ 26.92$	$\begin{array}{ c c }\hline 7.44\\ 7.72\end{array}$	$\begin{bmatrix} 25.92 \\ 26.88 \end{bmatrix}$	$7.56 \\ 7.84$	$25.89 \\ 26.85$	$\begin{array}{c c} 7.67 \\ 7.95 \end{array}$	$25.85 \\ 26.81$	$\begin{array}{c} 7.78 \\ 8.07 \end{array}$	27 28
	29 30	$27.88 \\ 28.84$	$\begin{bmatrix} 7.99 \\ 8.27 \end{bmatrix}$	$\begin{bmatrix} 27.84 \\ 28.80 \end{bmatrix}$	$8.11 \\ 8.39$	$\begin{bmatrix} 27.81 \\ 28.76 \end{bmatrix}$	$\begin{array}{c c} 8.24 \\ 8.52 \end{array}$	$\begin{bmatrix} 27.77 \\ 28.73 \end{bmatrix}$	8.36 8.65	29 30
	31 32	$\frac{29.80}{30.76}$	$\begin{array}{c c} 8.54 \\ 8.82 \end{array}$	$\begin{vmatrix} 29.76 \\ 30.72 \end{vmatrix}$	8.67 8.95	$   \begin{array}{r}     29.72 \\     30.68   \end{array} $	8.80 9.09	$\begin{array}{ c c } \hline 29.68 \\ 30.64 \\ \hline \end{array}$	$\begin{array}{ c c }\hline 8.93\\ 9.22\\ \hline\end{array}$	$\frac{31}{32}$
ı	33 34	$\frac{31.72}{32.68}$	$\begin{array}{ c c } 9.10 \\ 9.37 \end{array}$	$\begin{vmatrix} 31.68 \\ 32.64 \end{vmatrix}$	$\begin{array}{c} 9.23 \\ 9.51 \end{array}$	$\begin{bmatrix} 31.64 \\ 32.60 \end{bmatrix}$	$\begin{array}{c c} 9.37 \\ 9.66 \end{array}$	$\begin{vmatrix} 31.60 \\ 32.56 \end{vmatrix}$	$9.51 \\ 9.80$	33 34
	35 36	$33.64 \\ 34.61$	$\begin{array}{c c} 9.65 \\ 9.92 \end{array}$	$\begin{array}{ c c c }\hline 33.60 \\ 34.56 \\ \hline \end{array}$	$oxed{0.79}{10.07}$	$\begin{bmatrix} 33.56 \\ 34.52 \end{bmatrix}$	$\begin{bmatrix} 9.94 \\ 10.22 \end{bmatrix}$	$33.51 \\ 34.47$	$10.09 \\ 10.38$	35 36
	37 38	$35.57 \\ 36.53$	$\begin{bmatrix} 10.20 \\ 10.47 \end{bmatrix}$	$\begin{vmatrix} 35.52 \\ 36.48 \end{vmatrix}$	$\begin{bmatrix} 10.35 \\ 10.63 \end{bmatrix}$	$\begin{vmatrix} 35.48 \\ 36.44 \end{vmatrix}$	$\begin{bmatrix} 10.51 \\ 10.79 \end{bmatrix}$	$\begin{vmatrix} 35.43 \\ 36.39 \end{vmatrix}$	$\begin{array}{c} 10.66 \\ 10.95 \end{array}$	37 38
10 10 to	$\begin{vmatrix} 39 \\ 40 \end{vmatrix}$	$\frac{37.49}{38.45}$	$\begin{bmatrix} 10.75 \\ 11.03 \end{bmatrix}$	$\frac{37.44}{38.40}$	$\begin{array}{c} 10.91 \\ 11.19 \end{array}$	$\begin{vmatrix} 37.39 \\ 38.35 \end{vmatrix}$	$\begin{array}{c} 11.08 \\ 11.36 \end{array}$	$\begin{bmatrix} 37.35 \\ 38.30 \end{bmatrix}$	$11.24 \\ 11.53$	39 40
-	41 42	$\frac{39.41}{40.37}$	$11.30 \\ 11.58$	$   \begin{array}{c c}     39.36 \\     40.32   \end{array} $	$\begin{array}{ c c c }\hline 11.47\\11.75\\ \end{array}$	$39.31 \\ 40.27$	$\begin{array}{c} \hline 11.64 \\ 11.93 \end{array}$	$\overline{39.26} \\ 40.22$	$11.82 \\ 12.10$	41 42
The same of	43 44	$\frac{41.33}{42.30}$	$11.85 \\ 12.13$	$ \begin{array}{c} 41.28 \\ 42.24 \end{array} $	$\begin{array}{c} 12.03 \\ 12.31 \end{array}$	$\begin{vmatrix} 41.23 \\ 42.19 \end{vmatrix}$	$\begin{bmatrix} 12.21 \\ 12.50 \end{bmatrix}$	41.18 42.13	12.39 12.68	43 44
	45 46	$\frac{43.26}{44.22}$	$\begin{array}{c c} 12.40 \\ 12.68 \end{array}$	$\begin{array}{ c c }\hline 43.20\\ 44.16\\ \hline\end{array}$	$\begin{array}{c} 12.59 \\ 12.87 \end{array}$	$43.15 \\ 44.11$	$\begin{array}{c} 12.78 \\ 13.06 \end{array}$	$\begin{vmatrix} 43.09 \\ 44.05 \end{vmatrix}$	12.97 $13.26$	45
	47 48	45.18 46.14	$\begin{bmatrix} 12.95 \\ 13.23 \end{bmatrix}$	$\begin{array}{ c c }\hline 45.12\\ 46.08\\ \hline\end{array}$	$\begin{array}{c c} 13.15 \\ 13.43 \end{array}$	$\begin{array}{c} 45.06 \\ 46.02 \end{array}$	$\begin{array}{ c c }\hline 13.35\\ 13.63\\ \hline\end{array}$	$45.01 \\ 45.96$	13.55 13.83	47 48
	49 50	$\frac{47.10}{48.06}$	$\begin{bmatrix} 13.51 \\ 13.78 \end{bmatrix}$	47.04   13.71		46.98  $ 47.94 $	$13.92 \\ 14.20$	$\frac{46.92}{47.88}$	$14.12 \\ 14.41$	49 50
	Distance.	Dep.	Lat.	Dep. Lat.		Dep.	Lat.	Dep.	Lat.	
	Dist	74]	Deg.	733	Deg.	731	Deg.	731	Deg.	Distance.
l				1						

	16.1	Deg.	161	Dog	161	Deg.	163	Dog	H
Distance.	101	Jeg.	104	Deg.	102	Deg.	104		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
51 52	$\frac{49.02}{49.99}$	$\begin{array}{ c c }\hline 14.06 \\ 14.33 \\ \hline \end{array}$	48.96  $ 49.92 $	$14.27 \\ 14.55$	48.90 49.86	$   \begin{array}{c c}     14.48 \\     14.77   \end{array} $	$\begin{vmatrix} 48.84 \\ 49.79 \end{vmatrix}$	$14.70 \\ 14.99$	51 52
53 54	$\begin{bmatrix} 50.95 \\ 51.91 \end{bmatrix}$	$\begin{array}{ c c }\hline 14.61\\ 14.88\\ \hline\end{array}$	$ 50.88  \\ 51.84 $	14.83   15.11	$ 50.82  \\ 51.78 $	$\begin{array}{c c} 15.05 \\ 15.34 \end{array}$	$\begin{bmatrix} 50.75 \\ 51.71 \end{bmatrix}$	15.27   15.56	53 54
55 56	$\begin{bmatrix} 52.87 \\ 53.83 \end{bmatrix}$	$\begin{array}{c c} 15.16 \\ 15.44 \end{array}$	$\begin{bmatrix} 52.80 \\ 53.76 \end{bmatrix}$	$15.39 \\ 15.67$	$\begin{bmatrix} 52.74 \\ 53.69 \end{bmatrix}$	$\begin{array}{c c} 15.62 \\ 15.90 \end{array}$	$\begin{bmatrix} 52.67 \\ 53.62 \end{bmatrix}$	$15.85 \\ 16.14$	55 56
57 58	$\begin{bmatrix} 54.79 \\ 55.75 \end{bmatrix}$	$15.71 \\ 15.99$	54.72 55.68	$15.95 \\ 16.23$	54.65 55.61	$\begin{array}{c c} 16.19 \\ 16.47 \end{array}$	54.58 55.54	$\begin{array}{c c} 16.43 \\ 16.72 \end{array}$	57 58
59 60	$\begin{bmatrix} 56.71 \\ 57.68 \end{bmatrix}$	$\begin{array}{c c} 16.26 \\ 16.54 \end{array}$	$\begin{bmatrix} 56.64 \\ 57.60 \end{bmatrix}$	$16.51 \\ 16.79$	$56.57 \\ 57.53$	$\begin{array}{c c} 16.76 \\ 17.04 \end{array}$	$\begin{array}{ c c } 56.50 \\ 57.45 \end{array}$	$\begin{array}{c c} 17.00 \\ 17.29 \end{array}$	59 60
$\frac{\overline{61}}{62}$	58.64 59.60	16.81 17.09	$58.56 \\ 59.52$	$\begin{array}{c} \overline{17.07} \\ 17.35 \end{array}$	58.49 59.45	$\begin{array}{c} \hline 17.32 \\ 17.61 \end{array}$	$\begin{array}{ c c } \hline 58.41 \\ 59.37 \\ \hline \end{array}$	$17.58 \\ 17.87$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$
63 64	$\begin{vmatrix} 60.56 \\ 61.52 \end{vmatrix}$	$17.37 \\ 17.64$	$60.48 \\ 61.44$	17.63 17.91	60.41	17.89 18.18	60.33	$\begin{array}{c c} 18.16 \\ 18.44 \end{array}$	63 64
65 66	$\begin{vmatrix} 62.48 \\ 63.44 \end{vmatrix}$	$17.92 \\ 18.19$	$\begin{array}{c c} 62.40 \\ 63.36 \end{array}$	$   \begin{array}{c c}     18.19 \\     18.47   \end{array} $	$62.32 \\ 63.28$	18.46 18.74	$\begin{vmatrix} 62.24 \\ 63.20 \end{vmatrix}$	$\begin{array}{c c} 18.73 \\ 19.02 \end{array}$	65 66
67 68	$\begin{vmatrix} 64.40 \\ 65.37 \end{vmatrix}$	18.47 18.74	$\begin{vmatrix} 64.32 \\ 65.28 \end{vmatrix}$	18.75 19.03	$\begin{vmatrix} 64.24 \\ 65.20 \end{vmatrix}$	19.03 19.31	$64.16 \\ 65.11$	$\begin{array}{c c} 19.31 \\ 19.60 \end{array}$	67 68
69 70	$\begin{bmatrix} 66.33 \\ 67.29 \end{bmatrix}$	$\begin{array}{c c} 19.02 \\ 19.29 \end{array}$	$66.24 \\ 67.20$	19.31 19.59	$\begin{vmatrix} 66.16 \\ 67.12 \end{vmatrix}$	$   \begin{array}{c c}     19.60 \\     19.88   \end{array} $	$66.07 \\ 67.03$	$   \begin{array}{c c}     19.89 \\     20.17   \end{array} $	69 70
$\frac{71}{72}$	$\begin{array}{ c c }\hline 68.25 \\ 69.21 \\\hline \end{array}$	19.57 19.85	$68.16 \\ 69.12$	$\frac{19.87}{20.15}$	68.08	$\frac{20.17}{20.45}$	$67.99 \\ 68.95$	20.46 $20.75$	$\begin{bmatrix} 71 \\ 72 \end{bmatrix}$
73 74	$\begin{vmatrix} 09.21 \\ 70.17 \\ 71.13 \end{vmatrix}$	20.12 20.40	$\begin{vmatrix} 09.12 \\ 70.08 \\ 71.04 \end{vmatrix}$	$\begin{bmatrix} 20.13 \\ 20.43 \\ 20.71 \end{bmatrix}$	$\begin{vmatrix} 69.03 \\ 69.99 \\ 70.95 \end{vmatrix}$	$\begin{bmatrix} 20.45 \\ 20.73 \\ 21.02 \end{bmatrix}$	69.90 70.86	$\begin{bmatrix} 21.04 \\ 21.33 \end{bmatrix}$	73 74
75 76	$72.09 \\ 73.06$	$\begin{bmatrix} 20.40 \\ 20.67 \\ 20.95 \end{bmatrix}$	$\begin{vmatrix} 72.04 \\ 72.00 \\ 72.96 \end{vmatrix}$	$\begin{bmatrix} 20.71 \\ 20.99 \\ 21.27 \end{bmatrix}$	71.91	$\begin{bmatrix} 21.02 \\ 21.30 \\ 21.59 \end{bmatrix}$	71.82 $72.78$	$\begin{bmatrix} 21.61 \\ 21.90 \end{bmatrix}$	75 76
77 78	$74.02 \\ 74.98$	$\begin{vmatrix} 20.93 \\ 21.22 \\ 21.50 \end{vmatrix}$	73.92 $74.88$	$\begin{bmatrix} 21.27 \\ 21.55 \\ 21.83 \end{bmatrix}$	$egin{array}{c} 72.87 \ 73.83 \ 74.79 \ \end{array}$	21.87 $22.15$	73.73 $74.69$	$\begin{bmatrix} 21.30 \\ 22.19 \\ 22.48 \end{bmatrix}$	77 78
79 80	75.94 76.90	$\begin{bmatrix} 21.78 \\ 21.78 \\ 22.05 \end{bmatrix}$	75.84 76.80	$\begin{bmatrix} 22.11 \\ 22.39 \end{bmatrix}$	75.75 76.71	22.13 $22.44$ $22.72$	75.65 76.61	$\begin{bmatrix} 22.77 \\ 23.06 \end{bmatrix}$	79 80
81	$\overline{77.86}$	22.33	77.76	$\overline{22.67}$	77.66	23.01	77.56	$\overline{23.34}$	81
82 83	78.82	$oxed{22.60}{22.88}$	78.72	22.95 $23.23$	78.62  $ 79.58 $	23.29 $23.57$	78.52	$\begin{vmatrix} 23.63 \\ 23.92 \end{vmatrix}$	82 83
84 85	80.75	23.15	80.64	$\begin{vmatrix} 23.51 \\ 23.79 \\ 0.77 \end{vmatrix}$	80.54	$\begin{vmatrix} 23.86 \\ 24.14 \end{vmatrix}$	80.44	$\begin{vmatrix} 24.21 \\ 24.50 \\ 24.70 \end{vmatrix}$	84 85
86 87	82.67	$\begin{vmatrix} 23.70 \\ 23.98 \\ 34.96 \end{vmatrix}$	$\begin{vmatrix} 82.56 \\ 83.52 \end{vmatrix}$	$\begin{vmatrix} 24.07 \\ 24.35 \end{vmatrix}$	82.46	$\begin{vmatrix} 24.43 \\ 24.71 \end{vmatrix}$	82.35	$\begin{vmatrix} 24.78 \\ 25.07 \\ 0.00 \end{vmatrix}$	86
88 89	84.59	$\begin{vmatrix} 24.26 \\ 24.53 \\ 94.91 \end{vmatrix}$	84.48	24.62	84.38	$\begin{vmatrix} 24.99 \\ 25.28 \\ 25.56 \end{vmatrix}$	84.27	25.36 25.65	88 89
$\begin{array}{ c c }\hline 90\\\hline 91\\ \end{array}$	$\frac{86.51}{87.47}$	$\begin{array}{ c c }\hline 24.81 \\ \hline 25.08 \\ \hline \end{array}$	$\frac{86.40}{87.36}$	$\frac{25.18}{25.46}$	$86.29 \over 87.25$	$\begin{array}{ c c }\hline 25.56 \\ \hline 25.85 \\ \hline \end{array}$	86.18 $87.14$	$\frac{25.94}{26.23}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$
92 93	88.44	$\begin{bmatrix} 25.36 \\ 25.63 \end{bmatrix}$	88.32 89.28	$\begin{bmatrix} 25.74 \\ 26.02 \end{bmatrix}$	$ 88.21 \\ 89.17$	$\begin{vmatrix} 26.13 \\ 26.41 \end{vmatrix}$	88.10	$\begin{vmatrix} 26.51 \\ 26.80 \end{vmatrix}$	92 93
94 95	$  90.36 \\ 91.32  $	$\begin{bmatrix} 25.91 \\ 26.19 \end{bmatrix}$	$90.24 \\ 91.20$	$\begin{vmatrix} 26.30 \\ 26.58 \end{vmatrix}$	90.13  $  91.09 $	$\begin{vmatrix} 26.70 \\ 26.98 \end{vmatrix}$	$\begin{vmatrix} 90.01 \\ 90.97 \end{vmatrix}$	$\begin{vmatrix} 27.09 \\ 27.38 \end{vmatrix}$	94 95
96 97	$\begin{vmatrix} 92.28 \\ 93.24 \end{vmatrix}$	$\begin{bmatrix} 26.46 \\ 26.74 \end{bmatrix}$	$92.16 \\ 93.12$	$\begin{vmatrix} 26.86 \\ 27.14 \end{vmatrix}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	27.27 27.55	$91.93 \\ 92.88$	$\begin{vmatrix} 27.67 \\ 27.95 \end{vmatrix}$	96 97
98 99	$  94.20 \\ 95.16  $	$\begin{vmatrix} 27.01 \\ 27.29 \end{vmatrix}$	94.08 95.04	$\begin{vmatrix} 27.42 \\ 27.70 \end{vmatrix}$	$93.96 \\ 94.92$	27.83 28.12	93.84  $  94.80 $	28.24 28.53	98 99
100	$\frac{96.13}{}$	$\boxed{\frac{27.56}{}}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$		95.88	28.40	95.76	28.82	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
Dist	74]	74 Deg. 73¾ Deg.		Deg.	73½ Deg.		73½ Deg.		Dist
_	1	734 Deg.			II.		1		1

Dista	17	Deg.	174	Deg.	171	Deg.	173	Deg.	Dist
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance
1 2 3 4 5 6 7 8 9	0.96 1.91 2.87 3.83 4.78 5.74 6.69 7.65 8.61 9.56	0.58 0.88 1.17 1.46 1.75 2.05 2.34 2.63	$\begin{array}{ c c c c }\hline 0.95 \\ 1.91 \\ 2.87 \\ 3.82 \\ 4.78 \\ 5.73 \\ 6.69 \\ 7.64 \\ 8.60 \\ 9.55 \\ \end{array}$	0.30 0.59 0.89 1.19 1.48 1.78 2.08 2.37 2.67 2.97	0.95 1.91 2.86 3.81 4.77 5.72 6.68 7.63 8.58	0.30 0.60 0.90 1.20 1.50 1.80 2.10 2.41 2.71	0.95 1.90 2.86 3.81 4.76 5.71 6.67 7.62 8.57	$\begin{array}{c} 0.30 \\ 0.61 \\ 0.91 \\ 1.22 \\ 1.52 \\ 1.83 \\ 2.13 \\ 2.44 \\ 2.74 \\ 3.05 \end{array}$	1 2 3 4 5 6 7 8
10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 27 28 29 30 31 32 33 34 35 36 37 38 39	9.56 10.52 11.48 12.43 13.39 14.34 15.30 16.26 17.21 18.17 19.13 20.08 21.04 21.99 22.95 23.91 24.86 25.82 26.78 27.73 28.69 29.65 30.60 31.56 32.51 33.47 34.43 35.38 36.34 37.30	2.92 3.22 3.51 3.80 4.09 4.39 4.68 4.97 5.26 5.56 5.85 6.14 6.43 6.72 7.02 7.31 7.60 7.89 8.19 8.48 8.77 9.06 9.36 9.36 9.94 10.23 10.53 10.82 11.11 11.40	9.55 10.51 11.46 12.42 13.37 14.33 15.28 16.24 17.19 18.15 19.10 20.06 21.01 21.97 22.92 23.88 24.83 25.79 26.74 27.70 28.65 29.61 30.56 31.52 32.47 33.43 34.38 35.34 36.29 37.25	2.97 3.26 3.56 3.85 4.15 4.45 4.74 5.04 5.34 5.63 6.52 6.52 6.52 7.41 7.71 8.01 8.30 8.60 8.90 9.19 9.49 9.79 10.08 10.38 10.68 10.97 11.27 11.57	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{ c c c c c }\hline 3.01\\\hline 3.31\\\hline 3.61\\\hline 3.91\\\hline 4.21\\\hline 4.51\\\hline 4.81\\\hline 5.11\\\hline 5.41\\\hline 5.71\\\hline 6.01\\\hline 6.31\\\hline 6.62\\\hline 6.92\\\hline 7.22\\\hline 7.52\\\hline 7.82\\\hline 8.42\\\hline 8.42\\\hline 8.72\\\hline 9.02\\\hline 9.32\\\hline 9.92\\\hline 10.22\\\hline 10.52\\\hline 10.83\\\hline 11.13\\\hline 11.43\\\hline \end{array}$	$\begin{array}{ c c c c c }\hline 9.52\\\hline 10.48\\\hline 11.43\\\hline 12.38\\\hline 13.33\\\hline 14.29\\\hline 15.24\\\hline 16.19\\\hline 17.14\\\hline 18.10\\\hline 19.05\\\hline 20.00\\\hline 20.95\\\hline 21.91\\\hline 22.86\\\hline 23.81\\\hline 24.76\\\hline 25.71\\\hline 26.67\\\hline 27.62\\\hline 28.57\\\hline 29.52\\\hline 30.48\\\hline 31.43\\\hline 32.38\\\hline 34.29\\\hline 35.24\\\hline 36.19\\\hline \end{array}$	$\begin{array}{ c c c c c }\hline 3.05\\\hline 3.35\\\hline 3.66\\\hline 3.96\\\hline 4.27\\\hline 4.57\\\hline 4.57\\\hline 4.88\\\hline 5.18\\\hline 5.49\\\hline 5.79\\\hline 6.10\\\hline 6.40\\\hline 6.71\\\hline 7.01\\\hline 7.32\\\hline 7.62\\\hline 7.93\\\hline 8.23\\\hline 8.54\\\hline 8.84\\\hline 9.15\\\hline 9.45\\\hline 9.76\\\hline 10.06\\\hline 10.37\\\hline 10.67\\\hline 10.98\\\hline 11.28\\\hline 11.58\\\hline \end{array}$	10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38
40 41 42 43 44 45 46 47 48 49 50	38.25 39.21 40.16 41.12 42.08 43.03 43.99 44.95 45.90 46.86 47.82	11.63 11.99 12.28 12.57 12.86 13.16 13.45 13.74 14.63 14.63	$     \begin{array}{r}       38.20 \\       \hline       39.16 \\       40.11 \\       41.07 \\       42.02 \\       42.98 \\       43.93 \\       44.89 \\       45.84 \\       46.80 \\       47.75     \end{array} $	11.86 12.16 12.45 12.75 13.05 13.34 13.64 13.94 14.23 14.53 14.83	$     \begin{array}{r}       37.19 \\       38.15 \\       \hline       39.10 \\       40.06 \\       41.01 \\       41.96 \\       42.92 \\       43.87 \\       44.82 \\       45.78 \\       46.73 \\       47.69 \\     \end{array} $	11.73 12.03 12.33 12.63 12.93 13.23 13.53 13.83 14.13 14.43 14.73 15.04	$   \begin{vmatrix}     37.14 \\     38.10   \end{vmatrix}   \begin{vmatrix}     39.05 \\     40.00 \\     40.95 \\     41.91 \\     42.86 \\     43.81 \\     44.76 \\     45.71 \\     46.67 \\     47.62   \end{vmatrix} $	11.89 12.19 12.50 12.80 13.11 13.41 13.72 14.02 14.33 14.63 14.94 15.24	39 40 41 42 43 44 45 46 47 48 49 50
Distance.	73 I	Lat.	Dep.   72¾ I	Lat. Deg.	Dep. 721	Lat. Deg.	Dep.   721	Lat. Deg.	Distance.

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Dista	17 I	eg.	174	Deg.	171/2	Deg.	173	Deg.	Dista
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce
istance   152345567890   6634656787777777789   823456788885678	Lat.  48.77 49.73 50.68 51.64 52.60 53.55 54.51 55.47 56.42 57.38  58.33 59.29 60.25 61.20 62.16 63.12 64.07 65.03 65.99 66.94  67.90 68.85 69.81 70.77 71.72 72.68 73.64 74.59 75.55 76.50  77.46 78.42 79.37 80.33 81.29 82.24 83.20 84.15	Dep.  14.91 15.20 15.50 15.79 16.08 16.37 16.67 16.96 17.25 17.54 17.83 18.42 18.71 19.00 19.30 19.59 19.88 20.17 20.47 20.76 21.05 21.34 21.64 21.93 22.22 22.51 22.80 23.10 23.39 23.68 23.97 24.27 24.56 24.85 25.14 25.44 25.73	Lat.  48.71 49.66 50.62 51.57 52.53 53.48 54.44 55.39 56.35 57.30  58.26 59.21 60.17 61.12 62.08 63.03 63.99 64.94 65.90 66.85 67.81 68.76 69.72 70.67 71.63 72.58 73.54 74.49 75.45 76.40  77.36 78.31 79.27 80.22 81.18 82.13 83.09 84.04	Dep.  15.12 15.42 15.42 15.72 16.01 16.31 16.61 16.90 17.20 17.50 17.79 18.09 18.39 18.68 19.28 19.28 19.57 19.87 20.46 20.76 21.05 21.05 21.65 21.94 22.24 22.54 22.54 22.24 22.54 22.54 22.24 22.54	Lat.  48.64 49.59 50.55 51.50 52.45 53.41 54.36 55.32 56.27 57.22  58.18 59.13 60.08 61.04 61.99 62.95 63.90 64.85 65.81 66.76 67.71 68.67 69.62 70.58 71.53 72.48 73.44 74.39 75.34 76.30  77.25 78.20 79.16 80.11 81.07 82.02 82.97 83.93	Dep.  15.34 15.64 15.94 16.24 16.54 17.14 17.74 18.04  18.34 18.64 19.25 19.55 19.55 20.15 20.45 20.75 21.05  21.35 21.65 21.95 22.25 22.55 23.15 23.46 24.66 25.96 25.86 26.16 26.46	Lat.    48.57   49.52   50.48   51.43   52.38   53.33   54.29   55.24   56.10   57.14   58.10   59.05   60.95   61.91   62.86   63.81   64.76   65.72   66.67   67.62   68.57   69.52   70.48   71.43   72.38   73.33   74.29   75.24   76.19   77.14   78.10   79.05   80.00   80.95   81.91   82.86   83.81	Dep.  15.55 16.16 16.46 16.77 17.07 17.38 17.68 17.99 18.29 18.60 18.90 19.21 19.51 19.82 20.12 20.43 20.73 21.04 21.34 21.65 22.26 22.86 23.17 23.47 23.78 24.08 24.69 25.00 25.61 26.52 26.52 26.83	istance   512   523   544   555   567   589   6162   636   646   657   667   688   657   677   789   812   824   824   825   826   827   828   8
88 89	85.11	26.02	85.00	26.39	84.88	26.76 26.76 27.06	84.76	$\begin{vmatrix} 26.83 \\ 27.13 \\ 27.44 \end{vmatrix}$	889 89 90
90 91 92 93 94 95 96 97 98 99 100	$\begin{array}{ c c c c c }\hline 86.07\\\hline 87.02\\ 87.98\\ 87.98\\ 89.89\\ 90.85\\ 91.81\\ 92.76\\ 93.72\\ 94.67\\ 95.63\\\hline \end{array}$	26.31 26.61 26.90 27.19 27.48 27.78 28.07 28.36 28.65 28.94 29.24	85.95 86.91 87.86 88.82 89.77 90.73 91.68 92.64 93.59 94.55 95.50	$\begin{array}{r} 26.69 \\ \hline 26.99 \\ 27.28 \\ 27.58 \\ 27.87 \\ 28.17 \\ 28.47 \\ 28.76 \\ 29.06 \\ 29.65 \\ \hline \end{array}$	$ \begin{vmatrix} 85.83 \\ 86.79 \\ 87.74 \\ 88.70 \\ 89.65 \\ 90.60 \\ 91.56 \\ 92.51 \\ 93.46 \\ 94.42 \\ 95.37 \\ \end{vmatrix} $	27.36 27.66 27.97 28.27 28.57 28.87 29.17 29.47 29.77 30.07	85.72 86.67 87.62 88.57 89.53 90.48 91.43 92.38 93.33 94.29 95.24	27.74 28.05 28.35 28.66 28.96 29.27 29.57 29.88 30.18 30.49	91 92 93 94 95 96 97 98 99
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
Dist	73	Deg.	723	Deg.	$72\frac{1}{2}$	Deg.	721	Deg.	Dist

Dist	18	Deg.	184	Deg.	18½	Deg.	183	Deg.	Dist
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
1 2 3 4 5 6 7 8 9 10	0.95 1.90 2.85 3.80 4.76 5.71 6.66 7.61 8.56 9.51	$\begin{array}{c} \hline 0.31 \\ 0.62 \\ 0.93 \\ 1.24 \\ 1.55 \\ 1.85 \\ 2.16 \\ 2.47 \\ 2.78 \\ 3.09 \\ \end{array}$	0.95 1.90 2.85 3.80 4.75 5.70 6.65 7.60 8.55 9.50		$\begin{array}{ c c c c }\hline 0.95 \\ 1.90 \\ 2.84 \\ 3.79 \\ 4.74 \\ 5.69 \\ 6.64 \\ 7.59 \\ 8.53 \\ 9.48 \\ \end{array}$	0.32 0.63 0.95 1.27 1.59 1.90 2.22 2.54 2.86 3.17	0.95 1.89 2.84 3.79 4.73 5.68 6.63 7.58 8.52 9.47	0.32 0.64 0.96 1.29 1.61 1.93 2.25 2.57 2.89 3.21	1 2 3 4 5 6 7 8 9
11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	10.46 11.41 12.36 13.31 14.27 15.22 16.17 17.12 18.07 19.02 19.97 20.92 21.87 22.83 23.78 24.73 25.68 26.63 27.58 28.53	3.40 3.71 4.02 4.33 4.64 4.94 5.25 5.56 5.87 6.18 6.49 6.80 7.11 7.42 7.73 8.03 8.34 8.65 8.96 9.27	10.45 11.40 12.35 13.30 14.25 15.00 16.14 17.09 18.04 18.99 19.94 20.89 21.84 22.79 23.74 24.69 25.64 26.59 27.54 28.49	3.44 3.76 4.07 4.38 4.70 5.01 5.32 5.64 5.95 6.26 6.58 6.89 7.20 7.52 7.83 8.14 8.46 8.77 9.08 9.39	10.43 11.38 12.33 13.28 14.22 15.17 16.12 17.07 18.02 18.97 19.91 20.86 21.81 22.76 23.71 24.66 25.60 26.55 27.50 28.45	3.49 3.81 4.12 4.44 4.76 5.03 5.39 5.71 6.03 6.35 6.66 6.98 7.30 7.62 7.93 8.25 8.57 8.88 9.20 9.52	10.42 11.36 12.31 13.26 14.20 15.15 16.10 17.04 17.99 18.94 19.89 20.83 21.78 22.73 23.67 24.62 25.57 26.51 27.46 28.41	3.54 3.86 4.18 4.50 4.82 5.14 5.46 5.79 6.11 6.43 6.75 7.07 7.39 7.71 8.04 8.36 8.68 9.00 9.32 9.64	11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 29 30
31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50	29.48 30.43 31.38 32.34 33.29 34.24 35.19 36.14 37.09 38.99 39.94 40.90 41.85 42.80 43.75 44.70 45.65 46.60 47.55	9.58 9.89 10.20 10.51 10.82 11.12 11.43 11.74 12.05 12.67 12.98 13.29 13.60 13.91 14.21 14.52 14.83 15.14 15.45	29.44 30.39 31.34 32.29 33.24 34.19 35.14 36.09 37.04 37.99 38.94 39.89 40.84 41.79 42.74 43.69 44.64 45.59 46.54 47.48	9.71 10.02 10.33 10.65 10.96 11.27 11.59 11.90 12.21 12.53 12.84 13.15 13.47 13.78 14.09 14.41 14.72 15.03 15.35 15.66	29.40 30.35 31.29 32.24 33.19 34.14 35.09 36.04 36.98 37.93 38.88 39.83 40.78 41.73 42.67 43.62 44.57 45.52 46.47 47.42	9.84 10.15 10.47 10.79 11.11 11.42 11.74 12.06 12.37 12.69 13.01 13.33 13.64 13.96 14.28 14.60 14.91 15.23 15.55 15.87	29.35 30.30 31.25 32.20 33.14 34.09 35.04 35.98 36.93 37.88 38.82 39.77 40.72 41.66 42.61 43.56 44.51 45.45 46.40 47.35	9.96 10.29 10.61 10.93 11.25 11.57 11.89 12.21 12.54 12.86 13.18 13.50 13.82 14.14 14.46 14.79 15.11 15.43 15.75 16.07	31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50
Distance.	Dep.         Lat.         Dep.         Lat.           72 Deg.         71\frac{3}{4} Deg.		Lat.	71½	Lat. Deg.	71½	Lat. Deg.	Distance.	

D	18	Deg.	181	Deg.	18	Deg.	183	Deg.	D
Distance.									Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51 52	18.50 49.45	15.76 16.07	$ \begin{array}{c} 48.43 \\ 49.38 \end{array} $	15.97 16.28	48.36  49.31	16.18 16.50	48.29	$\begin{vmatrix} 16.39 \\ 16.71 \end{vmatrix}$	51 52
53	50.41	16.38	50.33	16.60	50.26	16.82	50.19	17.04	53
54 55	$\begin{vmatrix} 51.36 \\ 52.31 \end{vmatrix}$	16.69 $  17.00$	51.28 $52.23$	16.91 $17.22$	$\begin{vmatrix} 51.21 \\ 52.16 \end{vmatrix}$	17.13 17.45	$\begin{vmatrix} 51.13 \\ 52.08 \end{vmatrix}$	17.36 $  17.68$	54 55
56 57	53.26 $54.21$	$  17.30 \\ 17.61  $	$53.18 \\ 54.13$	17.54 17.85	53.11 54.05	17.77	53.03	$\begin{vmatrix} 18.00 \\ 18.32 \end{vmatrix}$	56 57
58	55.16	17.92	55.08	18.16	55.00	18.40	54.92	18.64	58
59 60	56.11 57.06	18.23 18.54	56.03 $56.98$	$\begin{vmatrix} 18.48 \\ 18.79 \end{vmatrix}$	55.95	$18.72 \\ 19.04$	55.87 56.82	18.96 $  19.29$	59 60
61	58.01	18 85	57.93	19.10	57.85	19.36	57.76	19.61	61
62 63	$\begin{bmatrix} 58.97 \\ 59.92 \end{bmatrix}$	$\begin{vmatrix} 19.16 \\ 19.47 \end{vmatrix}$	58.88 59.83	$ \begin{array}{c c} 19.42 \\ 19.73 \end{array} $	58.80	$  19.67 \\   19.99  $	58.71 59.66	$19.93 \\ 20.25$	62 63
64	60.87	19.78	60.78	20.04	60.69	20.31	60.60	20.57	64
65 66	$\begin{vmatrix} 61.82 \\ 62.77 \end{vmatrix}$	$\begin{vmatrix} 20.09 \\ 20.40 \end{vmatrix}$	62.68	$\begin{vmatrix} 20.36 \\ 20.67 \end{vmatrix}$	$\begin{vmatrix} 61.64 \\ 62.59 \end{vmatrix}$	$\begin{bmatrix} 20.62 \\ 20.94 \end{bmatrix}$	$\begin{vmatrix} 61.55 \\ 62.50 \end{vmatrix}$	20.89 $21.22$	65 66
67	$\begin{vmatrix} 63.72 \\ 64.67 \end{vmatrix}$	$20.70 \\ 21.01$	$\begin{bmatrix} 63.63 \\ 64.58 \end{bmatrix}$	20.98 $21.30$	$\begin{vmatrix} 63.54 \\ 64.49 \end{vmatrix}$	$\begin{vmatrix} 21.26 \\ 21.58 \end{vmatrix}$	$63.44 \\ 64.39$	$\begin{vmatrix} 21.54 \\ 21.86 \end{vmatrix}$	67 68
69	65.62	21.32	65.53	21.61	65.43	21.89	65.34	22.18	69
$\frac{70}{71}$	$\frac{66.57}{67.53}$	$\frac{21.63}{21.94}$	$\frac{66.48}{67.43}$	$\frac{21.92}{22.23}$	$\frac{66.38}{67.33}$	$\frac{22.21}{22.53}$	$\frac{66.29}{67.23}$	$\frac{22.50}{22.82}$	$\left  \frac{70}{71} \right $
72	68.48	22.25	68.38	22.55	68.28	22.85	68.18	23.14	72
73 74	69.43	$\begin{vmatrix} 22.56 \\ 22.87 \end{vmatrix}$	$69.33 \\ 70.28$	$\begin{vmatrix} 22.86 \\ 23.17 \end{vmatrix}$	69.23	$\begin{bmatrix} 23.16 \\ 23.48 \end{bmatrix}$	69.13 $70.07$	$\begin{vmatrix} 23.47 \\ 23.79 \end{vmatrix}$	73 74
75	71.33	23.18	71.23	23.49	71.12	23.80	71.02	24.11	75
76	$\begin{vmatrix} 72.28 \\ 73.23 \end{vmatrix}$	$\left  egin{array}{c} 23.49 \ 23.79 \ \end{array} \right $	72.18 $73.13$	$\begin{vmatrix} 23.80 \\ 24.11 \end{vmatrix}$	$ \begin{array}{c} 72.07 \\ 73.02 \end{array} $	$\begin{vmatrix} 24.12 \\ 24.43 \end{vmatrix}$	$ 71.97 \\ 72.91$	$\begin{vmatrix} 24.43 \\ 24.75 \end{vmatrix}$	76 77
78 79	74.18 75.13	24:10	$ 74.08  \\ 75.03 $	24.43	$\begin{vmatrix} 73.97 \\ 74.92 \end{vmatrix}$	$24.75 \\ 25.07$	73.86 74.81	25.07	78 79
80	76.08	$\begin{bmatrix} 24.41 \\ 24.72 \end{bmatrix}$	75.98	$\begin{bmatrix} 24.74 \\ 25.05 \end{bmatrix}$	75.87	25.38	75.75	25.39 $25.72$	80
81	77.04	25.03	76.93	25.37	76.81 $77.76$	$\begin{bmatrix} 25.70 \\ 26.02 \end{bmatrix}$	76.70	26.04	81
82 83	77.99	25.34 25.65	77.88	$oxed{25.68} \ oxed{25.99}$	78.71	26.34	77.65	26.36 26.68	82 83
84 85	79.89	$\begin{bmatrix} 25.96 \\ 26.27 \end{bmatrix}$	$ 79.77  \\ 80.72$	$\begin{vmatrix} 26.31 \\ 26.62 \end{vmatrix}$	79.66	$\begin{bmatrix} 26.65 \\ 26.97 \end{bmatrix}$	79.54	$27.00 \\ 27.32$	84 85
86	81.79	26.58	81.67	26.93	81.56	27.29	81.44	27.64	86
87	82.74	$egin{array}{c} 26.88 \ 27.19 \ \hline \end{array}$	$\begin{vmatrix} 82.62 \\ 83.57 \end{vmatrix}$	$\begin{bmatrix} 27.25 \\ 27.56 \end{bmatrix}$	$\begin{vmatrix} 82.50 \\ 83.45 \end{vmatrix}$	$egin{array}{c c} 27.61 \ 27.92 \ \hline \end{array}$	$\begin{vmatrix} 82.38 \\ 83.33 \end{vmatrix}$	$27.97 \\ 28.29$	87 88
89	84.64	27.50	84.52	27.87	84.40	28.24	84.28	28.61	89
$\frac{90}{91}$	$\frac{85.60}{86.55}$	$\left \frac{27.81}{28.12}\right $	$\frac{85.47}{86.42}$	$\frac{28.18}{28.50}$	$\begin{array}{ c c }\hline 85.35\\\hline 86.30\\\hline \end{array}$	$\frac{28.56}{28.37}$	$\frac{85.22}{86.17}$	$\frac{28.93}{29.25}$	$\frac{90}{91}$
92	87.50	28.43	87.37	28.81	87.25	29.19	87.12	29.57	92
93 94	88.45	$\begin{bmatrix} 28.74 \\ 29.05 \end{bmatrix}$	$ 88.32  \\ 89.27 $	$\begin{bmatrix} 29.12 \\ 29.44 \end{bmatrix}$	88.19	$\begin{bmatrix} 29.51 \\ 29.83 \end{bmatrix}$	$\begin{array}{ c c } 88.06 \\ 89.01 \end{array}$	$\begin{array}{c} 29.89 \\ 30.22 \end{array}$	93 94
95	90.35	29.36	90.22	29.75	90.09	30.14	89.96	30.54	95
96 97	91.30  92.25	$\begin{bmatrix} 29.67 \\ 29.97 \end{bmatrix}$	$  \begin{array}{c} 91.17 \\ 92.12 \end{array}  $	$\frac{30.06}{30.38}$	$\begin{vmatrix} 91.04 \\ 91.99 \end{vmatrix}$	$\frac{30.46}{30.78}$	$  90.91 \\ 91.85  $	$30.86 \\ 31.18$	$\begin{array}{c} 96 \\ 97 \end{array}$
98	93.20	$\frac{30.28}{30.59}$	93.07	$\frac{30.69}{31.00}$	92.94 93.88	$\frac{31.10}{31.41}$	92.80  $ 93.75 $	$\frac{31.50}{31.82}$	98 99
99	$94.15 \\ 95.11$	30.99	$\begin{bmatrix} 94.02 \\ 94.97 \end{bmatrix}$	31.32	94.83	$\frac{31.41}{31.73}$	94.69	$\frac{31.62}{32.14}$	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	ance,
Dist	72 I	eg.	713	Deg.	$71\frac{1}{2}$	Deg.	714	Deg.	Distance
		0*							

Distance	. 19	Deg.	194	Deg.	191	Deg.	193	Deg.	Dis
ancė.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	tance
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 6 27 28 29 30 31 32 33 4 35 6 37 38 39 40 41 42 43 44 45 46 47	$ \begin{array}{ c c } \hline 0.95 \\ 1.89 \\ 2.84 \end{array} $	Dep.  0.33 0.65 0.98 1.30 1.63 1.95 2.28 2.60 2.93 3.26 3.58 3.91 4.23 4.56 4.88 5.21 5.53 5.86 6.19 6.51 6.84 7.16 7.49 7.81 8.14 8.46 8.79 9.12 9.44 9.77 10.09 10.42 10.74 11.07 11.39 11.72 12.05 12.37 12.70 13.35 13.67 14.00 14.32 14.65 14.98 15.30	Lat.  0.94 1.89 2.83 3.78 4.72 5.66 6.61 7.55 8.50 9.44 10.38 11.33 12.27 13.22 14.16 15.11 16.05 16.99 17.94 18.88 19.83 20.77 21.71 22.66 23.60 24.55 25.49 26.43 27.38 28.32 29.27 30.21 31.15 32.10 33.04 33.99 34.93 35.88 36.82 37.76 38.71 39.65 40.60 41.54 42.48 43.43 44.37	Dep.    0.33     0.66     0.99     1.32     1.65     1.98     2.31     2.64     2.97     3.30     3.63     3.96     4.29     4.62     4.95     5.28     5.60     5.93     6.26     6.59     6.92     7.25     7.58     7.91     8.24     8.57     8.90     9.23     9.56     9.89     10.22     10.55     10.88     11.21     11.54     11.87     12.20     13.52     13.52     14.81     14.51     14.84     15.17     15.50	Lat.  0.94 1.89 2.83 3.77 4.71 5.66 6.60 7.54 8.48 9.43 10.37 11.31 12.25 13.20 14.14 15.08 16.02 16.97 17.91 18.85 19.80 20.74 21.68 22.62 23.57 24.51 25.45 26.39 27.34 28.28 29.22 30.16 31.11 32.05 32.99 33.94 34.88 35.82 36.76 37.71 38.65 39.59 40.53 41.48 42.42 43.36 44.30	Dep.  0.33 0.67 1.00 1.34 1.67 2.00 2.34 2.67 3.00 3.34 3.67 4.01 4.34 4.67 5.01 5.34 5.67 6.01 6.34 6.68 7.01 7.34 7.68 8.01 8.35 8.68 9.01 9.35 9.68 10.01 10.35 11.68 11.02 11.35 11.68 12.02 12.35 12.68 13.69 14.02 14.35 13.69 15.02 15.36 15.69	Lat.  0.94 1.88 2.82 3.76 4.71 5.65 6.59 7.53 8.47 9.41 10.35 11.29 12.24 13.18 14.12 15.06 16.00 16.94 17.88 18.82 19.76 20.71 21.65 22.59 23.53 24.47 25.41 26.35 27.29 28.24 29.18 30.12 31.06 32.00 32.94 33.88 34.82 35.76 36.71 37.65 38.59 39.53 40.47 41.41 42.35 43.29 44.24	Dep.   0.34   0.68   1.01   1.35   1.69   2.03   2.37   2.70   3.04   3.38   3.72   4.06   4.39   4.73   5.07   5.41   5.74   6.08   6.42   6.76   7.10   7.43   7.77   8.11   8.45   8.79   9.12   9.46   9.80   10.14   10.48   11.15   11.49   11.83   12.17   12.50   12.84   13.18   13.52   13.85   14.19   14.53   14.53   14.53   14.53   14.53   15.54   15.54   15.58   15.54   15.88   15.54   15.88   15.54   15.88   15.54   15.55   15	Distance. 12345678910 11121314 15617 1890 21 22 23 24 25 26 27 8 29 30 31 32 33 34 35 6 37 38 39 40 41 24 34 44 45 46 47
48 49 50	$\begin{array}{c} 45.38 \\ 46.33 \\ 47.28 \end{array}$	$\begin{array}{c} 15.63 \\ 15.95 \\ 16.28 \end{array}$	$\begin{array}{c} 45.32 \\ 46.26 \\ 47.20 \end{array}$	15.83 16.15 16.48	45.25 46.19 47.13	16.02 16.36 16.69	$\begin{array}{c c} 45.18 \\ 46.12 \\ 47.06 \end{array}$	$   \begin{array}{c c}     16.22 \\     16.56 \\     16.90   \end{array} $	48 49 50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
Dist	71 I	eg.	$70\frac{3}{4}$ ]	Deg.	70 <u>‡</u> I	Deg.	701 ]	Deg.	Distance.

1			1		1				
Distance.	19 1	Deg.	191	Deg.	19½	Deg.	193	Deg.	Dista
nce.	· Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
51 52 53 54 55 56 57 58 60 61 62 63 64 65 66 67 68 70 71 72 73 74 75 77 77 77 77 77 77 77 77 77 77 77 77	48.22       49.17       50.11       51.06       52.00       52.95       53.89       54.84       55.79       56.73       57.68       58.62       59.57       60.51       61.46       62.40       63.35       64.30       65.24       66.19       67.13       68.08       69.97       70.91       71.86       72.80       73.75       74.70       75.64       76.59       77.53       78.48       79.42       80.37       81.31       82.26       83.21       84.15       85.10	16.60 16.93 17.26 17.58 17.91 18.23 18.56 18.88 19.21 19.53 19.86 20.19 20.51 20.84 21.16 21.49 21.81 22.14 22.46 22.79 23.12 23.44 23.77 24.09 24.42 24.74 25.07 26.05 26.05 27.02 27.35 28.65 28.98 29.30	48.15         49.09         50.04         50.98         51.92         52.87         53.81         54.76         55.70         56.65         57.59         58.53         59.48         60.42         61.37         62.31         63.25         64.20         65.14         66.09         67.03         67.97         68.92         69.86         70.81         71.75         72.69         73.64         74.58         75.53         76.47         77.42         78.36         79.30         80.25         81.19         82.14         83.08         84.97	16.81 17.14 17.47 17.80 18.13 18.46 18.79 19.12 19.45 19.78 20.11 20.44 20.77 21.10 21.43 21.76 22.09 22.42 22.75 23.08 23.41 23.74 24.07 24.40 24.73 25.06 25.39 25.72 26.05 26.38 27.69 28.67 29.67	48.07         49.96         50.90         51.85         52.79         53.73         54.67         55.62         56.56         57.50         58.44         59.39         60.33         61.27         62.21         63.16         64.10         65.04         65.98         66.93         67.87         68.81         69.76         70.70         71.64         72.58         73.53         74.47         75.41         76.35         77.30         78.24         79.18         80.12         83.90         84.84	17.02 17.36 17.69 18.03 18.36 18.69 19.03 19.36 19.69 20.03 20.36 20.70 21.03 21.36 21.70 22.03 22.37 22.70 23.03 24.03 24.70 24.03 24.70 25.04 25.37 26.70 27.04 27.37 27.71 28.04 29.37 29.71 30.04	48.00         48.94         49.88         50.82         51.76         52.71         53.65         54.59         55.53         56.47         57.41         58.35         59.29         60.24         61.18         62.12         63.06         64.00         64.94         65.82         67.76         68.71         69.65         70.59         71.53         72.47         73.41         74.35         75.29         76.24         77.18         78.12         79.06         80.00         81.88         82.82         83.76         84.71	17.23 17.57 17.91 18.25 18.59 18.92 19.26 19.60 19.94 20.27 20.61 20.95 21.29 21.63 21.96 22.30 22.64 22.98 23.32 23.65 23.99 24.33 24.67 25.01 25.34 25.68 26.70 27.71 28.05 29.40 29.74 30.07 30.41	Distance.   5123 545 556 78 96   612 66 66 67   712 73 74 75 66 77 78 90   82 88 88 89 90   612 612 612 612 612 612 612 612 612 612
91 92 93 94	86.04 86.99 87.93 88.88	$ \begin{array}{c c} 29.63 \\ 29.95 \\ 30.28 \\ 30.60 \end{array} $	85.91 86.86 87.80 88.74	30.00 30.33 30.66 30.99	85.78 86.72 87.67 88.61	$\begin{vmatrix} 30.38 \\ 30.71 \\ 31.04 \\ 31.38 \end{vmatrix}$	85.65 86.59 87.53 88.47	$\begin{vmatrix} 30.75 \\ 31.09 \\ 31.43 \\ 31.76 \end{vmatrix}$	91 92 93 94
95 96	$\begin{vmatrix} 89.82 \\ 90.77 \end{vmatrix}$	$\begin{vmatrix} 30.93 \\ 31.25 \end{vmatrix}$	89.69 90.63	$\frac{31.32}{31.65}$	89.55	$\frac{31.71}{32.05}$	89.41 90.35	$\begin{vmatrix} 32.10 \\ 32.44 \end{vmatrix}$	95 96
97 98 99 100	$egin{array}{c} 91.72 \\ 92.66 \\ 93.61 \\ 94.55 \\ \hline \end{array}$	$\begin{vmatrix} 31.58 \\ 31.91 \\ 32.23 \\ 32.56 \end{vmatrix}$	$egin{array}{c} 91.58 \\ 92.52 \\ 93.46 \\ 94.41 \\ \hline \end{array}$	$\begin{vmatrix} 31.98 \\ 32.31 \\ 32.64 \\ 32.97 \end{vmatrix}$	$   \begin{vmatrix}     91.44 \\     92.38 \\     93.32 \\     94.26   \end{vmatrix} $	$\begin{vmatrix} 32.38 \\ 32.71 \\ 33.05 \\ 33.38 \end{vmatrix}$	$egin{array}{c} 91.29 \\ 92.24 \\ 93.18 \\ 94.12 \\ \end{array}$	$\begin{vmatrix} 32.78 \\ 33.12 \\ 33.45 \\ 33.79 \end{vmatrix}$	97 98 99 100
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	I
Distance.	71 ]	Deg.	70¾ Deg.		$70\frac{1}{2}$	Deg.	70¼ Deg.		Distance.

-	1		11						
Distance	20	Deg.	201	Deg.	2012	Deg.	203	Deg.	Distance.
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce
1 2 3 4 5 6 7 8 9 10	$egin{array}{c} 1.88 \\ 2.82 \\ 3.76 \\ 4.70 \\ 5.64 \\ 6.58 \\ 7.52 \\ 8.46 \\ \end{array}$	0.68	0.94 1.88 2.81 3.75 4.69 5.63 6.57 7.51 8.44 9.38	0.35 0.69 1.04 1.38 1.73 2.08 2.42 2.77 3.12 3.46	0.94 1.87 2.81 3.75 4.68 5.62 6.56 7.49 8.43 9.37	0.35 0.70 1.05 1.40 1.75 2.10 2.45 2.80 3.15 3.50	0.94 1.87 2.81 3.74 4.68 5.61 6.55 7.48 8.42 9.35	0.35 0.71 1.06 1.42 1.77 2.13 2.48 2.83 3.19 3.54	1 2 3 4 5 6 7 8 9 10
11 12 13 14 15 16 17 18 19 20	10.34 11.28 12.22 13.16 14.10 15.04 15.97 16.91 17.85 18.79	3.76 4.10 4.45 4.79 5.13 5.47 5.81 6.16 6.50 6.84	10.32 11.26 12.20 13.13 14.07 15.01 15.95 16.89 17.83 18.76	3.81 4.15 4.50 4.85 5.19 5.54 5.88 6.23 6.58 6.92	10.30 11.24 12.18 13.11 14.05 14.99 15.92 16.86 17.80 18.73	3.85 4.20 4.55 4.90 5.25 5.60 5.95 6.30 6.65 7.00	10.29 11.22 12.16 13.09 14.03 14.96 15.90 16.83 17.77 18.70	3.90 4.25 4.61 4.96 5.31 5.67 6.02 6.38 6.73 7.09	11 12 13 14 15 16 17 18 19 20
21 22 23 24 25 26 27 28 29 30	$ \begin{array}{c} 19.73 \\ 20.67 \\ 21.61 \\ 22.55 \\ 23.49 \\ 24.43 \\ 25.37 \\ 26.31 \\ 27.25 \\ 28.19 \end{array} $	7.18 7.52 7.87 8.21 8.55 8.89 9.23 9.58 9.92 10.26	19.70 20.64 21.58 22.52 23.45 24.39 25.33 26.27 27.21 28.15	7.27 7.61 7.96 8.31 8.65 9.00 9.35 9.69 10.04 10.38	19.67 20.61 21.54 22.48 23.42 24.35 25.29 26.23 27.16 28.10	7.35 7.70 8.05 8.40 8.76 9.11 9.46 9.81 10.16 10.51	19.64 20.57 21.51 22.44 23.38 24.31 25.25 26.18 27.12 28.05	7.44 7.79 8.15 8.50 8.86 9.21 9.57 9.92 10.27 10.63	21 22 23 24 25 26 27 28 29 30
31 32 33 34 35 36 37 38 39 40	29.13 30.07 31.01 31.95 32.89 33.83 34.77 35.71 36.65 37.59	10.60 10.94 11.29 11.63 11.97 12.31 12.65 13.00 13.34 13.68	29.08 30.02 30.96 31.90 32.84 33.77 34.71 35.65 36.59 37.53	10.73 11.08 11.42 11.77 12.11 12.46 12.81 13.15 13.50 13.84	29.04 29.97 30.91 31.85 32.78 33.72 34.66 35.59 36.53 37.47	10.86 11.21 11.56 11.91 12.26 12.61 12.96 13.31 13.66 14.01	28.99 29.92 30.86 31.79 32.73 33.66 34.60 35.54 36.47 37.41	10.98 11.34 11.69 12.05 12.40 12.75 13.11 13.46 13.82 14.17	31 32 33 34 35 36 37 38 39 40
41 42 43 44 45 46 47 48 49 50	38.53 39.47 40.41 41.35 42.29 43.23 44.17 45.11 46.04 46.98	14.02 14.36 14.71 15.05 15.39 15.73 16.07 16.42 16.76 17.10	38.47 39.40 40.34 41.28 42.22 43.16 44.09 45.03 45.97 46.91	14.19 14.54 14.88 15.23 15.58 15.92 16.27 16.61 16.96 17.31	38.40 39.34 40.28 41.21 42.15 43.09 44.02 44.96 45.90 46.83	14.36 14.71 15.06 15.41 15.76 16.11 16.46 16.81 17.16 17.51	38.34 39.28 40.21 41.15 42.08 43.02 43.95 44.89 45.82 46.76	14.53 14.88 15.23 15.59 15.94 16.30 16.65 17.01 17.36 17.71	41 42 43 44 45 46 47 48 49 50
Distance.	Dep. 70 I	Lat.	$\frac{\text{Dep. }}{69\frac{3}{4}}$	Lat. Deg.	Dep. 691 1	Lat. Deg.	Dep.   694	Lat. Deg.	Distance.

		20 Deg. 201 Deg.			****			I	
Dist	20 I	Deg.	. 201 ]	Deg.	$. 20\frac{1}{2}$	Deg.	$20\frac{3}{4}$	Deg.	Dist
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
51 52	$  \overline{47.92}   48.86  $	$\frac{17.44}{17.79}$	1~.35 48.79	17.65 18.00	$\frac{1}{47.77}$ $\frac{1}{48.71}$	17.86 18.21	$\overline{47.69}$ $48.63$	18.07 18.42	51 52
53 54	49.80 50.74	18.13 18.47	$\begin{vmatrix} 49.72 \\ 50.66 \end{vmatrix}$	18.34 18.69	49.64 50.58	18.56 18.91	$\frac{49.56}{50.50}$	$   \begin{array}{c c}     \hline     18.78 \\     \hline     19.13   \end{array} $	53 54
55 56	51.68	18.81	51.60 52.54	19.04 19.38	51.52 $52.45$	$19.26 \\ 19.61$	$51.43 \\ 52.37$	$   \begin{array}{c c}     19.49 \\     19.84   \end{array} $	55 56
57 58	$\begin{bmatrix} 53.56 \\ 54.50 \end{bmatrix}$	19.50 19.84	$\begin{bmatrix} 53.48 \\ 54.42 \end{bmatrix}$	$   \begin{array}{c c}     \hline       19.73 \\       20.07   \end{array} $	53.39 54.33	$   \begin{array}{c c}     19.96 \\     20.31   \end{array} $	$53.30 \\ 54.24$	$\begin{bmatrix} 20.19 \\ 20.55 \end{bmatrix}$	57 58
59 60	55.44 56.38	$\begin{vmatrix} 20.18 \\ 20.52 \end{vmatrix}$	$\begin{bmatrix} 55.35 \\ 56.29 \end{bmatrix}$	$20.42 \\ 20.77$	55.26 56.20	$\begin{vmatrix} 20.66 \\ 21.01 \end{vmatrix}$	55.17 56.11	$\begin{bmatrix} 20.90 \\ 21.26 \end{bmatrix}$	59 60
$\begin{array}{ c c } \hline 61 \\ 62 \\ \hline \end{array}$	57.32 58.26	20.86 $21.21$	57.23 $58.17$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	57.14 58.07	$21.36 \\ 21.71$	57.04 57.98	$\frac{21.61}{21.97}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$
63 64	59.20 60.14	$\begin{vmatrix} 21.55 \\ 21.89 \end{vmatrix}$	59.11 60.04	21.81 22.15	59.01 59.95	$\begin{vmatrix} 22.06 \\ 22.41 \end{vmatrix}$	58.91 59.85	$\begin{bmatrix} 22.32 \\ 22.67 \end{bmatrix}$	63 64
65 66	$\begin{vmatrix} 61.08 \\ 62.02 \end{vmatrix}$	$\begin{bmatrix} 22.23 \\ 22.57 \end{bmatrix}$	$\begin{vmatrix} 60.98 \\ 61.92 \end{vmatrix}$	$22.50 \\ 22.84$	60.88	$\begin{bmatrix} 22.76 \\ 23.11 \end{bmatrix}$	$60.78 \ 61.72$	$\begin{vmatrix} 23.03 \\ 23.38 \end{vmatrix}$	65 66
67 68	$\begin{vmatrix} 62.96 \\ 63.90 \end{vmatrix}$	$egin{bmatrix} 22.92\ 23.26 \end{bmatrix}$	$\begin{vmatrix} 62.86 \\ 63.80 \end{vmatrix}$	$23.19 \\ 23.54$	$\begin{vmatrix} 62.76 \\ 63.69 \end{vmatrix}$	23.46 23.81	$\begin{bmatrix} 62.65 \\ 63.59 \end{bmatrix}$	$\begin{vmatrix} 23.74 \\ 24.09 \end{vmatrix}$	67 68
69 70	$\begin{vmatrix} 64.84 \\ 65.78 \end{vmatrix}$	$\begin{vmatrix} 23.60 \\ 23.94 \end{vmatrix}$	$64.74 \\ 65.67$	$23.88 \\ 24.23$	64.63	$\begin{vmatrix} 24.16 \\ 24.51 \end{vmatrix}$	$\begin{array}{c} 64.52 \\ 65.46 \end{array}$	$24.45 \\ 24.80$	$\begin{array}{c} 69 \\ 70 \end{array}$
71 72	66.72 67.66	$\begin{bmatrix} 24.28 \\ 24.63 \end{bmatrix}$	$66.61 \\ 67.55$	$24.57 \\ 24.92$	$66.50 \\ 67.44$	$24.86 \\ 25.21$	$66.39 \\ 67.33$	$25.15 \\ 25.51$	71 72
73 74	$\begin{vmatrix} 68.60 \\ 69.54 \end{vmatrix}$	$\begin{bmatrix} 24.97 \\ 25.31 \end{bmatrix}$	$\begin{bmatrix} 68.49 \\ 69.43 \end{bmatrix}$	$\begin{array}{c} 25.27 \\ 25.61 \end{array}$	68.38 $69.31$	$\begin{bmatrix} 25.57 \\ 25.92 \end{bmatrix}$	$\begin{vmatrix} 68.26 \\ 69.20 \end{vmatrix}$	$\begin{bmatrix} 25.86 \\ 26.22 \end{bmatrix}$	73 74
75 76	$\begin{vmatrix} 70.48 \\ 71.42 \end{vmatrix}$	25.65 25.99	70.36	$\begin{bmatrix} 25.96 \\ 26.30 \end{bmatrix}$	70.25 $  71.19$	$\begin{vmatrix} 26.27 \\ 26.62 \end{vmatrix}$	70.14	$\begin{vmatrix} 26.57 \\ 26.93 \\ 26.93 \end{vmatrix}$	75 76
77 78	$\begin{vmatrix} 72.36 \\ 73.30 \end{vmatrix}$	$\begin{vmatrix} 26.34 \\ 26.68 \\ 27.09 \end{vmatrix}$	72.24	$\begin{vmatrix} 26.65 \\ 27.00 \end{vmatrix}$	72.12	26.97	72.01	27.28 27.63	77 78
79 80	74.24 75.18	$\begin{bmatrix} 27.02 \\ 27.36 \end{bmatrix}$	74.12 75.06	27.34 $27.69$	$74.00 \\ 74.93$	27.67 $28.02$	73.88 $74.81$	$\begin{bmatrix} 27.99 \\ 28.34 \\ \hline \hline 38.34 \end{bmatrix}$	79 80
81 82		27.70 28.05	75.99 76.93	28.04 28.38	75.87	28.37	75.75	28.70 29.05	81 82
83	78.93	$\begin{bmatrix} 28.39 \\ 28.73 \\ 0.07 \end{bmatrix}$	77.87	28.73	77.74	$\begin{vmatrix} 29.07 \\ 29.42 \\ 20.77 \end{vmatrix}$	77.62	29.41	83 84
85	80.81	$egin{array}{c} 29.07 \ 29.41 \ 29.76 \ \end{array}$	79.75	$\begin{vmatrix} 29.42 \\ 29.77 \\ 20.11 \end{vmatrix}$	79.62	$\begin{vmatrix} 29.77 \\ 30.12 \\ 20.47 \end{vmatrix}$	$\begin{vmatrix} 79.49 \\ 80.42 \\ 81.36 \end{vmatrix}$	$\begin{vmatrix} 30.11 \\ 30.47 \\ 30.82 \end{vmatrix}$	85 86 87
87 88 89	82.69	$\begin{vmatrix} 29.76 \\ 30.10 \\ 30.44 \end{vmatrix}$	81.62 82.56 83.50	$\begin{vmatrix} 30.11 \\ 30.46 \\ 30.80 \end{vmatrix}$	$\begin{vmatrix} 81.49 \\ 82.43 \\ 83.36 \end{vmatrix}$	$\begin{vmatrix} 30.47 \\ 30.82 \\ 31.17 \end{vmatrix}$	82.29 83.23	31.18	88 89
90	84.57	30.78	84.44	31.15	84.30	31.52	84.16	31.89	90
91 92	86.45	31.12	85.38	$\begin{vmatrix} 31.50 \\ 31.84 \\ 22.10 \end{vmatrix}$	85.24	$\begin{vmatrix} 31.87 \\ 32.22 \\ 22.57 \end{vmatrix}$	$\begin{vmatrix} 85.10 \\ 86.03 \\ 86.97 \end{vmatrix}$	$\begin{vmatrix} 32.24 \\ 32.59 \\ 32.95 \end{vmatrix}$	$   \begin{array}{c c}     91 \\     92 \\     93   \end{array} $
93	88.33	$\begin{vmatrix} 31.81 \\ 32.15 \\ 32.49 \end{vmatrix}$	$\begin{vmatrix} 87.25 \\ 88.19 \\ 89.13 \end{vmatrix}$	$\begin{vmatrix} 32.19 \\ 32.54 \\ 32.88 \end{vmatrix}$	87.11	$\begin{vmatrix} 32.57 \\ 32.92 \\ 33.27 \end{vmatrix}$	87.90 88.84	33.30 33.66	93 94 95
95 96 97	90.21	$\begin{vmatrix} 32.49 \\ 32.83 \\ 33.18 \end{vmatrix}$	90.07	33.23 33.57	$\begin{vmatrix} 88.98 \\ 89.92 \\ 90.86 \end{vmatrix}$	33.62 33.97	89.77	$\begin{vmatrix} 34.01 \\ 34.37 \end{vmatrix}$	96 97
98	92.09	33.52 33.86	91.94 92.88	$\begin{vmatrix} 33.92 \\ 34.27 \end{vmatrix}$	$\begin{vmatrix} 90.80 \\ 91.79 \\ 92.73 \end{vmatrix}$	$\begin{vmatrix} 34.32 \\ 34.67 \end{vmatrix}$	91.64 $92.58$	$\begin{vmatrix} 34.72 \\ 35.07 \end{vmatrix}$	98. 99
100	93.97	$\frac{34.20}{}$	93.82	34.61	93.67	$\frac{35.02}{}$	93.51	35.43	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
Dist	70	Deg.	693	Deg.	$69\frac{1}{2}$	Deg.	691	Deg	Dist
-							11		

Dist	21	Deg.	214	Deg.	$21\frac{1}{2}$	Deg.	213	Deg.	Dist
ance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ance.
Distance 1234567890 111231451678190 2122234567890 312334567890 41243	Lat.  0.93 1.87 2.80 3.73 4.67 5.60 6.54 7.47 8.40 9.34 10.27 11.20 12.14 13.07 14.94 15.87 16.80 17.74 18.67 19.61 20.54 21.47 22.41 23.34 24.27 25.21 26.14 27.07 28.01 28.94 29.87 30.81 31.74 32.68 33.61 34.54 35.48 36.41 37.34 38.28 39.21 40.14	Dep.    0.36     0.72     1.08     1.43     1.79     2.15     2.51     2.87     3.23     3.58     3.94     4.30     4.66     5.02     5.38     5.73     6.09     6.45     6.81     7.17     7.53     7.88     8.24     8.60     8.96     9.32     9.68     10.03     10.75     11.11     11.47     11.83     12.18     12.54     12.90     13.26     13.98     14.69     15.05     15.41	Lat.  0.93 1.86 2.80 3.73 4.66 5.59 6.52 7.46 8.39 9.32 10.25 11.18 12.12 13.05 13.98 14.91 15.84 16.78 17.71 18.64 19.57 20.50 21.44 22.37 23.30 24.23 25.16 26.10 27.03 27.96 28.89 29.82 30.76 31.69 32.62 33.55 34.48 35.42 36.35 37.28 38.21 39.14 40.08	Dep.    0.36   0.72   1.09   1.45   1.81   2.17   2.54   2.90   3.26   3.62   3.99   4.35   4.71   5.07   5.44   5.80   6.16   6.52   6.89   7.25   7.61   7.97   8.34   8.70   9.06   9.42   9.79   10.15   10.51   10.87   11.24   11.60   12.32   12.69   13.05   13.41   13.77   14.14   14.50   14.86   15.22   15.58   1	Lat.  0.93 1.86 2.79 3.72 4.65 5.58 6.51 7.44 8.37 9.30 10.23 11.17 12.10 13.03 13.96 14.89 15.82 16.75 17.68 18.61 19.54 20.47 21.40 22.33 23.26 24.19 25.12 26.05 26.98 27.91 28.84 29.77 30.70 31.63 32.56 33.50 34.43 35.36 36.29 37.22 38.15 39.08 40.01	Dep.  0.37 0.73 1.10 1.47 1.83 2.20 2.57 2.93 3.30 3.67  4.03 4.40 4.76 5.13 5.50 6.23 6.60 6.96 7.33  7.70 8.06 8.43 8.80 9.16 9.53 9.90 10.26 10.63 11.00  11.36 11.73 12.09 12.46 12.83 13.19 13.56 13.93 14.29 14.66  15.03 15.39 15.76	Lat.  0.93 1.86 2.79 3.72 4.64 5.57 6.50 7.43 8.36 9.29 10.22 11.15 12.07 13.00 13.93 14.86 15.79 16.72 17.65 18.58 19.50 20.43 21.36 22.29 23.22 24.15 25.08 26.01 26.94 27.86 28.79 29.72 30.65 31.58 32.51 33.44 34.37 35.29 36.22 37.15 38.08 39.01 39.94	Dep.  0.37 0.74 1.11 1.48 1.85 2.22 2.59 2.96 3.34 3.71 4.08 4.45 4.82 5.19 5.56 5.93 6.30 6.67 7.04 7.41 7.78 8.15 8.52 8.89 9.26 9.63 10.01 10.38 10.75 11.12 11.49 11.86 12.23 12.60 12.97 13.34 13.71 14.08 14.45 14.82 15.19 15.56 15.93	Distance 12345678910 1121314 15617 188 199 20 21223 24 256 27 28 29 30 31 32 33 44 42 43
44 45 46 47 48 49 50	$\begin{array}{c} 41.08 \\ 42.01 \\ 42.94 \\ 43.88 \\ 44.81 \\ 45.75 \\ 46.68 \end{array}$	15.77 16.13 16.48 16.84 17.20 17.56 17.92	$\begin{array}{c} 41.01 \\ 41.94 \\ 42.87 \\ 43.80 \\ 44.74 \\ 45.67 \\ 46.60 \end{array}$	15.95 16.31 16.67 17.03 17.40 17.76 18.12	$\begin{array}{c} 40.94 \\ 41.87 \\ 42.80 \\ 43.73 \\ 44.66 \\ 45.59 \\ 46.52 \end{array}$	16.13 16.49 16.86 17.23 17.59 17.96 18.33	40.87 41.80 42.73 43.65 44.58 45.51 46.44	16.30 16.68 17.05 17.42 17.79 18.16 18.53	44 45 46 47 48 49 50
Distance.	Dep.	Lat.	Dep. 633	Lat. Deg.	Dep.   68½	Lat. Deg.	Dep.	Lat. Deg.	Distance.

Dista	21 I	Deg.	214	Deg.	21½	Deg.	$21\frac{3}{4}$	Deg.	Dist
ınce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ance
Distance.   552   554   555   557   589   616   626   636   646   657	Lat.  47.61 48.55 49.48 50.41 51.35 52.28 53.21 54.15 55.08 56.01  56.95 57.88 58.82 59.75 60.68 61.62 62.55 63.48 64.42 65.35  66.28 67.22 68.15 69.08 70.02 70.95 71.89 72.82 73.75 74.69  75.62 76.55 77.49 78.42 79.35 80.29 81.22 82.16 83.09 84.02  84.96 85.89 86.82 87.76 88.69 89.62 90.56	Dep.  18.28 18.64 18.99 19.35 19.71 20.07 20.43 20.79 21.14 21.50 21.86 22.22 22.58 22.94 23.29 23.65 24.01 24.37 24.73 25.09 25.44 27.59 27.95 28.31 28.67 29.03 29.39 29.74 30.46 30.82 31.18 31.54 31.54 31.89 32.25 32.61 32.97 33.33 33.69 34.04 34.76	Lat.  47.53 48.46 49.40 50.33 51.26 52.19 53.12 54.06 54.99 55.92  56.85 57.78 58.72 59.65 60.58 61.51 62.44 63.38 64.31 65.24  66.17 67.10 68.04 68.97 69.90 70.83 71.76 72.70 73.63 74.56  75.49 76.42 77.36 77.36 77.36 78.29 79.22 80.15 81.08 82.02 82.95 83.88 84.81 85.74 86.68 87.61 88.54 89.47 90.40	Dep.  18.48 18.85 19.21 19.57 19.93 20.30 20.66 21.02 21.38 21.75 22.11 22.47 22.83 23.20 23.56 23.92 24.28 24.65 25.01 25.73 26.10 26.46 26.82 27.18 27.55 27.91 28.27 28.63 29.00 29.36 29.72 30.08 30.44 30.81 31.17 31.53 31.89 32.26 32.98 33.34 33.71 34.07 34.43 34.79 35.16	Lat.  47.45 48.38 49.31 50.24 51.17 52.10 53.03 53.96 54.89 55.83  56.76 57.69 58.62 59.55 60.48 61.41 62.34 63.27 64.20 65.13 66.06 66.99 67.92 68.85 69.78 70.71 71.64 72.57 73.50 74.43  75.36 76.29 77.22 78.16 79.09 80.02 80.95 81.88 82.81 83.74  84.67 85.60 86.53 87.46 88.39 89.32 90.25	Dep.  18.69 19.06 19.42 19.79 20.16 20.52 20.89 21.26 21.62 21.99 22.36 22.72 23.09 23.46 24.19 24.56 24.92 25.29 25.66 26.02 26.39 26.75 27.12 27.49 27.85 28.22 29.69 30.05 30.42 30.79 31.15 31.52 31.89 32.25 32.62 32.99 33.35 33.72 34.08 34.45 35.55	Lat.  47.37 48.30 49.23 50.16 51.08 52.01 52.94 53.87 54.80 55.73  56.66 57.59 58.52 59.44 60.37 61.30 62.23 63.16 64.09 65.02 65.95 66.87 67.80 68.73 69.66 70.59 71.52 72.45 73.38 74.30  75.23 76.16 77.09 78.95 79.88 80.81 81.74 82.66 83.59 84.52 85.45 86.38 87.31 88.24 89.17 90.09	Dep.  18.90 19.27 19.64 20.01 20.38 20.75 21.12 21.49 21.86 22.23 22.60 22.97 23.35 23.72 24.09 24.46 24.83 25.20 25.57 25.94  26.31 26.68 27.05 27.42 27.79 28.16 28.53 28.90 29.27 29.64 30.02 30.39 30.76 31.13 31.50 31.87 32.24 32.61 32.98 33.35 33.72 34.09 34.46 34.83 35.20 35.57 35.94	Distance.   512 53 54 556 57 58 560   612 63 64 656 667 68 69 70   712 73 74 75 76 77 80   812 83 84 856 87 88 99   912 93 94 95 97 97 97 97 97 97 97 97 97 97 97 97 97
98 99 100	$\begin{vmatrix} 91.49 \\ 92.42 \\ 93.36 \end{vmatrix}$	35.12 35.48 35.84	$\begin{array}{ c c c c }\hline 91.34 \\ 92.27 \\ 93.20 \\\hline \end{array}$	$\begin{vmatrix} 35.52 \\ 35.88 \\ 36.24 \end{vmatrix}$	$   \begin{array}{c c}     91.18 \\     92.11 \\     93.04   \end{array} $	35.92 36.28 36.65	$ \begin{array}{c c} 91.02 \\ 91.95 \\ 92.88 \end{array} $	$\begin{vmatrix} 36.31 \\ 36.69 \\ 37.06 \end{vmatrix}$	98 99 100
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
Distance.	69	Deg.	683	Deg.	$68\frac{1}{2}$	Deg.	684	Deg.	Distance.

-	1				-				
Distance	22	Deg.	224	Deg.	22	b Deg.	224	Deg.	Dist
		Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance
1 2 3 4 4 5 6 6 7 8 8 9 9 1 1 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	$egin{array}{c cccc} 1.85 & 2.78 & 3.71 & 4.64 & 5.56 & 6.49 & 7.42 & 8.34 & 9.27 & $	0.75 1.12 1.50 1.87 2.25 2.62 3.00 3.37 3.75	0.93 1.85 2.78 3.70 4.63 5.55 6.48 7.40 8.33 9.26	0.38 0.76 1.14 1.51 1.89 2.27 2.65 3.03 3.41 3.79	1.85 2.77 3.70 4.62 5.54 6.47 7.39 8.31 9.24	0.77 1.15 1.53 1.91 2.30 2.68 3.06 3.44 3.83	0.92 1.84 2.77 3.69 4.61 5.53 6.46 7.38 8.30 9.22	0.77 1.16 1.55 1.93 2.32 2.71 3.09 3.48 3.87	1 2 3 4 5 6 7 8 9 10
112 133 144 155 166 177 188 199 20 21 222 233 244 255 266 277 288 299 30 31 32 33 34 44 445 466 477 489 50 90 90 90 90 90 90 90 90 90 90 90 90 90	11.13 12.05 12.98 13.91 14.83 15.76 16.69 17.62 18.54 19.47 20.40 21.33 22.25 23.18 24.11 25.03 25.96 26.89 27.82 28.74 29.67 30.60 31.52 32.45 33.38 34.31 35.23 36.16 37.09 38.01 38.94 39.87 40.80 41.72 42.65 43.58 44.50 45.43 46.36 Dep.	4.12 4.50 4.87 5.24 5.62 5.99 6.37 6.74 7.12 7.49 7.87 8.24 8.62 8.99 9.37 9.74 10.11 10.49 10.86 11.24 11.61 11.99 12.36 12.74 13.11 13.49 13.86 14.24 14.61 14.98 15.36 15.73 16.11 17.98 18.36 18.73 Lat.	10.18 11.11 12.03 12.96 13.88 14.81 15.73 16.66 17.59 18.51 19.44 20.36 21.29 22.21 23.14 24.06 24.99 25.92 26.84 27.77 28.69 29.62 30.54 31.47 32.39 33.32 34.24 35.17 36.10 37.02 37.95 38.87 39.80 40.72 41.65 42.57 43.50 40.72 41.65 42.57 43.50 40.72 41.65 42.57 43.50 44.43 45.35 46.28 Dep.	4.17 4.54 4.92 5.30 5.68 6.06 6.44 6.82 7.19 7.57 7.95 8.33 8.71 9.09 9.47 9.84 10.22 10.60 10.98 11.36 11.74 12.12 12.50 12.87 13.25 13.63 14.01 14.39 14.77 15.15 15.52 15.90 16.28 16.66 17.04 17.42 17.80 18.18 18.55 18.93 Lat.	10.16 11.09 12.01 12.93 13.86 14.78 15.71 16.63 17.55 18.48 19.40 20.33 21.25 22.17 23.10 24.02 24.94 25.87 26.79 27.72 28.64 29.56 30.49 31.41 32.34 33.26 34.18 35.11 36.03 36.96 37.88 38.80 39.73 40.65 41.57 42.50 43.42 44.35 45.27 46.19 Dep.	4.21 4.59 4.97 5.36 5.74 6.12 6.51 6.89 7.27 7.65 8.04 8.42 8.80 9.18 9.57 9.95 10.33 10.72 11.10 11.48 11.86 12.25 12.63 13.01 13.39 13.78 14.16 14.54 14.54 14.92 15.31 15.69 16.84 17.22 17.60 17.99 18.37 18.75 19.13 Lat.	10.14 11.07 11.99 12.91 13.83 14.76 15.68 16.60 17.52 18.44 19.37 20.29 21.21 22.13 23.05 23.98 24.90 25.82 26.74 27.67 28.59 29.51 30.43 31.35 32.28 33.20 34.12 35.04 35.97 36.89 37.81 38.73 39.65 40.58 41.50 42.42 43.34 44.27 45.19 46.11 Dep.	4.25 4.64 5.03 5.41 5.80 6.19 6.57 6.96 7.35 7.73 8.12 8.51 8.89 9.28 9.67 10.05 10.44 10.83 11.21 11.60 11.99 12.37 12.76 13.15 13.53 13.92 14.31 14.70 15.08 15.47 15.86 16.24 16.63 17.02 17.79 18.18 18.56 18.95 19.34 Lat.	11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 45 46 47 48 49 50 49 49 49 49 49 49 49 49 49 49 49 49 49
Dis	68 I	eg.	67 <u>₹</u> I	Deg.	$67\frac{1}{2}$	Deg.	674 1	Deg.	Dist

D:	22 ]	Deg.	221	Deg.	$22\frac{1}{2}$	Deg.	$22\frac{3}{4}$	Deg.	D
Distance	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
51 52 53 54	47.29 48.21 49.14 50.07	19.10 19.48 19.85 20.23	$ \begin{array}{r}   \hline     47.20 \\     48.13 \\     49.05 \\     49.98 \end{array} $	$   \begin{array}{r}     \hline             19.31 \\             19.69 \\             20.07 \\             20.45   \end{array} $	47.12 48.04 48.97 49.89	$ \begin{array}{r} 19.52 \\ 19.90 \\ 20.28 \\ 20.66 \end{array} $	47.03 47.95 48.88 49.80	19.72 20.11 20.59 20.88	51 52 53 54
55 56 57 58	51.00 51.92 52.85 53.78	20.60 $20.98$ $21.35$ $21.73$	50.90 51.83 52.76 53.68	20.43 20.83 21.20 21.58 21.96	50.81 51.74 52.66 53.59	21.05 $21.43$ $21.81$ $22.20$	50.72 51.64 52.57 53.49	21.27 21.66 22.04 22.43	55 56 57 58
59 60	54.70 55.63	$\frac{22.10}{22.48}$	54.61 55.53	$\begin{bmatrix} 22.34 \\ 22.72 \end{bmatrix}$	54.51 55.43	$22.58 \ 22.96$	54.41 55.33	$\frac{22.82}{23.20}$	59 60
61 62 63 64	56.56 57.49 58.41 59.34	22.85 23.23 23.60 23.97	56.47 57.38 58.31 59.23	23.10 23.48 23.85 24.23	56.36 57.28 58.20 59.13	23.34 23.73 24.11 24.49	56.25 57.18 58.10 59.02	23.59 23.98 24.36 24.75	61 62 63 64
65 66 67 68	$\begin{vmatrix} 60.27 \\ 61.19 \\ 62.12 \\ 63.05 \end{vmatrix}$	24.35/24.72 $25.10$ $25.47$	$ \begin{vmatrix} 60.16 \\ 61.09 \\ 62.01 \\ 62.94 \end{vmatrix} $	$\begin{array}{c} 24.61 \\ 24.99 \\ 25.37 \\ 25.75 \end{array}$	$\begin{bmatrix} 60.05 \\ 60.98 \\ 61.90 \\ 62.82 \end{bmatrix}$	$egin{array}{c} 24.87 \ 25.26 \ 25.64 \ 26.02 \ \end{array}$	$\begin{bmatrix} 59.94 \\ 60.87 \\ 61.79 \\ 62.71 \end{bmatrix}$	$\begin{array}{c} 25.14 \\ 25.52 \\ 25.91 \\ 26.30 \end{array}$	65 66 67 68
$\begin{array}{c} 69 \\ 70 \\ \hline 71 \end{array}$	$\frac{63.98}{64.90}$ $\frac{65.83}{65.83}$	$\begin{array}{ c c c }\hline 25.85 \\ 26.22 \\ \hline \hline 26.60 \\ \hline \end{array}$	$\begin{vmatrix} 63.86 \\ 64.79 \\ \hline 65.71 \end{vmatrix}$	$ \begin{array}{r} 26.13 \\ 26.51 \\ \hline 26.88 \end{array} $	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\frac{26.41}{26.79} \\ \hline 27.17$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$ \begin{vmatrix} 69 \\ 70 \\ \hline 71 \end{vmatrix} $
72 73 74	66.76 67.68 68.61	26.97 27.35 27.72	66.64 67.56 68.49	27.26 27.64 28.02	$\begin{vmatrix} 66.52 \\ 67.44 \\ 68.37 \end{vmatrix}$	27.55 27.94 28.32	$\begin{bmatrix} 66.40 \\ 67.32 \\ 68.24 \end{bmatrix}$	27.84 28.23 28.62	72 73 74
75 76 77 78	$\begin{vmatrix} 69.54 \\ 70.47 \\ 71.39 \\ 72.32 \end{vmatrix}$	28.10 28.47 28.84 29.22	$\begin{bmatrix} 69.42 \\ 70.34 \\ 71.27 \\ 72.19 \end{bmatrix}$	$egin{array}{c} 28.40 \ 28.78 \ 29.16 \ 29.53 \ \end{array}$	$\begin{vmatrix} 69.29 \\ 70.21 \\ 71.14 \\ 72.06 \end{vmatrix}$	$egin{array}{c} 28.70 \\ 29.08 \\ 29.47 \\ 29.85 \\ \hline \end{array}$	$ \begin{vmatrix} 69.17 \\ 70.09 \\ 71.01 \\ 71.93 \end{vmatrix} $	$\begin{bmatrix} 29.00 \\ 29.39 \\ 29.78 \\ 30.16 \end{bmatrix}$	75 76 77 78
$\begin{array}{c} 79 \\ 80 \\ \hline 81 \end{array}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$ \begin{array}{r} 29.59 \\ 29.97 \\ \hline 30.34 \end{array} $	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{ c c c c c c }\hline 72.99 \\ 73.91 \\ \hline 74.83 \\ \hline \end{array}$	$\begin{vmatrix} 30.23 \\ 30.61 \\ \hline 31.00 \end{vmatrix}$	$\begin{array}{ c c c c c c }\hline 72.85 \\ 73.78 \\ \hline 74.70 \\ \hline \end{array}$	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	$ \begin{vmatrix} 79 \\ 80 \\ \hline 81 \end{vmatrix} $
82 83 84	76.03 76.96 77.88	$\begin{vmatrix} 30.72 \\ 31.09 \\ 31.47 \end{vmatrix}$	75.89 76.82 77.75	31.05 31.43 31.81	75.76 76.68 77.61	31.38 31.76 32.15	75.62 76.54 77.46	$\begin{vmatrix} 31.71 \\ 32.10 \\ 32.48 \end{vmatrix}$	82 83 84
85 86 87 88	78.81 79.74 80.66 81.59	31.84 32.22 32.59 32.97	78.67 79.60 80.52 81.45	$\begin{vmatrix} 32.19 \\ 32.56 \\ 32.94 \\ 33.32 \end{vmatrix}$	78.53 79.45 80.38 81.30	32.53 32.91 33.29 33.68	$oxed{78.39} \ 79.31 \ 80.23 \ 81.15$	$\begin{vmatrix} 32.87 \\ 33.26 \\ 33.64 \\ 34.03 \end{vmatrix}$	85 86 87 88
89 90	$   \begin{vmatrix}     82.52 \\     83.45   \end{vmatrix} $	$\frac{33.34}{33.71}$	$   \begin{bmatrix}     82.37 \\     83.30   \end{bmatrix} $	$\begin{vmatrix} 33.70 \\ 34.08 \end{vmatrix}$	$   \begin{array}{r}     82.23 \\     83.15   \end{array} $	$   \begin{vmatrix}     34.06 \\     34.44   \end{vmatrix} $	$82.08 \\ 83.00$	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	89 90
91 92 93 94	84.37 85.30 86.23 87.16	$egin{array}{c} 34.09 \ 34.46 \ 34.84 \ 35.21 \ \end{array}$	$egin{array}{c} 84.22 \\ 85.15 \\ 86.08 \\ 87.00 \\ \hline \end{array}$	34.46 34.84 35.21 35.59	$\begin{vmatrix} 84.07 \\ 85.00 \\ 85.92 \\ 86.84 \end{vmatrix}$	$\begin{vmatrix} 34.82 \\ 35.21 \\ 35.59 \\ 35.97 \end{vmatrix}$	$\begin{vmatrix} 83.92 \\ 84.84 \\ 85.76 \\ 86.69 \end{vmatrix}$	35.19 35.58 35.96 36.35	91 92 93 94
95 96 97	88.08 89.01 89.94	35.59 35.96 36.34	87.93 88.85 89.78	35.97 36.35 36.73	87.77 88.69 89.62	$\begin{vmatrix} 36.35 \\ 36.74 \\ 37.12 \end{vmatrix}$	87.61 88.53 89.45	$\begin{vmatrix} 36.74 \\ 37.12 \\ 37.51 \end{vmatrix}$	95 96 97
98 99 100	$   \begin{array}{c c}     90.86 \\     91.79 \\     92.72   \end{array} $	$   \begin{array}{r}     36.71 \\     37.09 \\     37.46   \end{array} $	$   \begin{vmatrix}     90.70 \\     91.63 \\     92.55   \end{vmatrix} $	$   \begin{array}{r}     37.11 \\     37.49 \\     37.86   \end{array} $	$   \begin{array}{c}     90.54 \\     91.46 \\     92.39   \end{array} $	37.50 37.89 38.27	$ \begin{array}{c c} 90.38 \\ 91.30 \\ 92.22 \end{array} $	$   \begin{array}{r}     37.90 \\     38.28 \\     38.67   \end{array} $	98 99 100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
Dist	68 1	Deg.	673	Deg.	67½	Deg.	674	Deg.	Dist

1		A ROOM					Name of the last		
Distance	23 I	Deg.	234	Deg.	$23\frac{1}{2}$	Deg.	233	Deg.	Distance.
3	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	псе
1 2 3 4 5 6 7 8 9	0.92 1.84 2.76 3.68 4.60 5.52 6.44 7.36 8.28 9.20	0.39 0.78 1.17 1.56 1.95 2.34 2.74 3.13 3.52 3.91	0.92 1.84 2.76 3.68 4.59 5.51 6.43 7.35 8.27 9.19	0.39 0.79 1.18 1.58 1.97 2.37 2.76 3.16 3.55 3.95	0.92 1.83 2.75 3.67 4.59 5.50 6.42 7.34 8.25 9.17	0.40 0.80 1.20 1.59 1.99 2.39 2.79 3.19 3.59 3.99	0.92 1.83 2.75 3.66 4.58 5.49 6.41 7.32 8.24 9.15	0.40 0.81 1.21 1.61 2.01 2.42 2.82 3.22 3.62 4.03	1 2 3 4 5 6 7 8 9
11 12 13 14 15 16 17 18 19 20	10.13 11.05 11.97 12.89 13.81 14.73 15.65 16.57 17.49 18.41	4.30 4.69 5.08 5.47 5.86 6.25 6.64 7.03 7.42 7.81	10.11 11.03 11.94 12.86 13.78 14.70 15.62 16.54 17.40 18.38	4.34 4.74 5.13 5.53 5.92 6.32 6.71 7.11 7.50 7.89	10.09 11.00 11.92 12.84 13.76 14.67 15.59 16.51 17.42 18.34	4.39 4.78 5.18 5.58 5.98 6.38 6.78. 7.18 7.58 7.97	10.07 10.98 11.90 12.81 13.73 14.64 15.56 16.48 17.39 18.31	4.43 4.83 5.24 5.64 6.04 6.44 6.85 7.25 7.65 8.05	11 12 13 14 15 16 17 18 19 20
21 22 23 24 25 26 27 28 29 30	19.33 20.25 21.17 22.09 23.01 23.93 24.85 25.77 26.69 27.62	8.21 8.60 8.99 9.38 9.77 10.16 10.55 10.94 11.33 11.72	19.29 20.21 21.13 22.05 22.97 23.89 24.81 25.73 26.64 27.56	8.29 8.68 9.08 9.47 9.87 10.26 10.66 11.05 11.45 11.84	19.26 20.18 21.09 22.01 22.93 23.84 24.76 25.68 26.59 27.51	8.37 8.77 9.17 9.57 9.97 10.37 11.16 11.56 11.96	19.22 20.14 21.05 21.97 22.88 23.80 24.71 25.63 26.54 27.46	8.46 8.86 9.26 9.67 10.07 10.47 10.87 11.28 11.68 12.08	21 22 23 24 25 26 27 28 29 30
31 32 33 34 35 36 37 38 39 40	28.54 29.46 30.38 31.30 32.22 33.14 34.06 34.98 35.90 36.82	12.11 12.50 12.89 13.28 13.68 14.07 14.46 14.85 15.24 15.63	28.48 29.40 30.32 31.24 32.16 33.08 34.00 34.91 35.83 36.75	12.24 12.63 13.03 13.42 13.82 14.21 14.61 15.00 15.39 15.79	28.43 29.35 30.26 31.18 32.10 33.01 33.93 34.85 35.77 36.68	12.36 12.76 13.16 13.56 13.96 14.35 14.75 15.15 15.55	28.37 29.29 30.21 31.12 32.04 32.95 33.87 34.78 35.70 36.61	12.49 12.89 13.29 13.69 14.10 14.50 14.50 15.30 15.71 16.11	31 32 33 34 35 36 37 38 39 40
41 42 43 44 45 46 47 48 49 50	37.74 38.66 39.58 40.50 41.42 42.34 43.26 44.18 45.10 46.03	16.02 16.41 16.80 17.19 17.58 17.97 18.36 18.76 19.15	37.67 38.59 39.51 40.43 41.35 42.26 43.18 44.10 45.02 45.94	16.18 16.58 16.97 17.37 17.76 18.16 18.55 18.95 19.34 19.74	37.60 38.52 39.43 40.35 41.27 42.18 43.10 44.02 44.94 45.85	16.35 16.75 17.15 17.54 17.94 18.34 18.74 19.14 19.54 19.94	37.53 38.44 39.36 40.27 41.19 42.10 43.02 43.93 44.85 45.77	16.51 16.92 17.32 17.72 18.12 18.53 18.53 19.33 19.73 20.14	41 42 43 44 45 46 47 48 49 50
Distance.	Dep. 67	Lat. Deg.	$\begin{array}{ c c }\hline \text{Dep.}\\\hline & 66\frac{3}{4}\\\hline \end{array}$	Lat.	Dep. 66½	Lat. Deg.	Dep. 664	Lat. Deg.	Distance.

D	23	Deg.	231	Deg.	23±	Deg.	233	Deg.	U
Distance.	Lat.		I.at.	(	Lat.	Dep.		1	istance
4		Dep.		Dep.			Lat.	Dep.	
51 52	46.95  $ 47.87 $	$\begin{vmatrix} 19.93 \\ 20.32 \end{vmatrix}$	46.86  $ 47.78 $	$\begin{vmatrix} 20.13 \\ 20.53 \end{vmatrix}$	$  46.77 \\ 47.69  $	$\begin{vmatrix} 20.34 \\ 20.73 \end{vmatrix}$	46.68	$\begin{vmatrix} 20.54 \\ 20.94 \end{vmatrix}$	51 52
53 54	$\begin{vmatrix} 48.79 \\ 49.71 \end{vmatrix}$	20.71	48.70	20.92	48.60	21.13	48.51	21.35	53
55	50.63	$\begin{vmatrix} 21.10 \\ 21.49 \end{vmatrix}$	$  49.61 \\ 50.53  $	$\begin{vmatrix} 21.32 \\ 21.71 \end{vmatrix}$	$  49.52 \\ 50.44  $	$\begin{vmatrix} 21.53 \\ 21.93 \end{vmatrix}$	49.43 50.34	$\begin{vmatrix} 21.75 \\ 22.15 \end{vmatrix}$	54 55
56 57	51.55	$\begin{vmatrix} 21.88 \\ 22.27 \end{vmatrix}$	51.45	$22.11 \\ 22.50$	51.36	$\begin{vmatrix} 22.33 \\ 22.73 \end{vmatrix}$	$51.26 \\ 52.17$	$\begin{vmatrix} 22.55 \\ 22.96 \end{vmatrix}$	56 57
58	53.39	22.66	53.29	22.90	53.19	23.13	53.09	23.36	58
59 50	54.31 55.23	$\begin{vmatrix} 23.05 \\ 23.44 \end{vmatrix}$	54.21 55.13	$\begin{vmatrix} 23.29 \\ 23.68 \end{vmatrix}$	54.11	$\begin{vmatrix} 23.53 \\ 23.92 \end{vmatrix}$	54.00 54.92	$\begin{vmatrix} 23.76 \\ 24.16 \end{vmatrix}$	59 60
$\frac{70}{61}$	56.15	23.83	56.05	$\frac{23.08}{24.08}$	55.94	24.32	55.83	$\frac{24.10}{24.57}$	$-\frac{61}{61}$
62 63	57.07  $ 57.99 $	$24.23 \\ 24.62$	56.97	$\begin{vmatrix} 24.47 \\ 24.87 \end{vmatrix}$	56.86	$\begin{vmatrix} 24.72 \\ 25.12 \end{vmatrix}$	56.75 57.66	$\begin{vmatrix} 24.97 \\ 25.37 \end{vmatrix}$	62 63
64	58.91	25.01	58.80	25.26	58.69	25.52	58.58	25.78	64
65 66	$\begin{vmatrix} 59.83 \\ 60.75 \end{vmatrix}$	$\begin{vmatrix} 25.40 \\ 25.79 \end{vmatrix}$	59.72 $60.64$	$\begin{vmatrix} 25.66 \\ 26.05 \end{vmatrix}$	59.61  60.53	$\begin{vmatrix} 25.92 \\ 26.32 \end{vmatrix}$	$59.50 \\ 60.41$	$\begin{vmatrix} 26.18 \\ 26.58 \end{vmatrix}$	65 66
67	61.67	26.18	61.56	26.45	61.44	26.72	61.33	26.98	67
68	$\begin{vmatrix} 62.59 \\ 63.51 \end{vmatrix}$	$\begin{vmatrix} 26.57 \\ 26.96 \end{vmatrix}$	$\begin{vmatrix} 62.48 \\ 63.40 \end{vmatrix}$	$\begin{vmatrix} 26.84 \\ 27.24 \end{vmatrix}$	$\begin{vmatrix} 62.36 \\ 63.28 \end{vmatrix}$	$\begin{vmatrix} 27.11 \\ 27.51 \end{vmatrix}$	$\begin{vmatrix} 62.24 \\ 63.16 \end{vmatrix}$	$\begin{vmatrix} 27.39 \\ 27.79 \end{vmatrix}$	68
70	64.44	27.35	64.32	27.63	64.19	27.91	64.07	28.19	70
71 72	65.36 66.28	$\begin{vmatrix} 27.74 \\ 28.13 \end{vmatrix}$	65.23	$\begin{bmatrix} 28.03 \\ 28.42 \end{bmatrix}$	$\begin{vmatrix} 65.11 \\ 66.03 \end{vmatrix}$	$\begin{vmatrix} 28.31 \\ 28.71 \end{vmatrix}$	$64.99 \\ 65.90$	28.59 $29.00$	71 72
73	67.20	28.52	67.07	28.82	66.95	29.11	66.82	29.40	73
74 75	$\begin{vmatrix} 68.12 \\ 69.04 \end{vmatrix}$	$\begin{vmatrix} 28.91 \\ 29.30 \end{vmatrix}$	$\begin{vmatrix} 67.99 \\ 68.91 \end{vmatrix}$	29.21 $29.61$	67.86	$\begin{bmatrix} 29.51 \\ 29.91 \end{bmatrix}$	67.73	$\begin{vmatrix} 29.80 \\ 30.21 \end{vmatrix}$	74 75
76	$\begin{vmatrix} 69.95 \\ 70.88 \end{vmatrix}$	$\begin{vmatrix} 29.70 \\ 30.09 \end{vmatrix}$	69.83	30.00	69.70	$30.30 \\ 30.70$	$69.56 \\ 70.48$	$30.61 \\ 31.01$	76 77
78	71.80	30.48	71.67	$30.40 \\ 30.79$	70.61	31.10	71.39	31.41	78
79 80	$\begin{vmatrix} 72.72 \\ 73.64 \end{vmatrix}$	$\begin{vmatrix} 30.87 \\ 31.26 \end{vmatrix}$	72.58 73.50	$\frac{31.18}{31.58}$	72.45	$\begin{vmatrix} 31.50 \\ 31.90 \end{vmatrix}$	$72.31 \\ 73.22$	$\begin{vmatrix} 31.82 \\ 32.22 \end{vmatrix}$	79 80
81	74.56	$\overline{31.65}$	74.42	$\frac{31.97}{31.97}$	$\frac{74.28}{}$	32.30	74.14	$\frac{32.62}{}$	81
82 83	75.48	$\begin{vmatrix} 32.04 \\ 32.43 \end{vmatrix}$	75.34 76.26	$\begin{vmatrix} 32.37 \\ 32.76 \end{vmatrix}$	75.20	$\begin{vmatrix} 32.70 \\ 33.10 \end{vmatrix}$	75.06 $75.97$	$\begin{vmatrix} 33.03 \\ 33.43 \end{vmatrix}$	82 83
84	77.32	32.82	77.18	33.16	77.03	33.49	76.89	33.83	84
85	78.24	$\frac{33.21}{33.60}$	$78.10 \\ 79.02$	$\begin{vmatrix} 33.55 \\ 33.95 \end{vmatrix}$	77.95	$\left  \begin{array}{c} 33.89 \\ 34.29 \end{array} \right $	77.80 78.72	$\begin{vmatrix} 34.23 \\ 34.64 \end{vmatrix}$	85 86
87	80.08	33.99	79.93	34.34	79.78	34.69	79.63	35.04	87
88	$\begin{vmatrix} 81.00 \\ 81.92 \end{vmatrix}$	$34.38 \\ 34.78$	80.85	$\begin{array}{ c c }\hline 34.74\\ 35.13\\ \hline\end{array}$	80.70	$\begin{vmatrix} 35.09 \\ 35.49 \end{vmatrix}$	80.55	35.44 35.84	88 89
90	82.85	35.17	82.69	35.53	82.54	35.89	82.38	36.25	90
91 92	83.77	$\begin{array}{c} 35.56 \\ 35.95 \end{array}$	$\begin{vmatrix} 83.61 \\ 84.53 \end{vmatrix}$	$\begin{bmatrix} 35.92 \\ 36.32 \end{bmatrix}$	83.45	$\begin{bmatrix} 36.29 \\ 36.68 \end{bmatrix}$	$\begin{bmatrix} 83.29 \\ 84.21 \end{bmatrix}$	$ 36.65  \\ 37.05 $	91 92
93	85.61	36.34	85.45	36.71	85.29	37.08	85.12	37.46	93
94 95	86.53	$36.73 \\ 37.12$	$86.37 \ 87.29$	$\begin{vmatrix} 37.11 \\ 37.50 \end{vmatrix}$	$\begin{vmatrix} 86.20 \\ 87.12 \end{vmatrix}$	$\begin{vmatrix} 37.48 \\ 37.88 \end{vmatrix}$	$ 86.04  \\ 86.95$	$\frac{37.86}{38.26}$	94 95
96	88.37	37.51	88.20	37.90	88.04	$\frac{38.28}{38.68}$	87.87	38.66	96
97 98	$\begin{vmatrix} 89.29 \\ 90.21 \end{vmatrix}$	$\begin{array}{c} 37.90 \\ 38.29 \end{array}$	$\begin{bmatrix} 89.12 \\ 90.04 \end{bmatrix}$	38.29 38.68	88.95 89.87 90.79	39.08	89.70	$39.07 \\ 39.47$	$\begin{array}{c} 97 \\ 98 \end{array}$
99	$91.13 \\ 92.05$	$\frac{38.68}{39.07}$	90.96  $ 91.88 $			$\begin{vmatrix} 39.48 \\ 39.87 \end{vmatrix}$	$90.62 \\ 91.53$	$\frac{39.87}{40.27}$	$\frac{99}{100}$
<b>44</b>	Dep.	Lat.	Dep.	Lat.	91.71 Dep.	Lat.	Dep.	Lat.	
Distance.		T				-			Distance
Ü	67 I	eg.	$66\frac{3}{4}$	Deg.	$66\frac{1}{2}$	Deg.	661	Deg.	Di
									7

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) Ist	24 ]	Deg.	241	Deg.	$24\frac{1}{2}$	Deg.	$24\frac{3}{4}$	Deg.	Lists
nce	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
	0.91 1.83 2.74 3.65 4.57 5.48 6.39 7.31 8.22 9.14 10.05 10.96 11.88 12.79 13.70 14.62 15.53 16.44 17.36 18.27 19.18 20.10 21.01 21.93 22.84 63.39 7.31 8.22 9.14 10.05 11.88 12.79 13.70 14.62 15.53 16.44 17.36 18.27 19.18 20.10 21.01 21.93 22.84 63.39 7.31 83.22 84.67 85.58 86.49 27.41 28.32 29.23 30.15 31.97 32.89 33.80 34.71	0.41 0.81 1.22 1.63 2.03 2.44 2.85 3.25 3.66 4.07 4.47 4.48 5.29 5.69 6.10 6.51 6.92 7.32 7.73 8.13 8.54 8.95 9.35 9.76 10.17 10.58 11.80 12.20 12.61 13.42 13.42 13.42 14.64 15.05 15.46	Lat.  0.91 1.82 2.74 3.65 4.56 5.47 6.38 7.29 8.21 9.12 10.03 10.94 11.85 12.76 13.68 14.59 15.50 16.41 17.32 18.24 19.15 20.06 20.97 21.88 22.79 23.71 24.62 25.53 26.44 27.35 28.26 29.18 30.09 31.00 31.91 32.82 33.74 34.65 35.56	Dep.  0.41 0.82 1.23 1.64 2.05 2.46 2.87 3.29 3.70 4.11 4.52 4.93 5.34 5.75 6.16 6.57 6.98 7.39 7.80 8.21  8.63 9.04 9.45 9.86 10.27 10.68 11.09 11.50 11.91 12.32 12.73 13.14 13.55 13.96 14.38 14.79 15.20 15.61 16.02	Lat.  0.91 1.82 2.73 3.64 4.55 5.46 6.37 7.28 8.19 9.10 10.01 10.92 11.83 12.74 13.65 14.56 15.47 16.38 17.29 18.20 19.11 20.02 20.93 21.84 22.75 23.66 24.57 25.48 26.39 27.30 28.21 29.12 30.03 30.94 31.85 32.76 33.67 34.58 35.49	$\begin{array}{c} 0.41 \\ 0.83 \\ 1.24 \\ 1.66 \\ 2.07 \\ 2.49 \\ 2.90 \\ 3.32 \\ 3.73 \\ 4.15 \\ \hline 4.56 \\ 4.98 \\ 5.39 \\ 5.81 \\ 6.22 \\ 6.64 \\ 7.05 \\ 7.46 \\ 7.88 \\ 8.29 \\ \hline \hline 8.71 \\ 9.12 \\ 9.54 \\ 9.95 \\ 10.37 \\ 10.78 \\ 11.20 \\ 11.61 \\ 12.03 \\ 12.44 \\ \hline 12.86 \\ \hline \end{array}$	Lat.    0.91   1.82   2.72   3.63   4.54   5.45   6.36   7.27   8.17   9.08   9.99   10.90   11.81   12.71   13.62   14.53   15.44   16.35   17.25   18.16   19.07   19.98   20.89   21.80   22.70   23.61   24.52   25.43   26.34   27.24   28.15   29.06   29.97   30.88   31.78   32.69   33.60   34.51   35.42	Dep.  0.42 0.84 1.26 1.67 2.09 2.51 2.93 3.35 3.77 4.19 4.61 5.02 5.44 5.86 6.28 6.70 7.12 7.54 7.95 8.37 8.79 9.21 9.63 10.47 10.89 11.30 11.72 12.14 12.56 12.98 13.40 13.82 14.65 15.07 15.49 15.91 16.33	Table: 1234567890 11121314567890 11213145617890 2122324567890 333456789 36789
40 40 41 42 42 44 44	$ \begin{array}{c c} 36.54 \\ \hline 37.46 \\ 38.37 \\ 39.28 \\ 40.20 \end{array} $	15.86 16.27 16.68 17.08 17.49 17.90 18.30	$ \begin{array}{r} 35.56 \\ 36.47 \\ \hline 37.38 \\ 38.29 \\ 39.21 \\ 40.12 \\ 41.03 \end{array} $	16.02 $16.43$ $16.84$ $17.25$ $17.66$ $18.07$ $18.48$	$   \begin{array}{r}     35.49 \\     36.40 \\     \hline     37.31 \\     38.22 \\     39.13 \\     40.04 \\     40.95   \end{array} $	16.17 $16.59$ $17.00$ $17.42$ $17.83$ $18.25$ $18.66$	36.33 37.23 38.14 39.05 39.96 40.87	$\begin{array}{r} 16.75 \\ \hline 17.16 \\ 17.58 \\ 18.00 \\ 18.42 \\ 18.84 \end{array}$	39 40 41 42 43 44 45
46 47 48 49 50	$\begin{bmatrix} 42.02 \\ 42.94 \\ 43.85 \\ 44.76 \\ 45.68 \end{bmatrix}$	18.71 19.12 19.52 19.93 20.34	41.94 42.85 43.76 44.68 45.59	18.89 19.30 19.71 20.13 20.54	41.86 42.77 43.68 44.59 45.50	$   \begin{array}{c}     19.08 \\     19.49 \\     19.91 \\     20.32 \\     20.73   \end{array} $	$\begin{array}{r} 41.77 \\ 42.68 \\ 43.59 \\ 44.50 \\ 45.41 \\ \hline \end{array}$	$ \begin{array}{c c} 19.26 \\ 19.68 \\ 20.10 \\ 20.51 \\ 20.93 \end{array} $	46 47 48 49 50
nce.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	nce.
Distance.	66 ]	Deg.	653	Deg.	$65\frac{1}{2}$	Deg.	651/4	Deg.	Distance.

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Distance.	24	Deg.	244	Deg.	24½	Deg.	243	Deg.	Dista
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	istance.
51 52 53	46.59 47.50 48.42	$ \begin{array}{ c c c c c } \hline 20.74 \\ 21.15 \\ 21.56 \\ \end{array} $	46.50 47.41 48.32	$ \begin{array}{r}   20.95 \\   21.36 \\   21.77 \end{array} $	46.41 47.32 48.23	21.15 21.56 21.98	46.32 47.22 48.13	21.35 21.77 22.19	51 52 53
54 55 56	$\begin{vmatrix} 49.33 \\ 50.24 \\ 51.16 \end{vmatrix}$	$\begin{vmatrix} 21.96 \\ 22.37 \\ 22.78 \end{vmatrix}$	49.24 50.15 51.06	$\begin{bmatrix} 22.18 \\ 22.59 \\ 23.00 \end{bmatrix}$	49.14 50.05 50.96	$\begin{vmatrix} 22.39 \\ 22.81 \\ 23.22 \end{vmatrix}$	49.04   49.95   50.86	$\begin{vmatrix} 22.61 \\ 23.03 \\ 23.44 \end{vmatrix}$	54 55 56
57 58 59	$\begin{bmatrix} 52.07 \\ 52.99 \\ 53.90 \end{bmatrix}$	$\begin{vmatrix} 23.18 \\ 23.59 \\ 24.00 \end{vmatrix}$	51.97 52.88 53.79	23.41 23.82 24.23	51.87 52.78 53.69	$\begin{vmatrix} 23.64 \\ 24.05 \\ 24.47 \end{vmatrix}$	51.76 52.67 53.58	$\begin{vmatrix} 23.86 \\ 24.28 \\ 24.70 \end{vmatrix}$	57 58 59
$\frac{60}{61}$	$\frac{54.81}{55.73}$	$\frac{24.40}{24.81}$	$\frac{54.71}{55.62}$	$\frac{24.64}{25.05}$	54.60	24.88	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\frac{25.12}{25.54}$	$\begin{array}{ c c }\hline 60 \\ \hline 61 \\ \hline \end{array}$
62 63	56.64 57.55	25.22 25.62	56.53 57.44	25.46 25.88	55.51 56.42 57.33	$\begin{vmatrix} 25.30 \\ 25.71 \\ 26.13 \end{vmatrix}$	$\begin{vmatrix} 56.30 \\ 57.21 \end{vmatrix}$	25.96 26.38	62 63
64 65 66	$\begin{vmatrix} 58.47 \\ 59.38 \\ 60.29 \end{vmatrix}$	26.03 26.44 26.84	58.35 59.26 60.18	$egin{array}{c cccc} 59.26 & 26.70 \ 60.18 & 27.11 \ 61.09 & 27.52 \ \end{array}$		$\begin{vmatrix} 26.54 \\ 26.96 \\ 27.37 \end{vmatrix}$	58.12 59.03 59.94	$\begin{vmatrix} 26.79 \\ 27.21 \\ 27.63 \end{vmatrix}$	64 65 66
67 68	$\begin{vmatrix} 61.21 \\ 62.12 \end{vmatrix}$	27.25 27.66	$61.09 \\ 62.00$	$27.52 \\ 27.93$	$\begin{vmatrix} 60.06 \\ 60.97 \\ 61.88 \end{vmatrix}$	$\begin{bmatrix} 27.78 \\ 28.20 \end{bmatrix}$	60.85  $ 61.75 $	28.05 28.47	67 68
69 70	$\begin{bmatrix} 63.03 \\ 63.95 \\ \hline 34.00 \end{bmatrix}$	$\frac{28.06}{28.47}$	$\frac{62.91}{63.82}$	$   \begin{array}{r}     28.34 \\     28.75 \\     \hline     00.10 \\   \end{array} $	$\begin{array}{ c c c }\hline 62.79 \\ 63.70 \\ \hline \hline & & & & \\ \hline \end{array}$	$     \begin{array}{ c c c c c c c c c c c c c c c c c c c$	62.66 $63.57$	$\frac{28.89}{29.31}$	69 70
71 72 73	$\begin{vmatrix} 64.86 \\ 65.78 \\ 66.69 \end{vmatrix}$	28.88 29.28 29.69	64.74 65.65 66.56	29.16 29.57 29.98	$\begin{vmatrix} 64.61 \\ 65.52 \\ 66.43 \end{vmatrix}$	$oxed{29.44} \ 29.86 \ 30.27$	64.48 65.39 66.29	29.72 30.14 30.56	71 72 73
74 75 76	67.60	$\frac{30.10}{30.51}$	67.47	$\begin{vmatrix} 30.39 \\ 30.80 \end{vmatrix}$	67.34  $ 68.25 $	$30.69 \\ 31.10$	67.20  $ 68.11 $	30.98	74 75
77 78	$\begin{vmatrix} 69.43 \\ 70.34 \\ 71.26 \end{vmatrix}$	$\begin{vmatrix} 30.91 \\ 31.32 \\ 31.73 \end{vmatrix}$	$\begin{vmatrix} 69.29 \\ 70.21 \\ 71.12 \end{vmatrix}$	$\begin{vmatrix} 31.21 \\ 31.63 \\ 32.04 \end{vmatrix}$	$\begin{bmatrix} 69.16 \\ 70.07 \\ 70.98 \end{bmatrix}$	$\begin{vmatrix} 31.52 \\ 31.93 \\ 32.35 \end{vmatrix}$	69.02 69.93 70.84	$\begin{vmatrix} 31.82 \\ 32.24 \\ 32.66 \end{vmatrix}$	76 77 78
79 80	72.17 $73.08$	$\frac{32.13}{32.54}$	72.03 $72.94$	$\frac{32.45}{32.86}$	$\begin{vmatrix} 71.89 \\ 72.80 \end{vmatrix}$	32.76 33.18	71.74 $72.65$	$\frac{33.07}{33.49}$	79 80
81 82 83	74.00 74.91 75.82	32.95 33.35 33.76	73.85 74.76 75.68	$     \begin{array}{r}       33.27 \\       33.68 \\       34.09     \end{array} $	73.71 $74.62$ $75.53$	$     \begin{array}{r}       33.59 \\       34.00 \\       34.42     \end{array} $	73.56 74.47 75.38	33.91 $34.33$ $34.75$	81 82 83
84 85	76.74	$34.17 \\ 34.57$	76.59	$34.50 \\ 34.91$	76.44	$\frac{34.83}{35.25}$	76.28 77.19	35.17 35.59	84 85
86 87 88	78.56 79.48 80.39	$\begin{vmatrix} 34.98 \\ 35.39 \\ 35.79 \end{vmatrix}$	78.41 $79.32$ $80.24$	$\begin{vmatrix} 35.32 \\ 35.73 \\ 36.14 \end{vmatrix}$	78 26 79.17 80.08	$\begin{vmatrix} 35.66 \\ 36.08 \\ 36.49 \end{vmatrix}$	$\begin{vmatrix} 78.10 \\ 79.01 \\ 79.92 \end{vmatrix}$	$\begin{vmatrix} 36.00 \\ 36.42 \\ 36.84 \end{vmatrix}$	86 87 88
89 90	$   \begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\frac{36.20}{36.61}$	$81.15 \\ 82.06$	$\frac{36.55}{36.96}$	80.99 81.90	$   \begin{vmatrix}     36.91 \\     37.32   \end{vmatrix} $	$   \begin{array}{r}     80.82 \\     81.73   \end{array} $	$\frac{37.26}{37.68}$	89 90
91 92	83.13	37.01	82.97	37.38	82.81 83.72	37.74 38.15	82.64	38.10 $38.52$	91 92
93 94 95	84.96 85.87 86.79	37.83 38.23 38.64	84.79 85.71 86.62	$\begin{vmatrix} 38.20 \\ 38.61 \\ 39.02 \end{vmatrix}$	84.63 85.54 86.45	$   \begin{array}{c}     38.57 \\     38.98 \\     39.40   \end{array} $	$\begin{vmatrix} 84.46 \\ 85.37 \\ 86.27 \end{vmatrix}$	38.94 39.35 39.77	93 94 95
96 97	87.70 88.61	39.05 39.45	87.53 88.44	$\frac{39.43}{39.84}$	87.36 88.27	39.81 40.23	87.18 88.09	40.19	96 97
98 99 100	89.53 90.44 91.35	$   \begin{array}{r}     39.86 \\     40.27 \\     40.67   \end{array} $	89.35 90.26 91.18	$\begin{array}{c c} 40.25 \\ 40.66 \\ 41.07 \end{array}$	89.18 90.09 91.00	40.64 41.05 41.47	89.00 89.91 90.81	$41.03 \\ 41.45 \\ 41.87$	$\begin{array}{c} 98 \\ 99 \\ 100 \end{array}$
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
Dist	66 I	eg.	65¾ ]	Deg.	65½	Deg.	654 ]	Deg.	Distance.
	]	10*		1					

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	Distance.	25	Deg.	251	Deg.	25½	Deg.	<i>2</i> 5¾	Deg.	Distance.
ı	nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
	1	0.91	0.42	0.90	0.43	0.90	0.43	0.90	0.43	1
	2	1.81	0.85	1.81	0.85	1.81	0.86	1.80	0.87	2
	3	2.72	1.27	2.71	1.28	2.71	1.29	2.70	1.30	3
	4	3.63	1.69	3.62	1.71	3.61	1.72	3.60	1.74	4
	5	4.53	2.11	4.52	2.13	4.51	2.15	4.50	2.17	5
	6	5.44	2.54	5.43	2.56	5.42	2.58	5.40	2.61	6
	7	6.34	2.96	6.33	2.99	6.32	3.01	6.30	3.04	7
	8	7.25	3.38	7.24	3.41	7.22	3.44	7.21	3.48	8
	9	8.16	3.80	8.14	3.84	8.12	3.87	8.11	3.91	9
	10	9.06	4.23	9.04	4.27	9.03	4.31	9.01	4.34	10
	11	9.97	4.65	9.95	4.69	9.93	4.74	9.91	4.78	11
	12	10.88	5.07	10.85	5.12	10.83	5.17	10.81	5.21	12
	13	11.78	5.49	11.76	5.55	11.73	5.60	11.71	5.65	13
	14	12.69	5.92	12.66	5.97	12.64	6.03	12.61	6.08	14
	15	13.59	6.34	13.57	6.40	13.54	6.46	13.51	6.52	15
	16	14.50	6.76	14.47	6.83	14.44	6.89	14.41	6.95	16
	17	15.41	7.18	15.38	7.25	15.34	7.32	15.31	7.39	17
	18	16.31	7.61	16.28	7.68	16.25	7.75	16.21	7.82	18
	19	17.22	8.03	17.18	8.10	17.15	8.18	17.11	8.25	19
	20	18.13	8.45	18.09	8.53	18.05	8.61	18.01	8.69	20
6/4/2	21	19.03	8.87	18.99	8.96	18.95	9.04	18.91	9.12	21
	22	19.94	9.30	19.90	9.38	19.86	9.47	19.82	9.56	22
	23	20.85	9.72	20.80	9.81	20.76	9.90	20.72	9.99	23
	24	21.75	10.14	21.71	10.24	21.66	10.33	21.62	10.43	24
	25	22.66	10.57	22.61	10.66	22.56	10.76	22.52	10.86	25
	26	23.56	10.99	23.52	11.09	23.47	11.19	23.42	11.30	26
	27	24.47	11.41	24.42	11.52	24.37	11.62	24.32	11.73	27
	28	25.38	11.83	25.32	11.94	25.27	12.05	25.22	12.16	28
	29	26.28	12.26	26.23	12.37	26.17	12.48	26.12	12.60	29
	30	27.19	12.68	27.13	12.80	27.08	12.92	27.02	13.03	30
	31	28.10	13.10	28.04	13.22	27.98	13.35	27.92	13.47	31
	32	29.00	13.52	28.94	13.65	28.88	13.78	28.82	13.90	32
	33	29.91	13.95	29.85	14.08	29.79	14.21	29.72	14.34	33
	34	30.31	4.37	30.75	14.50	30.69	14.64	30.62	14.77	34
	35	31.72	14.79	31.66	14.93	31.59	15.07	31.52	15.21	35
	36	32.63	15.21	32.56	15.36	32.49	15.50	32.43	15.64	36
	37	33.53	15.64	33.46	15.78	33.40	15.93	33.33	16.07	37
	38	34.44	16.06	34.37	16.21	34.30	16.36	34.23	16.51	38
	39	35.35	16.48	35.27	16.64	35.20	16.79	35.13	16.94	39
	40	36.25	16.90	36.18	17.06	36.10	17.22	36.03	17.38	40
	41	37.16	17.33	37.08	17.49	37.01	17.65	36.93	17.81	41
	42	38.06	17.75	37.99	17.92	37.91	18.08	37.83	18.25	42
	43	38.97	18.17	38.89	18.34	38.81	18.51	38.73	18.68	43
	44	39.88	18.60	39.80	18.77	39.71	18.94	39.63	19.12	44
	45	40.78	19.02	40.70	19.20	40.62	19.37	40.53	19.55	45
	46	41.69	19.44	41.60	19.62	41.52	19.80	41.43	19.98	46
	47	42.60	19.86	42.51	20.05	42.42	20.23	42.33	20.42	47
	48	43.50	20.29	43.41	20.48	43.32	20.66	43.23	20.85	48
	49	44.41	20.71	44.32	20.90	44.23	21.10	44.13	21.29	49
	50	45.32	21.13	45.22	21.33	45.13	21.53	45.03	21.72	50
	Distance.	Dep. 65	Lat. Deg.	Dep. 643	Lat. Deg.	Dep. 64½	Lat. Deg.	Dep. 641	Lat. Deg.	Distance.

ABLE.

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Distance.	25 I	Deg.	$25\frac{1}{4}$	Deg.	251/2	Deg.	253	Deg.	Distance.
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce
51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 70 71 72 73 74 75 76 77 78 79	46.22         47.13         48.93         49.85         50.75         51.66         52.57         53.47         54.38         55.28         56.19         57.10         58.91         59.82         60.72         61.63         62.54         63.44         64.35         65.25         66.16         67.07         67.97         68.88         69.79         70.69         71.60	21.55 21.98 22.40 22.82 23.24 23.67 24.09 24.51 24.93 25.36 25.78 26.20 26.62 27.05 27.47 27.89 28.32 28.74 29.16 29.58 30.01 30.43 30.85 31.27 31.70 32.12 32.54 32.96 33.39	46.13         47.03         47.94         48.84         49.74         50.65         51.55         52.46         53.36         54.27         55.17         56.08         56.98         57.89         59.69         60.60         61.50         62.41         63.31         64.22         66.03         67.83         68.74         69.64         70.55         71.45	21.75 22.18 22.61 23.03 23.46 23.89 24.31 24.74 25.17 25.59 26.02 26.45 26.87 27.30 27.73 28.15 28.58 29.01 29.43 29.86 30.29 30.71 31.57 31.99 32.42 32.85 33.27 33.70	46.03 46.93 47.84 48.74 49.64 50.54 51.45 52.35 53.25 54.16 55.06 56.86 57.77 59.57 60.47 61.38 62.28 63.18 64.08 64.99 65.89 66.79 67.69 68.60 70.40 71.30	21.96 22.39 22.82 23.25 23.68 24.11 24.54 24.97 25.40 25.83 26.26 26.69 27.12 27.55 27.98 28.41 29.27 29.71 30.14 30.57 31.43 31.86 32.29 32.72 33.15 33.58 34.01	45.94       46.84       47.74       48.64       49.54       50.44       51.34       52.24       53.14       54.94       56.74       57.64       58.55       60.35       61.25       63.05       63.95       64.85       67.55       68.45       70.25       71.16	22.16 22.59 23.03 23.46 23.89 24.33 24.76 25.20 25.63 26.07 26.50 26.50 26.50 27.37 27.80 28.24 29.54 29.54 29.54 29.98 30.41 30.85 31.71 32.15 32.58 33.45 33.89 34.32	51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79
80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100	$\begin{array}{r} 72.50 \\ \hline 73.41 \\ 74.32 \\ 75.22 \\ 76.13 \\ 77.04 \\ 77.94 \\ 78.85 \\ 79.76 \\ 80.66 \\ 81.57 \\ \hline 82.47 \\ 83.38 \\ 84.29 \\ 85.19 \\ 86.10 \\ 87.01 \\ 87.91 \\ 88.82 \\ 89.72 \\ 90.63 \\ \hline\end{array}$	33.81 34.23 34.65 35.08 35.50 35.50 35.92 36.35 36.77 37.19 37.61 38.04 38.46 38.88 39.30 39.73 40.15 40.57 40.99 41.42 41.84 42.26	72.36 73.26 74.17 75.07 75.97 76.88 77.78 78.69 79.59 80.50 81.40 82.31 83.21 84.11 85.02 85.92 86.83 87.73 88.64 89.54 90.45	34.13 34.55 34.98 35.41 35.83 36.26 36.68 37.11 37.54 37.96 38.39 38.82 39.24 39.67 40.10 40.52 40.95 41.38 41.80 42.23 42.66	72.21 73.11 74.01 75.82 76.72 77.62 78.52 79.43 80.33 81.23 82.14 83.04 83.94 84.84 85.75 86.65 87.55 88.45 89.36 90.26	34.44 34.87 35.30 35.73 36.16 36.59 37.02 37.45 37.88 38.32 38.75 39.61 40.04 40.47 40.90 41.33 41.76 42.19 42.62 43.05	72.96 72.96 73.86 74.76 75.66 76.56 77.46 79.26 80.16 81.06 81.96 82.86 83.76 84.67 85.57 86.47 87.37 88.27 89.17 90.07	34.76 35.19 35.62 36.06 36.49 36.93 37.36 37.80 38.23 38.67 39.10 39.53 39.97 40.40 40.84 41.27 41.71 42.14 42.58 43.44	80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100
Distance.	Dep. 65	Lat. Deg.	Dep. 6434	Lat. Deg.	Dep. 64½	Lat. Deg.	Dep. 641	Lat. Deg.	Distance.

	1		11		Ti.		11		
Distance	26	Deg.	264	Deg.	261	Deg.		Deg.	Distance.
1		Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce
1 2 3 4 5 6 7 8 9	3.60	0.44 0.88 1.32 1.75 2.19 2.63 3.07 3.51 3.95	0.90 1.79 2.69 3.59 4.48 5.38 6.28 7.17 8.07	0.44 0.88 1.33 1.77 2.21 2.65 3.10 3.54 3.98	0.89 1.79 2.68 3.58 4.47 5.37 6.26 7.16 8.05	0.45 0.89 1.34 1.78 2.23 2.68 3.12 3.57 4.02	0.89 1.79 2.68 3.57 4.46 5.36 6.25 7.14 8.04	0.45 0.90 1.35 1.80 2.25 2.70 3.15 3.60 4.05	1 2 3 4 5 6 7 8 9
$\frac{10}{11}$	$\begin{array}{ c c }\hline 8.99\\\hline 9.89\end{array}$	$\begin{array}{ c c }\hline 4.38 \\ \hline 4.82 \\ \hline \end{array}$	$\frac{8.97}{9.87}$	$\frac{4.42}{4.87}$	$\frac{8.95}{9.84}$	4.46	8.93	4.50	10
12 13 14 15 16 17 18 19 20	10.79 11.68 12.58 13.48 14.38 15.28 16.18 17.08 17.98	5.26 5.70 6.14 6.58 7.01 7.45 7.89 8.33 8.77	10.76 11.66 12.56 13.45 14.35 15.25 16.14 17.04 17.94	5.31 5.75 6.19 6.63 7.08 7.52 7.96 8.40 8.85	9.84 10.74 11.63 12.53 13.42 14.32 15.21 16.11 17.00 17.90	4.91 5.35 5.80 6.25 6.69 7.14 7.59 8.03 8.48 8.92	$ \begin{vmatrix} 9.82 \\ 10.72 \\ 11.61 \\ 12.50 \\ 13.39 \\ 14.29 \\ 15.18 \\ 16.07 \\ 16.97 \\ 17.86 $	4.95 5.40 5.85 6.30 6.75 7.20 7.65 8.10 8.55 9.60	11 12 13 14 15 16 17 18 19 20
21 22 23 24 25 26 27 28 29 30	$\begin{array}{c} 18.87 \\ 19.77 \\ 20.67 \\ 21.57 \\ 22.47 \\ 23.37 \\ 24.27 \\ 25.17 \\ 26.06 \\ 26.96 \end{array}$	$\begin{array}{r} 9.21 \\ 9.64 \\ 10.08 \\ 10.52 \\ 10.96 \\ 11.40 \\ 11.84 \\ 12.27 \\ 12.71 \\ 13.15 \end{array}$	$\begin{array}{c} 18.83 \\ 19.73 \\ 20.63 \\ 21.52 \\ 22.42 \\ 23.32 \\ 24.22 \\ 25.11 \\ 26.01 \\ 26.91 \end{array}$	9.29 9.73 10.17 10.61 11.06 11.50 11.94 12.38 12.83 13.27	$\begin{array}{ c c c c }\hline 18.79 \\ 19.69 \\ 20.58 \\ 21.48 \\ 22.37 \\ 23.27 \\ 24.16 \\ 25.06 \\ 25.95 \\ 26.85 \\ \hline \end{array}$	9.37 9.82 10.26 10.71 11.15 11.60 12.05 12.49 12.94 13.39	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	9.45 9.90 10.35 10.80 11.25 11.70 12.15 12.60 13.05 13.50	21 22 23 24 25 26 27 28 29 30
31 32 33 34 35 36 37 38 39 40	27.86 28.76 29.66 30.56 31.46 32.36 33.26 34.15 35.05 35.95	13.59 14.03 14.47 14.90 15.34 15.78 16.22 16.66 17.10 17.53	27.80 28.70 29.60 30.49 31.39 32.29 33.18 34.08 34.98 35.87	13.71 14.15 14.60 15.04 15.48 15.92 16.36 16.81 17.25 17.69	27.74 28.64 29.53 30.43 31.32 32.22 33.11 34.01 34.90 35.80	13.83 14.28 14.72 15.17 15.62 16.06 16.51 16.96 17.40 17.85	27.68 28.58 29.47 30.36 31.25 32.15 33.04 33.93 34.83 35.72	13.55 14.40 14.85 15.30 15.75 16.20 16.65 17.10 17.55 18.00	31 32 33 34 35 36 37 38 39 40
41 42 43 44 45 46 47 48 49 50	36.85 37.75 38.65 39.55 40.45 41.34 42.24 43.14 44.04 44.94	17.97 18.41 18.85 19.29 19.73 20.17 20.60 21.04 21.48 21.92	36.77 37.67 38.57 39.46 40.36 41.26 42.15 43.05 43.95 44.84	18.13 18.58 19.02 19.46 19.90 20.35 20.79 21.23 21.67 22.11	36.69 37.59 38.48 39.38 40.27 41.17 42.06 42.96 43.85 44.75	18.29 18.74 19.19 19.63 20.08 20.53 20.97 21.42 21.86 22.31	36.61 37.51 38.40 39.29 40.18 41.08 41.97 42.86 43.76 44.65	18.45 18.90 19.35 19.80 20.25 20.70 21.15 21.60 22.05 22.50	41 42 43 44 45 46 47 48 49 50
Distance.	Dep. 64 I	Lat.	Dep. 633 1	Lat.	$ \begin{array}{c c} \hline \text{Dep.} \\ \hline 63\frac{1}{2} \end{array} $	Lat. Deg.	Dep. 631	Lat.	Distance.

Dista	26 ]	Deg.	261	Deg.	$26\frac{1}{2}$	Deg.	26}	Deg.	Dista
ınce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ınce.
$\begin{array}{c} \text{Distance.} \\  552345567890  \\  66666667890  \\  772345577789  \\  88888890  \\  99349993  \\  88888890  \\  99349993  \\  8888899  \\  99349993  \\  8888899  \\  99349993  \\  99349993  \\  99349993  \\  99349993  \\  99349993  \\  993493  \\  993493  \\  9$	45.84 46.74 47.64 48.53 49.43 50.33 51.23 52.13 53.03 54.83 55.73 56.62 57.52 58.42 59.32 62.92 62.92 63.81 64.71 65.61 66.51 67.41 68.31 70.11 71.00 71.90 72.80 73.70 74.60 75.50 76.40 77.30 78.20 79.99 80.89 81.79 82.69 83.59	22.36         22.80         23.23         23.67         24.11         24.55         24.99         25.43         25.86         26.74         27.18         27.62         28.06         28.49         28.93         29.37         29.81         30.69         31.12         31.56         32.00         32.44         32.88         33.37         36.38	45.74         46.64         47.53         48.43         49.33         50.22         51.12         52.02         53.81         54.71         55.61         56.50         57.40         58.30         60.99         61.88         62.78         63.68         64.57         65.47         67.27         68.16         69.96         70.85         71.75         72.65         73.54         74.44         75.34         76.23         77.13         78.92         80.72         81.62         82.51         83.41	22.56 23.00 23.44 23.88 24.33 24.77 25.21 25.65 26.09 26.54 26.98 27.42 27.86 28.31 28.75 29.19 29.63 30.96 31.40 31.84 32.29 32.73 33.17 33.61 34.06 34.50 34.94 35.38 35.83 36.27 36.71 37.15 37.59 38.48 38 38.48 38 38 38 38 38 38 38 38 38 38 38 38 38	45.64         46.54         47.43         48.33         49.22         50.12         51.01         52.80         53.70         54.59         56.38         57.28         58.17         59.96         60.86         61.75         62.65         63.54         64.44         65.33         67.12         68.91         69.80         70.70         71.59         72.49         73.38         74.28         75.17         76.96         77.86         78.75         79.65         80.54         81.44         82.33         83.23	22.76 23.20 23.65 24.09 24.54 24.99 25.43 25.88 26.33 26.77 27.22 27.66 28.11 28.56 29.00 29.45 29.90 30.34 30.79 31.23 31.68 32.13 32.57 33.02 33.46 34.80 35.25 35.70 36.59 37.03 37.48 37.93 37.48 37.93 38.37 38.82 39.27 39.71 40.60 41.05 41.50	45.54 46.43 47.33 48.22 49.11 50.01 50.90 51.79 52.69 53.58 54.47 55.36 56.26 57.15 58.04 59.83 60.72 61.62 62.51 63.40 64.29 65.19 66.08 66.97 67.87 68.76 69.65 70.55 71.44 72.33 73.22 74.12 75.01 75.90 76.80 77.69 78.58 80.72 68.76 82.15 83.05	22.96 23.41 23.86 24.31 24.76 25.21 25.66 26.11 26.56 27.01 27.46 27.91 28.36 28.81 29.26 29.71 30.16 31.06 31.51 31.96 32.41 32.86 33.31 34.21 34.66 35.11 35.56 36.91 37.36 37.81 39.61 40.96 41.41 41.86	Distance.   5123 545 556 578 590   612 63 645 667 68 690   71 72 73 74 75 76 77 78 90   812 83 84 85 88 89 91 92 934
94 95 96 97 98 99	$egin{array}{c} 84.49 \\ 85.39 \\ 86.28 \\ 87.18 \\ 88.08 \\ 88.98 \\ 89.88 \\ \end{array}$	41.21 41.65 42.08 42.52 42.96 43.40 43.84	$egin{array}{c} 84.31 \\ 85.20 \\ 86.10 \\ 87.00 \\ 87.89 \\ 88.79 \\ 89.69 \\ \hline \end{array}$	$egin{array}{c} 41.58 \\ 42.02 \\ 42.46 \\ 42.90 \\ 43.34 \\ 43.79 \\ 44.23 \\ \hline \end{array}$	84.12 85.02 85.91 86.81 87.70 88.60 89.49	41.94 42.39 42.83 43.28 43.73 44.17 44.62	83.94 84.83 85.73 86.62 87.51 88.40 89.30	42.31 42.76 43.21 43.66 44.11 44.56 45.01	94 95 96 97 98 99 100
Distance.	Dep.	Lat.			Dep.	Lat.	Dep.	Lat.	Distance.
Dista	64 I	eg.	633	Deg.	631	Deg.	634	Deg.	Dista

N.	1	-	11						
Distance.	27	Deg.	274	Deg.	$27\frac{1}{2}$	Deg.	273	Deg.'	Distance
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce
1 2 3 4 5	$ \begin{array}{ c c c c } \hline 0.89 \\ 1.78 \\ 2.67 \\ 3.56 \\ 4.45 \\ \end{array} $	$\begin{array}{c} 0.45 \\ 0.91 \\ 1.36 \\ 1.82 \\ 2.27 \end{array}$	$\begin{array}{c c} 0.89 \\ 1.78 \\ 2.67 \\ 3.56 \\ 4.45 \end{array}$	$\begin{array}{ c c c c }\hline 0.46 \\ 0.92 \\ 1.37 \\ 1.83 \\ 2.29 \\ \end{array}$	$ \begin{array}{ c c c c c } \hline 0.89 \\ 1.77 \\ 2.66 \\ 3.55 \\ 4.44 \end{array} $	$\begin{array}{c c} 0.46 \\ 0.92 \\ 1.39 \\ 1.85 \\ 2.31 \end{array}$	$ \begin{array}{r} 0.88 \\ 1.77 \\ 2.65 \\ 3.54 \\ 4.42 \end{array} $	$ \begin{array}{ c c c c c } \hline 0.47 \\ 0.93 \\ 1.40 \\ 1.86 \\ 2.33 \\ \end{array} $	1 2 3 4 5
6 7 8 9 10	$\begin{bmatrix} 5.35 \\ 6.24 \\ 7.13 \\ 8.02 \\ 8.91 \end{bmatrix}$	2.72 3.18 3.63 4.09 4.54	5.33 6.22 7.11 8.00 8.89	2.75 3.21 3.66 4.12 4.58	$\begin{bmatrix} 5.32 \\ 6.21 \\ 7.10 \\ 7.98 \\ 8.87 \end{bmatrix}$	2.77 3.23 3.69 4.16 4.62	5.31 6.19 7.08 7.96 8.85	2.79 3.26 3.72 4.19 4.66	6 7 8 9 10
11 12 13 14 15 16 17	9.80 10.69 11.58 12.47 13.37 14.26 15.15	4.09 5.45 5.90 6.36 6.81 7.26 7.72	9.78 10.67 11.56 12.45 13.34 14.22	5.04 5.49 5.95 6.41 6.87 7.33	9.76 10.64 11.53 12.42 13.31 14.19	5.08 5.54 6.00 6.46 6.93 7.39	$\begin{array}{ c c c c c c }\hline 9.73 \\ 10.62 \\ 11.50 \\ 12.39 \\ 13.27 \\ 14.16 \\ \end{array}$	5.12 5.59 6.05 6.52 6.98 7.45	11 12 13 14 15 16
$ \begin{array}{c c} 18 \\ 19 \\ 20 \\ \hline 21 \end{array} $	$ \begin{array}{r} 13.13 \\ 16.04 \\ 16.93 \\ 17.82 \\ \hline 18.71 \end{array} $	$ \begin{array}{r} 7.72 \\ 8.17 \\ 8.63 \\ 9.08 \\ \hline 9.53 \end{array} $	$ \begin{array}{r} 15.11 \\ 16.00 \\ 16.89 \\ 17.78 \\ \hline 18.67 \end{array} $	7.78 8.24 8.70 9.16  9.62	$ \begin{array}{r} 15.08 \\ 15.97 \\ 16.85 \\ 17.74 \\ \hline 18.63 \end{array} $	$ \begin{array}{r} 7.85 \\ 8.31 \\ 8.77 \\ 9.23 \\ \hline 9.70 \end{array} $	$ \begin{array}{c c} 15.04 \\ 15.93 \\ 16.81 \\ 17.70 \\ \hline 19.59 \end{array} $	7.92 $8.38$ $8.85$ $9.31$	17 18 19 20
22 23 24 25	$ \begin{array}{c c} 19.60 \\ 20.49 \\ 21.38 \\ 22.28 \end{array} $	9.99 $10.44$ $10.90$ $11.35$	$ \begin{array}{c} 19.56 \\ 20.45 \\ 21.34 \\ 22.23 \end{array} $	10.07 $10.53$ $10.99$ $11.45$	$ \begin{array}{c c} 19.51 \\ 20.40 \\ 21.29 \\ 22.18 \end{array} $	10.16 $10.62$ $11.08$ $11.54$	$ \begin{array}{c c} 18.58 \\ 19.47 \\ 20.35 \\ 21.24 \\ 22.12 \end{array} $	9.78 10.24 10.71 11.17 11.64	21 22 23 24 25
26 27 28 29 30	23.17 24.06 24.95 25.84 26.73	$\begin{array}{c} 11.80 \\ 12.26 \\ 12.71 \\ 13.17 \\ 13.62 \end{array}$	$egin{array}{c} 23.11 \\ 24.00 \\ 24.89 \\ 25.78 \\ 26.67 \\ \hline \end{array}$	11.90 $12.36$ $12.82$ $13.28$ $13.74$	$egin{array}{c} 23.06 \\ 23.95 \\ 24.84 \\ 25.72 \\ 26.61 \\ \hline \end{array}$	12.01 12.47 12.93 13.39 13.85	$egin{array}{c} 23.01 \\ 23.89 \\ 24.78 \\ 25.66 \\ 26.55 \\ \hline \end{array}$	12.11 $12.57$ $13.04$ $13.50$ $13.97$	26 27 28 29 30
31 32 33 34	27.62 28.51 29.40 30.29	14.07 14.53 14.98 15.44	27.56 28.45 29.34 30.23	14.19 14.65 15.11 15.57	27.50 28.38 29.27 30.16	14.31 14.78 15.24 15.70	27.43 28.32 29.20 30.09	14.43 14.90 15.37 15.83	31 32 33 34
35 36 37 38 39	$   \begin{array}{r}     31.19 \\     32.08 \\     32.97 \\     33.86 \\     34.75   \end{array} $	15.89 $16.34$ $16.80$ $17.25$ $17.71$	$egin{array}{c} 31.12 \ 32.00 \ 32.89 \ 33.78 \ 34.67 \ \end{array}$	16.03 16.48 16.94 17.40 17.86	$egin{array}{c} 31.05 \ 31.93 \ 32.82 \ 33.71 \ 34.59 \ \end{array}$	16.16 16.62 17.08 17.55 18.01	30.97 31.86 32.74 33.63 34.51	16.30 16.76 17.23 17.69 18.16	35 36 37 38 39
$ \begin{array}{c c} 40 \\ \hline 41 \\ 42 \\ 43 \\ 44 \end{array} $	35.64 36.53 37.42 38.31	$ \begin{array}{r} 18.16 \\ \hline 18.61 \\ 19.07 \\ 19.52 \end{array} $	$ \begin{array}{r} 35.56 \\ \hline 36.45 \\ 37.34 \\ 38.23 \end{array} $	$ \begin{array}{c c} 18.31 \\ \hline 18.77 \\ 19.23 \\ 19.69 \end{array} $	$ \begin{array}{r} 35.48 \\ \hline 36.37 \\ 37.25 \\ 38.14 \end{array} $	$ \begin{array}{r} 18.47 \\ \hline 18.93 \\ 19.39 \\ 19.86 \end{array} $	$   \begin{array}{r}     35.40 \\     \hline     36.28 \\     37.17 \\     38.05   \end{array} $	$ \begin{array}{r} 18.62 \\ \hline 19.09 \\ 19.56 \\ 20.02 \end{array} $	$ \begin{array}{c c}     \hline       40 \\       \hline       41 \\       42 \\       43 \end{array} $
44 45 46 47 48	39.20 $40.10$ $40.99$ $41.88$ $42.77$	$     \begin{array}{c}       19.98 \\       20.43 \\       20.88 \\       21.34 \\       21.79     \end{array} $	$   \begin{array}{r}     39.12 \\     40.01 \\     40.89 \\     41.78 \\     42.67   \end{array} $	20.15 20.60 21.06 21.52 21.98	39.03 39.92 40.80 41.69 42.58	20.32 20.78 21.24 21.70 22.16	$   \begin{vmatrix}     38.94 \\     39.82 \\     40.71 \\     41.59   \end{vmatrix} $	20.49 20.95 21.42 21.88	44 45 46 47
49 50	$\frac{43.66}{44.55}$	$\frac{22.25}{22.70}$	$\frac{43.56}{44.45}$	$\begin{array}{c c} 21.38 \\ 22.44 \\ 22.89 \end{array}$	$\begin{array}{ c c c c c }\hline 43.58 \\ 43.46 \\ \hline 44.35 \\ \hline \end{array}$	$\begin{array}{c c} 22.10 \\ 22.63 \\ 23.09 \end{array}$	$\begin{array}{r} 42.48 \\ 43.36 \\ 44.25 \end{array}$	$\begin{array}{c} 22.35 \\ 22.82 \\ 23.28 \end{array}$	48 49 50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
Di	63 I	Deg.	$62\frac{3}{4}$ ]	Deg.	$62\frac{1}{2}$	Deg.	621	Deg.	Dis

Dista	27 ]	Deg.	274	Deg.	$27\frac{1}{2}$	Deg.	$27\frac{3}{4}$ ]	Deg.	Dista
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ınce.
Distance.   512 534 556 578 560   612 63 645 667 689 70   712 73 74 75 76 77 78 98   812 83 84 856 88 89	45.44         46.33         47.22         48.11         49.90         50.79         51.68         52.57         53.46         54.35         55.24         56.13         57.92         58.81         59.70         60.59         61.48         62.37         63.26         64.15         65.93         66.83         67.72         68.61         69.50         70.39         71.28         72.17         73.06         73.95         74.84         75.74         76.63         77.52         78.41         79.30	23.15 23.61 24.06 24.52 24.97 25.42 25.88 26.33 26.79 27.24 27.69 28.15 28.60 29.06 29.51 29.96 30.42 30.87 31.33 31.78 32.23 32.69 33.14 33.60 34.05 34.50 34.50 35.41 35.87 36.32 36.77 37.23 37.68 38.14 38.59 39.95 40.41	45.34         46.23         47.12         48.01         48.90         49.78         50.67         51.56         52.45         53.34         54.23         56.91         56.92         56.93         60.45         61.34         62.23         63.12         64.01         64.90         65.79         66.68         67.57         68.45         69.34         70.23         71.12         72.01         73.79         74.68         75.57         76.46         77.34         78.23         79.12	23.35 23.81 24.27 24.73 25.18 25.64 26.10 26.56 27.01 27.47 27.93 28.39 28.85 29.30 29.76 30.22 30.68 31.14 31.59 32.51 32.97 33.42 33.88 34.34 34.34 35.26 35.71 36.63 37.09 37.55 38.46 38.92 39.38 39.83 40.29 40.75	45.24         46.12         47.01         47.90         48.79         49.67         50.56         51.45         52.33         53.22         54.11         54.99         55.88         56.77         57.66         58.54         59.43         60.32         61.20         62.98         63.86         64.75         65.64         66.53         67.41         68.30         69.19         70.96         71.85         72.73         73.62         74.51         75.40         76.28         77.17         78.06         78.94	Dep.  23.55 24.01 24.47 24.93 25.40 25.86 26.32 26.78 27.24 27.70 28.17 28.63 29.09 29.55 30.01 30.48 30.94 31.40 31.86 32.32 32.78 33.25 33.71 34.17 34.63 35.09 35.55 36.02 36.48 36.94 37.40 37.86 38.79 39.25 39.71 40.17 40.63 41.10	45.13         46.02         46.90         47.79         48.67         49.56         50.44         51.33         52.21         53.98         54.87         55.75         56.64         57.52         58.41         59.29         61.06         61.95         62.83         63.72         64.60         65.49         66.37         67.26         68.14         69.91         70.80         71.68         72.57         73.45         74.34         75.22         76.11         76.99         77.88         78.76	23.75 24.21 24.68 25.14 25.61 26.07 26.54 27.01 27.47 27.94 28.40 28.87 29.33 29.80 30.26 30.73 31.20 31.66 32.13 32.59 33.06 33.52 33.99 34.46 34.92 35.85 36.32 36.78 37.71 38.18 39.58 40.04 40.51 40.97 41.44	Distance.   512   534   555   560   61   62   636   64   655   666   670   712   73   74   75   77   78   81   82   83   84   85   88   89
90 91 92 93 94 95 96	$\begin{array}{ c c c c c }\hline 80.19 \\ \hline 81.08 \\ 81.97 \\ 82.86 \\ 83.75 \\ 84.65 \\ 85.54 \\\hline \end{array}$	$\begin{array}{ c c c }\hline 40.86\\\hline 41.31\\\hline 41.77\\\hline 42.22\\\hline 42.68\\\hline 43.13\\\hline 43.58\\\hline \end{array}$	$\begin{array}{ c c c c }\hline 80.01 \\ \hline 80.90 \\ 81.79 \\ 82.68 \\ 83.57 \\ 84.46 \\ 85.35 \\\hline\end{array}$	$ \begin{vmatrix} 41.21 \\ 41.67 \\ 42.12 \\ 42.58 \\ 43.04 \\ 43.50 \\ 43.96 \end{vmatrix} $	$\begin{array}{ c c c c }\hline 79.83\\\hline 80.72\\81.60\\82.49\\83.38\\84.27\\85.15\\\hline\end{array}$	$\begin{array}{r} 41.56 \\ \hline 42.02 \\ 42.48 \\ 42.94 \\ 43.40 \\ 43.87 \\ 44.33 \\ \end{array}$	$\begin{array}{ c c c c c }\hline 79.65 \\ \hline 80.53 \\ 81.42 \\ 82.30 \\ 83.19 \\ 84.07 \\ 84.96 \\\hline\end{array}$	$\begin{array}{r} 41.91 \\ 42.37 \\ 42.84 \\ 43.30 \\ 43.77 \\ 44.23 \\ 44.70 \end{array}$	90 91 92 93 94 95 96
97 98 99 100	$ \begin{array}{r} 86.43 \\ 87.32 \\ 88.21 \\ 89.10 \end{array} $	44.04 44.49 44.95 45.40	$ \begin{array}{r} 86.23 \\ 87.12 \\ 88.01 \\ 88.90 \end{array} $	44.41 44.87 45.33 45.79	86.04 86.93 87.81 88.70	44.79 45.25 45.71 46.17	85.84 86.73 87.61 88.50	45.16 45.63 46.10 46.56	97 98 99 100
Distance.	Dep.         Lat.           63 Deg.         62\frac{3}{4} Deg.			Dep. 62½	Lat. Deg.	Dep. 621	Deg.	Distance.	

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Distance	28	Deg.	281	Deg.	. 28	¹ Deg.	284	Deg.	Distance.
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce
55 66 77 89	$egin{array}{c c} 1.77 \\ 2.65 \\ 3.53 \\ 4.41 \\ 5.30 \\ 6.18 \\ 7.06 \\ 7.95 \\ \end{array}$	$\begin{bmatrix} 0.94 \\ 1.41 \\ 1.88 \\ 2.35 \\ 2.82 \\ 3.29 \\ 3.76 \\ 4.23 \end{bmatrix}$	0.88 1.76 2.64 3.52 4.40 5.29 6.17 7.05 7.93	0.47 0.95 1.42 1.89 2.37 2.84 3.31 3.79 4.26	0.88 1.76 2.64 3.52 4.39 5.27 6.15 7.03 7.91	0.95 1.43 1.91 2.39 2.86 3.34 3.82 4.29	0.88 1.75 2.63 3.51 4.38 5.26 6.14 7.01 7.89	0.48 0.96 1.44 1.92 2.40 2.89 3.37 3.85 4.33	1 2 3 4 5 6 7 8 9
10 11 12 13 14 15 16 17 18 19	$\begin{array}{ c c c c c }\hline 9.71\\ 10.60\\ 11.48\\ 12.36\\ 13.24\\ 14.13\\ 15.01\\ 15.89\\ 16.78\\ \end{array}$	5.16 5.63 6.10 6.57 7.04 7.51 7.98 8.45 8.92	$\begin{array}{ c c c c c }\hline 8.81 \\ \hline 9.69 \\ 10.57 \\ 11.45 \\ 12.33 \\ 13.21 \\ 14.09 \\ 14.98 \\ 15.86 \\ 16.74 \\ \hline \end{array}$	$\begin{array}{ c c c }\hline 4.73\\\hline 5.21\\5.68\\6.15\\6.63\\7.10\\7.57\\8.05\\8.52\\8.99\\\hline\end{array}$	$\begin{array}{ c c c c c }\hline 8.79 \\ \hline 9.67 \\ 10.55 \\ 11.42 \\ 12.30 \\ 13.18 \\ 14.06 \\ 14.94 \\ 15.82 \\ 16.70 \\ \hline \end{array}$	$\begin{array}{ c c c }\hline 4.77\\\hline 5.25\\5.73\\6.20\\6.68\\7.16\\7.63\\8.11\\8.59\\9.07\\\hline\end{array}$	$\begin{array}{ c c c c c }\hline 8.77 \\ \hline 9.64 \\ 10.52 \\ 11.40 \\ 12.27 \\ 13.15 \\ 14.03 \\ 14.90 \\ 15.78 \\ 16.66 \\ \hline \end{array}$	$\begin{array}{r} 4.81 \\ \hline 5.29 \\ 5.77 \\ 6.25 \\ 6.73 \\ 7.21 \\ 7.70 \\ 8.18 \\ 8.66 \\ 9.14 \\ \end{array}$	10 11 12 13 14 15 16 17 18 19
20 21 22 23 24 25 26 27 28 29 30	$\begin{array}{c c} 17.66 \\ \hline 18.54 \\ 19.42 \\ 20.31 \\ 21.19 \\ 22.07 \\ 22.96 \\ 23.84 \\ 24.72 \\ 25.61 \\ 26.49 \\ \end{array}$	$\begin{array}{r} 9.39 \\ \hline 9.86 \\ 10.33 \\ 10.80 \\ 11.27 \\ 11.74 \\ 12.21 \\ 12.68 \\ 13.15 \\ 13.61 \\ 14.08 \\ \end{array}$	$\begin{array}{ c c c }\hline 17.62\\\hline 18.50\\\hline 19.38\\20.26\\\hline 21.14\\22.02\\22.90\\23.78\\24.66\\25.55\\26.43\\\hline \end{array}$	$\begin{array}{ c c c c }\hline 9.47\\\hline 9.94\\\hline 10.41\\\hline 10.89\\\hline 11.36\\\hline 11.83\\\hline 12.31\\\hline 12.78\\\hline 13.25\\\hline 13.73\\\hline 14.20\\\hline \end{array}$	$\begin{array}{ c c c }\hline 17.58\\\hline 18.46\\19.33\\20.21\\21.09\\21.97\\22.85\\23.73\\24.61\\25.49\\26.36\\\hline\end{array}$	9.54 10.02 10.50 10.97 11.45 11.93 12.41 12.88 13.36 13.84 14.31	17.53 18.41 19.29 20.16 21.04 21.92 22.79 23.67 24.55 25.43 26.30	9.62 10.10 10.58 11.06 11.54 12.02 12.51 12.99 13.47 13.95 14.43	20 21 22 23 24 25 26 27 28 29 30
31 32 33 34 35 36 37 38 39 40	27.37 28.25 29.14 30.02 30.90 31.79 32.67 33.55 34.43 35.32	14.55 15.02 15.49 15.96 16.43 16.90 17.37 17.84 18.31 18.78	27.31 28.19 29.07 29.95 30.83 31.71 32.59 33.47 34.35 35.24	14.67 15.15 15.62 16.09 16.57 17.04 17.51 17.99 18.46 18.93	27.24 28.12 29.00 29.88 30.76 31.64 32.52 33.39 34.27 35.15	14.79 15.27 15.75 16.22 16.70 17.18 17.65 18.13 18.61 19.09	27.18 28.06 28.93 29.81 30.69 31.56 32.44 33.32 34.19 35.07	14.91 15.39 15.87 16.35 16.83 17.32 17.80 18.28 18.76 19.24	31 32 33 34 35 36 37 38 39 40
41 42 43 44 45 46 47 48 49 50	36.20 37.08 37.97 38.85 39.73 40.62 41.50 42.38 43.26 44.15	19.25 19.72 20.19 20.66 21.13 21.60 22.07 22.53 23.00 23.47	36.12 37.00 37.88 38.76 39.64 40.52 41.40 42.28 43.16 44.04	19.41 19.88 20.35 20.83 21.30 21.77 22.25 22.72 23.19 23.67	36.03 36.91 37.79 38.67 39.55 40.43 41.30 42.18 43.06 43.94	19.56 20.04 20.52 20.99 21.47 21.95 22.43 22.90 23.38 23.86	35.95 36.82 37.70 38.58 39.45 40.33 41.21 42.08 42.96 43.84	19.72 20.20 20.68 21.16 21.64 22.13 22.61 23.09 23.57 24.05	41 42 43 44 45 46 47 48 49 50
Distance.	Dep. 62 I	Lat.	Dep. 613 1	Lat.	Dep. 61½	Lat.	Dep. 614 I	Lat.	Distance.

Distance.	28 1	Deg.	284	Deg.	28½	Deg.	283 :	Deg.	Distance
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce
51 52 53 54 55 56	45.03 45.91 46.80 47.68 48.56 49.45	23.94 24.41 24.88 25.35 25.82 26.29	44.93 45.81 46.69 47.57 48.45 49.33	24.14 24.61 25.09 25.56 26.03 26.51	44.82 45.70 46.58 47.46 48.33 49.21	24.34 24.81 25.29 25.77 26.24 26.72	44.71 45.59 46.47 47.34 48.22 49.10	24.53 25.01 25.49 25.97 26.45 26.94	51 52 53 54 55 56
57 58 59 60	$\begin{vmatrix} 50.33 \\ 51.21 \\ 52.09 \\ 52.98 \\ \hline 53.96 \end{vmatrix}$	$ \begin{array}{r} 26.76 \\ 27.23 \\ 27.70 \\ 28.17 \end{array} $	50.21 51.09 51.97 52.85	$ \begin{array}{r} 26.98 \\ 27.45 \\ 27.93 \\ 28.40 \\ \hline \end{array} $	50.09 $50.97$ $51.85$ $52.73$	$   \begin{array}{r}     27.20 \\     27.68 \\     28.15 \\     28.63 \\     \hline     \end{array} $	$ \begin{array}{r} 49.97 \\ 50.85 \\ 51.73 \\ \underline{52.60} \\ \hline \end{array} $	$ \begin{array}{r} 27.42 \\ 27.90 \\ 28.38 \\ \underline{28.86} \\ 0.24 \end{array} $	57 58 59 60
61 62 63 64 65 66 67 68 69	53.86 54.74 55.63 56.51 57.39 58.27 59.16 60.04 60.92	28.64 29.11 29.58 30.05 30.52 30.99 31.45 31.92 32.39	53.73 54.62 55.50 56.38 57.26 58.14 59.02 59.90 60.78	28.87 29.35 29.82 30.29 30.77 31.24 31.71 32.19 32.66	53.61 54.49 55.37 56.24 57.12 58.00 58.88 59.76 60.64	29.11 29.58 30.06 30.54 31.02 31.49 31.97 32.45 32.92	53.48 54.36 55.23 56.11 56.99 57.86 58.74 59.62 60.49	29.34 29.82 30.30 30.78 31.26 31.75 32.23 32.71 33.19	61 62 63 64 65 66 67 68
70 71 72 73 74 75	$\begin{array}{r} 61.81 \\ \hline 62.69 \\ 63.57 \\ 64.46 \\ 65.34 \\ 66.22 \end{array}$	32.85 33.33 33.80 34.27 34.74 35.21	$ \begin{array}{r} 61.66 \\ \hline 62.54 \\ 63.42 \\ 64.30 \\ 65.19 \\ 66.07 \end{array} $	$\begin{array}{r} 33.13 \\ \hline 33.61 \\ 34.08 \\ 34.55 \\ 35.03 \\ 35.50 \\ \end{array}$	$ \begin{array}{r} 61.52 \\ \hline 62.40 \\ 63.27 \\ 64.15 \\ 65.03 \\ 65.91 \end{array} $	33.40 33.88 34.36 34.83 35.31 35.79	$\begin{array}{r} 61.37 \\ \hline 62.25 \\ 63.12 \\ 64.00 \\ 64.88 \\ 65.75 \\ \end{array}$	$\begin{array}{r} 33.67 \\ \hline 34.15 \\ 34.63 \\ 35.11 \\ 35.59 \\ 36.07 \\ \end{array}$	70 71 72 73 74 75
76 77 78 79 80 81	$   \begin{array}{r}     67.10 \\     67.99 \\     68.87 \\     69.75 \\     70.64 \\     \hline     71.52   \end{array} $	$ \begin{array}{r} 35.68 \\ 36.15 \\ 36.62 \\ 37.09 \\ 37.56 \\ \hline 38.03 \end{array} $	$ \begin{array}{r} 66.95 \\ 67.83 \\ 68.71 \\ 69.59 \\ 70.47 \\ \hline 71.35 \end{array} $	$ \begin{array}{r} 35.97 \\ 36.45 \\ 36.92 \\ 37.39 \\ 37.87 \\ \hline 38.34 \end{array} $	$\begin{bmatrix} 66.79 \\ 67.67 \\ 68.55 \\ 69.43 \\ 70.31 \\ \hline 71.18 \end{bmatrix}$	$ \begin{array}{r} 36.26 \\ 36.74 \\ 37.22 \\ 37.70 \\ 38.17 \\ \hline 38.65 \end{array} $	$\begin{bmatrix} 66.63 \\ 67.51 \\ 68.38 \\ 69.26 \\ 70.14 \\ \hline 71.01 \\ \end{bmatrix}$	$ \begin{vmatrix} 36.56 \\ 37.04 \\ 37.52 \\ 38.00 \\ 38.48 \\ \hline 38.96 \end{vmatrix} $	$ \begin{array}{c c} 76 \\ 77 \\ 78 \\ 79 \\ 80 \\ \hline 81 \end{array} $
82 83 84 85 86 87 88 89	72.40 73.28 74.17 75.05 75.93 76.82 77.70 78.58	38.50 38.97 39.44 39.91 40.37 40.84 41.31 41.78	72.23 73.11 73.99 74.88 75.76 76.64 77.52 78.40	38.81 39.29 39.76 40.23 40.71 41.18 41.65 42.13	72.06 72.94 73.82 74.70 75.58 76.46 77.34 78.21	39.13 39.60 40.08 40.56 41.04 41.51 41.99 42.47	71.89 72.77 73.64 74.52 75.40 76.28 77.15 78.03	39.44 39.92 40.40 40.88 41.36 41.85 42.33 42.81	82 83 84 85 86 87 88 89
90 91 92 93 94 95 96 97	$\begin{array}{ c c c c }\hline 79.47\\\hline 80.35\\81.23\\82.11\\83.00\\83.88\\84.76\\85.65\\\hline\end{array}$	$\begin{array}{r} 42.25 \\ 42.72 \\ 43.19 \\ 43.66 \\ 44.13 \\ 44.60 \\ 45.07 \\ 45.54 \end{array}$	79.28 80.16 81.04 81.92 82.80 83.68 84.57 85.45	$\begin{array}{r} 42.60 \\ \hline 43.07 \\ 43.55 \\ 44.02 \\ 44.49 \\ 44.97 \\ 45.44 \\ 45.91 \\ \end{array}$	79.09 79.97 80.85 81.73 82.61 83.49 84.37 85.25	$\begin{array}{ c c c }\hline 42.94\\\hline 43.42\\43.90\\44.38\\44.85\\45.33\\45.81\\46.28\\\hline\end{array}$	$\begin{array}{ c c c c c }\hline 78.91\\\hline 79.78\\80.66\\81.54\\82.41\\83.29\\84.17\\85.04\\\hline \end{array}$	$\begin{array}{ c c c }\hline 43.29\\\hline 43.77\\\hline 44.25\\\hline 44.73\\\hline 45.21\\\hline 45.69\\\hline 46.17\\\hline 46.66\\\hline\end{array}$	90 91 92 93 94 95 96 97
98 99 100	86.53 87.41 88.29	$\begin{array}{r} 46.01 \\ 46.48 \\ 46.95 \\ \hline \end{array}$	86.33 87.21 88.09	$\begin{array}{r} 46.39 \\ 46.86 \\ 47.33 \\ \hline \end{array}$	86.12 87.00 87.88	$\begin{array}{c} 46.76 \\ 47.24 \\ 47.72 \\ \hline \end{array}$	85.92 86.80 87.67	$ \begin{array}{r} 47.14 \\ 47.62 \\ 48.10 \end{array} $	98 99 100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
Ö	62 I	eg.	613	Deg.	6112	Deg.	614	Deg.	Di

-	1	(	1						
Distance.	29	Deg.	291	Deg.	29½	Deg.	29¾	Deg.	Dist
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ance
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	0.87         1.75         2.62         3.50         4.37         5.25         6.12         7.00         7.875         9.62         10.50         11.37         12.24         13.12         13.99         14.87         15.74         16.62         17.49         18.37         19.24         20.12         20.99         21.87         22.74         23.61         24.49         25.36         26.24         27.11         27.99         28.86         29.74         30.61         31.49         32.36         36.73         37.61         38.48         39.36         40.23         41.11         41.98         42.86	Dep.  0.48 0.97 1.45 1.94 2.42 2.91 3.39 3.88 4.36 4.85 5.33 5.82 6.30 6.79 7.27 7.76 8.24 8.73 9.21 9.70 10.18 10.67 11.15 11.64 12.12 12.60 13.09 13.57 14.06 14.54 15.03 15.51 16.00 16.48 16.97 17.45 17.45 17.45 17.94 18.42 18.91 19.39 19.88 20.36 20.85 21.33 21.82 22.30 22.79 23.27 23.76	0.87 1.74 2.62 3.49 4.36 5.23 6.11 6.98 7.85 8.72 9.60 10.47 11.34 12.21 13.09 13.96 14.83 15.70 16.58 17.45 18.32 19.19 20.07 20.94 21.81 22.68 24.43 25.30 26.17 27.05 27.92 28.79 29.66 30.54 31.41 32.28 33.15 34.03 34.90 35.77 36.64 37.52 38.39 39.26 40.13 41.81 41.88 42.75	Dep.    0.49     0.49     0.98     1.47     1.95     2.44     2.93     3.42     3.91     4.40     4.89     5.37     5.86     6.35     6.84     7.33     7.82     8.80     9.77     10.26     10.75     11.24     11.73     12.22     12.70     13.68     14.17     14.66     15.15     15.64     16.61     17.59     18.08     18.57     19.06     19.54     20.03     20.52     21.01     21.99     22.48     22.97     23.45     23.94	Lat.  0.87 1.74 2.61 3.48 4.35 5.22 6.09 6.96 7.83 8.70  9.57 10.44 11.31 12.18 13.06 13.93 14.80 15.67 16.54 17.41 18.28 19.15 20.02 20.89 21.76 22.63 23.50 24.37 25.24 26.11 26.98 27.85 28.72 29.59 30.46 31.33 32.20 33.07 33.94 34.81 35.68 36.55 37.43 38.30 39.17 40.04 40.91 41.78 42.65	Dep.    0.49     0.49     0.98     1.48     1.97     2.46     2.95     3.45     3.94     4.43     4.92     5.42     5.42     5.91     6.40     6.89     7.39     7.88     8.37     8.86     9.85     10.34     10.83     11.33     11.82     12.31     12.80     13.30     13.79     14.28     14.77     15.27     15.27     15.76     16.25     16.25     17.73     18.22     19.70     20.19     20.68     21.17     21.67     22.65     23.14     23.63     24.13     24.13     24.13     24.13     25.25     26.26     27.27     27.27	Lat.  0.87 1.74 2.60 3.47 4.34 5.21 6.08 6.95 7.81 8.68 9.55 10.42 11.29 12.15 13.02 13.89 14.76 15.63 16.50 17.36 18.23 19.10 19.97 20.84 21.70 22.57 23.44 24.31 25.18 26.05 26.91 27.78 28.65 29.52 30.39 31.26 32.12 32.99 33.86 34.73 35.60 36.46 37.33 38.20 39.07 39.94 40.81 41.67 42.54	Dep.  0.50 0.99 1.49 1.98 2.48 2.98 3.47 3.97 4.47 4.96 5.46 5.95 6.45 6.45 6.45 6.95 7.44 7.94 8.44 8.93 9.92 10.42 10.92 11.41 11.91 12.41 11.91 12.41 11.91 12.41 11.91 12.41 11.91 12.41 11.91 12.41 11.91 12.41 11.91 12.41 11.91 12.41 11.91 12.41 11.91 13.40 13.89 14.89 15.38 16.	Distance. 1234567890 112314567890 21223425627890 312334356378390 412434456474849
50 300	$\frac{43.73}{\text{Dep.}}$	$\frac{24.24}{\text{Lat.}}$	$\frac{43.62}{\text{Dep.}}$	24.43 Lat.	$\frac{43.52}{\text{Dep.}}$	24.62 Lat.	$\frac{43.41}{\text{Dep.}}$	24.81 Lat.	50
Distance.	61	Deg.		Deg.		Deg.		Deg.	Distance.

Dista	29 1	Deg.	294	Deg.	29 <u>1</u>	Deg.	293	Deg.	Dista
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
Distance   512   553   556   578   559   616   626   636   645   656   6	44.61         45.48         46.35         47.23         48.10         48.98         49.85         50.73         51.60         52.48         53.35         54.23         55.10         55.98         56.85         57.72         58.60         59.47         60.35         61.22         62.10         62.97         63.85         64.72         65.60         66.47         67.35         68.22         69.09         77.84         75.22         76.97         77.84         78.72         80.46         81.34	24.73         25.21         25.69         26.18         26.66         27.15         27.63         28.12         28.60         29.09         29.57         30.06         31.51         32.00         32.48         32.97         33.45         33.94         34.42         34.91         35.39         35.88         36.85         37.33         37.82         38.30         38.78         39.27         39.75         40.24         40.72         41.69         42.18         43.63         44.12         44.60         45.09	44.50         45.37         46.24         47.11         47.99         48.86         49.73         50.60         51.48         52.35         53.22         54.09         54.97         55.84         59.33         60.20         61.07         61.95         62.82         63.69         64.56         65.44         66.31         67.18         68.93         69.80         70.57         71.54         72.42         73.29         74.16         75.91         76.78         77.65         78.52         79.40         80.27         81.14	24.92         25.41         25.90         26.39         26.87         27.36         27.85         28.34         28.83         29.81         30.29         30.78         31.27         31.76         32.25         32.74         33.23         34.69         35.18         35.67         36.16         36.65         37.14         37.62         38.11         38.60         39.09         39.58         40.56         41.04         41.53         42.51         43.98         44.46         44.95         45.44	44.39         45.26         46.13         47.00         47.87         48.74         49.61         50.48         51.35         52.22         53.09         53.96         54.83         55.70         56.57         57.44         59.18         60.92         61.80         62.67         63.54         64.41         65.28         66.15         67.02         67.89         68.76         69.63         70.50         71.37         72.24         73.11         73.98         74.85         75.72         76.59         77.46         78.33         79.20         80.94	25.11 25.61 26.10 26.59 27.08 27.58 28.07 28.56 29.05 29.55 30.04 30.53 31.02 31.52 32.01 32.50 32.99 33.48 34.47 34.96 35.45 35.45 36.44 36.93 37.92 38.41 38.90 39.39 39.89 40.38 40.87 41.36 41.86 42.35 42.84 43.83 44.81 45.30 45.80	44.28         45.15         46.01         46.88         47.75         48.62         49.49         50.36         51.22         52.96         53.83         54.70         55.56         56.43         57.30         59.91         60.77         61.64         62.51         63.38         64.25         65.11         65.98         66.85         67.72         68.59         69.46         70.32         71.19         72.06         72.93         73.80         74.67         75.53         76.40         77.27         78.14         79.87         80.74	25.31 25.80 26.80 27.29 27.79 28.28 29.28 29.77 30.27 30.27 30.27 30.27 31.26 31.76 32.25 33.25 33.74 34.24 34.74 35.23 35.73 36.22 37.72 37.71 38.21 38.70 39.20 39.70 40.69 41.68 42.18 42.67 43.67 44.66 45.65 46.15	Distance: 52 53 55 55 56 66 66 66 67 77 78 88 85 88 90 91 923
94 95 96 97 98	$egin{array}{c} 83.09 \\ 83.96 \\ 84.84 \\ 85.71 \\ 86.59 \\ \hline \end{array}$	$\begin{vmatrix} 47.51 \\ 48.00 \end{vmatrix}$	82.01 82.89 83.76 84.63 85.50 86.38		81.81 82.68 83.55 84.42 85.29 86.17	$\begin{array}{c} 46.29 \\ 46.78 \\ 47.27 \\ 47.77 \\ 48.26 \\ 48.75 \end{array}$	81.61 82.48 83.35 84.22 85.08 85.95	$\begin{vmatrix} 46.64 \\ 47.14 \\ 47.64 \\ 48.13 \\ 48.63 \\ 49.13 \\ 40.69 \end{vmatrix}$	94 95 96 97 98 99
$\frac{100}{2}$	$\frac{87.46}{\text{Dep.}}$	$\frac{48.48}{\text{Lat.}}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$		$\frac{87.04}{\text{Dep.}}$	49.24 Lat.	$\frac{86.82}{\text{Dep.}}$	$\frac{49.62}{\text{Lat.}}$	$\frac{100}{9}$
Distance.		Deg.		Deg.		Deg.		Deg.	Distance.

Dista	30 :	Deg.	301	Deg.	$30\frac{1}{2}$	Deg.	30¾	Deg.	Dista
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ınce.
Distance. 12345678910   111213141516178190   212223425627282930   3123334	Lat.  0.87 1.73 2.60 3.46 4.33 5.20 6.06 6.93 7.79 8.66  9.53 10.39 11.26 12.12 12.99 13.86 14.72 15.59 16.45 17.32 18.19 19.05 19.92 20.78 21.65 22.52 23.38 24.25 25.11 25.98 26.85 27.71 28.58 29.44	Dep.    0.50	Lat.  0.86 1.73 2.59 3.46 4.32 5.18 6.05 6.91 7.77 8.64  9.50 10.37 11.23 12.09 12.96 13.82 14.69 15.55 16.41 17.28  18.14 19.00 19.87 20.73 21.60 22.46 23.32 24.19 25.05 25.92 26.78 27.64 28.51 29.37	Dep.   0.50   1.01   1.51   2.02   2.52   3.02   3.53   4.03   4.53   5.04   5.54   6.05   6.55   7.05   7.56   8.06   8.56   9.07   9.57   10.08   10.58   11.08   11.59   12.09   12.59   13.10   13.60   14.11   15.11   15.62   16.62   17.13	Lat.  0.86 1.72 2.58 3.45 4.31 5.17 6.03 6.89 7.75 8.62  9.48 10.34 11.20 12.06 12.92 13.79 14.65 15.51 16.37 17.23  18.09 18.96 19.82 20.68 21.54 22.40 23.26 24.13 24.99 25.85 26.71 27.57 28.43 29.30	Dep.    0.51   1.02   1.52   2.03   2.54   3.05   4.06   4.57   5.08     5.58   6.09   6.60   7.11   7.61   8.12   8.63   9.14   9.64   10.15   10.66   11.17   11.67   12.18   12.69   13.20   13.70   14.21   14.72   15.23   15.73   16.24   16.75   17.26	Lat.  0.86 1.72 2.58 3.44 4.30 5.16 6.02 6.88 7.73 8.59  9.45 10.31 11.17 12.03 12.89 13.75 14.61 15.47 16.33 17.19 18.05 18.91 19.77 20.63 21.49 22.34 23.20 24.06 24.92 25.78  26.64 27.50 28.36 29.22	Dep.    0.51	Distance. 123456789101121314561781902122324525230132334
35 36 37 38 39 40	30.31 31.18 32.04 32.91 33.77 34.64	17.50 18.00 18.50 19.00 19.50 20.00	30.23 31.10 31.96 32.83 33.69 34.55	17.63 18.14 18.64 19.14 19.65 20.15	30.16 31.02 31.88 32.74 33.60 34.47	17.76 18.27 18.78 19.29 19.79 20.30	30.08 30.94 31.80 32.66 33.52 34.38	17.90 18.41 18.92 19.43 19.94 20.45	35 36 37 38 39 40
41 42 43 44 45 46 47 48 49 50	35.51 36.37 37.24 38.11 38.97 39.84 40.70 41.57 42.44 43.30	20.50 21.00 21.50 22.00 22.50 23.00 23.50 24.00 24.50 25.00	35.42 36.28 37.14 38.01 38.87 39.74 40.60 41.46 42.33 43.19	20.65 21.16 21.66 22.17 22.67 23.17 23.68 24.18 24.68 25.19	35.33 36.19 37.05 37.91 38.77 39.63 40.50 41.36 42.22 43.08	20.81 21.32 21.82 22.33 22.84 23.35 23.85 24.36 24.87 25.38	35.24 36.10 36.95 37.81 38.67 39.53 40.39 41.25 42.11 42.97	20.96 21.47 21.99 22.50 23.01 23.52 24.03 24.54 25.05 25.56	41 42 43 44 45 46 47 48 49 50
Distance.	Dep. 60 I	Lat.	Dep.   59 <sup>3</sup> / <sub>4</sub> ]	Lat. Deg.	Dep. 59½	Lat. Deg.	Dep. 594	Lat.	Distance.

		-			Constant of the Constant of th				-
Distance	30 I	Deg.	301	Deg.	301	Deg.	303	Deg.	Distance
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
51 52 53 54 55 56	44.17 45.03 45.90 46.77 47.63 48.50	25.50 26.00 26.50 27.00 27.50 28.00	44.06 44.92 45.78 46.65 47.51 48.37	25.69 26.20 26.70 27.20 27.71 28.21	43.94 44.80 45.67 46.53 47.39 48.25	25.88 26.39 26.90 27.41 27.91 28.42	43.83 44.69 45.55 46.41 47.27 48.13	26.08 26.59 27.10 27.61 28.12 28.63	51 52 53 54 55 56
57 58 59 60	$ \begin{array}{r} 49.36 \\ 50.23 \\ 51.10 \\ \underline{51.96} \\ \phantom{00000000000000000000000000000000000$	$ \begin{array}{c} 28.50 \\ 29.00 \\ 29.50 \\ 30.00 \end{array} $	$ \begin{array}{r} 49.24 \\ 50.10 \\ 50.97 \\ \underline{51.83} \\ \underline{59.60} \end{array} $	$   \begin{array}{r}     28.72 \\     29.22 \\     29.72 \\     \hline     30.23 \\     \hline     \hline     20.72 \\     \hline     \end{array} $	$ \begin{array}{r} 49.11 \\ 49.97 \\ 50.84 \\ \underline{51.70} \\ 59.56 \end{array} $	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{r} 48.99 \\ 49.85 \\ 50.70 \\ \underline{51.56} \\ \hline 59.40 \end{array} $	$ \begin{array}{r} 29.14 \\ 29.65 \\ 30.17 \\ 30.68 \\ \hline 21.10 \end{array} $	57 58 59 60
61 62 63 64 65	52.83 53.69 54.56 55.43 56.29	$   \begin{vmatrix}     30.50 \\     31.00 \\     31.50 \\     32.00 \\     32.50 $	52.69 53.56 54.42 55.29 56.15	30.73 31.23 31.74 32.24 32.75	52.56 53.42 54.28 55.14 56.01	30.96 $31.47$ $31.97$ $32.48$ $32.99$	52.42 53.28 54.14 55.00 55.86	31.19 31.70 32.21 32.72 33.23	61 62 63 64 65
66 67 68 69 70	57.16 58.02 59.89 59.76 60.62	33.00 33.50 34.00 34.50 35.00	57.01 57.88 58.74 59.60 60.47	33.25 33.75 34.26 34.76 35.26	56.87 57.73 58.59 59.45 60.31	33.50 34.01 34.51 35.02 35.53	56.72 57.58 58.44 59.30 60.16	33.75 34.26 34.77 35.28 35.79	66 67 68 69 70
71 72 73 74 75	61.49 62.35 63.22 64.09 64.95	35.50 36.00 36.50 37.00 37.50	61.33 62.20 63.06 63.92 64.79	35.77 36.27 36.78 37.28 37.78	$\begin{array}{c} 61.18 \\ 62.04 \\ 62.90 \\ 63.76 \\ 64.62 \end{array}$	36.04 36.54 37.05 37.56 38.07	61.02 61.88 62.74 63.60 64.46	36.30 36.81 37.32 37.84 38.35	71 72 73 74 75
76 77 78 79 80	65.82 66.68 67.55 68.42 69.28	38.00 38.50 39.00 39.50 40.00	65.65 66.52 67.38 68.24 69.11	38.29 38.79 39.29 39.80 40.30	65.48 66.35 67.21 68.07 68.93	38.57 39.08 39.59 40.10 40.60	65.31 66.17 67.03 67.89 68.75	38.86 39.37 39.88 40.39 40.90	76 77 78 79 80
81 82 83 84 85 86	70.15 71.01 71.88 72.75 73.61 74.48	40.50 41.00 41.50 42.00 42.50 43.00	69.97 70.83 71.70 72.56 73.43 74.29	40.81 41.31 41.81 42.32 42.82 43.32	69.79 70.65 71.52 72.38 73.24 74.10 74.96	41.11 41.62 42.13 42.63 43.14 43.65 44.16	69.61 70.47 71.33 72.19 73.05 73.91 74.77	41.41 41.93 42.44 42.95 43.46 43.97 44.48	81 82 83 84 85 86
$ \begin{array}{c c} 87 \\ 88 \\ 89 \\ 90 \\ \hline 91 \end{array} $	$ \begin{array}{r} 75.34 \\ 76.21 \\ 77.08 \\ 77.94 \\ \hline 78.81 \end{array} $	$\begin{array}{r} 43.50 \\ 44.00 \\ 44.50 \\ \underline{45.00} \\ \hline 45.50 \end{array}$	$   \begin{array}{c c}     75.15 \\     76.02 \\     76.88 \\     77.75 \\     \hline     78.61   \end{array} $	$\begin{array}{r} 43.83 \\ 44.33 \\ 44.84 \\ \hline 45.34 \\ \hline \hline 45.84 \\ \end{array}$	$   \begin{array}{r}     74.90 \\     75.82 \\     76.68 \\     77.55 \\     \hline     78.41   \end{array} $	$ \begin{array}{r} 44.10 \\ 44.66 \\ 45.17 \\ 45.68 \\ \hline 46.19 \end{array} $	$   \begin{array}{r}     75.63 \\     76.49 \\     77.35 \\     \hline     78.21   \end{array} $	$ \begin{array}{r} 44.48 \\ 44.99 \\ 45.51 \\ 46.02 \\ \hline 46.53 \end{array} $	87 88 89 90 91
92 93 94 95	$   \begin{array}{r}     79.67 \\     80.54 \\     81.41 \\     82.27   \end{array} $	$\begin{array}{c} 46.00 \\ 46.50 \\ 47.00 \\ 47.50 \end{array}$	$\begin{bmatrix} 79.47 \\ 80.34 \\ 81.20 \\ 82.06 \end{bmatrix}$	46.35 46.85 47.35 47.86	79.27 80.13 80.99 81.85	46.69 47.20 47.71 48.22	79.07 79.92 80.78 81.64	47.04 47.55 48.06 48.57	92 93 94 95
96 97 98 99 100	83.14 84.00 84.87 85.74 86.60	$egin{array}{c} 48.00 \\ 48.50 \\ 49.00 \\ 49.50 \\ 50.00 \\ \end{array}$	82.93 83.79 84.66 85.52 86.38	$egin{array}{c} 48.36 \\ 48.87 \\ 49.37 \\ 49.87 \\ 50.38 \\ \hline \end{array}$	82.72 83.58 84.44 85.30 86.16	48.72 $49.23$ $49.74$ $50.25$ $50.75$	82.50 83.36 84.22 85.08 85.94	49.08 49.60 50.11 50.62 51.13	96 97 98 99 100
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	nce.
Distance.	60	Deg.	593	Deg.	59½	Deg.	594	Deg.	Distance.

	1				11		17		
Distance	31	Deg.	314	Deg.	31	Deg.	31	deg.	Distance.
ıcė.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce
1 2 3 4 5 6 7 8 9	$ \begin{array}{ c c } \hline 1.71 \\ 2.57 \\ 3.43 \\ 4.29 \end{array} $	$\begin{array}{c c} 1.03 \\ 1.55 \\ 2.06 \\ 2.58 \\ 3.09 \\ 3.61 \end{array}$	2.56 3.42 4.27 5.13 5.98 6.84 7.69	1.04 1.56 2.08 2.59 3.11 3.63 4.15 4.67	1.71 2.56 3.41 4.26 5.12 5.97 6.82 7.67	$\begin{bmatrix} 1.04\\ 1.57\\ 2.09\\ 2.61\\ 3.13\\ 3.66\\ 4.18\\ 4.70 \end{bmatrix}$	1.70 2.55 3.40 4.25 5.10 5.95 6.80 7.65	1.05 1.58 2.10 2.63 3.16 3.68 4.21 4.74	1 2 3 4 5 6 7 8 9
10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 48 48 48 48 48 48 48 48 48		$ \begin{array}{r r} 5.15 \\ \hline 5.67 \\ 6.18 \end{array} $	8.55 9.40 10.26 11.11 11.97 12.82 13.68 14.53 15.39 16.24 17.10 17.95 18.81 19.66 20.52 21.37 22.23 23.08 23.94 24.79 25.65 26.50 27.36 28.21 29.07 29.92 30.78 31.63 32.49 33.34 34.20 35.05 37.62 38.47 39.33 40.18 41.04 41.89	5.19 5.71 6.23 6.74 7.26 7.78 8.30 8.82 9.34 9.86 10.38 10.89 11.41 11.93 12.45 12.97 13.49 14.01 14.53 15.56 16.08 16.60 17.12 17.64 18.16 18.68 19.19 19.71 20.23 20.75 21.27 21.79 22.31 22.83 23.86 24.38 24.90 25.42	$\begin{array}{ c c c c }\hline 8.53\\\hline 9.38\\\hline 10.23\\\hline 11.08\\\hline 11.94\\\hline 12.79\\\hline 13.64\\\hline 14.49\\\hline 15.35\\\hline 16.20\\\hline 17.05\\\hline 17.91\\\hline 18.76\\\hline 19.61\\\hline 20.46\\\hline 21.32\\\hline 22.17\\\hline 23.02\\\hline 23.87\\\hline 24.73\\\hline 25.58\\\hline 26.43\\\hline 27.28\\\hline 28.14\\\hline 28.99\\\hline 29.84\\\hline 30.70\\\hline 31.55\\\hline 32.40\\\hline 33.25\\\hline 34.11\\\hline 34.96\\\hline 35.81\\\hline 36.66\\\hline 37.52\\\hline 38.37\\\hline 39.22\\\hline 40.07\\\hline 40.93\\\hline 41.78\\\hline \end{array}$	$\begin{array}{ c c c }\hline 5.22\\\hline 5.75\\\hline 6.27\\\hline 6.79\\\hline 7.31\\\hline 7.84\\\hline 8.36\\8.88\\\hline\end{array}$	$\begin{array}{ c c c c c }\hline 8.50 \\ \hline 9.35 \\ 10.20 \\ 11.05 \\ 11.90 \\ 12.76 \\ 13.61 \\ 14.46 \\ 15.31 \\ 16.16 \\ 17.01 \\ \hline 17.86 \\ 18.71 \\ 19.56 \\ 20.41 \\ 21.26 \\ 22.11 \\ 22.96 \\ 23.81 \\ 24.66 \\ 25.51 \\ \hline 26.36 \\ 27.21 \\ 28.06 \\ 28.91 \\ 29.76 \\ 30.61 \\ 31.46 \\ 32.31 \\ 33.16 \\ 34.01 \\ \hline 34.86 \\ 35.71 \\ 36.57 \\ 37.42 \\ 38.27 \\ 39.12 \\ 39.97 \\ 40.82 \\ 41.67 \\ \hline \end{array}$	$\begin{array}{r} 5.26 \\ \hline 5.79 \\ 6.31 \\ 6.84 \\ 7.37 \\ 7.89 \\ 8.42 \\ 8.95 \\ 9.47 \\ 10.00 \\ 10.52 \\ \hline 11.05 \\ 11.58 \\ 12.10 \\ 12.63 \\ 13.16 \\ 13.68 \\ 14.21 \\ 14.73 \\ 15.26 \\ 15.79 \\ \hline 16.31 \\ 16.84 \\ 17.37 \\ 17.89 \\ 18.42 \\ 19.47 \\ 20.00 \\ 20.52 \\ 21.05 \\ \hline 21.57 \\ 22.10 \\ 22.63 \\ 24.21 \\ 24.73 \\ 25.26 \\ \hline \end{array}$	10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48
50	$\frac{42.86}{}$	25.75	$\frac{42.75}{}$	$\frac{25.94}{}$	42.63	26.12	$\frac{41.07}{42.52}$	$\begin{array}{c c} 25.78 \\ \hline 26.31 \end{array}$	49 50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	nce.
Dist	59 I	Deg.	58¾ I	Deg.	58½ ]	Deg.	58 <del>1</del> I	Deg.	Distance.

-	1		11		11		1		
Distance.	31	Deg.	311	Deg.	$31\frac{1}{2}$	Deg.	3134	Deg.	Dista
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81	43.72         44.57         45.43         46.29         47.14         48.00         48.86         49.72         50.57         51.43         52.29         53.14         54.86         55.72         56.57         57.43         58.29         59.14         60.00         60.86         61.72         62.57         63.43         64.29         65.14         66.00         66.86         67.72         68.57         69.43	26.27 26.78 27.30 27.81 28.33 28.84 29.36 29.87 30.39 30.90 31.42 31.93 32.45 32.45 32.96 33.48 33.99 34.51 35.02 35.54 36.05 36.57 37.08 37.60 38.11 38.63 39.14 39.66 40.17 40.69 41.20 41.72	43.60       44.46       45.31       46.17       47.02       47.88       48.73       49.58       50.44       51.29       52.15       53.00       53.86       54.71       55.57       56.42       57.28       58.13       59.84       60.70       61.55       62.41       63.26       64.12       64.97       65.83       67.54       68.39       69.25	26.46 26.98 27.49 28.01 28.53 29.05 29.57 30.09 30.61 31.13 31.65 32.16 32.68 33.20 33.72 34.24 34.76 35.28 35.80 36.31 36.83 37.35 37.87 38.39 38.91 39.95 40.46 40.98 41.50 42.02	43.48       44.34       45.19       46.04       46.90       47.75       48.60       49.45       50.31       51.16       52.01       52.86       53.72       54.57       57.13       57.98       58.83       59.68       60.54       61.39       62.24       63.10       63.95       64.80       65.65       66.51       67.36       68.21       69.06	26.65 27.17 27.69 28.21 28.24 29.26 29.78 30.30 30.83 31.35 31.87 32.39 32.92 33.44 33.96 34.48 35.01 35.53 36.05 36.57 37.10 37.62 38.14 38.66 39.19 39.71 40.23 41.28 41.80 42.32	43.37         44.22         45.92         46.77         47.62         48.47         49.32         50.17         51.87         52.72         53.57         54.42         55.27         56.98         57.82         59.52         60.37         61.23         62.08         63.78         64.63         67.18         68.03         68.88	26.84 27.36 27.89 28.42 28.94 29.47 29.99 30.52 31.05 31.57 32.10 32.63 33.15 33.68 34.20 34.73 35.26 35.78 36.31 36.83 37.36 37.89 38.41 38.94 39.47 39.99 40.52 41.04 41.57 42.10 42.62	Distance.   512 53 54 556 57 89 60 61 62 63 64 65 66 67 77 78 79 80 81 82
81 82 83 84 85 86 87 88 90	70.29 71.14 72.00 72.86 73.72 74.57 75.43 76.29 77.15	42.23 42.75 43.26 43.78. 44.29 44.81 45.32 45.84 46.35	70.10 70.96 71.81 72.67 73.52 74.38 75.23 76.09 76.94	42.54 43.06 43.58 44.10 44.61 45.13 45.65 46.17 46.69	69.06 69.92 70.77 71.62 72.47 73.33 74.18 75.03 75.88 76.74	42.32 42.84 43.37 43.89 44.41 44.93 45.46 45.98 46.50 47.02	69.73 70.58 71.43 72.28 73.13 73.98 74.83 75.68 76.53	43.15 43.68 44.20 44.73 45.25 45.78 46.31 46.83 47.36	82 83 84 85 86 87 88 89 90
91 92 93 94 95 96 97 98 99 100	78.00 78.86 79.72 80.57 81.43 82.29 83.15 84.00 84.86 85.72	46.87 47.38 47.90 48.41 48.93 49.44 49.96 50.47 50.99 51.50	77.80 78.65 79.51 80.36 81.22 82.07 82.93 83.78 84.64 85.49	47.21 47.73 48.25 48.76 49.28 49.80 50.32 50.84 51.36 51.88	77.59 78.44 79.30 80.15 81.00 81.85 82.71 83.56 84.41 85.26	47.55 48.07 48.59 49.11 49.64 50.16 50.68 51.20 51.73 52.25	77.38 78.23 79.08 79.93 80.78 81.63 82.48 83.33 84.18 85.04	47.89 48.41 48.94 49.47 49.99 50.52 51.04 51.57 52.10 52.62	91 92 93 94 95 96 97 98 99 100
. Distance.	Dep. 59 I	Lat. Deg.	Dep. 583	Lat. Deg.	Dep. 58½	Lat. Deg.	Dep. 581	Lat. Deg.	Distance.

Dist	32	Deg.	324	Deg.	$32\frac{1}{2}$	Deg.	323	Deg.	Dist
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance
1 2 3	$0.85 \\ 1.70$	$\begin{array}{ c c }\hline 0.53\\ 1.06\\ \end{array}$	$\begin{array}{ c c } \hline 0.85 \\ 1.69 \\ \hline \end{array}$	$0.53 \\ 1.07$	0.84	$\begin{array}{ c c }\hline 0.54\\ 1.07\\ \end{array}$	0.84	$\begin{array}{ c c }\hline 0.54\\ 1.08\\ \end{array}$	$\frac{1}{2}$
$\begin{vmatrix} 3 \\ 4 \end{vmatrix}$	$\begin{vmatrix} 2.54 \\ 3.39 \end{vmatrix}$		2.54 3.38	$1.60 \\ 2.13$	2.53 3.3~	$\begin{vmatrix} 1.61 \\ 2.15 \end{vmatrix}$	2.52 3.36	1.62 2.16	2 3 4
5 6	$\begin{vmatrix} 4.24 \\ 5.09 \end{vmatrix}$	2.65	$4.23 \\ 5.07$	$\begin{vmatrix} 2.67 \\ 3.20 \end{vmatrix}$	$\begin{vmatrix} 4.22 \\ 5.06 \end{vmatrix}$	$\begin{vmatrix} 2.69 \\ 3.22 \end{vmatrix}$	4.21 5.05	$\begin{vmatrix} 2.70 \\ 3.25 \end{vmatrix}$	5 6
8	5.94	$\begin{vmatrix} 3.71 \\ 4.24 \end{vmatrix}$	$5.92 \\ 6.77$	$\begin{vmatrix} 3.74 \\ 4.27 \end{vmatrix}$	5.90 6.75	$\begin{vmatrix} 3.76 \\ 4.30 \end{vmatrix}$	5.89	3.79 4.33	8
9	7.63 8.48	4.77 5.30	7.61 8.46	4.80 5.34	7.59 8.43	4.84 5.37	7.57 8.41	4.87 5.41	9 10
11 12	$9.33 \\ 10.18$	5.83 6.36	$\frac{9.30}{10.15}$	$\begin{bmatrix} 5.87 \\ 6.40 \end{bmatrix}$	$9.28 \\ 10.12$	5.91 6.45	$\begin{array}{ c c }\hline 9.25\\10.09\end{array}$	5.95 6.49	11 12
13 14	$\begin{vmatrix} 11.02 \\ 11.87 \end{vmatrix}$	6.89	10.99	$6.94 \\ 7.47$	10.96	$\begin{vmatrix} 6.98 \\ 7.52 \end{vmatrix}$	10.93 $11.77$	7.03 $7.57$	13 14
15 16	$\begin{vmatrix} 12.72 \\ 13.57 \end{vmatrix}$	7.95 8.48	$12.69 \\ 13.53$	8.00	12.65 13.49	8.06	12.62 13.46	8.11	15 16
17 18	$\begin{vmatrix} 14.42 \\ 15.26 \end{vmatrix}$	$9.01 \\ 9.54$	$  14.38 \\ 15.22  $	$9.07 \\ 9.61$	14.34 15.18	9.13 $9.67$	14.30 15.14	$9.20 \\ 9.74$	17 18
19 20	16.11 16.96	10.07 $10.60$	16.07 $16.91$	$10.14 \\ 10.67$	$16.02 \\ 16.87$	$\begin{vmatrix} 10.21 \\ 10.75 \end{vmatrix}$	$  15.98 \\ 16.82 $	$\begin{bmatrix} 10.28 \\ 10.82 \end{bmatrix}$	19 20
21 22	17.81 18.66	11.13	17.76 18.61	$11.21 \\ 11.74$	17.71 18.55	$  11.28 \\ 11.82 $	17.66 18.50	11.36 11.90	21 22
23 24	$\begin{vmatrix} 19.51 \\ 20.35 \end{vmatrix}$	$\begin{vmatrix} 12.19 \\ 12.72 \end{vmatrix}$	$\begin{array}{c} 19.45 \\ 20.30 \end{array}$	$12.27 \\ 12.81$	$19.40 \\ 20.24$	$\begin{vmatrix} 12.36 \\ 12.90 \end{vmatrix}$	19.34 20.18	12.44 $12.98$	23 24
25 26	$\begin{vmatrix} 21.20 \\ 22.05 \end{vmatrix}$	$\begin{vmatrix} 13.25 \\ 13.78 \end{vmatrix}$	$\begin{vmatrix} 21.14 \\ 21.99 \end{vmatrix}$	$13.34 \\ 13.87$	$\begin{vmatrix} 21.08 \\ 21.93 \end{vmatrix}$	$\begin{bmatrix} 13.43 \\ 13.97 \end{bmatrix}$	$21.03 \\ 21.87$	$\begin{array}{c} 13.52 \\ 14.07 \end{array}$	25 26
27 28	$\begin{bmatrix} 22.90 \\ 23.75 \end{bmatrix}$	$  14.31 \\ 14.84  $	$\begin{vmatrix} 22.83 \\ 23.68 \end{vmatrix}$	$14.41 \\ 14.94$	$22.77 \\ 23.61$	$14.51 \\ 15.04$	$\begin{vmatrix} 22.71 \\ 23.55 \end{vmatrix}$	14.61 15.15	27 28
$\begin{array}{ c c } 29 \\ 30 \\ \end{array}$	24.59 $25.44$	$15.37 \\ 15.90$	$\begin{vmatrix} 24.53 \\ 25.37 \end{vmatrix}$	$\begin{array}{c} 15.47 \\ 16.01 \end{array}$	$\begin{vmatrix} 24.46 \\ 25.30 \end{vmatrix}$	$\begin{vmatrix} 15.58 \\ 16.12 \end{vmatrix}$	$\begin{bmatrix} 24.39 \\ 25.23 \end{bmatrix}$	$\begin{array}{c} 15.69 \\ 16.23 \end{array}$	29 30
31 32	$\begin{vmatrix} 26.29 \\ 27.14 \end{vmatrix}$	$\begin{vmatrix} 16.43 \\ 16.96 \end{vmatrix}$	$26.22 \\ 27.06$	$16.54 \\ 17.08$	$26.15 \\ 26.99$	$16.66 \\ 17.19$	$26.07 \\ 26.91$	$16.77 \\ 17.31$	31 32
33 34	27.99 28.83	$  \begin{array}{c c} 17.49 \\ 18.02 \end{array}  $	$\begin{vmatrix} 27.91 \\ 28.75 \end{vmatrix}$	17.61 18.14	27.83 28.68	$17.73 \\ 18.27$	$\begin{bmatrix} 27.75 \\ 28.60 \end{bmatrix}$	17.85 18.39	$\begin{bmatrix} 33 \\ 34 \end{bmatrix}$
35 36	$29.68 \\ 30.53$	$\begin{array}{ c c }\hline 18.55\\ 19.08\\ \end{array}$	$\left  egin{array}{c} 29.60 \ 30.45 \end{array} \right $	$18.68 \\ 19.21$	$\begin{bmatrix} 29.52 \\ 30.36 \end{bmatrix}$	$18.81 \\ 19.34$	$\begin{vmatrix} 29.44 \\ 30.28 \end{vmatrix}$	18.93 19.48	35 36
37 38	$\begin{vmatrix} 31.38 \\ 32.23 \end{vmatrix}$	$\begin{bmatrix} 19.61 \\ 20.14 \end{bmatrix}$	$\begin{vmatrix} 31.29 \\ 32.14 \end{vmatrix}$	$   \begin{array}{c c}     19.74 \\     20.28   \end{array} $	$\begin{vmatrix} 31.21 \\ 32.05 \end{vmatrix}$	$19.88 \\ 20.42$	$\begin{vmatrix} 31.12 \\ 31.96 \end{vmatrix}$	$20.02 \\ 20.56$	37 38
$\begin{array}{c} 39 \\ 40 \end{array}$	$\frac{33.07}{33.92}$	$\begin{bmatrix} 20.67 \\ 21.20 \end{bmatrix}$	$\begin{vmatrix} 32.98 \\ 33.83 \end{vmatrix}$	$20.81 \\ 21.34$	$\begin{vmatrix} 32.89 \\ 33.74 \end{vmatrix}$	20.95 $21.49$	$\begin{vmatrix} 32.80 \\ 33.64 \end{vmatrix}$	21.10 21.64	39 40
41 42	$\frac{34.77}{35.62}$	$21.73 \\ 22.26$	$34.67 \\ 35.52$	21.88 22.41	$34.58 \\ 35.42$	$22.03 \\ 22.57$	$34.48 \\ 35.32$	$22.18 \ 22.72$	41 42
43 44	$36.47 \\ 37.31$	$\begin{bmatrix} 22.79 \\ 23.32 \end{bmatrix}$	$\begin{vmatrix} 36.37 \\ 37.21 \end{vmatrix}$	$\begin{bmatrix} 22.95 \\ 23.48 \end{bmatrix}$	$36.27 \\ 37.11$	$\begin{bmatrix} 23.10 \\ 23.64 \end{bmatrix}$	$\frac{36.16}{37.01}$	$\begin{bmatrix} 23.26 \\ 23.80 \end{bmatrix}$	43
45 46	$\frac{38.16}{39.01}$	23.85 24.38	$\begin{array}{c c} 38.06 \\ 38.90 \end{array}$	$24.01 \\ 24.55$	37.95 38.80	24.18 24.72	$37.85 \\ 38.69$	24.34 24.88	45 46
47 48	$   \begin{array}{c}     39.86 \\     40.71   \end{array} $	24.91 25.44	$\begin{vmatrix} 39.75 \\ 40.59 \end{vmatrix}$	25.08 25.61	$\begin{bmatrix} 39.64 \\ 40.48 \end{bmatrix}$	$25.25 \ 25.79$	$   \begin{array}{c c}     39.53 \\     40.37   \end{array} $	$\begin{bmatrix} 25.43 \\ 25.97 \end{bmatrix}$	47 48
49 50	$\frac{41.55}{42.40}$	$\begin{bmatrix} 25.97 \\ 26.50 \end{bmatrix}$	$\frac{41.44}{42.29}$	26.15 26.68	$\frac{41.33}{42.17}$	$\frac{26.33}{26.86}$	$\frac{41.21}{42.05}$	$26.51 \\ 27.05$	49 50
Distancc.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	mce.
Dist	58 I	Deg.	57 <del>3</del>	Deg.	57 <u>±</u> I	Deg.	574 ]	Deg.	Distance.
O STATE OF THE PARTY OF THE PAR	PARTICULAR		Street and	Charle Market & Michigan	4				

-			1	1					-
Dista	32 1	Deg.	321	Deg.	32½	Deg.	324	Deg.	Dista
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
Distance.   512 534 556 578 590   612 63 64 65 66 679   712 73 74 756 77 78 90   812 834 856 87 89 90	43.25         44.10         44.95         45.79         46.64         47.49         48.34         49.19         50.03         51.73         52.58         53.43         54.28         57.67         58.52         59.36         60.21         61.91         62.76         63.60         64.45         65.30         66.15         67.00         67.84         72.08         73.78         74.63         75.48         76.32	27.03 27.56 28.09 28.62 29.15 29.68 30.21 30.74 31.27 31.80 32.33 32.85 33.38 33.91 34.44 34.97 35.50 36.56 37.09 37.62 38.15 38.68 39.21 39.74 40.27 40.80 41.33 41.86 42.39 42.92 43.45 43.98 44.51 45.04 45.57 46.63 47.69	43.13         43.98         44.82         45.67         46.51         47.36         48.21         49.05         49.90         50.74         51.59         52.44         53.28         54.13         54.97         55.82         56.66         57.51         58.36         59.20         60.05         63.43         64.28         65.12         65.97         66.81         67.66         68.50         69.35         70.20         71.04         71.89         73.58         74.42         75.27         76.12	27.21 27.75 28.28 28.82 29.35 29.88 30.42 30.95 31.48 32.02 32.55 33.08 33.62 34.15 34.68 35.22 35.75 36.29 36.82 37.35 37.89 38.42 39.49 40.02 40.55 41.09 41.62 42.16 42.69 44.29 44.82 45.36 47.49 48.03	43.01         43.86         44.70         45.54         46.39         47.23         48.92         49.76         50.60         51.45         52.29         53.13         53.98         54.82         55.66         56.51         57.35         58.19         59.88         60.72         61.57         62.41         63.25         64.10         64.94         65.78         66.63         67.47         68.31         69.16         70.00         70.84         71.69         73.38         74.22         75.06         75.91	27.40         27.94         28.48         29.55         30.63         31.16         31.70         32.24         32.31         33.31         33.35.46         36.00         36.54         37.07         37.61         38.15         38.69         39.22         39.76         40.30         40.83         41.91         42.45         42.98         43.52         44.06         45.13         45.67         46.21         46.75         47.28         47.28         48.36	42.89         43.73         44.58         45.42         46.26         47.10         47.94         48.78         49.62         50.46         51.30         52.14         52.99         53.83         54.67         55.51         56.35         57.19         58.03         58.87         61.40         62.24         63.08         63.92         64.76         65.60         66.44         67.28         68.12         68.97         69.81         70.65         71.49         72.33         73.17         74.01         74.85         75.69	27.59       28.13       28.67       29.21       29.75       30.29       30.84       31.38       31.92       32.46       33.00       33.54       34.62       35.16       35.70       36.25       36.79       37.33       37.87       38.41       38.95       39.49       40.03       40.57       41.11       41.65       42.70       43.82       44.90       45.44       45.98       46.52       47.61       48.69	Distance.   51
91 92 93 94 95 96 97 98 99 100	77.17 78.02 78.87 79.72 80.56 81.41 82.26 83.11 83.96 84.80	48.22 48.75 49.28 49.81 50.34 50.87 51.40 51.93 52.46 52.99	76.96 77.81 78.65 79.50 80.34 81.19 82.04 82.88 83.73 84.57	48.56 49.09 49.63 50.16 50.69 51.23 51.76 52.29 52.83 53.36	76.75 77.59 78.44 79.28 80.12 80.97 81.81 82.65 83.50 84.34	48.89 49.43 49.97 50.51 51.04 51.58 52.12 52.66 53.19 53.73	$ \begin{vmatrix} 76.53 \\ 77.38 \\ 78.22 \\ 79.06 \\ 79.90 \\ 80.74 \\ 81.58 \\ 82.42 \\ 83.26 \\ 84.10 \end{vmatrix} $	49.23 49 77 50.31 50.85 51.39 51.93 52.47 53.02 53.56 54.10	91 92 93 94 95 96 97 98 99 100
nce.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	nce.
Distance.	58 1	Deg.	573	Deg.	57½	Deg.	574	Deg.	Distance.

Dist	33	Deg.	334	Deg.	33½	Deg.	333	Deg.	Dis
Distance.		Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
1 2 3 4 4 5 6 7 8 9	$egin{array}{c cccc} 2 & 1.68 \\ 2.52 \\ 3.35 \\ 4.19 \\ 5.03 \\ 7.58 \\ 6.71 \\ 7.55 \\ \end{array}$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	1.67	0.55 1.10 1.64 2.19 2.74 3.29 3.84 4.39 4.93 5.48	0.83 1.67 2.50 3.34 4.17 5.00 5.84 6.67 7.50 8.34	$\begin{bmatrix} 1.10 \\ 1.66 \\ 2.21 \\ 2.76 \\ 3.31 \\ 3.86 \\ 4.42 \\ 4.97 \end{bmatrix}$	0.83 1.66 2.49 3.33 4.16 4.99 5.82 6.65 7.48 8.31	1.11 1.67 2.22 2.78 3.33 3.89 4.44 5.00	1 2 3 4 5 6 7 8 9
11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36	$ \begin{array}{c} 9.23 \\ 10.06 \\ 10.90 \\ 11.74 \\ 12.58 \\ 13.42 \\ 14.26 \\ 15.10 \\ 15.93 \\ 16.77 \\ 17.61 \\ 18.45 \\ 19.29 \\ 20.13 \\ 20.97 \\ 21.81 \\ 22.64 \\ 23.48 \\ 24.32 \\ 25.16 \\ 26.00 \\ 26.84 \\ 27.68 \\ 28.51 \\ 29.35 \\ 30.19 $	5.99 6.54 7.08 7.62 8.17 8.71 9.26 9.80 10.35 10.89 11.44 11.98 12.53 13.62 14.16 14.71 15.25 15.79 16.34 16.88 17.43 17.97 18.52 19.06 19.61	9.20 10.04 10.87 11.71 12.54 13.38 14.22 15.05 15.89 16.73 17.56 18.40 19.23 20.07 20.91 21.74 22.58 23.42 24.25 25.09 25.92 26.76 27.60 28.43 29.27 30.11	6.03 6.58 7.13 7.68 8.22 8.77 9.32 9.87 10.42 10.97 11.51 12.06 12.61 13.16 13.71 14.26 14.80 15.35 15.90 16.45 17.00 17.55 18.09 18.64 19.19 19.74	8.34 9.17 10.01 10.84 11.67 12.51 13.34 14.18 15.01 15.84 16.68 17.51 18.35 19.18 20.01 20.85 21.68 22.51 23.35 24.18 25.02 25.85 26.68 27.52 28.35 29.19 30.02	6.07 6.62 7.18 7.73 8.28 8.83 9.38 9.93 10.49 11.04 11.59 12.14 12.69 13.25 13.80 14.35 14.90 15.45 16.01 16.56 17.11 17.66 18.21 18.77 19.32 19.87	8.31 9.15 9.98 10.81 11.64 12.47 13.30 14.13 14.97 15.80 16.63 17.46 18.29 19.12 19.96 20.79 21.62 22.45 23.28 24.11 24.94 25.78 26.61 27.44 28.27 29.10 29.93	5.56 6.11 6.67 7.22 7.78 8.33 8.89 9.44 10.00 10.56 11.11 11.67 12.22 12.78 13.33 13.89 14.44 15.00 15.56 16.11 16.67 17.22 17.78 18.33 18.89 19.44 20.00	10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36
37 38 39 40 41 42 43 44 45 46 47 48 49 50	31.03 31.87 32.71 33.55 34.39 35.22 36.06 36.90 37.74 38.58 39.42 40.26 41.09 41.93	20.15 20.70 21.24 21.79 22.33 22.87 23.42 23.96 24.51 25.05 25.60 26.14 26.69 27.23	30.94 31.78 32.62 33.45 34.29 35.12 35.96 36.80 37.63 38.47 39.31 40.14 40.98 41.81	20.29 20.84 21.38 21.93 22.48 23.03 23.58 24.12 24.67 25.22 25.77 26.32 26.87 27.41	30.85 31.69 32.52 33.36 34.19 35.02 35.86 36.69 37.52 38.36 39.19 40.03 40.86 41.69	20.42 20.97 21.53 22.68 22.63 23.18 23.73 24.29 24.84 25.39 25.94 26.49 27.04 27.60	30.76 31.60 32.43 33.26 34.09 34.92 35.75 36.58 37.42 38.25 39.08 39.91 40.74 41.57	20.56 21.11 21.67 22.22 22.78 23.33 23.89 24.45 25.00 25.56 26.11 26.67 27.22 27.78	37 38 39 40 41 42 43 44 45 46 47 48 49 50
Distance.	<u>Dep</u> 57 1	Lat.	Dep.   563 I	Lat.	Dep.   56½	Lat. Deg.	Dep.   56¼ I	Lat. Deg.	Distance.

100	í				1		1			
	Distance.	33 I	Deg.	<b>3</b> 31	Deg.	$33\frac{1}{2}$	Deg.	333	Deg.	Distance.
	nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep	Lat.	Dep.	nce.
Service Services	51 52	$42.77 \\ 43.61$	27.78 28.32	42.65 43.49	$27.96 \\ 28.51$	$42.53 \\ 43.36$	$\frac{28.15}{28.70}$	$42.40 \\ 43.24$	28.33 28.89	51 52
10. VIN. 40.	53	44.45	28.87	44.32	29.06	44.20	29.25	44.07	29.45	53
	54 55	$45.29 \\ 46.13$	$ \begin{array}{c c} 29.41 \\ 29.96 \end{array} $	$\frac{45.16}{46.00}$	$\frac{29.61}{30.16}$	45.03 45.86	$\begin{bmatrix} 29.80 \\ 30.36 \end{bmatrix}$	$44.90 \\ 45.73$	$30.00 \mid 30.56 \mid$	54 55
100	56 57	$\frac{46.97}{47.80}$	$\frac{30.50}{31.04}$	$\frac{46.83}{47.67}$	$\frac{30.70}{31.25}$	$46.70 \\ 47.53$	$\frac{30.91}{31.46}$	$\frac{46.56}{47.39}$	$\frac{31.11}{31.67}$	56 57
The state of the s	58 59	48.64 49.48	$\frac{31.59}{32.13}$	$\frac{48.50}{49.34}$	$\frac{31.80}{32.35}$	$\frac{48.37}{49.20}$	$\frac{32.01}{32.56}$	48.23 49.06	$\frac{32.22}{32.78}$	58 59
TABLET	60	50.32	32.68	50.18	32.90	50.03	33.12	49.89	33.33	60
Contract	$\begin{array}{c c} 61 \\ 62 \end{array}$	$51.16 \\ 52.00$	$\frac{33.22}{33.77}$	$51.01 \\ 51.85$	$\begin{array}{c c} 33.45 \\ 33.99 \end{array}$	$50.87 \\ 51.70$	$\begin{array}{c c} 33.67 \\ 34.22 \end{array}$	$50.72 \\ 51.55$	$\frac{33.89}{34.45}$	61 62
30000	63 64	52.84 53.67	$34.31 \\ 34.86$	$52.69 \\ 53.52$	$\begin{array}{c c} 34.54 \\ 35.09 \end{array}$	52.53 53.37	$\begin{bmatrix} 34.77 \\ 35.32 \end{bmatrix}$	$52.38 \\ 53.21$	$\frac{35.00}{35.56}$	63 64
SENER SPEE	65 66	54.51 55.35	$\begin{bmatrix} 35.40 \\ 35.95 \end{bmatrix}$	54.36 55.19	35.64	$54.20 \\ 55.04$	$35.88 \\ 36.43$	54.05	36.11 36.67	65 66
Name and A	67	56.19	36.49	56.03	$\begin{vmatrix} 36.19 \\ 36.74 \end{vmatrix}$	55.87	36.98	54.88	37.22	67
No. Actual	68 69	57.03 57.87	$\begin{array}{ c c c }\hline 37.04 \\ \hline 37.58 \\ \hline \end{array}$	56.87 57.70	$\begin{bmatrix} 37.28 \\ 37.83 \end{bmatrix}$	56.70 57.54	$\begin{array}{c} 37.53 \\ 38.08 \end{array}$	$56.54 \\ 57.37$	$\frac{37.78}{38.33}$	68 69
24.05	$\frac{70}{71}$	$\frac{58.71}{59.55}$	$\frac{38.12}{38.67}$	$\frac{58.54}{59.38}$	$\frac{38.38}{38.93}$	$\frac{58.37}{59.21}$	$\frac{38.64}{39.19}$	$\begin{array}{ c c }\hline 58.20\\ \hline 59.03\\ \hline \end{array}$	$\frac{38.89}{39.45}$	$\frac{70}{71}$
The Cont	72	60.38	39.21	60.21	39.48	60.04	$   \begin{array}{c c}     39.74 \\     40.29   \end{array} $	59.87	40.00	72
# 20 E 20	73 74	$\begin{array}{c} 61.22 \\ 62.06 \end{array}$	$\begin{bmatrix} 39.76 \\ 40.30 \end{bmatrix}$	$\begin{array}{c} 61.05 \\ 61.89 \end{array}$	$egin{array}{c c} 40.03 & \\ 40.57 & \\ \end{array}$	60.87 $61.71$	40.84	$\begin{bmatrix} 60.70 \\ 61.53 \end{bmatrix}$	40.56	73 74
100 CO	75 76	$62.90 \\ 63.74$	$ 40.85  \  41.39 $	$\begin{array}{c} 62.72 \\ 63.56 \end{array}$	$\begin{vmatrix} 41.12 \\ 41.67 \end{vmatrix}$	$62.54 \\ 63.38$	$\begin{vmatrix} 41.40 \\ 41.95 \end{vmatrix}$	$\begin{bmatrix} 62.36 \\ 63.19 \end{bmatrix}$	$\frac{41.67}{42.22}$	75 76
A Transfer	77	$64.58 \\ 65.42$	41.94  $ 42.48 $	$64.39 \\ 65.23$	$ \begin{array}{c} 42.22 \\ 42.77 \end{array} $	$64.21 \\ 65.04$	$ \begin{array}{c} 42.50 \\ 43.05 \end{array} $	$\begin{array}{ c c }\hline 64.02\\ 64.85\end{array}$	$\frac{42.78}{43.33}$	77
Total Section	79 80	$66.25 \\ 67.09$	$\begin{vmatrix} 43.03 \\ 43.57 \end{vmatrix}$	66.07	$\begin{vmatrix} 43.32 \\ 43.86 \end{vmatrix}$	65.88 66.71	43.60  $ 44.15 $	$65.69 \\ 66.52$	43.89 44.45	79 80
Chicago April	81	$\overline{67.93}$	44.12	67.74	44.41	67.54	44.71	67.35	45.00	81
	82 83	68.77 $69.61$	$\begin{vmatrix} 44.66 \\ 45.20 \end{vmatrix}$	68.58  $ 69.41 $	$ 44.96  \\  45.51 $	68.38 $69.21$	45.26  45.81	$\begin{vmatrix} 68.18 \\ 69.01 \end{vmatrix}$	$\begin{array}{c} 45.56 \\ 46.11 \end{array}$	82 83
Contract of	84 85	70.45 $71.29$	$\begin{vmatrix} 45.75 \\ 46.29 \end{vmatrix}$	70.25	$\left  \begin{array}{c} 46.06 \\ 46.60 \end{array} \right $	70.05	$ \begin{array}{c} 46.36 \\ 46.91 \end{array} $	69.84	$\frac{46.67}{47.22}$	84 85
and March	86 87	$72.13 \\ 72.96$	$\begin{vmatrix} 46.84 \\ 47.38 \end{vmatrix}$	71.92 $72.76$	47.15  $ 47.70 $	$71.71 \\ 72.55$	$  47.47 \\ 48.02 $	$71.51 \\ 72.34$	47.78	86 87
To Manager	88	73.80	47.93	73.59	48.25	73.38	$\begin{vmatrix} 48.57 \\ 49.12 \end{vmatrix}$	73.17 $74.00$	48.89	88
	89	$74.64 \\ 75.48$	$\begin{vmatrix} 48.47 \\ 49.02 \end{vmatrix}$	$74.43 \\ 75.27$	$ 48.80 \\ 49.35 $	$74.22 \\ 75.05$	49.67	74.83	$\begin{array}{ c c }\hline 49.45\\ 50.00\\ \hline\end{array}$	90
	91 92	76.32	49.56 50.11	$76.10 \\ 76.94$	$ \begin{array}{c} 49.89 \\ 50.44 \\ \end{array} $	75.88 76.72	50.23	75.66 76.50	50.56	91 92
	93	78.00 78.83	50.65 51.20	77.77	50.99	77.55 78.39	51.33 51.88	77.33	$\begin{bmatrix} 51.67 \\ 52.22 \end{bmatrix}$	93 94
	94 95	79.67	51.74	79.45	52.09	79.22	52.43	78.99	52.78	95
	96 97	$\begin{vmatrix} 80.51 \\ 81.35 \end{vmatrix}$	52.29	$\begin{vmatrix} 80.28 \\ 81.12 \end{vmatrix}$	52.64	$   \begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{vmatrix} 52.99 \\ 53.54 \end{vmatrix}$	79.82 80.65	53.33 53.89	96 97
	98 99	$\begin{vmatrix} 82.19 \\ 83.03 \end{vmatrix}$	$\begin{vmatrix} 53.37 \\ 53.92 \end{vmatrix}$	81.96 82.79	$\begin{vmatrix} 53.73 \\ 54.28 \end{vmatrix}$	$ 81.72 \\ 82.55$	54.09	81.48  82.32	54.45  $ 55.00 $	98
	100	83.87	$\frac{54.46}{}$	83.63	54.83	$\frac{83.39}{}$	$\frac{55.19}{7}$	83.15	55.56	$\frac{100}{2}$
	Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	Dist	57	Deg.	563	Deg.	561	Deg.	561	Deg.	Dist
			5		0	2	3			

8	1		(1	-			77		
Distance	34	Deg.	344	Deg.	34	Deg.	34	deg.	Distance.
1		Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce
1 2 3 4	$egin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{vmatrix} 1.12 \\ 1.68 \\ 2.24 \end{vmatrix}$	$ \begin{array}{c c} 0.83 \\ 1.65 \\ 2.48 \\ 3.31 \end{array} $	$ \begin{array}{c c} 0.56 \\ 1.13 \\ 1.69 \\ 2.25 \end{array} $	$ \begin{array}{ c c c c } \hline 0.82 \\ 1.65 \\ 2.47 \\ 3.30 \end{array} $	$\begin{bmatrix} 1.13 \\ 1.70 \end{bmatrix}$	$\begin{array}{c c} 1.64 \\ 2.46 \end{array}$	$\begin{bmatrix} 1.14 \\ 1.71 \end{bmatrix}$	$\frac{1}{2}$
5 6 7 8	4.97 $5.80$	$\begin{bmatrix} 3.36 \\ 3.91 \end{bmatrix}$	4.13 4.96 5.79	2.81 3.38 3.94	4.12 4.94 5.77	$oxed{ egin{array}{c} 2.83 \ 3.40 \ 3.96 \ \end{array} }$	4.11 4.93 5.75	$\begin{vmatrix} 2.85 \\ 3.42 \\ 3.99 \end{vmatrix}$	5 6 7
10	$\begin{array}{ c c }\hline 7.46\\ 8.29\end{array}$	$\begin{bmatrix} 5.03 \\ 5.59 \end{bmatrix}$	6.61 7.44 8.27	$ \begin{array}{ c c } 4.50 \\ 5.07 \\ 5.63 \end{array} $	$ \begin{array}{ c c c } \hline 6.59 \\ 7.42 \\ 8.24 \end{array} $	5.10 5.66	$\begin{bmatrix} 7.39 \\ 8.22 \end{bmatrix}$	$\begin{bmatrix} 5.13 \\ 5.70 \end{bmatrix}$	8 9 10
11 12 13 14		$ \begin{array}{ c c c } 6.15 \\ 6.71 \\ 7.27 \\ 7.83 \\ \end{array} $	$ \begin{array}{ c c c c c } 9.09 \\ 9.92 \\ 10.75 \\ 11.57 \end{array} $	6.19 6.75 7.32 7.88	$ \begin{array}{c c} 9.07 \\ 9.89 \\ 10.71 \\ 11.54 \end{array} $	$ \begin{array}{ c c } 6.80 \\ 7.36 \\ 7.93 \end{array} $	$ \begin{array}{ c c c c c } \hline 9.04 \\ 9.86 \\ 10.68 \\ 11.50 \end{array} $	$\begin{bmatrix} 6.27 \\ 6.84 \\ 7.41 \\ 7.98 \end{bmatrix}$	11 12 13 14
15 16 17 18	$\begin{vmatrix} 12.44 \\ 13.26 \\ 14.09 \\ 14.92 \end{vmatrix}$	$ \begin{array}{ c c } 8.39 \\ 8.95 \\ 9.51 \\ 10.07 \end{array} $	$\begin{array}{ c c c }\hline 12.40\\ 13.23\\ 14.05\\ 14.88\\ \hline \end{array}$	$ \begin{vmatrix} 8.44 \\ 9.00 \\ 9.57 \\ 10.13 \end{vmatrix} $	$\begin{array}{ c c c c }\hline 12.36 \\ 13.19 \\ 14.01 \\ 14.83 \\\hline \end{array}$	$\begin{vmatrix} 8.50 \\ 9.06 \\ 9.63 \\ 10.20 \end{vmatrix}$	12.32 13.15 13.97 14.79	$ \begin{vmatrix} 8.55 \\ 9.12 \\ 9.69 \\ 10.26 \end{vmatrix} $	15 16 17 18
19 20	15.75 $16.58$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$15.71 \\ 16.53$	10.69 $11.26$	$15.66 \\ 16.48$	$\begin{vmatrix} 10.76 \\ 11.33 \end{vmatrix}$	15.61 16.43	10.83	19 20
V 21 22 23 24	$ \begin{array}{c c} 17.41 \\ 18.24 \\ 19.07 \\ 19.90 \end{array} $	11.74 12.30 12.86 13.42	$ \begin{array}{c c} 17.36 \\ 18.18 \\ 19.01 \\ 19.84 \end{array} $	11.82 12.38 12.94 13.51	$\begin{vmatrix} 17.31 \\ 18.13 \\ 18.95 \\ 19.78 \end{vmatrix}$	11.89 12.46 13.03 13.59	17.25 18.08 18.90 19.72	11.97 12.54 13.11 13.68	21 22 23 24
25 26 27 28	$\begin{vmatrix} 20.73 \\ 21.55 \\ 22.38 \\ 23.21 \end{vmatrix}$	13.98 14.54 15.10 15 66	$\begin{vmatrix} 20.66 \\ 21.49 \\ 22.32 \\ 23.14 \end{vmatrix}$	$   \begin{array}{c c}     14.07 \\     14.63 \\     15.20 \\     15.76   \end{array} $	$\begin{bmatrix} 20.60 \\ 21.43 \\ 22.25 \\ 23.08 \end{bmatrix}$	14.16 14.73 15.29 15.86	$\begin{bmatrix} 20.54 \\ 21.36 \\ 22.18 \\ 23.01 \end{bmatrix}$	14.25 14.82 15.39 15.96	25 26 27 28
$\begin{array}{c} 29 \\ 30 \\ \hline \end{array}$	$\begin{vmatrix} 24.04 \\ 24.87 \\ \hline 25.70 \end{vmatrix}$	$16.22 \\ 16.78$	23.97 $24.80$	$16.32 \\ 16.88$	$\begin{vmatrix} 23.90 \\ 24.72 \end{vmatrix}$	$16.43 \\ 16.99$	$\begin{vmatrix} 23.83 \\ 24.65 \end{vmatrix}$	$16.53 \\ 17.10$	$\begin{array}{c c} 29 \\ 30 \end{array}$
31 32 33 34	$\begin{bmatrix} 25.70 \\ 26.53 \\ 27.36 \\ 28.19 \end{bmatrix}$	17.33 $  17.89 $ $  18.45 $ $  19.01$	25.62 26.45 27.28	17.45 18.01 18.57	25.55 26.37 27.20	17.56 18.12 18.69	25.47 26.29 27.11	17.67 18.24 18.81	31 32 33
35 36 37	29.02 29.85 30.67	$\begin{vmatrix} 19.57 \\ 19.57 \\ 20.13 \\ 20.69 \end{vmatrix}$	$egin{array}{c} 28.10 \ 28.93 \ 29.76 \ 30.58 \ \hline \end{array}$	$ \begin{array}{c c} 19.14 \\ 19.70 \\ 20.26 \\ 20.82 \end{array} $	$egin{array}{c} 28.02 \\ 28.84 \\ 29.67 \\ 30.49 \\ \hline \end{array}$	$ \begin{array}{c} 19.26 \\ 19.82 \\ 20.39 \\ 20.96 \end{array} $	$egin{array}{c} 27.94 \ 28.76 \ 29.58 \ 30.40 \ \end{array}$	$ \begin{array}{c} 19.38 \\ 19.95 \\ 20.52 \\ 21.00 \end{array} $	34 35 36
38 39 40	31.50 32.33 33.16	21.25 21.81 22.37	$     \begin{array}{c}       31.41 \\       32.24 \\       33.06     \end{array} $	21.39 21.95 22.51	$   \begin{array}{c}     31.32 \\     32.14 \\     32.97   \end{array} $	21.52 $22.09$ $22.66$	$\begin{vmatrix} 30.40 \\ 31.22 \\ 32.04 \\ 32.87 \end{vmatrix}$	$     \begin{bmatrix}       21.09 \\       21.66 \\       22.23 \\       22.80     \end{bmatrix} $	37 38 39 40
41 42 43	33.99 34.82 35.65	22.93 23.49 24.05	33.89 34.72 35.54	23.07 23.64 24.20	33.79 34.61 35.44	23.22 $23.79$ $24.36$	$     \begin{array}{r}       33.69 \\       34.51 \\       35.33     \end{array} $	23.37 23.94 24.51	41 42 43
44 45 46 47	36.48 37.31 38.14 38.96	24.60 25.16 25.72	36.37 37.20 38.02	$     \begin{bmatrix}     24.76 \\     25.33 \\     25.89     \end{bmatrix} $	36.26 37.09 37.91	24.92 25.49 26.05	$\begin{vmatrix} 36.15 \\ 36.97 \\ 37.80 \end{vmatrix}$	25.08 25.65 26.22	44 45 46
48 49 50	39.79 40.62 41.45	$     \begin{bmatrix}     26.28 \\     26.84 \\     27.40 \\     27.96     \end{bmatrix} $	38.85 39.68 40.50 41.33	26.45 27.01 27.58 28.14	38.73 39.56 40.38 41.21	26.62 27.19 27.75 28.32	$   \begin{vmatrix}     38.62 \\     39.44 \\     40.26 \\     41.08   \end{vmatrix} $	26.79 27.36 27.93 28.50	47 48 49 50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
Dista	56 I	Deg.	55¾ I	Deg.	55 <u>‡</u> I	Deg.	55 <del>1</del> I	Deg.	Distance.

I make the same	1		11		(martin)	2 TO 15 12 12 12 12 12 12 12 12 12 12 12 12 12			
Distance.	34	Deg.	341	Deg.	$34\frac{1}{2}$	Deg.	343	Deg.	Distance.
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
51 52 53 54 55 56	42.28 43.11 43.94 44.77 45.60 46.43	28.52 29.08 29.64 30.20 30.76 31.31	42.16 42.98 43.81 44.64 45.46 46.29	28.70 29.27 29.83 30.39 30.95 31.52	42.03 42.85 43.68 44.50 45.33 46.15	28.89 29.45 30.02 30.59 31.15 31.72	41.90 42.73 43.55 44.37 45.19 46.01	29.07 29.64 30.21 30.78 31.35 31.92	51 52 53 54 55 56
$   \begin{array}{r}     57 \\     58 \\     59 \\     \hline     60 \\     \hline     61   \end{array} $	$\begin{array}{c} 47.26 \\ 48.08 \\ 48.91 \\ 49.74 \\ \hline 50.57 \end{array}$	$ \begin{array}{c} 31.87 \\ 32.43 \\ 32.99 \\ 33.55 \\ \hline 34.11 \end{array} $	$ \begin{array}{r} 40.23 \\ 47.12 \\ 47.94 \\ 48.77 \\ 49.60 \\ \hline 50.42 \end{array} $	$ \begin{array}{c} 32.08 \\ 32.64 \\ 33.21 \\ 33.77 \\ \hline 34.33 \end{array} $	$\begin{array}{r} 46.13 \\ 46.98 \\ 47.80 \\ 48.62 \\ \hline 49.45 \\ \hline 50.27 \end{array}$	32.29 32.85 33.42 33.98 34.55	$ \begin{array}{r} 46.83 \\ 47.66 \\ 48.48 \\ \underline{49.30} \\ 50.12 \end{array} $	$   \begin{array}{r}     32.49 \\     33.06 \\     33.63 \\     \hline     34.20 \\     \hline     34.77 $	57 58 59 60 61
62 63 64 65 66	51.40 52.23 53.06 53.89 54.72	34.67 35.23 35.79 36.35 36.91	51.25 52.08 52.90 53.73 54.55	34.89 35.46 36.02 36.58 37.15	51.10 51.92 52.74 53.57 54.39	35.12 35.68 36.25 36.82 37.38	50.94 51.76 52.59 53.41 54.23	35.34 35.91 36.48 37.05 37.62	62 63 64 65 66
$ \begin{array}{c c} 67 \\ 68 \\ 69 \\ 70 \\ \hline 71 \\ 70 \end{array} $	55.55 56.37 57.20 58.03	$   \begin{vmatrix}     37.46 \\     38.03 \\     38.58 \\     \hline     39.14 \\     \hline     39.70 \\     40.26 $	55.38 56.21 57.03 57.86 59.69	37.71 38.27 38.83 39.40 39.96	55.22 56.04 56.86 57.69 58.51	37.95 38.52 39.08 39.65 40.21	55.05 55.87 56.69 57.52 58.34	$   \begin{array}{r}     38.19 \\     38.76 \\     39.33 \\     \hline     39.90 \\     \hline     40.47 \\     41.04 \\   \end{array} $	$   \begin{array}{c c}     67 \\     68 \\     69 \\     70 \\     \hline     71 \\     72 \\   \end{array} $
72 73 74 75 76 77	$   \begin{bmatrix}     59.69 \\     60.52 \\     61.35 \\     62.18 \\     63.01 \\     63.84 $	$\begin{vmatrix} 40.26 \\ 40.82 \\ 41.38 \\ 41.94 \\ 42.50 \\ 43.06 \end{vmatrix}$	59.51 60.34 61.17 61.99 62.82 63.65	$\begin{array}{c} 40.52 \\ 41.08 \\ 41.65 \\ 42.21 \\ 42.77 \\ 43.34 \end{array}$	59.34 60.16 60.99 61.81 62.63 63.46	40.78 41.35 41.91 42.48 43.05 43.61	59.16 59.98 60.80 61.62 62.45 63.27	41.04 41.61 42.18 42.75 43.32 43.89	72 73 74 75 76 77
78 79 80 81	$ \begin{array}{r} 64.66 \\ 65.49 \\ 66.32 \\ \hline 67.15 \end{array} $	$ \begin{array}{r} 43.62 \\ 44.18 \\ 44.74 \\ \hline 45.29 \end{array} $	$ \begin{array}{r} 64.47 \\ 65.30 \\ 66.13 \\ \hline 66.95 \end{array} $	$ \begin{array}{r} 43.90 \\ 44.46 \\ 45.02 \\ \hline 45.59 \end{array} $	$ \begin{array}{r} 64.28 \\ 65.11 \\ 65.93 \\ \hline 66.75 \end{array} $	$44.18  44.75  45.31  \hline 45.88$	$64.09 \\ 64.91 \\ 65.73 \\ \hline 66.55$	$44.46  45.03  45.60  \hline 46.17$	78 79 80 81
82 83 84 85 86 87	67.98 68.81 69.64 70.47 71.30 72.13	45.85 46.41 46.97 47.53 48.09 48.65	67.78 68.61 69.43 70.26 71.09 71.91	46.15 46.71 47.28 47.84 48.40 48.96	$     \begin{array}{r}       67.58 \\       68.40 \\       69.23 \\       70.05 \\       70.87 \\       71.70     \end{array} $	46.45 47.01 47.58 48.14 48.71 49.28	67.37 68.20 69.02 69.84 70.66 71.48	46.74 47.31 47.88 48.45 49.02 49.59	82 83 84 85 86 87
88 89 90 91	$ \begin{array}{r} 72.96 \\ 73.78 \\ 74.61 \\ \hline 75.44 \end{array} $	$ \begin{array}{r} 49.21 \\ 49.77 \\ 50.33 \\ \hline 50.89 \end{array} $	$ \begin{array}{ c c c c c } \hline 72.74 \\ 73.57 \\ 74.39 \\ \hline 75.22 \end{array} $	$ \begin{array}{r} 49.53 \\ 50.09 \\ 50.65 \\ \hline 51.22 \end{array} $	$ \begin{array}{r} 72.52 \\ 73.35 \\ 74.17 \\ \hline 75.00 \end{array} $	$49.84$ $50.41$ $50.98$ $\overline{51.54}$	$   \begin{array}{r}     72.30 \\     73.13 \\     73.95 \\     \hline     74.77   \end{array} $	50.16 50.73 51.30 51.87	88 89 90 91
92 93 94 95 96	76.27 77.10 77.93 78.76 79.59	51.45 52.00 52.56 53.12 53.68	76.05 76.87 77.70 78.53 79.35	51.78 52.34 52.90 53.47 54.03	75.82 $76.64$ $77.47$ $78.29$ $79.12$	52.11 52.68 53.24 53.81 54.37	75.59 76.41 77.23 78.06 78.88	52.44 53.01 53.58 54.15 54.72	92 93 94 95 96
97 98 99 100	80.42 81.25 82.07 82.90	54.24 54.80 55.36 55.92	$\begin{vmatrix} 80.18 \\ 81.01 \\ 81.83 \\ 82.66 \end{vmatrix}$	54.59 55.15 55.72 56.28	79.94 80.76 81.59 82.41	54.94 55.51 56.07 56.64	$ \begin{array}{c c} 79.70 \\ 80.52 \\ 81.34 \\ 82.16 \end{array} $	55.29 55.86 56.43 57.00	97 98 99 100
Distance.	Dep. 56 1	Lat. Deg.	Dep. 55\frac{3}{4}	Deg.	55½	Lat. Deg.	Dep. 55½	Lat. Deg.	Distance.

									-
Distance.	35	Deg.	351/4	Deg.	35½	Deg.	35∄	Deg.	Distance.
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
$\frac{1}{2}$	$\begin{array}{ c c }\hline 0.82\\ 1.64\\ \end{array}$	$0.57 \\ 1.15$	$\begin{array}{c} 0.82 \\ 1.63 \end{array}$	0.58 1.15	$\begin{array}{c} 0.81 \\ 1.63 \end{array}$	$0.58 \\ 1.16$	$0.81 \\ 1.62$	0.58 $1.17$	1 2 3
3	2.46	1.72	2.45	1.73	2.44	1.74	2.43	1.75	$\begin{vmatrix} z \\ 3 \end{vmatrix}$
4 5	$\begin{vmatrix} 3.28 \\ 4.10 \end{vmatrix}$	$2.29 \\ 2.87$	$\frac{3.27}{4.08}$	$\begin{array}{c} 2.31 \\ 2.89 \end{array}$	$\frac{3.26}{4.07}$	$\begin{bmatrix} 2.32 \\ 2.90 \end{bmatrix}$	$\frac{3.25}{4.06}$	$2.34 \\ 2.92$	4 5
6 7	4.91 5.73	3.44 4.01	$\begin{vmatrix} 4.90 \\ 5.72 \end{vmatrix}$	$\frac{3.46}{4.04}$	4.88 5.70	$\begin{bmatrix} 3.48 \\ 4.06 \end{bmatrix}$	4.87	3.51	6
8	6.55	4.59	6.53	4.62	6.51	4.65	$\begin{array}{ c c }\hline 5.68\\ 6.49\end{array}$	4.09	7 8
10	7.37 8.19	$\begin{bmatrix} 5.16 \\ 5.74 \end{bmatrix}$	$\begin{bmatrix} 7.35 \\ 8.17 \end{bmatrix}$	$5.19 \\ 5.77$	7.33 8.14	$\begin{bmatrix} 5.23 \\ 5.81 \end{bmatrix}$	$\begin{vmatrix} 7.30 \\ 8.12 \end{vmatrix}$	$\begin{array}{c c} 5.26 \\ 5.84 \end{array}$	9
11 12	9.01	6.88	8.98 9.80	$\begin{array}{c} 6.35 \\ 6.93 \end{array}$	8.96 9.77	$\begin{array}{c} 6.39 \\ 6.97 \end{array}$	$8.93 \\ 9.74$	$\frac{6.43}{7.01}$	11
13	10.65	7.46	10.62	7.50	10.58	7.55	10.55	7.60	12 13
14 15	$  \begin{array}{c} 11.47 \\ 12.29 \end{array}  $	$\begin{array}{c c} 8.03 \\ 8.60 \end{array}$	$  \begin{array}{c} 11.43 \\ 12.25 \end{array}  $	$\begin{array}{c} 8.08 \\ 8.66 \end{array}$	$\begin{array}{ c c }\hline 11.40\\12.21\end{array}$	8.13 8.71	11.36 $  12.17$	8.18	14 15
16 17	$\begin{vmatrix} 13.11 \\ 13.93 \end{vmatrix}$	$9.18 \\ 9.75$	13.07	$\begin{array}{c} 9.23 \\ 9.81 \end{array}$	13.03	9.29	12.99	9.35	16
18	14.74	10.32	$  13.88 \\ 14.70  $	10.39	$  13.84 \\ 14.65  $	$\begin{array}{c} 9.87 \\ 10.45 \end{array}$	13.80 $  14.61$	$9.93 \\ 10.52$	17 18
19 20	15.56   16.38	10.90 11.47	$\begin{vmatrix} 15.52 \\ 16.33 \end{vmatrix}$	$\begin{array}{c} 10.97 \\ 11.54 \end{array}$	$\begin{array}{ c c }\hline 15.47\\ 16.28\\ \hline\end{array}$	11.03   11.61	$\begin{array}{ c c }\hline 15.42\\ 16.23\\ \hline\end{array}$	11.10	19 20
21	$\overline{17.20}$	12.05	17.15	12.12	17.10	12.19	17.04	12.27	$\overline{21}$
22 23	$18.02 \\ 18.84$	$12.62 \\ 13.19$	$  17.97 \\ 18.78  $	$12.70 \\ 13.27$	17.91 $18.72$	$\begin{array}{c c} 12.78 \\ 13.36 \end{array}$	17.85	$12.85 \\ 13.44$	22 23
24 25	$\begin{array}{ c c }\hline 19.66 \\ 20.48\end{array}$	$\begin{array}{c} 13.77 \\ 14.34 \end{array}$	$  19.60 \\ 20.42 $	$\begin{array}{c c} 13.85 \\ 14.43 \end{array}$	$   \begin{array}{c}     19.54 \\     20.35   \end{array} $	$\begin{array}{c} 13.94 \\ 14.52 \end{array}$	$   \begin{vmatrix}     19.48 \\     20.29   \end{vmatrix} $	14.02 14.61	24
26	21.30	14.91	21.23	15.01	21.17	15.10	21.10	15.19	25 26
27 28	$\begin{vmatrix} 22.12 \\ 22.94 \end{vmatrix}$	$\begin{array}{c c} 15.49 \\ 16.06 \end{array}$	$\begin{bmatrix} 22.05 \\ 22.87 \end{bmatrix}$	$15.58 \\ 16.16$	$\begin{vmatrix} 21.98 \\ 22.80 \end{vmatrix}$	$\begin{array}{c} 15.68 \\ 16.26 \end{array}$	$\begin{vmatrix} 21.91 \\ 22.72 \end{vmatrix}$	15.77 16.36	27 28
29 30	$\begin{vmatrix} 23.76 \\ 24.57 \end{vmatrix}$	$\begin{array}{c c} 16.63 \\ 17.21 \end{array}$	$\begin{vmatrix} 23.68 \\ 24.50 \end{vmatrix}$	$16.74 \\ 17.31$	$23.61 \\ 24.42$	$\begin{bmatrix} 16.84 \\ 17.42 \end{bmatrix}$	$23.54 \\ 24.35$	$16.94 \\ 17.53$	29
31	$\overline{25.39}$	17.78	$\overline{25.32}$	17.89	$\overline{25.24}$	18.00	25.16	18.11	$\frac{30}{31}$
32 33	$\begin{vmatrix} 26.21 \\ 27.03 \end{vmatrix}$	$\begin{array}{c} 18.35 \\ 18.93 \end{array}$	$\begin{bmatrix} 26.13 \\ 26.95 \end{bmatrix}$	$\begin{array}{c} 18.47 \\ 19.05 \end{array}$	$\begin{bmatrix} 26.05 \\ 26.87 \end{bmatrix}$	$\begin{array}{ c c } 18.58 \\ 19.16 \end{array}$	$\begin{vmatrix} 25.97 \\ 26.78 \end{vmatrix}$	$18.70 \\ 19.28$	32 33
34	27.85	19.50	27.77	19.62	27.68	19.74	27.59	19.86	34
35 36	$\begin{bmatrix} 28.67 \\ 29.49 \end{bmatrix}$	$\begin{bmatrix} 20.08 \\ 20.65 \end{bmatrix}$	$\begin{bmatrix} 28.58 \\ 29.40 \end{bmatrix}$	$\begin{bmatrix} 20.20 \\ 20.78 \end{bmatrix}$	$\begin{bmatrix} 28.49 \\ 29.31 \end{bmatrix}$	$egin{array}{c c} 20.32 \ 20.91 \end{array}$	$\begin{bmatrix} 28.41 \\ 29.22 \end{bmatrix}$	$\begin{array}{c} 20.45 \\ 21.03 \end{array}$	35 36
37 38	$\begin{vmatrix} 30.31 \\ 31.13 \end{vmatrix}$	$\begin{bmatrix} 21.22 \\ 21.80 \end{bmatrix}$	$\begin{vmatrix} 30.22 \\ 31.03 \end{vmatrix}$	$\begin{bmatrix} 21.35 \\ 21.93 \end{bmatrix}$	$\begin{vmatrix} 30.12 \\ 30.94 \end{vmatrix}$	$\begin{bmatrix} 21.49 \\ 22.07 \end{bmatrix}$	$\begin{vmatrix} 30.03 \\ 30.84 \end{vmatrix}$	$\begin{array}{c} 21.62 \\ 22.20 \end{array}$	37 38
39	$\begin{vmatrix} 31.95 \\ 32.77 \end{vmatrix}$	22.37	31.85	22.51	31.75	22.65	31.65	22.79	39
$\frac{40}{41}$	$\frac{32.77}{33.59}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\frac{32.67}{33.48}$	$\begin{array}{ c c c }\hline 23.09 \\ \hline 23.66 \\ \hline \end{array}$	$\frac{32.56}{33.38}$	$\frac{23.23}{23.81}$	$\frac{32.46}{33.27}$	$\frac{23.37}{23.95}$	$\frac{40}{41}$
42 43	$\frac{34.40}{35.22}$	$\begin{vmatrix} 24.09 \\ 24.66 \end{vmatrix}$	34.30	24.24	$\frac{34.19}{35.01}$	$24.39 \\ 24.97$	34.09	24.54	42
44	36.04	25.24	35.12 35.93	$24.82 \\ 25.39$	35.82	25.55	$\begin{vmatrix} 34.90 \\ 35.71 \end{vmatrix}$	$25.12 \\ 25.71$	43 44
45 46	36.86 37.68	$\begin{bmatrix} 25.81 \\ 26.38 \end{bmatrix}$	$\begin{vmatrix} 36.75 \\ 37.57 \end{vmatrix}$	$\begin{bmatrix} 25.97 \\ 26.55 \end{bmatrix}$	$\begin{array}{ c c c c }\hline 36.64 \\ 37.45 \\ \hline \end{array}$	$26.13 \\ 26.71$	$\begin{vmatrix} 36.52 \\ 37.33 \end{vmatrix}$	$26.29 \\ 26.88$	45 46
47 48	$\begin{vmatrix} 38.50 \\ 39.32 \end{vmatrix}$	$\begin{vmatrix} 26.96 \\ 27.53 \end{vmatrix}$	$\begin{vmatrix} 38.38 \\ 39.20 \end{vmatrix}$	$\begin{bmatrix} 27.13 \\ 27.70 \end{bmatrix}$	38.26 39.08	$27.29 \\ 27.87$	38.14	27.46	47
49	40.14	28.11	40.02	28.28	39.89	28.45	$\begin{vmatrix} 38.96 \\ 39.77 \end{vmatrix}$	28.04 28.63	48 49
$\frac{50}{6}$	$\frac{40.96}{\text{Dep.}}$	28.68 Lat.	40.83 Don	28.86 Tot	140.71 Den	29.04 Lot	40.58 Dan	29.21	$\frac{50}{6}$
Distance.	Бер.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
Dist	55 ]	Deg.	543	Deg.	541	Deg.	541	Deg.	Dist

					N		II.		
Dista	35 I	Deg.	351	Deg.	35½	Deg.	35¾	Deg.	Dista
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce
Distance   512 53 55 56 7 8 9 60   612 55 55 55 56 66 66 67 68 69 7   772 73 74 75 77 78 9   812 83 84 85 88 89 90   912 30   912	Lat.  41.78 42.60 43.42 44.23 45.05 45.87 46.69 47.51 48.33 49.15  49.97 50.79 51.61 52.43 53.24 54.96 54.88 55.70 56.52 57.34  58.16 58.98 59.80 60.62 61.44 62.26 63.07 63.89 64.71 65.53  66.35 67.17 67.99 68.81 69.63 70.45 71.27 72.09 73.72 74.54 75.36	Dep.  29.25 29.83 30.40 30.97 31.55 32.12 32.69 33.27 33.84 34.41 34.99 35.56 36.14 36.71 37.28 37.86 38.43 39.00 39.58 40.15 40.72 41.30 41.87 42.44 43.02 43.59 44.17 44.74 45.31 45.89 46.46 47.03 47.61 48.18 48.75 49.33 49.90 50.47 51.05 51.62 52.20 52.77	Lat.  41.65 42.47 43.28 44.10 44.92 45.73 46.55 47.37 48.18 49.00 49.82 50.63 51.45 52.27 53.08 53.90 54.71 55.53 56.35 57.16 57.98 58.80 59.61 60.43 61.25 62.06 62.88 63.70 64.51 65.33 66.15 66.96 67.78 68.60 69.41 70.23 71.05 71.86 72.68 73.50 74.31 75.13	Dep.  29.43 30.01 30.59 31.17 31.74 32.32 32.90 33.47 34.05 34.63 35.21 35.78 36.36 36.94 37.51 38.09 38.67 39.25 39.82 40.40 40.98 41.55 42.13 42.71 43.29 43.86 44.44 45.02 45.59 46.17 46.75 47.33 47.90 48.48 49.06 49.63 50.21 50.79 51.37 51.94 52.52 53.10		1			Distance.   552 554 556 57 89 60   612 63 64 65 66 67 88 90   71 72 73 74 75 76 77 89   82 84 85 88 89 91 92 60 10 10 10 10 10 10 10 10 10 10 10 10 10
93 94 95 96 97 98 99	$egin{array}{c} 76.18 \\ 77.69 \\ 77.82 \\ 78.64 \\ 79.46 \\ 80.28 \\ 81.10 \\ \hline \end{array}$	53.34 53.92 54.49 55.06 55.64 56.21 56.78	75.95 76.76 77.58 78.40 79.21 80.03 80.85	53.67 54.25 54.83 55.41 55.98 56.56 57.14	76.53 77.34 78.16 78.97 79.78 80.60	54.59 55.17 55.75 56.33 56.91 57.49	76.29 77.10 77.91 78.72 79.53 80.35	54.92 55.50 56.09 56.67 57.26 57.84	93 94 95 96 97 98 99
100	81.92	57.36	81.66	57.71	81.41	58.07	81.16	58.42	100
ance	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	ance
Distance.	55	Deg.	543	Deg.	541/2	Deg.	544	Deg.	Distance.

			-						-
Distance	36	Deg.	361	Deg.	36½	Deg.	363	Deg.	Distance.
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ince.
1 2 3 4 5 6 7 8 9 10	$egin{array}{c cccc} 1.62 & 1.62 \\ 2.43 & 2.43 \\ 3.24 & 4.05 \\ 4.85 & 4.85 \\ 5.66 & 6.47 \\ 7.28 & 8.09 \\ \hline \end{array}$	1.18 1.76 2.35 2.94 3.53 4.11 4.70 5.29 5.88	$\begin{array}{ c c c }\hline 0.81\\ 1.61\\ 2.42\\ 3.23\\ 4.03\\ 4.84\\ 5.65\\ 6.45\\ 7.26\\ 8.06\\ \end{array}$	0.59 1.18 1.77 2.37 2.96 3.55 4.14 4.73 5.32 5.91	$\begin{array}{c} 0.80 \\ 1.61 \\ 2.41 \\ 3.22 \\ 4.02 \\ 4.82 \\ 5.63 \\ 6.43 \\ 7.23 \\ 8.04 \end{array}$	1.19 1.78 2.38 2.97 3.57 4.16 4.76 5.35		0.60 1.20 1.79 2.39 2.99 3.59 4.19 4.79 5.38 5.98	
11 12 13 14 15 16 17 18 19	$egin{array}{c} 9.71 \\ 10.52 \\ 11.33 \\ 12.14 \\ 12.94 \\ 13.75 \\ 14.56 \\ 15.37 \\ \hline \end{array}$	7.05 7.64 8.23 8.82 9.40 9.99 10.58 11.17	$ \begin{vmatrix} 8.87 \\ 9.68 \\ 10.48 \\ 11.29 \\ 12.10 \\ 12.90 \\ 13.71 \\ 14.52 \\ 15.32 \end{vmatrix} $	$\begin{bmatrix} 6.50 \\ 7.10 \\ 7.69 \\ 8.28 \\ 8.87 \\ 9.46 \\ 10.05 \\ 10.64 \\ 11.23 \\ \end{bmatrix}$	8.84 9.65 10.45 11.25 12.06 12.86 13.67 14.47 15.27	$\begin{bmatrix} 6.54 \\ 7.14 \\ 7.73 \\ 8.33 \\ 8.92 \\ 9.52 \\ 10.11 \\ 10.71 \\ 11.30 \\ \end{bmatrix}$	8.81 9.61 10.42 11.22 12.02 12.82 13.62 14.42 15.22	6.58 7.18 7.78 8.38 8.97 9.57 10.17 10.77 11.37	11 12 13 14 15 16 17 18 19
20 21 22 23 24 25 26 27 28 29 30	$ \begin{array}{ c c c c c } \hline 16.99 \\ 17.80 \\ 18.61 \end{array} $	$\begin{array}{c} 11.76 \\ \hline 12.34 \\ 12.93 \\ 13.52 \\ 14.11 \\ 14.69 \\ 15.28 \\ 15.87 \\ 16.46 \\ 17.05 \\ 17.63 \\ \end{array}$	$\begin{bmatrix} 16.13 \\ \hline 16.94 \\ 17.74 \\ 18.55 \\ 19.35 \\ 20.16 \\ 20.97 \\ 21.77 \\ 22.58 \\ 23.39 \\ 24.10 \\ \end{bmatrix}$	$\begin{array}{ c c c c c }\hline 11.83\\\hline 12.42\\\hline 13.01\\\hline 13.60\\\hline 14.19\\\hline 14.78\\\hline 15.37\\\hline 15.97\\\hline 16.56\\\hline 17.15\\\hline 17.71\\\hline \end{array}$	$ \begin{array}{r} 16.08 \\ \hline 16.88 \\ 17.68 \\ 18.49 \\ 19.29 \\ 20.10 \\ 20.90 \\ 21.70 \\ 22.51 \\ 23.31 \\ 24.12 \\ 24.12 \\ 24.12 \\ 24.12 \\ 24.12 \\ 25.12 \\ 24.1$	$ \begin{array}{r} 11.90 \\ 12.49 \\ 13.09 \\ 13.68 \\ 14.28 \\ 14.87 \\ 15.47 \\ 16.06 \\ 16.65 \\ 17.25 $	$ \begin{vmatrix} 16.03 \\ \hline 16.83 \\ 17.63 \\ 18.43 \\ 19.23 \\ 20.03 \\ 20.83 \\ 21.63 \\ 22.44 \\ 23.24 \end{vmatrix} $	11.97 12.56 13.16 13.76 14.36 14.96 15.56 16.15 16.75	20 21 22 23 24 25 26 27 28 29
31 32 33 34 35 36 37 38 39 40	25.08 25.89 26.70 27.51 28.32 29.12 29.93 30.74 31.55 32.36	18.22 18.81 19.40 19.98 20.57 21.16 21.75 22.34 22.92 23.51	24.19 25.00 25.81 26.61 27.42 28.23 29.03 29.84 30.64 31.45 32.26	17.74 18.33 18.92 19.51 20.10 20.70 21.29 21.88 22.47 23.06 23.65	$\begin{array}{r} 24.12 \\ \hline 24.92 \\ 25.72 \\ 26.53 \\ 27.33 \\ 28.13 \\ 28.94 \\ 29.74 \\ 30.55 \\ 31.35 \\ 32.15 \\ \end{array}$	17.84 18.44 19.03 19.63 20.22 20.82 21.41 22.01 22.60 23.20 23.79	$\begin{array}{ c c c c }\hline 24.04\\\hline 24.84\\25.64\\26.44\\27.24\\28.04\\28.85\\29.65\\30.45\\31.25\\32.05\\\hline\end{array}$	17.95 18.55 19.15 19.74 20.34 20.94 21.54 22.14 22.74 23.33 23.93	30 31 32 33 34 35 36 37 38 39 40
41 42 43 44 45 46 47 48 49 50	33.17 33.98 34.79 35.60 36.41 37.21 38.02 38.83 39.64 40.45	24.10 24.69 25.27 25.86 26.45 27.04 27.63 28.21 28.80 29.39	33.06 33.87 34.68 35.48 36.29 37.10 37.90 38.71 39.52 40.32	24.24 24.83 25.43 26.02 26.61 27.20 27.79 28.38 28.97 29.57	32.96 33.76 34.57 35.37 36.17 36.98 37.78 38.59 39.39 40.19	24.39 24.98 25.58 26.17 26.77 27.36 27.96 28.55 29.15 29.74	32.85 33.65 34.45 35.26 36.06 36.86 37.66 38.46 39.26 40.06	24.53 25.13 25.73 26.33 26.92 27.52 28.12 28.72 29.32 29.92	41 42 43 44 45 46 47 48 49 50
Distance.	Dep.   54 I	Lat.	Dep.   53¾ I	Deg.	Dep.   53½	Deg.	Dep.   53½ ]	Lat. Deg.	Distance.

-	1		11						-
Distance.	36	Deg.	361	Deg.	36½	Deg.	363	Deg.	Dist
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
51 52	$\frac{41.26}{42.07}$		41.13	$\begin{vmatrix} 30.16 \\ 30.75 \end{vmatrix}$	41.00 41.80	$\begin{vmatrix} 30.34 \\ 30.93 \end{vmatrix}$	40.86	$\frac{30.51}{31.11}$	51 52
53 54	42.88	31.15	42.74 43.55	31.34 31.93	42.60 43.41	$\begin{vmatrix} 31.53 \\ 32.12 \end{vmatrix}$	$\begin{vmatrix} 42.47 \\ 43.27 \end{vmatrix}$	$\begin{vmatrix} 31.71 \\ 32.31 \end{vmatrix}$	53 54
55 56			44.35	32.52	44.21	$\begin{vmatrix} 32.72 \\ 33.31 \end{vmatrix}$	44.07	$\begin{vmatrix} 32.91 \\ 33.51 \end{vmatrix}$	55
57	46.11	33.50	45.97	33.70	45.02 45.82	33.90	45.67	34.10	56 57
59 60	$\begin{vmatrix} 46.92 \\ 47.73 \\ 49.54 \end{vmatrix}$	$\begin{vmatrix} 34.09 \\ 34.68 \\ 35.97 \end{vmatrix}$	46.77	34.30	46.62	34.50	46.47 $47.27$	34.70 35.30	58 59
61	$\begin{array}{ c c }\hline 48.54\\\hline 49.35\end{array}$	$\frac{35.27}{35.85}$	$\frac{48.39}{49.19}$	$\frac{35.48}{36.07}$	$  \frac{48.23}{49.04}  $	$\frac{35.69}{36.28}$	$\frac{48.08}{48.88}$	$\frac{35.90}{36.50}$	$\left  \begin{array}{c} 60 \\ \hline 61 \end{array} \right $
62 63	$\begin{vmatrix} 50.16 \\ 50.97 \end{vmatrix}$	$\begin{vmatrix} 36.44 \\ 37.03 \end{vmatrix}$	$\begin{bmatrix} 50.00 \\ 50.81 \end{bmatrix}$	$\begin{vmatrix} 36.66 \\ 37.25 \end{vmatrix}$	49.84 50.64	$36.88 \\ 37.47$	49.68  $ 50.48 $	37.10 37.69	$\begin{array}{ c c } 62 \\ 63 \end{array}$
64 65	51.78 52.59	$\begin{vmatrix} 37.62 \\ 38.21 \end{vmatrix}$	$51.61 \\ 52.42$	$37.84 \\ 38.44$	$51.45 \\ 52.25$	$\begin{vmatrix} 38.07 \\ 38.66 \end{vmatrix}$	51.28 52.08	38.29 38.89	64 65
$\begin{array}{c c} 66 \\ 67 \end{array}$	$\begin{vmatrix} 53.40 \\ 54.20 \end{vmatrix}$	38.79 39.38	$53.23 \\ 54.03$	$\frac{39.03}{39.62}$	53.05 53.86	$\begin{vmatrix} 39.26 \\ 39.85 \end{vmatrix}$	52.88 53.68	39.49 40.09	66 67
68 69	55.01 55.82	$\begin{vmatrix} 39.97 \\ 40.56 \end{vmatrix}$	54.84 55.64	40.21 40.80	54.66 55.47	40.45  $ 41.04 $	54.49 55.29	40.69 41.28	68 69
70	56.63	41.14	56.45	41.39	56.27	41.64	56.09	$\frac{41.88}{42.48}$	70
71 72	57.44	$\begin{vmatrix} 41.73 \\ 42.32 \\ 49.01 \end{vmatrix}$	57.26 58.06	41.98 42.57	57.07	$\begin{vmatrix} 42.23 \\ 42.83 \end{vmatrix}$	56.89	43.08	71 72
73 74	$\begin{vmatrix} 59.06 \\ 59.87 \end{vmatrix}$	$ \begin{array}{c c} 42.91 \\ 43.50 \\ \end{array} $	$\begin{bmatrix} 58.87 \\ 59.68 \end{bmatrix}$	43.17	58.68	$\begin{vmatrix} 43.42 \\ 44.02 \end{vmatrix}$	58.49	43.68	73 74
75 76	$\begin{vmatrix} 60.68 \\ 61.49 \end{vmatrix}$	$\begin{vmatrix} 44.08 \\ 44.67 \end{vmatrix}$	$\begin{bmatrix} 60.48 \\ 61.29 \end{bmatrix}$	$ 44.35  \\ 44.94 $	60.29 $61.09$	$ \begin{array}{c} 44.61 \\ 45.21 \\ \end{array} $	$\begin{vmatrix} 60.09 \\ 60.90 \end{vmatrix}$	44.87	75 76
77 78	$\begin{vmatrix} 62.29 \\ 63.10 \end{vmatrix}$	45.26 45.85	$\begin{bmatrix} 62.10 \\ 62.90 \end{bmatrix}$	$45.53 \\ 46.12$	$\begin{vmatrix} 61.90 \\ 62.70 \end{vmatrix}$	$\begin{vmatrix} 45.80 \\ 46.40 \end{vmatrix}$	$\begin{vmatrix} 61.70 \\ 62.50 \end{vmatrix}$	$\begin{vmatrix} 46.07 \\ 46.67 \end{vmatrix}$	77 78
79 80	$63.91 \\ 64.72$	$ \begin{array}{c} 46.43 \\ 47.02 \\ \end{array} $	$\begin{bmatrix} 63.71 \\ 64.52 \end{bmatrix}$	$46.71 \\ 47.30$	$\begin{vmatrix} 63.50 \\ 64.31 \end{vmatrix}$	$\begin{vmatrix} 46.99 \\ 47.59 \end{vmatrix}$	$\begin{vmatrix} 63.30 \\ 64.10 \end{vmatrix}$	47.27  47.87	79 80
81 82	$65.53 \\ 66.34$	$47.61 \\ 48.20$	65.32 66.13	47.90 48.49	$65.11 \\ 65.92$	48.18 48.78	$64.90 \\ 65.70$	48.46 49.06	81 82
83 84	67.15 67.96	$\begin{vmatrix} 48.79 \\ 49.37 \end{vmatrix}$	$66.93 \\ 67.74$	$ \begin{array}{c c} 49.08 \\ 49.67 \end{array} $	66.72 $67.52$	$\begin{vmatrix} 49.37 \\ 49.97 \end{vmatrix}$	$66.50 \\ 67.31$	49.66 50.26	83 84
85 86	68.77 69.58	49.96	68.55 69.35	50.26 50.85	68.33 $69.13$	50.56 51.15	68.11 68.91	50.86	85 86
87	70.38	50.55   51.14	70.16	51.44	69.94	[51.75]	69.71 $70.51$	52.05 52.65	87 88
88 89	$71.19 \\ 72.00 \\ 79.01$	51.73	70.97	52.04 52.63	70.74	52.34	71.31	53.25	89
$\frac{90}{91}$	$\frac{72.81}{73.62}$	$\begin{array}{ c c }\hline 52.90 \\ \hline 53.49 \\ \hline \end{array}$	$\frac{72.58}{73.39}$	$\frac{53.22}{53.81}$	$\frac{72.35}{73.15}$	$\frac{53.53}{54.13}$	$\frac{72.11}{72.91}$	$\frac{53.85}{54.45}$	$\frac{90}{91}$
92 93	$74.43 \\ 75.24$	$\begin{bmatrix} 54.08 \\ 54.66 \end{bmatrix}$	74.19 75.00	54.40 54.99	$\begin{bmatrix} 73.95 \\ 74.76 \end{bmatrix}$	$\begin{bmatrix} 54.72 \\ 55.32 \end{bmatrix}$	$73.72 \\ 74.52$	55.05 55.64	92 93
94 95	76.05 76.86	55.25 55.84	75.81 76.61	55.58 56.17	$\begin{bmatrix} 75.56 \\ 76.37 \end{bmatrix}$	$55.91 \\ 56.51$	$75.32 \\ 76.12$	$56.24 \\ 56.84$	94 95
96 97	77.67 78.47	56.43 57.02	77.42 78.23	56.77 57.36	77.17	$\begin{bmatrix} 57.10 \\ 57.70 \end{bmatrix}$	$76.92 \\ 77.72$	57.44 58.04	96 97
98 99	$79.28 \\ 80.09$	$57.60 \\ 58.19$	79.03	57.95   58.54	78.78 79.58	58.29 58.89	$78.52 \\ 79.32$	$58.64 \\ 59.23$	98 99
100	80.90	$ \underline{58.78} $	80.64	59.13	$\frac{80.39}{}$	59.48	80.13	59.83	100
ance	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance
Distance.	54 I	eg.	53‡ I	Deg.	53½ ]	Deg.	531 ]	Deg.	Dist

Di	37	Deg.	374	Deg.	371	Deg.	373	Deg.	E
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.		Distance
1	0.80	0.60	0.80	0.61	$\frac{1}{0.79}$	0.61	0.79	Dep. 0.61	- <u>c</u>
3	$\begin{vmatrix} 1.60 \\ 2.40 \\ 2.40 \end{vmatrix}$	1.20	$\begin{bmatrix} 1.59 \\ 2.39 \end{bmatrix}$	1.21	$1.59 \\ 2.38$	1.22	$1.58 \\ 2.37$	1.22	2 3
4 5 6	3.19	$\begin{vmatrix} 2.41 \\ 3.01 \\ 2.61 \end{vmatrix}$	$\begin{array}{c} 3.18 \\ 3.98 \\ 4.79 \end{array}$	3.03	$\begin{vmatrix} 3.17 \\ 3.97 \\ 4.82 \end{vmatrix}$	3.04	$\begin{vmatrix} 3.16 \\ 3.95 \end{vmatrix}$	$\begin{vmatrix} 2.45 \\ 3.06 \end{vmatrix}$	4 5
8	$\begin{array}{ c c } 4.79 \\ 5.59 \\ 6.39 \end{array}$	$ \begin{array}{ c c } 3.61 \\ 4.21 \\ 4.81 \end{array} $	$ \begin{array}{c c} 4.78 \\ 5.57 \\ 6.37 \end{array} $	$\begin{vmatrix} 3.63 \\ 4.24 \\ 4.24 \end{vmatrix}$	4.76 5.55	3.65	4.74 5.53	$\frac{3.67}{4.29}$	6 7
9	7.19 7.99	5.42 6.02	7.16 7.96	4.84 5.45 6.05	$\begin{bmatrix} 6.35 \\ 7.14 \\ 7.93 \end{bmatrix}$	4.87 5.48 6.09	$\begin{array}{c c} 6.33 \\ 7.12 \\ 7.91 \end{array}$	$4.90 \\ 5.51 \\ 6.12$	8 9 10
11 12	8.78 9.58	$\frac{6.62}{7.22}$	$8.76 \\ -9.55$	$\begin{array}{ c c }\hline 6.66\\ 7.26\end{array}$	$8.73 \\ 9.52$	6.70 7.31	$   \begin{array}{r}     \hline                                $	$\frac{6.73}{7.35}$	$\begin{array}{c} \frac{10}{11} \\ 12 \end{array}$
13 14	10.38 $  11.18$	$\begin{bmatrix} 7.82 \\ 8.43 \end{bmatrix}$	10.35 11.14	7.87 8.47	10.31	7.91	$10.28 \\ 11.07$	7.96 8.57	13 $14$
15 16	11.98 $12.78$	$\begin{bmatrix} 9.03 \\ 9.63 \end{bmatrix}$	$\begin{vmatrix} 11.94 \\ 12.74 \end{vmatrix}$	$9.08 \\ 9.68$	$11.90 \\ 12.69$	$9.13 \\ 9.74$	$11.86 \\ 12.65$	$9.18 \\ 9.80$	15 16
17	13.58 14.38	$\begin{vmatrix} 10.23 \\ 10.83 \end{vmatrix}$	13.53 $14.33$	10.29 $10.90$	$\begin{vmatrix} 13.49 \\ 14.28 \end{vmatrix}$	$\begin{bmatrix} 10.35 \\ 10.96 \end{bmatrix}$	13.44 14.23	10.41 $11.02$	17 18
$\begin{array}{c} 19 \\ 20 \\ \hline \end{array}$	15.17	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	$15.12 \\ 15.92$	$\frac{11.50}{12.11}$	15.07 $15.87$	$\frac{11.57}{12.18}$	15.02 $15.81$	$\frac{11.63}{12.24}$	$\begin{array}{c} 19 \\ 20 \end{array}$
21 22	16.77	$\begin{vmatrix} 12.64 \\ 13.24 \\ \end{vmatrix}$	16.72 $17.51$	12.71 $13.32$	$16.66 \\ 17.45$	12.78 13.39	$\begin{array}{c} 16.60 \\ 17.40 \end{array}$	$\frac{12.86}{13.47}$	21 22
23 24 25	$\begin{vmatrix} 18.37 \\ 19.17 \\ 19.97 \end{vmatrix}$	$\begin{vmatrix} 13.84 \\ 14.44 \\ 15.05 \end{vmatrix}$	18.31 $19.10$ $19.90$	13.92 14.53	18.25	14.00	18.19	14.08 14.69	$\begin{array}{c} 23 \\ 24 \end{array}$
26 27	20.76 $21.56$	15.65 16.25	$\begin{vmatrix} 19.50 \\ 20.70 \\ 21.49 \end{vmatrix}$	15.13 $15.74$ $16.34$	$egin{array}{c} 19.83 \ 20.63 \ 21.42 \ \end{array}$	$15.22 \\ 15.83 \\ 16.44$	$\begin{vmatrix} 19.77 \\ 20.56 \\ 21.25 \end{vmatrix}$	15.31 15.92	25 26
$\begin{bmatrix} 28 \\ 29 \end{bmatrix}$	22.36 23.16	16.85 17.45	$\begin{bmatrix} 22.29 \\ 23.08 \end{bmatrix}$	16.95   17.55	$\begin{bmatrix} 21.42 \\ 22.21 \\ 23.01 \end{bmatrix}$	17.05 17.65	$\begin{vmatrix} 21.35 \\ 22.14 \\ 22.93 \end{vmatrix}$	16.53 17.14 17.75	27 28 29
$\frac{30}{31}$	$\frac{23.96}{24.76}$	$\frac{18.05}{18.66}$	$\frac{23.88}{24.68}$	$\frac{18.16}{18.76}$	$\frac{23.80}{24.59}$	$\frac{18.26}{18.87}$	$\frac{23.72}{24.51}$	18.37	30
32 33	25.56 $26.35$	19.26 19.86	25.47 $26.27$	19.37 19.97	25.39 26.18	$\begin{vmatrix} 16.87 \\ 19.48 \\ 20.09 \end{vmatrix}$	$\begin{vmatrix} 24.31 \\ 25.30 \\ 26.09 \end{vmatrix}$	$   \begin{array}{c c}     18.98 \\     19.59 \\     20.20   \end{array} $	31 32 33
34 35	$27.15 \\ 27.95$	$20.46 \\ 21.06$	27.06 27.86	$\begin{vmatrix} 20.58 \\ 21.19 \end{vmatrix}$	$\begin{bmatrix} 26.97 \\ 27.77 \end{bmatrix}$	$\begin{bmatrix} 20.70 \\ 20.70 \\ 21.31 \end{bmatrix}$	26.88 27.67	$\begin{bmatrix} 20.20 \\ 20.82 \\ 21.43 \end{bmatrix}$	34 35
36 37	$\begin{array}{c} 28.75 \\ 29.55 \end{array}$	$\begin{bmatrix} 21.67 \\ 22.27 \end{bmatrix}$	$\begin{array}{c} 28.66 \\ 29.45 \end{array}$	$21.79 \\ 22.40$	$28.56 \\ 29.35$	$\begin{bmatrix} 21.92 \\ 22.52 \end{bmatrix}$	$   \begin{array}{c}     28.46 \\     29.26   \end{array} $	$\begin{bmatrix} 22.04 \\ 22.65 \end{bmatrix}$	36 g 37 g
38 39	$30.35 \\ 31.15$	$22.87 \\ 23.47$	$\frac{30.25}{31.04}$	$\begin{array}{c} 23.00 \\ 23.61 \end{array}$	$30.15 \\ 30.94$	$23.13 \\ 23.74$	$\begin{vmatrix} 30.05 \\ 30.84 \end{vmatrix}$	$\frac{23.26}{23.88}$	38 39
$\frac{40}{41}$	$\frac{31.95}{32.74}$	$\frac{24.07}{24.67}$	$\frac{31.84}{32.64}$	$\frac{24.21}{24.82}$	$\frac{31.73}{32.53}$	$\begin{array}{ c c c }\hline 24.35 \\ \hline 24.96 \\ \hline \end{array}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\frac{24.49}{25.10}$	$\frac{40}{41}$
42 43	$\begin{vmatrix} 33.54 \\ 34.34 \end{vmatrix}$	25.28 25.88	$\frac{33.43}{34.23}$	$\begin{array}{c c} 25.42 \\ 26.03 \end{array}$	$33.32 \\ 34.11$	$\begin{bmatrix} 25.57 \\ 26.18 \end{bmatrix}$	$\begin{bmatrix} 33.21 \\ 34.00 \end{bmatrix}$	$\begin{bmatrix} 25.71 \\ 26.33 \end{bmatrix}$	42 43
44 45	$\begin{vmatrix} 35.14 \\ 35.94 \\ 36.74 \end{vmatrix}$	26.48 27.08	$35.02 \\ 35.82 \\ 36.69$	26.63	$\frac{34.91}{35.70}$	$\begin{vmatrix} 26.79 \\ 27.39 \end{vmatrix}$	$\frac{34.79}{35.58}$	$26.94 \\ 27.55$	44 45
46 47 48	$\begin{vmatrix} 36.74 \\ 37.54 \\ 38.33 \end{vmatrix}$	27.68 28.29	$36.62 \\ 37.41 \\ 39.21$	27.84	$36.49 \\ 37.29 \\ 39.09$	28.00	$\begin{vmatrix} 36.37 \\ 37.16 \\ 27.16 \end{vmatrix}$	$     \begin{array}{c c}       28.16 \\       28.77     \end{array} $	46
49 50	$\begin{vmatrix} 39.33 \\ 39.13 \\ 39.93 \end{vmatrix}$	$     \begin{array}{c c}       28.89 \\       29.49 \\       30.09     \end{array} $	$38.21 \\ 39.00 \\ 39.80$	$     \begin{array}{c c}       29.05 \\       29.66 \\       30.26     \end{array} $	$38.08 \\ 38.87 \\ 39.67$	$\begin{vmatrix} 29.22 \\ 29.83 \\ 20.44 \end{vmatrix}$	37.95 38.74	$\begin{vmatrix} 29.39 \\ 30.00 \\ 30.61 \end{vmatrix}$	48 49
	Qep.	Lat.	-		Dep.	30.44 Lat.	39.53 Dep.	130.61 Lat:	50 
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Dista	37 ]	Deg.	371	Deg.	37½	Deg.	373	Deg.	Dista
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce
Distance.   512   54   55   55   56   61   62   63   64   66   67   77   77   77   77   77	Lat.  40.73 41.53 42.33 43.13 43.92 44.72 45.52 46.32 47.12 49.52 50.31 51.11 52.71 53.51 54.31 55.11 55.90 56.70 57.50 58.30 59.10 59.90 60.70 61.49 62.29 63.09 63.89 64.69 65.49 67.09 67.88	Dep.  30.69 31.29 31.90 \$2.50 33.10 33.70 34.30 34.91 35.51 36.11 36.71 37.31 37.91 38.52 39.12 39.72 40.32 40.92 41.53 42.13 42.73 43.33 44.53 44.53 44.53 45.14 46.94 47.54 46.94 47.54 48.15 48.75 49.35 50.55 51.15	Lat.  40.60 41.39 42.19 42.98 43.78 44.58 45.37 46.17 46.96 47.76  48.56 49.35 50.15 50.94 51.74 52.54 53.33 54.13 54.92 55.72  56.52 57.31 58.11 58.90 59.70 60.50 61.29 62.88 63.68  64.48 65.27 66.86 67.66	Dep.  30.87 31.48 32.08 32.69 33.29 33.90 34.50 35.11 35.71 36.32 36.92 37.53 38.13 38.74 39.34 39.95 40.55 41.16 41.77 42.37 42.98 43.58 44.19 44.79 45.40 46.00 46.61 47.21 47.82 48.42 49.63 50.24 50.84 51.45	Lat.  40.46 41.25 42.05 42.84 43.63 44.43 45.22 46.01 46.81 47.60  48.39 49.19 49.98 50.77 52.36 53.15 53.95 54.74 55.53  56.33 57.12 57.91 58.71 59.50 60.29 61.09 61.88 62.67 63.47 64.26 65.05 66.64 67.43	Dep.  31.05 31.66 32.26 32.87 33.48 34.09 34.70 35.31 35.92 36.53 37.13 37.74 38.35 38.96 39.57 40.18 40.79 41.40 42.00 42.61 43.22 43.83 44.44 45.05 45.66 46.27 46.87 47.48 48.09 48.70 49.31 49.92 50.53 51.14 51.74	Lat.  40.33 41.12 41.91 42.70 43.49 44.28 45.07 45.86 46.65 47.44  48.23 49.02 49.81 50.60 51.39 52.19 52.98 53.77 54.56 55.35  56.14 56.93 57.72 58.51 59.30 60.09 60.88 61.67 62.46 63.26 64.05 64.84 65.63 66.42 67.21	Dep.  31.22 31.84 32.45 33.06 33.67 34.28 34.90 35.51 36.12 36.73 37.35 37.96 38.57 39.18 39.79 40.41 41.02 41.63 42.24 42.86 43.47 44.08 45.30 45.92 46.53 47.14 47.75 48.37 48.98  49.59 50.20 50.81 51.43 52.04	Distance. 512345567890 612355555560 6123666670 71237567890 81238456
86 87 88 89 90	68.68 69.48 70.28 71.08 71.88	51.76 52.36 52.96 53.56 54.16	68.46 69.25 70.05 70.84 71.64	52.06 52.66 53.27 53.87 54.48	68.23 69.02 69.82 70.61 71.40	52.35 52.96 53.57 54.18 54.79	68.00 $68.79$ $69.58$ $70.37$ $71.16$	52.65 53.26 53.88 54.49 55.10	86 87 88 89 90
91 92 93 94 95 96 97 98 99 100	72.68 73.47 74.27 75.07 75.87 76.67 77.47 78.27 79.06 79.86	54.77 55.37 55.97 56.57 57.17 57.77 58.38 58.98 59.58 60.18	$\begin{array}{c} 72.44 \\ 73.23 \\ 74.03 \\ 74.82 \\ 75.62 \\ 76.42 \\ 77.21 \\ 78.01 \\ 79.60 \\ \end{array}$	55.08 55.69 56.29 56.90 57.50 58.11 58.71 59.32 59.92 60.53	72.20 72.99 73.78 74.58 75.37 76.16 76.96 77.75 78.54 79.34	55.40 56.61 57.22 57.83 58.44 59.05 59.66 60.27 60.88	71.95 72.74 73.53 74.32 75.12 75.91 76.70 77.49 78.28 79.07	55.71 56.32 56.94 57.55 58.16 58.77 59.39 60.00 60.61 61.22	91 92 93 94 ,95 96 97 98 99 100
Distance.	Dep. 53 I	Lat.	Dep. Lat.  523 Deg.		Dep. 52½	Deg.	Dep.   Lat.   52½ Deg.		Distance.
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-	U	38	Deg.	381	Deg.	38.	l Deg.	30	Beg.	
	Distance					-		-	T Deg.	Distance.
-		<b>-</b>		Lat.	Dep.	Lat.	_	_	Dep.	nce.
	$\begin{vmatrix} 1\\2\\3 \end{vmatrix}$	1.58	1.23		0.62 $1.24$			0.78		
	4			$\begin{array}{ c c c c c } & 2.36 \\ & 3.14 \end{array}$	$\begin{vmatrix} 1.86 \\ 2.48 \end{vmatrix}$	$\parallel 2.35$	1.87	$\parallel 2.34$	1.88	3
	5 6	3.94	3.08	$\parallel$ 3.93	3.10	3.91	3.11	3.90	3.13	5
	7	5.52	4.31	4.71 5.50	$\begin{vmatrix} 3.71 \\ 4.33 \end{vmatrix}$		4.36	$\ \begin{array}{c} 4.68 \\ 5.46 \end{array}$	[ 3.76]	6
	$\frac{8}{9}$	7.09	5.54	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	4.95 5.57		4.98	$\begin{vmatrix} 6.24 \\ 7.02 \end{vmatrix}$	5.01	8
	$\frac{10}{11}$	$\begin{array}{ c c }\hline 7.88 \\ \hline 8.67 \\ \hline \end{array}$	6.16	7.85	6.19	7.83	6.23	7.80	6.26	9
į	12	9.46	7.39	8.64 9.42	$\begin{vmatrix} 6.81 \\ 7.43 \end{vmatrix}$	$\begin{array}{ c c c } 8.61 \\ 9.39 \end{array}$	$\begin{vmatrix} 6.85 \\ 7.47 \end{vmatrix}$	8.58 9.36		11 12
	13 14	10.24		$\begin{vmatrix} 10.21 \\ 10.99 \end{vmatrix}$	$\begin{array}{ c c } 8.05 \\ 8.67 \end{array}$	$\begin{vmatrix} 10.17 \\ 10.96 \end{vmatrix}$	8.09	10.14	8.14	13
	$\begin{array}{c} 15 \\ 16 \end{array}$	$\begin{vmatrix} 11.82 \\ 12.61 \end{vmatrix}$	$9.23 \\ 9.85$	11.78 12.57	9.29 $9.91$	11.74	9.34	11.70	9.39	14 15
	17 18	13.40	10.47	13.35	10.52	$\begin{vmatrix} 12.52 \\ 13.30 \end{vmatrix}$	10.58	12.48  $  13.26 $	$\begin{vmatrix} 10.01 \\ 10.64 \end{vmatrix}$	16
	19	14.18	11.70	14.14 14.92	$  11.14 \\ 11.76  $	14.09  $  14.87 $	11.21	14.04 14.82	11.27	18
Ì	$\frac{20}{21}$	$\begin{array}{ c c c }\hline 15.76 \\\hline 16.55 \\\hline \end{array}$	$\frac{12.31}{12.93}$	$\frac{15.71}{16.49}$	$\frac{12.38}{12.00}$	15.65	12.45	15.60	12.52	20
	22	17.34	13.54	17.28	$\begin{vmatrix} 13.00 \\ 13.62 \end{vmatrix}$	$   16.43 \\ 17.22 $	$\begin{vmatrix} 13.07 \\ 13.70 \end{vmatrix}$	$   16.38 \\ 17.16$	$\begin{vmatrix} 13.14 \\ 13.77 \end{vmatrix}$	$\begin{array}{ c c c }\hline 21\\22\\ \end{array}$
The second	23 24	18.12 18.91	14.16 14.78	18.06	14.24 14.86	$   18.00 \\    18.78$	14.32	17.94 18.72	$\begin{vmatrix} 14.40 \\ 15.02 \end{vmatrix}$	23
I	25 26	$\begin{vmatrix} 19.70 \\ 20.49 \end{vmatrix}$	15.39 16.01	$\begin{array}{ c c c }\hline 19.63 \\ 20.42 \\\hline \end{array}$	15.48 16.10	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	15.56	19.50	15.65	24 25
1	27 28	$\begin{vmatrix} 21.28 \\ 22.06 \end{vmatrix}$	16.62 $17.24$	21.20	16.72	21.13	16.81	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$  16.27 \\ 16.90  $	26 27
	29	22.85	17.85	$\begin{vmatrix} 21.99 \\ 22.77 \end{vmatrix}$	17.33 $17.95$	$\begin{vmatrix} 21.91 \\ 22.70 \end{vmatrix}$	17.43	$\begin{vmatrix} 21.84 \\ 22.62 \end{vmatrix}$	17.53 18.15	28 29
	$\frac{30}{31}$	$\frac{23.64}{24.43}$	$\frac{18.47}{19.09}$	$\frac{23.56}{24.34}$	$\frac{18.57}{19.19}$	$\frac{23.48}{24.26}$	$\frac{18.68}{19.30}$	23.40	18.78	30
	32 33	25.22	19.70	25.13	19.81	25.04	19.92	24.18 24.96	$\begin{vmatrix} 19.40 \\ 20.03 \end{vmatrix}$	$\begin{array}{c c} 31 \\ 32 \end{array}$
	34	$\begin{vmatrix} 26.00 \\ 26.79 \end{vmatrix}$	$\begin{bmatrix} 20.32 \\ 20.93 \end{bmatrix}$	$\begin{vmatrix} 25.92 \\ 26.70 \end{vmatrix}$	$\begin{array}{c} 20.43 \\ 21.05 \end{array}$	25.83 $26.61$	$\begin{vmatrix} 20.54 \\ 21.17 \end{vmatrix}$	$\begin{vmatrix} 25.74 \\ 26.52 \end{vmatrix}$	$20.66 \\ 21.28$	33 34
	35 36	$\begin{vmatrix} 27.58 \\ 28.37 \end{vmatrix}$	$\begin{vmatrix} 21.55 \\ 22.16 \end{vmatrix}$	$\begin{bmatrix} 27.49 \\ 28.27 \end{bmatrix}$	$21.67 \\ 22.29$	27.39 28.17	$\begin{vmatrix} 21.79 \\ 22.41 \end{vmatrix}$	27.30	21.91	35
1	37 38	$29.16 \\ 29.94$	$\begin{bmatrix} 22.78 \\ 23.40 \end{bmatrix}$	29.06	22.91	28.96	23.03	$28.08 \\ 28.86$	$\begin{vmatrix} 22.53 \\ 23.16 \end{vmatrix}$	36 37
	39	30.73	24.01	$\begin{vmatrix} 29.84 \\ 30.63 \end{vmatrix}$	23.53	$\begin{vmatrix} 29.74 \\ 30.52 \end{vmatrix}$	$\begin{vmatrix} 23.66 \\ 24.28 \end{vmatrix}$	$\begin{vmatrix} 29.64 \\ 30.42 \end{vmatrix}$	$23.79 \\ 24.41$	38 39
	$\frac{40}{41}$	$\frac{31.52}{32.31}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\frac{31.41}{32.20}$	$\frac{24.76}{25.38}$	$\frac{31.30}{32.09}$	24.90	31.20	25.04	40
	42 43	33.10	25.86	32.98	26.00	32.87	$\begin{vmatrix} 25.52 \\ 26.15 \end{vmatrix}$	$\begin{vmatrix} 31.98 \\ 32.76 \end{vmatrix}$	$25.66 \\ 26.29$	41 42
	44	$\frac{33.88}{34.67}$	$\begin{vmatrix} 26.47 \\ 27.09 \end{vmatrix}$	$\begin{bmatrix} 33.77 \\ 34.55 \end{bmatrix}$	$26.62 \ 27.24$	$\begin{bmatrix} 33.65 \\ 34.43 \end{bmatrix}$	$26.77 \\ 27.39$	$\begin{vmatrix} 33.53 \\ 34.31 \end{vmatrix}$	$\frac{26.91}{27.54}$	43
	45 46	$35.46 \\ 36.25$	$\begin{bmatrix} 27.70 \\ 28.32 \end{bmatrix}$	$\begin{bmatrix} 35.34 \\ 36.12 \end{bmatrix}$	27.86 28.48	$\begin{array}{c} 35.22 \\ 36.00 \end{array}$	28.01 28.64	35.09	28.17	44 45
	47 48	$\frac{37.04}{37.82}$	28.94 29.55	36.91	29.10	36.78	29.26	$\begin{bmatrix} 35.87 \\ 36.65 \end{bmatrix}$	$28.79 \\ 29.42$	46
	4.9	38.61	30.17	$\frac{37.70}{38.48}$	$\begin{bmatrix} 29.72 \\ 30.34 \end{bmatrix}$	$\begin{array}{c} 37.57 \\ 38.35 \end{array}$	$\begin{array}{c c} 29.88 \\ 30.50 \end{array}$	$\begin{vmatrix} 37.43 \\ 38.21 \end{vmatrix}$	$\frac{30.04}{30.67}$	48 49
	$\frac{50}{6}$	39.40	$\frac{30.78}{1}$	$\frac{39.27}{5}$	$\frac{30.95}{1}$	$\frac{39.13}{-}$	31.13	38.99	$\frac{31.30}{}$	50
	anc	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	nce.
	Distance.	52 I	eg.	51¾ I	Deg.	51½ ]	Dem	E 1 1 1		Distance.
					8	012	eg.	514 1	Jeg.	D

		00 D 001 D					11		1
Distance.	38	Deg.	381	Deg.	381	Deg.	383	Deg.	Distance.
псе.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
51 52	40.19		$\begin{array}{ c c }\hline 40.05\\ 40.84\\ \hline\end{array}$	$\frac{31.57}{32.19}$	$\begin{vmatrix} 39.91 \\ 40.70 \end{vmatrix}$	$\frac{31.75}{32.37}$	$\begin{array}{ c c c }\hline 39.77\\ 40.55\\ \end{array}$	$\begin{vmatrix} 31.92 \\ 32.55 \end{vmatrix}$	$\overline{51}$
53 54	41.76	32.63	$\begin{vmatrix} 41.62 \\ 42.41 \end{vmatrix}$	$\begin{vmatrix} 32.81 \\ 33.43 \end{vmatrix}$	$\begin{vmatrix} 41.48 \\ 42.26 \end{vmatrix}$	32.99 33.62	$\begin{vmatrix} 41.33 \\ 42.11 \end{vmatrix}$	$\begin{vmatrix} 33.17 \\ 33.80 \end{vmatrix}$	53
55	43.34	33.86	43.19	$\begin{vmatrix} 34.05 \\ 34.67 \end{vmatrix}$	43.04 43.83		$\begin{vmatrix} 42.89 \\ 43.67 \end{vmatrix}$	34.43 35.05	55 56
57 58	44.92	$\begin{vmatrix} 35.09 \\ 35.71 \end{vmatrix}$	44.76 45.55	35.29 35.91	44.61 45.39	35.48 36.11	44.45 45.23	35.68 36.30	57 58
59	46.49	36.32	46.33 47.12	$\begin{vmatrix} 36.53 \\ 37.15 \end{vmatrix}$	$\begin{vmatrix} 46.17 \\ 46.96 \end{vmatrix}$	36.73 37.35	46.01 46.79	36.93 37.56	59 60
61	48.07	37.56	47.90	37.76	47.74	37.97	47.57	38.18	$\overline{61}$
62	49.64	38.79	48.69	38.38	$\begin{vmatrix} 48.52 \\ 49.30 \end{vmatrix}$	$\begin{vmatrix} 38.60 \\ 39.22 \end{vmatrix}$	48.35	$\begin{vmatrix} 38.81 \\ 39.43 \\ 40.00 \end{vmatrix}$	62 63
64	51.22	$\begin{vmatrix} 39.40 \\ 40.02 \end{vmatrix}$	50.26	$\begin{vmatrix} 39.62 \\ 40.24 \\ 40.66 \end{vmatrix}$	$\begin{bmatrix} 50.09 \\ 50.87 \end{bmatrix}$	39.84	$\begin{vmatrix} 49.91 \\ 50.69 \end{vmatrix}$	$\begin{cases} 40.06 \\ 40.68 \end{cases}$	64 65
66	52.80	$\begin{vmatrix} 40.63 \\ 41.25 \end{vmatrix}$	51.83	$\begin{vmatrix} 40.86 \\ 41.48 \end{vmatrix}$	$\begin{vmatrix} 51.65 \\ 52.43 \end{vmatrix}$	$\begin{vmatrix} 41.09 \\ 41.71 \end{vmatrix}$	51.47	41.31	66 67
68	54.37	$\begin{vmatrix} 41.86 \\ 42.48 \end{vmatrix}$	53.40	$\begin{vmatrix} 42.10 \\ 42.72 \end{vmatrix}$	53.22  $  54.00 $	$\begin{vmatrix} 42.33 \\ 42.95 \end{vmatrix}$	53.03	$\begin{vmatrix} 42.56 \\ 43.19 \end{vmatrix}$	68 69
$\frac{70}{71}$	$\frac{55.16}{55.95}$	$\frac{ 43.10 }{43.71}$	$\frac{54.97}{55.76}$	$\frac{43.34}{43.96}$	$\frac{54.78}{55.57}$	$\frac{43.58}{44.20}$	$\frac{54.59}{55.37}$	$\frac{43.81}{44.44}$	$\left  \frac{70}{71} \right $
72 73	$\begin{vmatrix} 56.74 \\ 57.52 \end{vmatrix}$	44.33	56.54 57.33	$44.57 \\ 45.19$	56.35 $57.13$	44.82 45.44	56.15	$\begin{vmatrix} 45.07 \\ 45.69 \end{vmatrix}$	72 73
74 75	58.31 59.10	$\begin{vmatrix} 45.56 \\ 46.17 \end{vmatrix}$	58.11 58.90	45.81  46.43	57.91 58.70	$\begin{vmatrix} 46.07 \\ 46.69 \end{vmatrix}$	57.71 58.49	$46.32 \\ 46.94$	74 75
76	59.89 60.68	46.79  $ 47.41 $	$59.68 \\ 60.47$	47.05 47.67	$59.48 \\ 60.26$	$\begin{vmatrix} 47.31 \\ 47.93 \end{vmatrix}$	$59.27 \\ 60.05$	47.57  48.20	76 77
78 79	$\begin{vmatrix} 61.46 \\ 62.25 \end{vmatrix}$	48.02	$61.25 \\ 62.04$	48.29  48.91	$61.04 \\ 61.83$	48.56  $ 49.18 $	60.83	48.82 49.45	78 79
$\frac{80}{81}$	$\frac{63.04}{63.83}$	$\frac{49.25}{49.87}$	$\frac{62.83}{63.61}$	$\frac{49.53}{50.15}$	$\frac{62.61}{63.39}$	$\frac{49.80}{50.42}$	$\frac{62.39}{63.17}$	$\frac{50.07}{50.70}$	$\frac{80}{81}$
82 83	$\begin{vmatrix} 64.62 \\ 65.40 \end{vmatrix}$	$\begin{vmatrix} 50.48 \\ 51.10 \end{vmatrix}$	64.40 65.18	50.77 $51.38$	$\begin{vmatrix} 64.17 \\ 64.96 \end{vmatrix}$	$\begin{vmatrix} 51.05 \\ 51.67 \end{vmatrix}$	$63.95 \\ 64.73$	51.33 51.95	82 83
84 85	66.19	$\begin{vmatrix} 51.72 \\ 52.33 \end{vmatrix}$	65.97 66.75	$52.00 \\ 52.62$	65.74 66.52	$\begin{bmatrix} 52.29 \\ 52.91 \end{bmatrix}$	$65.51 \\ 66.29$	52.58 53.20	84 85
86 87	67.77	52.95 53.56	$67.54 \\ 68.32$	53.24 53.86	67.30 68.09	53.54 54.16	67.07 67.85	53.83 54.46	86 87
88 89	69.34 70.13	54.18 54.79	$69.11 \\ 69.89$	$54.48 \\ 55.10$	68.87 69.65	$54.78 \\ 55.40$	68.63 69.41	55.08 55.71	88
90	70.92	55.41	70.68	$\underline{55.72}$	70.43	56.03	70.19	56.33	90
91 92	71.71 72.50	56.03 56.64	71.46   72.25   73.03	56.34 56.96	$71.22 \\ 72.00 \\ 72.78$	56.65 57.27	70.97 $71.75$	56.96 57.58	91 92
93 94 05	$\begin{vmatrix} 73.28 \\ 74.07 \\ 74.86 \end{vmatrix}$	57.26 57.87	73.03 73.82	57.58 58.19	72.78 $73.57$ $74.35$	57.89 58.52	72.53	58.21 58.84 50.46	93
95 96 97	74.86	$\begin{vmatrix} 58.49 \\ 59.10 \\ 59.72 \end{vmatrix}$	74.61 75.39	58.81 59.43	74.35 75.13	59.14 59.76	74.09 74.87	59.46   60.09   60.71	95
97 98	76.44	$\begin{bmatrix} 59.72 \\ 60.33 \\ 60.05 \end{bmatrix}$	76.18 $76.96$ $77.75$	60.05	75.91   76.70   77.48	60.38 $61.01$	75.65   76.43   77.21	60.71 $61.34$	97 98
$\frac{99}{100}$	78.01	$\begin{array}{ c c }\hline 60.95 \\ \hline 61.57 \\ \hline \end{array}$	78.53	$\frac{61.29}{61.91}$	$\frac{77.48}{78.26}$	$\begin{array}{c c} 61.63 \\ \underline{62.25} \end{array}$	$\frac{77.21}{77.99}$	$\begin{array}{c c} 61.97 \\ 62.59 \end{array}$	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	ınce.
Dista	52 ]	52 Deg. 513 Deg.		51½ l	Deg.	51½ Deg.		Distance	
		52 Deg. 51\frac{3}{4} Deg.			2		014	8	

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Distance.	39	Deg.	391	Deg.	$39\frac{1}{2}$	Deg.	39¾	Deg.	Distance
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce
1 2 3 4 5 6 7 8 9 10	$ \begin{array}{ c c c } \hline 0.78 \\ 1.55 \\ 2.33 \\ 3.11 \end{array} $	0.63 1.26 1.89 2.52 3.15 3.78 4.41 5.03 5.66 6.29	0.77 1.55 2.32 3.10 3.87 4.65 5.42 6.20 6.97 7.74	0.63 1.27 1.90 2.53 3.16 3.80 4.43 5.06 5.69 6.33	0.77 1.54 2.31 3.09 3.86 4.63 5.40 6.17 6.94 7.72	0.64 1.27 1.91 2.54 3.18 3.82 4.45 5.09 5.72 6.36	0.77 1.54 2.31 3.08 3.84 4.61 5.38 6.15 6.92 7.69	0.64 1.28 1.92 2.56 3.20 3.84 4.48 5.12 5.75 6.39	1 2 3 4 5 6 7 8 9 10
11 12 13 14 15 16 17 18 19 20	8.55 9.33 10.10 10.88 11.66 12.43 13.21 13.99 14.77 15.54	6.92 7.55 8.18 8.81 9.44 10.07 10.70 11.33 11.96 12.59	8.52 9.29 10.07 10.84 11.62 12.39 13.16 13.94 14.71 15.49	6.96 7.59 8.23 8.86 9.49 10.12 10.76 11.39 12.02 12.65	8.49 9.26 10.03 10.80 11.57 12.35 13.12 13.89 14.66 15.43	7.00 7.63 8.27 8.91 9.54 10.18 10.81 11.45 12.09 12.72	8.46 9.23 9.99 10.76 11.53 12.30 13.07 13.84 14.61 15.38	7.03 7.67 8.31 8.95 9.59 10.23 10.87 11.51 12.15 12.79	11 12 13 14 15 16 17 18 19 20
21 22 23 24 25 26 27 28 29 30	16.32 17.10 17.87 18.65 19.43 20.21 20.98 21.76 22.54 23.31	13.22 13.84 14.47 15.10 15.73 16.36 16.99 17.62 18.25 18.88	16.26 17.04 17.81 18.59 19.36 20.13 20.91 21.68 22.46 23.23	13.29 13.92 14.55 15.18 15.82 16.45 17.08 17.72 18.35 18.98	16.20 16.98 17.75 18.52 19.29 20.06 20.83 21.61 22.38 23.15	13.36 13.99 14.63 15.27 15.90 16.54 17.17 17.81 18.45 19.08	16.15 16.91 17.68 18.45 19.22 19.99 20.76 21.53 22.30 23.07	13.43 14.07 14.71 15.35 15.99 16.63 17.26 17.90 18.54 19.18	21 22 23 24 25 26 27 28 29 30
31 32 33 34 35 36 37 38 39 40	24.09 24.87 25.65 26.42 27.20 27.98 28.75 29.53 30.31 31.09	19.51 20.14 20.77 21.40 22.03 22.66 23:28 23.91 24.54 25.17	24.01 24.78 25.55 26.33 27.10 27.88 28.65 29.43 30.20 30.98	19.61 20.25 20.88 21.51 22.14 22.78 23.41 24.04 24.68 25.31	23.92 24.69 25.46 26.24 27.01 27.78 28.55 29.32 30.09 30.86	19.72 20.35 20.99 21.63 22.26 22.90 23.53 24.17 24.81 25.44	23.83 24.60 25.37 26.14 26.91 27.68 28.45 29.22 29.98 30.75	19.82 20.46 21.10 21.74 22.38 23.02 23.66 24.30 24.94 25.58	31 32 33 34 35 36 37 38 39 40
41 42 43 44 45 46 47 48 49 50	31.86 32.64 33.42 34.19 34.97 35.75 36.53 37.30 38.08 38.86	25.80 26.43 27.06 27.69 28.32 28.95 29.58 30.21 30.84 31.47	31.75 32.52 33.30 34.07 34.85 35.62 36.40 37.17 37.95 38.72	25.94 26.57 27.21 27.84 28.47 29.10 29.74 30.37 31.00 31.64	31.64 32.41 33.18 33.95 34.72 35.49 36.27 37.04 37.81 38.58	26.08 26.72 27.35 27.99 28.62 29.26 29.90 30.53 31.17 31.80	31.52 32.29 33.06 33.83 34.60 35.37 36.14 36.90 37.67 38.44	26.22 26.86 27.50 28.14 28.77 29.41 30.05 30.69 31.33 31.97	41 42 43 44 45 46 47 48 49 50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Ustance.
Dis	51 I	Deg.	50¾ I	Deg.	501	Deg.	501	Deg.	)SI/
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Dista	39	Deg.	391	Deg.	39½	Deg.	393	Deg.	Dista
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
Distance.   552 54 556 578 59 60   62 66 66 678 690   77 77 77 77 78   82 38 48 58 89 9 9 9 39 9 4	Lat.  39.63 40.41 41.19 41.97 42.74 43.52 44.30 45.07 45.85 46.63  47.41 48.18 48.96 49.74 50.51 51.29 52.07 52.85 53.52 54.40  55.18 55.95 56.73 57.51 58.29 59.06 59.84 60.62 61.39 62.17 62.95 63.73 64.50 65.28 66.06 66.83 67.61 68.39 69.17 69.94 70.72 71.50 72.27 73.05	Dep.    32.10     32.72     33.35     33.98     34.61     35.24     35.87     36.50     37.13     37.76     38.39     39.02     39.65     40.28     40.91     41.54     42.79     43.42     44.05     44.68     45.31     45.94     46.57     47.20     47.83     48.46     49.09     49.72     50.35     50.97     51.60     52.23     52.86     53.49     54.12     54.75     55.38     56.64     57.27     57.90     58.53     59.16	Lat.    39.49     40.27     41.04     41.82     42.59     43.37     44.14     44.91     45.69     46.46     47.24     48.01     48.79     49.56     50.34     51.11     51.88     52.66     53.43     54.21     54.98     55.76     56.53     57.31     58.08     58.85     59.63     60.40     61.18     61.95     62.73     63.50     64.27     65.05     65.82     66.60     67.37     68.15     68.92     69.70     70.47     71.24     72.02     72.79	Dep.    32.27   32.90   33.53   34.17   34.80   35.43   36.06   36.70   37.33   37.96   38.60   39.23   39.86   40.49   41.13   41.76   42.39   44.29   44.92   45.55   46.82   47.45   48.09   48.72   49.35   49.35   49.98   50.62   51.25   51.88   52.51   53.78   54.41   55.05   55.68   56.32   56.94   57.58   58.21   58.84   59.47	Lat.  39.35 40.12 40.90 41.67 42.44 43.21 43.98 44.75 45.53 46.30  47.07 47.84 48.61 49.38 50.16 50.93 51.70 52.47 53.24 54.01  54.79 55.56 56.33 57.10 57.87 58.64 59.42 60.19 60.96 61.73 62.50 63.27 64.04 64.82 65.59 66.36 67.13 67.90 68.67 69.45 70.22 70.99 71.76 72.53	Dep.  32.44 33.08 33.71 34.35 34.98 35.62 36.26 36.89 37.53 38.16 38.80 39.44 40.07 40.71 41.35 41.98 42.62 43.25 43.89 44.53 45.16 45.80 46.43 47.07 47.71 48.34 48.98 49.61 50.25 50.89 51.52 52.16 52.79 53.43 54.07 55.34 55.97 56.61 57.25 57.88 58.52 59.16 59.79	Lat.  39.21 39.98 40.75 41.52 42.29 43.06 43.82 44.59 45.36 46.13  46.90 47.67 48.44 49.21 49.97 50.74 51.51 52.28 53.05 53.82  54.59 55.36 56.13 56.89 57.66 58.43 59.20 59.97 60.74 61.51 62.28 63.04 63.81 64.58 65.35 66.12 66.89 67.66 68.43 69.20 69.96 70.73 71.50 72.27	32.61 33.25 33.89 34.53 35.17 35.81 36.45 37.09 37.73 38.37 39.01 39.65 40.28 40.92 41.56 42.20 42.84 43.48 44.12 44.76 45.40 46.68 47.32 47.96 49.24 49.88 50.52 51.16 51.79 52.43 53.07 53.71 54.35 54.99 55.63 56.27 56.91 57.55 58.19 58.83 59.47 60.11	Distance.   512 534 556 578 596   612 63 64 65 66 679   712 73 74 756 778 90   812 834 856 889 90   912 934 94
95 96 97 98 99 100	73.83 74.61 75.38 76.16 76.94 77.71	59.79 60.41 61.04 61.67 62.30 62.93	73.57 74.34 75.12 75.89 76.66 77.44	60.11 60.74 61.37 62.01 62.64 63.27	$egin{array}{c} 73.30 \\ 74.08 \\ 74.85 \\ 75.62 \\ 76.39 \\ 77.16 \\ \hline \end{array}$	$egin{array}{c} 60.43 \\ 61.06 \\ 61.70 \\ 62.34 \\ 62.97 \\ 63.61 \\ \hline \end{array}$	$egin{array}{c} 73.04 \\ 73.81 \\ 74.58 \\ 75.35 \\ 76.12 \\ 76.88 \\ \end{array}$	60.75 61.39 62.03 62.66 63.30 63.94	95 96 97 98 99 100
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
Distance.	51 I	Deg.	503	Deg.	501	Deg.	504	Deg.	Distance.

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to to ta	40 Lat.	Deg.	40}	Deg.	40	Deg.	40	Deg.	Dist
-	_		Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ance
10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	0.65 1.29 1.94 2.58 3.23 3.88 4.52 5.17 5.82 6.46 7.11 7.75 8.40 9.05 9.69 10.34 10.98 11.63 12.28 12.92 13.57 14.21 14.86 15.51 16.15 16.15 16.15 16.15 16.15 16.15 16.20 17.45 19.38 20.03 20.68 21.32 21.97 22.61 23.91 24.55 25.84	0.76 1.52 2.28 3.04 3.80 4.56 5.32 6.08 6.84 7.60 8.36 9.12 9.89 10.65 11.41 12.17 12.93 13.69 14.45 15.21 15.97 16.73 17.49 18.25 19.01 19.77 20.53 21.29 22.05 22.81 23.57 24.33 25.09 25.85 26.61 27.37 28.13 28.90 29.66 30.42	0.65 1.30 1.95 2.60 3.25 3.90 4.55 5.20 5.84 6.49 7.14 7.79 8.44 9.09 9.74 10.39 11.04 11.69 12.34 12.99 13.64 14.29 14.94 15.59 16.24 16.89 17.54 18.18 18.18 18.18 19.48 20.13 20.78 21.43 22.08 22.73 23.38 24.68 25.33 25.98	$\begin{array}{ c c c c c }\hline 0.76 \\ 1.52 \\ 2.27 \\ 3.03 \\ 3.79 \\ 4.55 \\ 5.30 \\ 6.06 \\ 6.82 \\ 7.58 \\\hline \hline 8.33 \\ 9.09 \\ 9.85 \\ 10.61 \\ 11.36 \\ 12.12 \\ 12.88 \\ 13.64 \\ 14.39 \\ 15.15 \\\hline \hline 15.91 \\ 16.67 \\ 17.42 \\ 18.18 \\ 18.94 \\ 19.70 \\ 20.45 \\ 21.21 \\ 21.97 \\ 22.73 \\\hline 23.48 \\ 24.24 \\ 25.00 \\ 25.76 \\ 26.51 \\ 27.27 \\ 28.03 \\ 28.79 \\ 29.54 \\ 30.30 \\\hline \end{array}$	0.65 1.31 1.96 2.61 3.26 3.92 4.57 5.22 5.87 6.53 7.18 7.83 8.49 9.14 9.79 10.44 11.10 11.75 12.40 13.06 13.71 14.36 15.01 15.67 16.32 16.97 17.62 18.28 18.28 19.58 20.24 20.89 21.54 22.19 22.85 23.50 24.15 24.80 25.46 26.11	Distance. 12345678910 11121314 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40
41 42 43 44 45 46 47 48 49 50	31.41 32.17 32.94 33.71 34.47 35.24 36.00 36.77 37.54 38.30	26.35 27.00 27.64 28.28 28.93 29.57 30.21 30.85 31.50 32.14	31.29 32.06 32.82 33.58 34.35 35.11 35.87 36.64 37.40 38.16	26.49 27.14 27.78 28.43 29.08 29.72 30.37 31.01 31.66 32.31	31.18 31.94 32.70 33.46 34.22 34.98 35.74 36.50 37.26 38.02	26.63 27.28 27.93 28.58 29.23 29.87 30.52 31.17 31.82 32.47	31.06 31.82 32.58 33.33 34.09 34.85 35.61 36.36 37.12 37.88	26.76 27.42 28.07 28.72 29.37 30.03 30.68 31.33 31.99 32.64	41 42 43 44 45 46 47 48 49 50
Distance.	Dep. 50 1	Lat.	Dep. 493 I	Lat.	Dep.	Lat.	Dep. 494 ]	Lat.	Distance.

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שַ	40	Deg.	40}	Deg.	401	Deg.	403	Deg.	ם
ista									ista
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
51	39.07	${32.78}$	$\overline{38.92}$	32.95	38.78	${33.12}$	38.64	${33.29}$	51
52 53	$\begin{vmatrix} 39.83 \\ 40.60 \end{vmatrix}$	$\begin{vmatrix} 33.42 \\ 34.07 \end{vmatrix}$	39.69 40.45	$\begin{vmatrix} 33.60 \\ 34.24 \end{vmatrix}$	$\begin{vmatrix} 39.54 \\ 40.30 \end{vmatrix}$	$\begin{vmatrix} 33.77 \\ 34.42 \end{vmatrix}$	$\begin{vmatrix} 39.39 \\ 40.15 \end{vmatrix}$	$\begin{vmatrix} 33.94 \\ 34.60 \end{vmatrix}$	52 53
54	41.37	34.71	41.21	34.89	41.06	35.07	40.91	35.25	54
55 56	$\begin{vmatrix} 42.13 \\ 42.90 \end{vmatrix}$	$\begin{vmatrix} 35.35 \\ 36.00 \end{vmatrix}$	$ \begin{array}{c} 41.98 \\ 42.74 \end{array} $	35.54	41.82 42.58	35.72 36.37	$  41.67 \\ 42.42$	$\begin{vmatrix} 35.90 \\ 36.55 \end{vmatrix}$	55 56
57	43.66	36.64	43.50	36.83	43.34	37.02	43.18	37.21	57
58 59	$\begin{vmatrix} 44.43 \\ 45.20 \end{vmatrix}$	$\begin{vmatrix} 37.28 \\ 37.92 \end{vmatrix}$	$ 44.27 \\ 45.03 $	$\begin{vmatrix} 37.48 \\ 38.12 \end{vmatrix}$	44.10	$  37.67 \\   38.32 $	43.94  44.70	$\begin{vmatrix} 37.86 \\ 38.51 \end{vmatrix}$	58 59
$\frac{60}{61}$	45.96	$\frac{38.57}{39.91}$	$\frac{45.79}{40.50}$	$\frac{38.77}{38.41}$	$\frac{45.62}{13.00}$	38.97	45.45	$\frac{39.17}{20.22}$	60
61 62	$ 46.73 \\ 47.49$	$\begin{vmatrix} 39.21 \\ 39.85 \end{vmatrix}$	$ 46.56 \\ 47.32$	$\begin{vmatrix} 39.41 \\ 40.06 \end{vmatrix}$	46.38 47.15	$\frac{39.62}{40.27}$	$46.21 \\ 46.97$	$\begin{vmatrix} 39.82 \\ 40.47 \end{vmatrix}$	61 62
63 64	48.26	40.50	48.08	40.71	47.91	40.92	47.73	41.12	63
65	$\begin{vmatrix} 49.03 \\ 49.79 \end{vmatrix}$	$\begin{vmatrix} 41.14 \\ 41.78 \end{vmatrix}$	48.85	$\begin{vmatrix} 41.35 \\ 42.00 \end{vmatrix}$	$ 48.67 \\ 49.43$	$\begin{vmatrix} 41.56 \\ 42.21 \end{vmatrix}$	48.48	$\begin{vmatrix} 41.78 \\ 42.43 \end{vmatrix}$	64 65
66 67	$\begin{vmatrix} 50.56 \\ 51.32 \end{vmatrix}$	$\begin{vmatrix} 42.42 \\ 43.07 \end{vmatrix}$	50.37	$42.64 \\ 43.29$	50.19 50.95	$ 42.86 \\ 43.51$	50.00 50.76	$\begin{vmatrix} 43.08 \\ 43.73 \end{vmatrix}$	66 67
68	52.09	43.71	51.90	43.94	51.71	44.16	51.51	44.39	68
69 70	52.86	$\left \begin{smallmatrix} 44.35\\ 45.00 \end{smallmatrix}\right $	52.66	$ \begin{array}{c} 44.58 \\ 45.23 \end{array} $	$ \begin{array}{c} 52.47 \\ 53.23 \end{array} $	44.81	52.27 $53.03$	$  45.04 \\ 45.69 $	69 70
71	54.39	45.64	54.19	45.87	53.99	46.11	53.79	46.35	71
72 73	55.16	$\left  \begin{array}{c} 46.28 \\ 46.92 \end{array} \right $	54.95	$ \begin{array}{c} 46.52 \\ 47.17 \end{array} $	54.75	46.76  $ 47.41 $	54.54	47.00  $ 47.65 $	72 73
74	56.69	47.57	56.48	47.81	56.27	48.06	56.06	48.30	74
75 76	57.45	48.21  $ 48.85 $	57.24 58.01	$\begin{array}{ c c } 48.46 \\ 49.11 \end{array}$	57.03	$\begin{vmatrix} 48.71 \\ 49.36 \end{vmatrix}$	56.82 57.57	48.96  $ 49.61 $	75 76
77 78	58.99 59.75	49.49	58.77	49.75	58.55	50.01	58.33	$50.26 \\ 50.92$	77 78
79	60.52	$\begin{bmatrix} 50.14 \\ 50.78 \end{bmatrix}$	$\begin{vmatrix} 59.53 \\ 60.30 \end{vmatrix}$	$\begin{bmatrix} 50.40 \\ 51.04 \end{bmatrix}$	$\begin{bmatrix} 59.31 \\ 60.07 \end{bmatrix}$	$50.66 \\ 51.31$	59.09 59.85	51.57	79
80	$  \frac{61.28}{62.05}  $	$\frac{51.42}{59.07}$	$\frac{61.06}{61.02}$	$\frac{51.69}{52.34}$	$\frac{60.83}{61.50}$	$\frac{51.96}{59.61}$	$\frac{60.61}{61.00}$	$\frac{52.22}{59.97}$	$\frac{80}{81}$
81 82	62.05 $62.82$	$52.07 \ 52.71$	$61.82 \\ 62.59$	$52.34 \\ 52.98$	$61.59 \\ 62.35$	$52.61 \\ 53.25$	$61.36 \\ 62.12$	52.87 53.53	81 82
83 84	$\begin{vmatrix} 63.58 \\ 64.35 \end{vmatrix}$	53.35 53.99	$63.35 \\ 64.11$	$53.63 \\ 54.27$	$63.11 \\ 63.87$	$53.90 \\ 54.55$	$\begin{vmatrix} 62.88 \\ 63.64 \end{vmatrix}$	54.18 54.83	83 84
85	65.11	54.64	64.87	54.92	64.63	55.20	64.39	55.48	85
86 87	$ 65.88  \\ 66.65 $	$\begin{bmatrix} 55.28 \\ 55.92 \end{bmatrix}$	$\begin{bmatrix} 65.64 \\ 66.40 \end{bmatrix}$	$\begin{bmatrix} 55.57 \\ 56.21 \end{bmatrix}$	$\begin{bmatrix} 65.39 \\ 66.16 \end{bmatrix}$	$\begin{bmatrix} 55.85 \\ 56.50 \end{bmatrix}$	$65.15 \\ 65.91$	56.14 56.79	86 87
88	67.41	56.57	67.16	56.86	66.92	57.15	66.67	57.44	88
89 90	$\begin{bmatrix} 68.18 \\ 68.94 \end{bmatrix}$	$\begin{bmatrix} 57.21 \\ 57.85 \end{bmatrix}$	$\begin{bmatrix} 67.93 \\ 68.69 \end{bmatrix}$	57.50 58.15	$ 67.68  \\ 68.44 $	57.80 58.45	$\begin{vmatrix} 67.42 \\ 68.18 \end{vmatrix}$	58.10 58.75	89 90
91	69.71	58.49	69.45	58.80	$\overline{69.20}$	59.10	68.94	59.40	91
92	$  \begin{array}{c} 70.48 \\ 71.24 \end{array}  $	59.14  $ 59.78 $	$\left  egin{array}{c} 70.22 \ 70.98 \end{array} \right $	59.44   60.09	$\begin{bmatrix} 69.96 \\ 70.72 \end{bmatrix}$	$\begin{array}{c} 59.75 \\ 60.40 \end{array}$	$\left  egin{array}{c} 69.70 \ 70.45 \end{array} \right $	$\begin{bmatrix} 60.05 \\ 60.71 \end{bmatrix}$	92 93
94	$72.01 \\ 72.77$	60.42	71.74 72.51	60.74	$71.48 \\ 72.24$	$61.05 \\ 61.70$	$\begin{vmatrix} 71.21 \\ 71.97 \end{vmatrix}$	$\begin{array}{c} 61.36 \\ 62.01 \end{array}$	94 95
95 96	73.54	$\begin{vmatrix} 61.06 \\ 61.71 \end{vmatrix}$	73.27	$\begin{array}{c} 61.38 \\ 62.03 \end{array}$	73.00	62.35	72.73	62.66	9.6
97 98	$74.31 \\ 75.07$	$\begin{bmatrix} 62.35 \\ 62.99 \end{bmatrix}$	$\begin{bmatrix} 74.03 \\ 74.80 \end{bmatrix}$	$\begin{bmatrix} 62.67 \\ 63.32 \end{bmatrix}$	$\begin{array}{c c} 73.76 \\ 74.52 \end{array}$	$63.00 \mid 63.65 \mid$	$\begin{vmatrix} 73.48 \\ 74.24 \end{vmatrix}$	$\begin{array}{c} 63.32 \\ 63.97 \end{array}$	97 98
99	75.84 76.60	$63.64 \\ 64.28$	75.56 76.32	$63.97 \\ 64.61$	$75.28 \\ 76.04$	$\begin{bmatrix} 64.30 \\ 64.94 \end{bmatrix}$	75.00 75.76	$64.62 \\ 65.28$	99
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
Distance.									Distance.
Dis	50 ]	Deg.	493	Deg.	491	Deg.	491	Deg.	Dis

	T.				11		11		1
Dista	41	Deg.	414	Deg.	41½	Deg.	413	Deg.	Dista
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ance
Ustance. 12345678910 111213145678910 1121314561781920 22222223 242522223 2425222223 24252222222222	Lat.  0.75 1.51 2.26	Dep.  0.66 1.31 1.97 2.62 3.28	-					Dep.  0.67 1.33 2.00 2.66 3.33 4.00 4.66 5.33 5.99 6.66 7.32 7.99 8.66 9.32 9.99 10.65 11.32 11.99 12.65 13.32 13.98 14.65 15.32 13.98 14.65 17.31 17.98 18.64 19.31 19.98 20.64 21.31 23.97 24.64 25.30 25.97	Distance. 1234567890 112134151617890 212234567890 31234567890
41 42 43 44 45 46 47 48 49 50	30.19 30.94 31.70 32.45 33.21 33.96 34.72 35.47 36.23 36.98 37.74	26.90 27.55 28.21 28.87 29.52 30.18 30.83 31.49 32.15 32.80	30.07 30.83 31.58 32.33 33.08 33.83 34.58 35.34 36.09 36.84 37.59	27.03 27.69 28.35 29.01 29.67 30.33 30.99 31.65 32.31 32.97	30.71 31.46 32.21 32.95 33.70 34.45 35.20 35.95 36.70 37.45	26.50 27.17 27.83 28.49 29.16 29.82 30.48 31.14 31.81 32.47 33.13	29.84 30.59 31.33 32.08 32.83 33.57 34.32 35.06 35.81 36.56 37.30	26.64 27.30 27.97, 28.63 29.30 29.97 30.63 31.30 31.96 32.63 33.29	40 41 42 43 44 45 46 47 48 49 50
Distance.	Dep. 49 I	Lat.	$ \begin{array}{ c c } \hline \text{Dep.} & \\ \hline 48\frac{3}{4} & \\ \hline \end{array} $	Lat.	Dep. 48½	Lat. Deg.	Dep. 48½	Lat.	Distance.

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Distance.	41 I	Deg.	411	Deg.	41½	Deg.	413	Deg.	Distance.
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
51	38.49	33.46	38.34	33.63	38.20	33.79	38.05	33.96	51
52 53	$\frac{39.24}{40.00}$	$\frac{34.12}{34.77}$	$\begin{vmatrix} 39.10 \\ 39.85 \end{vmatrix}$	$\frac{34.29}{34.95}$	$\begin{vmatrix} 38.95 \\ 39.69 \end{vmatrix}$	$\begin{vmatrix} 34.46 \\ 35.12 \end{vmatrix}$	$\begin{vmatrix} 38.79 \\ 39.54 \end{vmatrix}$	$\frac{34.63}{35.29}$	52 53
54	40.75	35.43	40.60	35,60	40.44	35.78	40.29	35.96	54
55 56	$\begin{array}{c} 41.51 \\ 42.26 \end{array}$	$\begin{array}{c c} 36.08 \\ 36.74 \end{array}$	$ \begin{array}{c} 41.35 \\ 42.10 \end{array} $	$egin{array}{c} 36.26 \ 36.92 \end{array}$	$ \begin{array}{c} 41.19 \\ 41.94 \end{array} $	$\begin{vmatrix} 36.44 \\ 37.11 \end{vmatrix}$	41.03  $ 41.78 $	$\frac{36.62}{37.29}$	55 56
57	43.02	37.40	42.85	37.58	42.69	37.77	42.53	37.96	57
58 59	$\begin{array}{ c c } 43.77 \\ 44.53 \end{array}$	38.05 38.71	43.61  $ 44.36 $	$\frac{38.24}{38.90}$	43.44  $ 44.19 $	$\begin{vmatrix} 38.43 \\ 39.09 \end{vmatrix}$	$\begin{vmatrix} 43.27 \\ 44.02 \end{vmatrix}$	$\frac{38.62}{39.29}$	58 59
60	45.28	39.36	45.11	39.56	44.94	39.76	44.76	39.95	60
61 62	$ 46.04  \\ 46.79$	40.02  $ 40.68 $	$45.86 \\ 46.61$	$ 40.22  \  40.88 $	45.69  46.44	40.42	45.51  46.26	$\frac{40.62}{41.28}$	61 62
63	47.55	41.33	47.37	41.54	47.18	41.75	47.00	41.95	63
64 65	48.30  $ 49.06 $	$ \begin{array}{c} 41.99 \\ 42.64 \end{array} $	$ \begin{array}{c} 48.12 \\ 48.87 \end{array} $	$\begin{vmatrix} 42.20 \\ 42.86 \end{vmatrix}$	47.93	$\begin{vmatrix} 42.41 \\ 43.07 \end{vmatrix}$	47.75	$42.62 \\ 43.28$	64 65
66	49.81	43.30	49.62	43.52	49.43	43.73	49.24	43.95	66
67 68	50.57  $ 51.32 $	43.96  44.61	50.37	$ 44.18  \  44.84 $	50.18	$ \begin{array}{c} 44.40 \\ 45.06 \end{array} $	49.99 50.73	$\frac{44.61}{45.28}$	67 68
69	52.07	45.27	51.88	45.49	51.68	45.72	51.48	45.95	69
$\frac{70}{7}$	$\frac{52.83}{59.50}$	45.92	$\frac{52.63}{59.00}$	$\frac{46.15}{46.01}$	$\frac{52.43}{59.10}$	46.38	$\frac{52.22}{52.07}$	46.61	70
71 72	$\begin{vmatrix} 53.58 \\ 54.34 \end{vmatrix}$	$ 46.58  \ 47.24 $	53.38	46.81  47.47	$\begin{vmatrix} 53.18 \\ 53.92 \end{vmatrix}$	47.05 47.71	$\begin{bmatrix} 52.97 \\ 53.72 \end{bmatrix}$	47.28 47.94	71 72
73	55.09	47.89	54.88	48.13	54.67	48.37	54.46	48.61	73
74 75	55.85	$48.55 \\ 49.20$	$55.64 \\ 56.39$	$\begin{array}{c} 48.79 \\ 49.45 \end{array}$	58.42 56.17	$\begin{vmatrix} 49.03 \\ 49.70 \end{vmatrix}$	55.21 55.95	$49.28 \\ 49.94$	74 75
76	57.36	49.86	57.14	50.11	56.92	50.36	56.70	50.61	76 77
77	58.11 58.87	$50.52 \\ 51.17$	57.89	$\begin{bmatrix} 50.77 \\ 51.43 \end{bmatrix}$	57.67 58.42	$\begin{bmatrix} 51.02 \\ 51.68 \end{bmatrix}$	57.45 58.19	51.27	78
79 80	$\begin{bmatrix} 59.62 \\ 60.38 \end{bmatrix}$	51.83	59.40	$\left  egin{array}{c} 52.09 \ 52.75 \end{array} \right $	59.17 59.92	$\begin{vmatrix} 52.35 \\ 53.01 \end{vmatrix}$	58.94 59.68	$52.60 \\ 53.27$	79 80
81	$\frac{60.33}{61.13}$	$\frac{53.48}{53.14}$	$\frac{60.13}{60.90}$	$\frac{52.15}{53.41}$	$\frac{33.32}{60.67}$	$\frac{53.67}{53.67}$		$\frac{53.21}{53.94}$	81
82	61.89	53.80	61.65	54.07	61.41	54.33	61.18	54.60	82
83 84	$\begin{vmatrix} 62.64 \\ 63.40 \end{vmatrix}$	54.45	$62.40 \\ 63.15$	54.73	62.16 $62.91$	55.00 55.66	$61.92 \\ 62.67$	55.27 55.93	83 84
85	64.15	55.76	63.91	56.04	63.66	56.32	63.41	56.60	85
86 87	$  64.90 \\ 65.66  $	$\begin{bmatrix} 56.42 \\ 57.08 \end{bmatrix}$	$\begin{vmatrix} 64.66 \\ 65.41 \end{vmatrix}$	$\begin{array}{ c c c } 56.70 \\ 57.36 \end{array}$	64.41	56.99	$64.16 \\ 64.91$	57.27 57.93	86 87
88	66.41	57.73	66.16	58.02	65.91	58.31 58.97	65.65	58.60	88
89	$\begin{vmatrix} 67.17 \\ 67.92 \end{vmatrix}$	58.39 59.05	$66.91 \\ 67.67$	58.68   59.34	67.41	59.64	$66.40 \\ 67.15$	$\begin{array}{c} 59.26 \\ 59.93 \end{array}$	89 90
91	68.68	59.70	68.42	60.00	68.15	60.30	67.89	60.69	91
92 93	$\begin{vmatrix} 69.43 \\ 70.19 \end{vmatrix}$	60.36	$\begin{bmatrix} 69.17 \\ 69.92 \end{bmatrix}$	60.66	$\begin{vmatrix} 68.90 \\ 69.65 \end{vmatrix}$	60.96  $ 61.62 $	$68.64 \\ 69.38$	$\begin{vmatrix} 61.26 \\ 61.93 \end{vmatrix}$	$\begin{bmatrix} 92 \\ .93 \end{bmatrix}$
94	70.94	61.67	70.67	61.98	70.40	62.29	70.13	62.59	94
95 96	$\begin{vmatrix} 71.70 \\ 72.45 \end{vmatrix}$	$\begin{vmatrix} 62.33 \\ 62.98 \end{vmatrix}$	71.43 72.18	$\begin{bmatrix} 62.64 \\ 63.30 \end{bmatrix}$	$71.15 \\ 71.90$	$\begin{bmatrix} 62.95 \\ 63.61 \end{bmatrix}$	$70.88 \\ 71.62$	$\begin{vmatrix} 63.26 \\ 63.92 \end{vmatrix}$	95 96
97	73.21	63.64	72.93	63.96	72.65	64.27	72.37	64.59	97
98	$73.96 \\ 74.72$	$64.29 \\ 64.95$	$ 73.68  \\ 74.43$	$\left egin{array}{c} 64.62 \ 65.28 \ \end{array} ight $	73.40	$  64.94 \\ 65.60  $	$73.11 \\ 73.86$	65.26 $65.92$	$\begin{bmatrix} 98 \\ 99 \end{bmatrix}$
100	75.47	65.61	75.18	$\boxed{\frac{65.93}{}}$	74.90	$\boxed{66.26}$	74.61	66.59	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
star								-	stai
Di	49 1	Deg.	483	Deg.	481	Deg.	481	Deg.	Di
					-		*******		PROTECTION

Distance	42 I	eg.	421	Deg.	421	Deg.	423	Deg.	Distance
ınce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
1 2 3 4 5 6 7 8 9 10	0.74 1.49 2.23 2.97 3.72 4.46 5.20 5.95 6.69 7.43	0.67 1.34 2.01 2.68 3.35 4.01 4.68 5.35 6.02 6.69	0.74 1.48 2.22 2.96 3.70 4.44 5.18 5.92 6.66 7.40	0.67 1.34 2.02 2.69 3.36 4.03 4.71 5.38 6.05 6.72	0.74 1.47 2.21 2.95 3.69 4.42 5.16 5.90 6.64 7.37	0.68 1.35 2.03 2.70 3.38 4.05 4.73 5.40 6.08 6.76	0.73 1.47 2.20 2.94 3.67 4.41 5.14 5.87 6.61 7.34	0.68 1.36 2.04 2.72 3.39 4.07 4.75 5.43 6.11 6.79	1 2 3 4 5 6 7 8 9
11 12 13 14 15 16 17 18 19 20	8.17 8.92 9.66 10.40 11.15 11.89 12.63 13.38 14.12 14.86	7.36 8.03 8.70 9.37 10.04 10.71 11.38 12.04 12.71 13.38	8.14 8.88 9.62 10.36 11.10 11.84 12.58 13.32 14.06 14.80	7.40 8.07 8.74 9.41 10.09 10.76 11.43 12.10 12.77 13.45	8.11 8.85 9.58 10.32 11.06 11.80 12.53 13.27 14.01 14.75	7.43 8.11 8.78 9.46 10.13 10.81 11.48 12.16 12.84 13.51	8.08 8.81 9.55 10.28 11.01 11.75 12.48 13.22 13.95 14.69	7.47 8.15 8.82 9.50 10.18 10.86 11.54 12.22 12.90 13.58	11 12 13 14 15 16 17 18 19 20
21 22 23 24 25 26 27 28 29 30	15.61 16.35 17.09 17.84 18.58 19.32 20.06 20.81 21.55 22.29	14.05 14.72 15.39 16.06 16.73 17.40 18.07 18.74 19.40 20.07	15.54 16.28 17.02 17.77 18.51 19.25 19.99 20.73 21.47 22.21	14.12 14.79 15.46 16.14 16.81 17.48 18.15 18.83 19.50 20.17	15.48 16.22 16.96 17.69 18.43 19.17 19.91 20.64 21.38 22.12	14.19 14.86 15.54 16.21 16.89 17.57 18.24 18.92 19.59 20.27	15.42 16.16 16.89 17.62 18.36 19.09 19.83 20.56 21.30 22.03	14.25 14.93 15.61 16.29 16.97 17.65 18.33 19.01 19.69 20.36	21 22 23 24 25 26 27 28 29 30
31 32 33 34 35 36 37 38 39 40	23.04 23.78 24.52 25.27 26.01 26.75 27.50 28.24 28.98 29.73	20.74 21.41 22.08 22.75 23.42 24.09 24.76 25.43 26.10 26.77	22.95 23.69 24.43 25.17 25.91 26.65 27.39 28.13 28.87 29.61	20.84 21.52 22.19 22.86 23.53 24.21 24.88 25.55 26.22 26.89	22.86 23.59 24.33 25.07 25.80 26.54 27.28 28.02 28.75 29.49	20.94 21.62 22.29 22.97 23.65 24.32 25.00 25.67 26.35 27.02	22.76 23.50 24.23 24.97 25.70 26.44 27.17 27.90 28.64 29.37	21.04 21.72 22.40 23.08 23.76 24.44 25.12 25.79 26.47 27.15	31 32 33 34 35 36 37 38 39 40
41 42 43 44 45 46 47 48 49 50	30.47 31.21 31.96 32.70 33.44 34.18 34.93 35.67 36.41	27.43 28.10 28.77 29.44 30.11 30.78 31.45 32.12 32.79 33.46	30.35 31.09 31.83 32.57 33.31 34.05 34.79 35.53 36.27 37.01	27.57 28.24 28.91 29.58 30.26 30.93 31.60 32.27 32.95 33.62	30.23 30.97 31.70 32.44 33.18 33.91 34.65 35.39 36.13 36.86	27.70 28.37 29.05 29.73 30.40 31.08 31.75 32.43 33.10 33.78	30.11 30.84 31.58 32.31 33.04 33.78 34.51 35.25 35.98 36.72	27.83 28.51 29.19 29.87 30.55 31.22 31.90 32.58 33.26 33.94	41 42 43 44 45 46 47 48 49 50
Distance.	Dep. 48	Lat. Deg.	Dep. 47 <sup>3</sup> / <sub>4</sub>	Lat. Deg.	Dep. 47½	Lat. Deg.	Dep. 47¼	Lat. Deg.	Distance.

Distance	42 I	Deg.	421	Deg.	421	Deg.	423	Deg.	Dist
ance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
51 52 53 54 55 55 55 56 61 62 63 64 65 66 67 77 77 77 77 77 77 77 77 77 77 77	$37.90$ $38.64$ $39.39$ $40.13$ $40.87$ $41.62$ $42.36$ $43.10$ $43.85$ $44.59$ $\hline 45.33$ $46.07$ $46.82$ $47.56$ $48.30$ $49.05$ $49.79$ $50.53$ $51.28$ $52.02$ $\hline 52.76$ $53.51$ $54.25$ $54.99$ $55.74$ $56.48$ $57.22$ $57.97$ $58.71$ $59.45$ $\hline 60.19$ $60.94$ $61.68$ $62.42$ $63.17$ $63.91$	34.13 34.79 35.46 36.13 36.80 37.47 38.14 38.81 39.48 40.15 40.82 41.49 42.16 42.82 43.49 44.16 44.83 45.50 46.17 46.84 47.51 48.85 49.52 50.18 50.85 51.52 52.19 52.86 53.53 54.20 54.87 55.54 56.21 56.88 57.55	37.75 38.49 39.23 39.97 40.71 41.45 42.19 42.93 43.67 44.41 45.15 45.89 46.63 47.37 48.11 48.85 49.59 50.33 51.07 51.82 52.56 53.30 54.04 54.78 55.52 56.26 57.00 57.74 58.48 59.22 59.96 60.70 61.44 62.18 62.92 63.66	Dep.  34.29 34.96 35.64 36.31 36.98 37.65 38.32 39.00 39.67 40.34  41.69 42.36 43.70 44.38 45.05 45.72 46.39 47.07  47.74 48.41 49.08 49.76 50.43 51.10 51.77 52.44 53.12 53.79  54.46 55.13 55.81 56.48 57.15 57.82	Lat.       37.60       38.34       39.08       39.81       40.55       41.29       42.76       43.50       44.24       44.97       45.71       46.45       47.19       47.92       48.66       49.40       50.13       50.87       51.61       52.35       53.08       53.82       54.56       55.30       56.77       57.51       58.24       59.72       60.46       61.19       62.67       63.41	34.46       35.13       35.81       36.48       37.16       37.83       38.51       39.86       40.54       41.21       41.89       42.56       43.24       43.91       44.59       45.94       46.62       47.29       47.97       48.64       49.32       49.99       50.67       51.34       52.02       53.37       54.72       55.40       56.75       57.43       58.10	37.45 38.18 38.92 39.65 40.39 41.12 41.86 42.59 43.32 44.06 44.79 45.53 46.26 47.00 47.73 48.47 49.20 49.93 50.67 51.40 52.14 55.87 53.61 54.34 55.07 55.81 56.54 57.28 58.01 58.75 59.48 60.21 60.95 61.68 62.42 63.15	34.62 35.30 35.98 36.66 37.33 38.01 38.69 39.37 40.05 40.73 41.41 42.09 42.76 43.44 44.12 44.80 45.48 46.16 46.84 47.52 48.19 48.87 49.55 50.23 50.91 51.59 52.27 52.95 53.63 54.98 55.66 56.34 57.02 57.70 58.38	51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 70 71 72 73 74 75 77 78 79 80 81 82 83 84 85 86 86 87 87 87 87 87 87 87 87 87 87
$ \begin{vmatrix} 87 \\ 83 \\ 89 \\ 90 \\ \hline 91 \end{vmatrix} $	$ \begin{array}{r} 64.65 \\ 65.40 \\ 66.14 \\ 66.88 \\ \hline 67.63 \end{array} $	$ \begin{array}{r} 58.21 \\ 58.88 \\ 59.55 \\ 60.22 \\ \hline 60.89 \end{array} $	$ \begin{array}{r} 64.40 \\ 65.14 \\ 65.88 \\ 66.62 \\ \hline 67.36 \end{array} $	58.50 $59.17$ $59.84$ $60.51$	64.14 64.88 65.62 66.35	58.78 59.45 60.13 60.80	$\begin{bmatrix} 63.89 \\ 64.62 \\ 65.35 \\ 66.09 \\ \hline 66.82 \\ \end{bmatrix}$	$ \begin{array}{r} 59.06 \\ 59.73 \\ 60.41 \\ 61.09 \\ \hline 61.77 \end{array} $	$ \begin{array}{ c c } 87 \\ 88 \\ 89 \\ 90 \\ \hline 91 \end{array} $
92 93 94 95 96 97 98 99 100	68.37 69.11 69.86 70.60 71.34 72.08 72.83 73.57 74.31	61.56 62.23 62.90 63.57 64.24 64.91 65.57 66.24 66.91	68.10 68.84 69.58 70.32 71.06 71.80 72.54 73.28 74.02	61.19 61.86 62.53 63.20 63.87 64.55 65.22 65.89 66.56 67.24	67.09 67.83 68.57 69.30 70.04 70.78 71.52 72.25 72.99 73.73	61.48 62.15 62.83 63.51 64.18 64.86 65.53 66.21 66.88 67.56	67.56 68.29 69.03 69.76 70.49 71.23 71.96 72.70 73.43	62.45 63.13 63.81 64.49 65.16 65.84 66.52 67.20 67.88	92 93 94 95 96 97 98 99 100
Distance.	13°	Lat.	Dep. 473	Lat. Deg.	Dep. 47½	Lat. Deg.	Dep. 471	Lat. Deg.	Distance.

Distance.	43	Deg.	431	Deg.	431/2	Deg.	433	Deg.	Dist
ance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
1	0.73	0.68	0.73	0.69	0.73	0.69	0.72	0.69	1
2	1.46	1.36	1.46	1.37	1.45	1.38	1.44	1.38	2
3	2.19	2.05	2.19	2.06	2.18	2.07	2.17	2.07	3
4	2.93	2.73	2.91	2.74	2.90	2.75	2.89	2.77	4
5	3.66	3.41	3.64	3.43	3.63	3.44	3.61	3.46	5
6	4.39	4.09	4.37	4.11	4.35	4.13	4.33	4.15	6
7	5.12	4.77	5.10	4.80	5.08	4.82	5.06	4.84	7
8	5.85	5.46	5.83	5.48	5.80	5.51	5.78	5.53	8
9	6.58	6.14	6.56	6.17	6.53	6.20	6.50	6.22	9
10	7.31	6.82	7.28	6.85	7.25	6.88	7.22	6 92	10
11	8.04	7.50	8.01	7.54	7.98	7.57	7.95	7.61	11
12	8.78	8.18	8.74	8.22	8.70	8.26	8.67	8.30	12
13	9.51	8.87	9.47	8.91	9.43	8.95	9.39	8.99	13
14	10.24	9.55	10.20	9.59	10.16	9.64	10.11	9.68	14
15	10.97	10.23	10.93	10.28	10.88	10.33	10.84	10.37	15
16	11.70	10.91	11.65	10.96	11.61	11.01	11.56	11.06	16
17	12.43	11.59	12.38	11.65	12.33	11.70	12.28	11.76	17
18	13.16	12.28	13.11	12.33	13.06	12.39	13.00	12.45	18
19	13.90	12.96	13.84	13.02	13.78	13.08	13.72	13.14	19
20	14.63	13.64	14.57	13.70	14.51	13.77	14.45	13.83	20
-21 22 23 24 25 26 27 28 29 30	15.36 16.09 16.82 17.55 18.28 19.02 19.75 20.48 21.21 21.94	14.32 15.00 15.69 16.37 17.05 17.73 18.41 19.10 19.78 20.46	15.30 16.02 16.75 17.48 18.21 18.94 19.67 20.39 21.12 21.85	14.39 15.07 15.76 16.44 17.13 17.81 18 50 19.19 19.87 20.56	15.23 15.96 16.68 17.41 18.13 18.86 19.59 20.31 21.04 21.76	14.46 15.14 15.83 16.52 17.21 17.90 18.59 19.27 19.96 20.65	15.17 15.89 16.61 17.34 18.06 18.78 19.50 20.23 20.95 21.67	14.52 15.21 15.90 16.60 17.29 17.98 18.67 19.36 20.05 20.75	21 22 23 24 25 26 27 28 29
31	22.67	21.14	22.58	21.24	22.49	21.34	22.39	21.44	31
32	23.40	21.82	23.31	21.93	23.21	22.03	23.12	22.13	32
33	24.13	22.51	24.04	22.61	23.94	22.72	23.84	22.82	33
34	24.87	23.19	24.76	23.30	24.56	23.40	24.56	23.51	34
35	25.60	23.87	25.49	23.98	25.39	24.09	25.28	24.20	35
36	26.33	24.55	26.22	24.67	26.11	24.78	26.01	24.89	36
37	27.06	25.23	26.95	25.35	26.84	25.47	26.73	25.59	37
38	27.79	25.92	27.68	26.04	27.56	26.16	27.45	26.28	38
39	28.52	26.60	28.41	26.72	28.29	26.85	28.17	26.97	39
40	29.25	27.28	29.13	27.41	29.01	27.53	28.89	27.66	40
41	29.99	27.96	29.86	28.09	29.74	28.22	29.62	28.35	41
42	30.72	28.64	30.59	28.78	30.47	28.91	30.34	29.04	42
43	31.45	29.33	31.32	29.46	31.19	29.60	31.06	29.74	43
44	32.18	30.01	32.05	30.15	31.92	30.29	31.78	30.43	44
45	32.91	30.69	32.78	30.83	32.64	30.98	32.51	31.12	45
46	33.64	31.37	33.51	31.52	33.37	31.66	33.23	31.81	46
47	34.37	32.05	34.23	32.20	34.09	32.35	33.95	32.50	47
48	35.10	32.74	34.96	32.89	34.82	33.04	34.67	33.19	48
49	35.84	33.42	35.69	33.57	35.54	33.73	35.40	33.88	49
50	36.57	34.10	36.42	34.26	36.27	34.42	36.12	34.58	50
Distance.	Dep. 47	Lat.	Dep. 463	Lat. Deg.	Dep. 46½	Lat. Deg.	Dep. 461	Lat. Deg.	Distance.

Ы	12	Deg.	121	Deg.	121	Deg.	123	Deg.	
Distance	40	Deg.	404	Deg.	452	Deg.	401	Deg.	Distance.
_ •	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51 52 53	$\begin{vmatrix} 37.30 \\ 38.03 \\ 38.76 \end{vmatrix}$	34.78 35.46 36.15	$\begin{vmatrix} 37.15 \\ 37.88 \\ 38.60 \end{vmatrix}$	34.94 35.63 36.31	$   \begin{array}{r}     36.99 \\     37.72 \\     38.44   \end{array} $	$35.11 \\ 35.79 \\ 36.48$	36.84 37.56 38.29	35.27 35.96 36.65	51 52 53
54 55 56	$\begin{vmatrix} 39.49 \\ 40.22 \\ 40.96 \end{vmatrix}$	$\begin{vmatrix} 36.83 \\ 37.51 \\ 38.19 \end{vmatrix}$	$\begin{vmatrix} 39.33 \\ 40.06 \\ 40.79 \end{vmatrix}$	$\begin{vmatrix} 37.00 \\ 37.69 \\ 38.37 \end{vmatrix}$	$\begin{vmatrix} 39.17 \\ 39.90 \\ 40.62 \end{vmatrix}$	$\begin{vmatrix} 37.17 \\ 37.86 \\ 38.55 \end{vmatrix}$	$\begin{vmatrix} 39.01 \\ 39.73 \\ 40.45 \end{vmatrix}$	37.34 38.03 38.72	54 55 56
57 58 59	$\begin{vmatrix} 41.69 \\ 42.42 \\ 43.15 \end{vmatrix}$	$\begin{vmatrix} 38.87 \\ 39.56 \\ 40.24 \end{vmatrix}$	$\begin{vmatrix} 41.52 \\ 42.25 \\ 42.97 \end{vmatrix}$	$\begin{vmatrix} 39.06 \\ 39.74 \\ 40.43 \end{vmatrix}$	$\begin{vmatrix} 41.35 \\ 42.07 \\ 42.80 \end{vmatrix}$	$\begin{vmatrix} 39.24 \\ 39.92 \\ 40.61 \end{vmatrix}$	$\begin{vmatrix} 41.17 \\ 41.90 \\ 42.62 \end{vmatrix}$	$\begin{vmatrix} 39.42 \\ 40.11 \\ 40.80 \end{vmatrix}$	57 58 59
$\frac{60}{61}$	$\frac{ 43.88 }{44.61}$	$\frac{40.92}{41.60}$	$\frac{43.70}{44.43}$	$\frac{41.11}{41.80}$	$\frac{43.52}{44.25}$	$\frac{41.30}{41.99}$	$\begin{vmatrix} 43.34 \\ \overline{44.06} \end{vmatrix}$	$\frac{41.49}{42.18}$	$\left  \frac{60}{61} \right $
62 63 64	$\begin{vmatrix} 45.34 \\ 46.08 \\ 46.81 \end{vmatrix}$	$\begin{vmatrix} 42.28 \\ 42.97 \\ 43.65 \end{vmatrix}$	$\begin{vmatrix} 45.16 \\ 45.89 \\ 46.62 \end{vmatrix}$	42.48 43.17 43.85	$\begin{vmatrix} 44.97 \\ 45.70 \\ 46.42 \end{vmatrix}$	$\begin{vmatrix} 42.68 \\ 43.37 \\ 44.05 \end{vmatrix}$	44.79 45.51 46.23	$\begin{vmatrix} 42.87 \\ 43.57 \\ 44.26 \end{vmatrix}$	$\begin{array}{c c} 62 \\ 63 \\ 64 \end{array}$
65 66	47.54 48.27	$\begin{array}{ c c }\hline 44.33\\ 45.01\\ \hline\end{array}$	47.34 48.07	$44.54 \\ 45.22$	47.15  $ 47.87 $	$\begin{array}{ c c }\hline 44.74\\ 45.43\\ \hline\end{array}$	46.95 47.68	44.95 45.64	65 66
67 68 69	$\begin{vmatrix} 49.00 \\ 49.73 \\ 50.46 \end{vmatrix}$	$\begin{vmatrix} 45.69 \\ 46.38 \\ 47.06 \end{vmatrix}$	$\begin{vmatrix} 48.80 \\ 49.53 \\ 50.26 \end{vmatrix}$	$\begin{array}{c} 45.91 \\ 46.59 \\ 47.28 \end{array}$	$\begin{vmatrix} 48.60 \\ 49.33 \\ 50.05 \end{vmatrix}$	$egin{array}{c} 46.12 \ 46.81 \ 47.50 \ \end{array}$	48.40 49.12 49.84	$\begin{array}{c} 46.33 \\ 47.02 \\ 47.71 \end{array}$	67 68 69
$\frac{70}{71}$	$\frac{51.19}{51.93}$	$\frac{47.74}{48.42}$	$\frac{50.99}{51.71}$	$\frac{47.96}{48.65}$	$\frac{50.78}{51.50}$	$\frac{48.18}{48.87}$	$\begin{array}{ c c c }\hline 50.57\\\hline 51.29\\\hline \end{array}$	$\frac{48.41}{49.10}$	$\frac{70}{71}$
72 73 74	52.66 53.39 54.12	$\begin{vmatrix} 49.10 \\ 49.79 \\ 50.47 \end{vmatrix}$	52.44 53.17 53.90	$\begin{vmatrix} 49.33 \\ 50.02 \\ 50.70 \end{vmatrix}$	52.23 52.95 53.68	$\begin{vmatrix} 49.56 \\ 50.25 \\ 50.94 \end{vmatrix}$	52.01 52.73 53.45	$\begin{vmatrix} 49.79 \\ 50.48 \\ 51.17 \end{vmatrix}$	72 73 74
75 76	54.85 55.58	$51.15 \\ 51.83$	54.63 55.36	$51.39 \\ 52.07$	54.40 55.13	$51.63 \\ 52.31$	54.18 54.90	51.86 52.55	75 76
77 78 79	56.31 57.05 57.78	$\begin{bmatrix} 52.51 \\ 53.20 \\ 53.88 \end{bmatrix}$	56.08 56.81 57.54	$\begin{bmatrix} 52.76 \\ 53.44 \\ 54.13 \end{bmatrix}$	55.85 56.58 57.30	$\begin{bmatrix} 53.00 \\ 53.69 \\ 54.38 \end{bmatrix}$	55.62 56.34 57.07	53.25 53.94 54.63	77 78 79
$\frac{80}{81}$	$\frac{58.51}{59.24}$	$\frac{54.56}{55.24}$	$\frac{58.27}{59.00}$	$\frac{54.81}{55.50}$	$\frac{58.03}{58.76}$	$\frac{55.07}{55.76}$	$\begin{array}{ c c }\hline 57.79\\ \hline 58.51\\ \hline \end{array}$	$\frac{55.32}{56.01}$	$\frac{80}{81}$
82 83	59.97 60.70 61.43	55.92 56.61	59.73 60.45	56.18 56.87	$59.48 \\ 60.21$	56.45 57.13	59.23 59.96	56.70 57.40	82 83 84
84 85 86	$\begin{vmatrix} 62.17 \\ 62.90 \end{vmatrix}$	57.29 57.97 58.65	$\begin{vmatrix} 61.18 \\ 61.91 \\ 62.64 \end{vmatrix}$	57.56 58.24 58.93	$\begin{vmatrix} 60.93 \\ 61.66 \\ 62.38 \end{vmatrix}$	57.82 58.51 59.20	$\begin{vmatrix} 60.68 \\ 61.40 \\ 62.12 \end{vmatrix}$	58.09 58.78 59.47	85 86
87 88 89	$\begin{vmatrix} 63.63 \\ 64.36 \\ 65.09 \end{vmatrix}$	$\begin{bmatrix} 59.33 \\ 60.02 \\ 60.70 \end{bmatrix}$	$\begin{vmatrix} 63.37 \\ 64.10 \\ 64.82 \end{vmatrix}$	59.61 60.30 60.98	63.11 63.83 64.56	59.89 60.58 61.26	$\begin{bmatrix} 62.85 \\ 63.57 \\ 64.29 \end{bmatrix}$	$60.16 \\ 60.85 \\ 61.54$	87 88 89
$\frac{90}{91}$	$\frac{65.82}{66.55}$	$\frac{61.38}{62.06}$	$\frac{65.55}{66.28}$	$\frac{61.67}{62.35}$	$\frac{65.28}{66.01}$	$\frac{61.20}{62.64}$	$\frac{65.01}{65.74}$	$\frac{62.24}{62.93}$	$\frac{90}{91}$
92 93	$  67.28 \\ 68.02 $	$\begin{bmatrix} 62.74 \\ 63.43 \end{bmatrix}$	$67.01 \\ 67.74$	$\begin{bmatrix} 63.04 \\ 63.72 \end{bmatrix}$	66.73	$\begin{bmatrix} 63.33 \\ 64.02 \end{bmatrix}$	$66.46 \\ 67.18$	$\begin{array}{c} 63.62 \\ 64.31 \end{array}$	92 93
94 95 96	$\begin{vmatrix} 68.75 \\ 69.48 \\ 70.21 \end{vmatrix}$	$\begin{vmatrix} 64.11 \\ 64.79 \\ 65.47 \end{vmatrix}$	$\begin{vmatrix} 68.47 \\ 69.20 \\ 69.92 \end{vmatrix}$	$64.41 \ 65.09 \ 65.78$	$\begin{vmatrix} 68.19 \\ 68.91 \\ 69.64 \end{vmatrix}$	$64.71 \ 65.39 \ 66.08$	$\begin{vmatrix} 67.90 \\ 68.62 \\ 69.35 \end{vmatrix}$	$65.00 \\ 65.69 \\ 66.39$	94 95 96
97 98	$\begin{vmatrix} 70.21 \\ 70.94 \\ 71.67 \end{vmatrix}$	66.15	70.65	66.46 67.15	$\begin{vmatrix} 09.04 \\ 70.36 \\ 71.09 \end{vmatrix}$	$66.77 \\ 67.46$	$70.07 \\ 70.79$	$67.08 \\ 67.77$	97 98
99 100	$\begin{vmatrix} 72.40 \\ 73.14 \end{vmatrix}$	$\begin{array}{ c c }\hline 67.52 \\ 68.20 \\ \hline \end{array}$	$     \begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\frac{67.83}{68.52}$	$71.81 \\ 72.54$	68.15 68.84	$71.51 \\ 72.24$	$\frac{68.46}{69.15}$	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
Dist	47 I	47 Deg. 46 <sup>3</sup> Deg.		Deg.	$46\frac{1}{2}$	Deg.	461	Dist	
-	47 Deg. 464 Deg.								

		11		Ti				II		
Dista	44 Deg.	. 444	Deg.	44½	Deg.	443	Deg.	45	Deg.	Dista
nce.	Lat. De	p. Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ınce
19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	69 0.7 39 1.4 2.8 47 2.8 47 4.3 86 5.0 5.6 25 6.4 95 7.1 7.8 8.6 9.3 10.7 11.4 8.6 9.3 10.7 11.4 12.18 12.8 13.6 14.3 15.0 14.3 15.0 16.4 17.9 16.4 17.9 16.4 17.9 16.4 17.9 16.4 17.9 16.4 17.9 16.4 17.9 16.4 17.9 16.4 17.9 16.4 17.9 16.4 17.9 16.4 17.9 16.4 17.9 16.6 17.9 16.6 17.9 16.6 17.9 16.6 17.9 16.6 17.9 16.6 17.9 16.6 17.9 16.6 17.9 16.6 17.9 16.6 17.9 16.6 17.9 16.6 17.9 16.6 17.9 16.6 17.9 16.6 17.9 16.6 17.9 17.9 18.6 19.3 10.7	2         0.70           1.40         2.09           2.79         3.49           4.19         4.88           6.28         6.98           7.68         8.37           9.07         10.47           11.16         11.86           12.56         13.26           13.96         14.65           15.35         16.05           16.75         17.44           18.14         18.84           19.54         20.93           21.63         23.72           24.42         25.82           25.82         27.21           27.91         28.61           28.61         30.70           31.40         32.80           32.80         32.80	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	0.70 1.40 2.10 2.80 3.50 4.21 4.91 5.61 6.31 7.71 8.41 9.81 10.51 11.92 12.62 13.32 14.02 14.72 15.42 16.82 17.52 18.92 14.02 14.72 15.42 16.82 17.52 18.92 19.63 20.33 21.03 21.73 22.43 23.83 24.53 25.23 26.63 27.34 28.74 29.44 30.14	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	0.71 1.41 2.11 2.82 3.52 4.22 4.93 5.63 6.34 7.74 8.45 9.15 9.86 10.56 11.26 11.97 12.67 13.38 14.08 14.78 15.49 16.19 16.90 17.60 19.01 19.71 20.42 21.12 21.82 22.53 23.23 23.24 24.64 25.36 25.75 27.46 28.16 28.66 28.67 30.98 31.68 32.38 33.09	0.71 1.41 2.12 2.83 3.54 4.95 5.66 6.36 7.07 7.78 8.49 9.19 9.90 10.61 11.31 12.02 12.73 13.43 14.14 14.85 15.56 16.26 16.97 17.68 18.38 19.90 20.51 21.21 22.63 23.33 24.04 24.75 25.46 26.87 27.58 28.28 28.28 29.70 30.41 31.82 32.53 33.23	0.71 1.41 2.12 2.83 3.54 4.24 4.95 5.66 6.36 7.07 7.78 8.49 9.90 10.61 11.31 12.02 12.73 13.43 14.14 14.85 15.56 16.97 17.68 18.38 19.09 19.80 20.51 21.21 21.92 22.63 23.33 24.04 24.75 25.46 26.87 27.58 28.28 28.28 28.29 29.70 30.41 31.11 31.82	$\begin{array}{c} 4\\ 5\\ 6\\ 7\\ 8\\ 9\\ 10\\ \hline{1}\\ 1\\ 2\\ 3\\ 4\\ 4\\ 5\\ 6\\ 7\\ 7\\ 8\\ 9\\ 0\\ \hline{1}\\ 1\\ 2\\ 2\\ 2\\ 3\\ 2\\ 4\\ 2\\ 5\\ 6\\ 7\\ 8\\ 9\\ 0\\ \hline{1}\\ 1\\ 2\\ 2\\ 2\\ 3\\ 2\\ 4\\ 5\\ 6\\ 7\\ 8\\ 9\\ 0\\ \hline{1}\\ 4\\ 2\\ 3\\ 3\\ 4\\ 4\\ 5\\ 6\\ 7\\ 8\\ 9\\ 0\\ \hline{1}\\ 4\\ 2\\ 3\\ 3\\ 4\\ 4\\ 5\\ 6\\ 7\\ 8\\ 9\\ 0\\ \hline{1}\\ 4\\ 2\\ 3\\ 4\\ 4\\ 4\\ 5\\ 6\\ 7\\ 7\\ 8\\ 9\\ 0\\ \hline{1}\\ 4\\ 2\\ 3\\ 3\\ 4\\ 4\\ 5\\ 6\\ 7\\ 8\\ 9\\ 0\\ \hline{1}\\ 4\\ 2\\ 3\\ 4\\ 4\\ 4\\ 5\\ 6\\ 7\\ 8\\ 9\\ 0\\ 1\\ 4\\ 2\\ 3\\ 4\\ 4\\ 5\\ 6\\ 7\\ 8\\ 9\\ 0\\ 1\\ 4\\ 2\\ 3\\ 4\\ 4\\ 5\\ 6\\ 7\\ 8\\ 9\\ 0\\ 1\\ 1\\ 2\\ 2\\ 3\\ 1\\ 4\\ 2\\ 3\\ 4\\ 4\\ 5\\ 6\\ 7\\ 8\\ 9\\ 0\\ 1\\ 1\\ 2\\ 3\\ 1\\ 4\\ 2\\ 3\\ 4\\ 4\\ 5\\ 6\\ 7\\ 7\\ 8\\ 9\\ 0\\ 1\\ 1\\ 2\\ 2\\ 3\\ 1\\ 4\\ 3\\ 4\\ 4\\ 5\\ 6\\ 7\\ 8\\ 9\\ 0\\ 1\\ 1\\ 2\\ 2\\ 3\\ 1\\ 4\\ 3\\ 4\\ 4\\ 4\\ 4\\ 4\\ 4\\ 4\\ 4\\ 4\\ 4\\ 4\\ 4\\ 4\\$
50	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\frac{73}{35.85}$	2   34.89	$\frac{34.95}{35.66}$	$\frac{35.05}{}$	$\frac{34.80}{35.51}$	$\frac{35.20}{-}$	$\frac{35.36}{}$		
Distance.	Dep.   La	t. Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
Dis	46 Deg.	45-3	Deg.	451	Deg.	451	Deg.	45 I	eg.	Dist

Dis	44 Deg.	44\ Deg.	44½ De	eg.	443	Deg.	45]	Deg.	Dis
Distance.	Lat. Dep.	Lat. Dep.	Lat.   I	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
51 52 53 53 54 55 56 60 61 62 63 64 65 66 67 67 77 77 77 77 77 77 77	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$     \begin{array}{r} 36.53 \ 35.59 \ 37.25 \ 36.29 \ 37.96 \ 36.98 \ 37.68 \ 39.40 \ 38.38 \ 40.11 \ 39.08 \ 40.83 \ 39.77 \ 41.55 \ 40.47 \ 42.26 \ 41.17 \ 42.98 \ 41.87 \ 43.69 \ 42.57 \ 44.41 \ 43.26 \ 45.13 \ 43.96 \ 45.84 \ 44.66 \ 46.56 \ 45.36 \ 47.28 \ 46.05 \ 47.28 \ 46.05 \ 47.99 \ 46.75 \ 48.71 \ 47.45 \ 49.42 \ 48.15 \ 50.14 \ 48.85 \ 50.86 \ 49.54 \ 51.57 \ 50.24 \ 52.29 \ 50.94 \ 53.01 \ 51.64 \ 53.72 \ 52.33 \ 54.44 \ 53.03 \ 55.16 \ 53.73 \ 55.87 \ 54.43 \ 56.59 \ 55.13 \ 57.30 \ 55.87 \ 54.43 \ 56.59 \ 55.13 \ 57.30 \ 55.82 \ 58.02 \ 56.52 \ 58.74 \ 57.22 \ 59.45 \ 57.92 \ 60.17 \ 58.61 \ 60.89 \ 59.31 \ 61.60 \ 60.01 \ 62.32 \ 60.71 \ 63.03 \ 61.41 \ 63.75 \ 62.10 \ 64.47 \ 62.80 \ 65.90 \ 64.20 \ 66.62 \ 64.89 \ 65.18 \ 63.50 \ 65.90 \ 64.20 \ 66.62 \ 64.89 \ 66.62 \ 66.62 \ 64.89 \ 66.62 \ 66$	36.38 36 37.09 36 37.80 37 38.52 37 39.23 38 39.94 39 40.66 39 41.37 40 42.08 41 42.08 41 42.79 42 43.51 42 44.93 44 45.65 44 46.36 45 47.07 46 47.79 46 49.21 48 49.93 49 50.64 49 51.35 50 52.07 51 52.78 51 53.49 52 54.21 53 54.92 53 55.63 54 57.77 56 57.77 56 57.77 56 57.77 56 59.20 58 49.21 48 49.21 48 49.21 48 49.21 53 54.21 53 54.21 53 54.21 53 55.63 54 57.77 56 66.35 58 66.35 58 66.35 58 66.37 61 66.38 68 66.39 68 66.39 68	5.75 6.45 7.15 7.85 8.55 9.25 9.25 9.25 9.35 1.35 2.05 2.76 6.36 9.66 7.66 8.36 9.76 7.47 1.17 1.87 1.17 1.88 1.88	$ \begin{array}{r} 36.22 \\ 36.93 \\ 37.64 \\ 38.35 \\ 39.06 \\ 39.77 \\ 40.48 \\ 41.19 \\ 41.90 \\ 42.61 \\ 43.32 \\ 44.74 \\ 45.45 \\ 46.16 \\ 46.87 \\ 47.58 \\ 49.00 \\ 49.71 \\ 50.42 \\ 51.13 \\ 51.84 \\ 52.55 \\ 53.26 \\ 53.97 \\ 54.68 \\ 55.39 \\ 56.10 \\ 56.81 \\ 57.52 \\ 58.95 \\ 56.10 \\ 56.81 \\ 57.52 \\ 58.95 \\ 56.39 \\ 56.39 \\ 56.39 \\ 56.39 \\ 56.39 \\ 56.39 \\ 56.39 \\ 56.30 $	35.90 $36.61$ $37.31$ $38.02$ $38.72$ $39.42$ $40.13$ $40.83$ $41.54$ $42.24$ $42.94$ $43.65$ $45.06$ $45.76$ $46.46$ $47.17$ $48.58$ $49.28$ $49.28$ $49.98$ $50.69$ $51.39$ $52.10$ $53.51$ $54.21$ $55.62$ $57.03$ $57.73$ $58.43$ $59.84$ $60.55$ $61.25$ $61.95$ $62.66$ $63.36$ $64.77$ $65.47$	$ \begin{array}{r} 36.06\\36.77\\37.48\\38.18\\38.89\\39.60\\40.31\\41.01\\41.72\\42.43\\\overline{43.13}\\43.84\\44.55\\45.25\\45.96\\46.67\\47.38\\48.79\\49.50\\\overline{50.20}\\50.91\\51.62\\52.33\\53.74\\54.45\\55.15\\55.86\\56.57\\\overline{57.28}\\57.98\\59.40\\60.10\\60.81\\61.52\\62.23\\63.64\\64.35\\65.76\\65.76 \end{array} $	$ \begin{array}{r} 36.06\\36.77\\37.48\\38.18\\38.89\\39.60\\40.31\\41.01\\41.72\\42.43\\43.13\\43.84\\44.55\\45.25\\45.96\\46.67\\47.38\\48.08\\48.79\\49.50\\50.20\\50.91\\51.62\\52.33\\53.74\\54.45\\55.15\\55.86\\56.57\\\hline7.28\\57.98\\59.40\\60.10\\60.81\\61.52\\62.23\\62.93\\63.64\\\hline64.35\\65.76\\65.76 \end{array} $	$\begin{bmatrix} 51\\ 52\\ 53\\ 55\\ 56\\ 61\\ 62\\ 63\\ 66\\ 66\\ 66\\ 66\\ 66\\ 66\\ 66\\ 66\\ 66$
95 96 97 98 99	$68.34   65.99 \\ 69.06   66.69$		$egin{array}{c c} 67.76 & 66 \ 68.47 & 67 \ 69.19 & 68 \ 69.90 & 68 \ 70.61 & 69 \end{array}$	3.59 7.29 7.99 8.69	$egin{array}{c} 66.76 \\ 67.47 \\ 68.18 \\ 68.89 \\ 69.60 \\ 70.31 \\ 71.02 \\ \hline \end{array}$	66.88 67.59 68.29 68.99 69.70	67.18 $67.88$ $68.59$ $69.30$	67.18	94 95 96 97 98 99 100
Distance.	Dep. Lat.	Dep. Lat.		lat.	Dep.	Lat.	Dep.	Lat.	Distance.
Dist	46 Deg.	45} Deg.	45} Do	eg.	451	Deg.	45]	Deg.	Dist

## A TABLE OF NATURAL SINES.

I extra	. ()	Deg.	11 1 (	las	d o I	Total Marie Control	11 0 0			_	
1	Nat.	N. Co.	-	Deg.	Nat,	Deg.	Nat.	Deg.	II	eg.	
M		Since	Sine	Sine	Sine	Sine	Sine	Sine	Nat. Sine	N. Co- Sine	M
	0 000001 000029	0 Unit.		99985 99984		99939	05234	99863 99861	06976		60
_	2 00058	3 00000	01803	99984	03548	99937	05292	199860	$07005 \\ 07034$	99754 99752	59 58
		7 00000 3 00000	11	99983	03577	99936	05321	99858	07063	99750	57
		00000	11 - 2001	99982		99935	05350  05379	99857 99855	$07092 \\ 07121$	99748	
1 6	6 00178	5 00000	01920	99982	03664	99933	05408	99854	07150		54
8	7100204	8 00000 F 00000	$\begin{vmatrix} 01949 \\ 01978 \end{vmatrix}$	99981	$\begin{array}{c} 03693 \\ 03723 \end{array}$	99932	$\begin{vmatrix} 05437 \\ 05466 \end{vmatrix}$		07179	00. 110	
6	9 00262	2 00000	02007	99980	03752	99930		99851	$\begin{array}{c}  07208 \\  07237 \end{array}$	99740	52 51
11	) 00291  106320	100000 1100000	$\begin{vmatrix} 02036 \\ 02065 \end{vmatrix}$	99979			كالتاكينانات			99736	50
12	2 00349	99999	02094	99978		99927 $99926$	$05553 \\ 05582$	99846  $ 99844 $	$\begin{array}{c}  07295  \\  07324  \end{array}$	99734 99731	49 48
		99999		99977	03868	99925	05611	99842	07353	99729	47
15	6 60436	99999	02152  $ 02181 $	99977	03897	99924	$05640 \\ 05669$	99841  $ 99839 $	$\begin{bmatrix} 07382 \\ 07411 \end{bmatrix}$	99727 $99725$	46
16	00465	99999	02211	$9\overline{9976}$	03955	99922	05698	99838	$07411 \\ 07440$		$\frac{40}{44}$
17	00495	99999	02240	99975	03984	99921	05727	99836	07469	99721	43
			$\begin{vmatrix} 02269 \\ 02298 \end{vmatrix}$	99974	04013 $04042$	99919	05756	99834	$\begin{vmatrix} 07499 \\ 07527 \end{vmatrix}$		42
20	00582	99998	02327	99973	04071	99917	05814	99831	07556		$\begin{array}{c} 41 \\ 40 \end{array}$
21 22			$02356 \\ 02385$			99916	05844	99829	07585	99712	39
23	00669	99998	02414	99971	$\begin{bmatrix} 04129 \\ 04159 \end{bmatrix}$	99913	05902	99827	$\begin{array}{c}  07614 \\ 07643 \end{array}$	$\begin{vmatrix} 99710 \\ 99708 \end{vmatrix}$	38
24	$\frac{100698}{100727}$	99998	$02443 \\ 02472$		04188	99912	05931	99824	07672	99705	36
26	00756	99997	02501		$\begin{bmatrix} 04217 \\ 04246 \end{bmatrix}$	99911	05960	99822	$\begin{vmatrix} 07701 \\ 07730 \end{vmatrix}$	99703	35 34
27	00785	99997	92530	99968	04275	99909	06018	99819	O 144 - 1 - 1	99699	
29	00814	99996	$02560 \\ 02589$	99967	$04304 \\ 04333$	99907	06047	99817 99815	07788		32
			02618	99966	04362	99905	06105		$\begin{array}{c} 07817 \\ 07846 \end{array}$		31 30
31		99996	02647	99965	$\overline{04391}$	99504	06134	$\overline{99812}$	07875	99689	$\frac{1}{29}$
33	00931	99995	$02676 \\ 02705 \\ 02724$	99963	$04420 \\ 04449$	99902! 99901!	06163	99810	07904	99687	28
41.7	100000	!プラカカラフ	1021041	13 3 4 1 3 1 3 4 5 11	11144151	OGUSTA	141 <b>(30)</b> 11	COGGRE	10.7060		26
36	;01018 .01617	99995	$02763 \\ 02792$	99962	04507	99898	06250	99804	07991	99680	25
101	01075	,99894!	1028211	999501	[04565]	99896	063081	99801	68049	20678	24   23
		$99994 \\ 99994$	[12850]	999591	1045941	99894	06337	99799	03078	99673	22
40	01164	99993	02908	J9958	046531	998921	05395	99795	38126	99671 99668	21
41	01193	99993	92938	99957	04682	998901	06424	99793	08165	99666	19
43	01251	99992	$02967 \\ 02996$	$99955^{\circ}$	04711	992221	06453	99792	08194	99664	18
44	01280	99992	03025	99954	94769	$99886_{\parallel}$	06511	99788	08252	99659	17 16
2	$\frac{01309}{01338}$		03054		04793	5.9	06540	99786	08281	99657	15
47	01367	99991	$03083 \\ 03112$	$\frac{99952}{99952}$	$04827 \\ 04856$	99883   99889	06569 0659s	99784	$\begin{array}{c} 08310 \\ 08339 \end{array}$		14
48	[01396]	99990	1931411	999510	048859	99881	08697	99720	08266	00030	13 12
50	$01425 \\ 01454$	99989	03170 03199	99950 99949	04914	9987911	06656	99778	08397	99647	11
1 9 T	0.14831	898891	1032281	999421	04972	992761	06714	99776  99774	DOLEE	00010	10
1 04	01913	999891	03257 03286	999471	056013	998751	067421	907791	00101	nacoal	8
K O.T.	0.794.11	RSSeec	033 [6]	99945	05059.9	9987211	068024	9976211	02549	99537 $99635$	7
1 (1.7)	וטטטוט	333311	V <b>ə</b> 54011	999445	USUKK 9	9987011	069211	99766H	ハロニツェ	nacoal	5
JI	OTODOL	Baaaaall	03374	999421	05146	99869 99867	06889	$99764 \parallel 99762 \parallel$	98500 98620	99630	4
100	07094	aaasoll	03432	$99941 \ $	05175	$99866 \ $	06918,	997601	08658	996251	3 2
$\frac{69}{M}$	01716 N. Co-	99985 Nat.	03461 N. Co-	$99940_{  }$	05205	99864	06947	99758	38687	99622	1
	Sine	Sine	Sine	Sine	Sine	Sine	N. Co- Sine	Nat. Sine	V. Co- Sine	Nat. Sine	M
-	89 D	eg.	88 D	eg.	87 D	eg.	86 I	Deg.	85 I		1

-	5 Deg.	6 Deg.	7 Deg.	8 Deg.	9 Deg.	-1
M	N. S. N. CS.	N.S. N.CS.	N. S. N. CS.	N. S.   N. CS.		M
0	08716 99619	10453 99452	$12187   \overline{99255}  $	$\overline{13917} \overline{99027} $		60
$\begin{bmatrix} 1\\2 \end{bmatrix}$	$ 08745 99617 \\  08774 99614$	$ 10482 99449  \\ 10511 99446 $	$oxed{12216 99251} \ oxed{12245 99248}$	13946 99023	المستحداث المستحدات المستحدات	59 58
$\tilde{3}$		10540 99443		$ 13975 99019  \  14004 99015 $		57
4	08831 99609	10569 99440	12302 99240	14033 99011	15758 98751	56
5 C	08860 99607	10597 99437	12331 99237	14061 99006		55
$\frac{6}{7}$	$ 08889 99604 \\  08918 99602$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ 14090 99002  \\  14119 98998 $		54 53
8	08947 99599	10684 99428	12418 99226	14148 98994		52
9	08976 99596	10713 99424	12447 99222	14177 98990		51
$\begin{array}{c} 10 \\ 11 \end{array}$	$\begin{vmatrix} 09005 & 99594 \\ 09034 & 99591 \end{vmatrix}$	10742   99421   10771   99418	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$egin{array}{c c} 14205 & 98986 \ 14234 & 98982 \ \hline \end{array}$		50 49
$\frac{1}{12}$	09063 99588	10800 99415	12533 99211	14263 98978	1 1	48
	09092 99586	10829 99412	12562 99208	14292 98973	16017 98709	47
14 15		10858   99409   10887   99406		14320 98969		46
$\frac{15}{16}$	$\frac{ 09150 }{09179} \frac{ 99580 }{99578}$	$\frac{10887}{10916} \frac{99400}{99402}$	$\frac{ 12620 99200 }{ 12649 99197 }$	14349 98965	$\frac{16074}{16109} \frac{98700}{98605}$	$\frac{45}{44}$
17	09179 99578	10915 99402	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	14378 98961 14407 98957		N
18		10973 99396		14436 98953		
19	09266 99570	11002 99393	12735 99186	14464 98948		41
$\begin{array}{ c c } 20 \\ 21 \end{array}$	$\begin{vmatrix} 09295 & 99567 \\ 09324 & 99564 \end{vmatrix}$	11031  99390  $  11060  99386 $	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{vmatrix} 14493 & 98944 \\ 14522 & 98940 \end{vmatrix}$	$oxed{16218 38676} \ oxed{16246 98671}$	$\frac{40}{39}$
22		11089 99383	$\begin{vmatrix} 12733 & 99176 \\ 12822 & 99175 \end{vmatrix}$	14551 98936	16275 98667	38
23	09382 99559	11118 99380	12851 99171	14580 98931	16304 98662	37
24	$\begin{vmatrix} 09411 & 99556 \\ 09440 & 99553 \end{vmatrix}$		12880 99167	14608 98927	16333 98657	36
$\frac{25}{26}$		$\begin{vmatrix} 11176 & 99374 \\ 11205 & 99370 \end{vmatrix}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$oxed{ 14637 98923} \ oxed{ 14666 98919}$	$  16361 98652  \\   16390 98648 $	35 34
27	09498 99548	11234 99367	12966 99156	14695 98914	16419 98643	33
28		11263 99364		14723 98910		32
29   30		11291 99360   11320 99357	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$oxed{ 14752 98906} \ 14781 98902$		31 30
$\frac{30}{31}$	09614   99537	$\frac{11329}{11349} \frac{99354}{99354}$	$\frac{13033}{13081} \frac{99141}{99141}$	$\frac{14781}{14810} \frac{93902}{98897}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\frac{30}{29}$
32			13110 99137	14838 98893		28
33	09671 99531	11407 99347	13139 99133	14867 98889	16591 98614	27
	$ 09700 99528 \\  09729 99526$	$\begin{vmatrix} 11436 & 99344 \\ 11465 & 99341 \end{vmatrix}$	13168 99129 $  13197 99125$		16620  98609 $  16648  98604$	$\begin{bmatrix} 26 \\ 25 \end{bmatrix}$
	09758 99523			14954 98876		
37	09787 99520	11523 99334	13254 99118	14982 98871	16706 98595	23
	09816 99517		13283 99114			
	$ 09845 99514 \\  09874 99511$	$oxed{11580}oxed{99327} 11609oxed{99324}$	11			
41		11638 99320	13370 99102			
	09932 99506		11 1	10		
	$ 09961 99503 \\  09990 99500$			15155 98845 15184 98841		17 16
45				15212 98836		
$\overline{46}$				N		$\overline{14}$
47	10077 99491	11812  99300	13543 99079	15270 98827	16992  98546	
48		$egin{array}{c c c c c c c c c c c c c c c c c c c $		$\begin{array}{c c}  15292 98823 \\  15327 98818 \end{array}$		12 11
50						10
51	10192 99479	0  11927 99286	13658 99063	15385 98809	17107  98526	9
52				1		8 7
		$3 \  11985   99279 \\ 0 \  12014   99276 \\$				
55	5 10308 99467	7  12043  99272	13773  99047	15500  98791	17222 98506	5
		1 12071 99269				
55		$egin{array}{c c c c c c c c c c c c c c c c c c c $				
59		$5   12123   99258 \\ 12158   99258$				
M			N. CS. N. S.	N. CS. N.S.	N. CS. N. S.	M
	84 Deg.	83 Deg.	82 Deg.	81 Deg.	80 Deg.	
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1	10 De	g.	11 1	Deg.	12	Deg.	13 1	Deg.	14 1	Deg.	
M	N. S.   N	. cs.	N.S.	N. CS.	N.S.	N. CS.		N. CS.	N.S.		M
0	$  \overline{17365}   98$	8481		98163	20791	97815	22495	97437	$\overline{24192}$	$\overline{97030}$	$\overline{60}$
1	17393 98			98157	20820	97809	22523		24220		59
2	17422 98			98152	20848		22552		24249		58
$\begin{bmatrix} 3 \\ 4 \end{bmatrix}$	$  17451   98 \   17479   98$			$\frac{98146}{98140}$	$\begin{vmatrix} 20877 \\ 20905 \end{vmatrix}$	$97797 \\ 97791$	$\begin{vmatrix} 22580 \\ 22608 \end{vmatrix}$		24277 24305	$97008 \\ 97001$	57 56
5	17508 98		19224		20933			97404	24333		55
6	17537 98	3450	19252	98129	20962	97778	22665	97398	24362		54
7	17565 98	الأناطاك		98124			22693		24390		53
8	17594 98			$\frac{98118}{98112}$	21019 21047	97766			24418		52
$\frac{9}{10}$	$ 17623 98 \\ 17651 98$	- (	19366		21047	97754	$22750 \\ 22778$		24446 24474		50 50
11	17680 98		19395		21104		22807				49
12	17708 98			98096	21132	97742	22835	97358	24531	96945	48
13		3414	19452		21161	97735		97351	24559		47
14 15	$\frac{17766 98}{17794 98}$	3409	$19481 \\ 19509$		$\begin{vmatrix} 21189 \\ 21218 \end{vmatrix}$	$\begin{array}{c} 97729 \\ 97723 \end{array}$		97345	24587		46 45
			$\frac{13503}{19538}$		$\frac{21218}{21246}$		I	$\frac{97338}{07991}$			
16 17	17823 98 17852 98		19566		21240 $21275$			97331 97325	24644	96909	44
	17880 98		19595				23005			96902	
19	17909 98	-	19623	98056	21331	97698	23033				41
	17937 98		19652		21360	0.0010		97304	24756		40
21	17966 98		19680		21388	- 1		97298	24784		39
22 23	$17995   98 \\ 18023   98$	368	$19709 \\ 19737$		$21417 \\ 21445$	$97680 \\ 97673$	1 3	$97291 \\ 97284$	24813  $ 24841 $		38 37
$\frac{23}{24}$	18052 98		19766		21474			97278	24869		36
		352	19794	98021	21502	97661	23203	97271	24897	96851	35
	18109 98		19823			97655		97264	24925		34
27	18138 98		$19851 \\ 19880$			97648		97257	24953		33
	$18166   98 \\ 18195   98$		19908				$\begin{vmatrix} 23288 \\ 23316 \end{vmatrix}$	$97251 \\ 97244$	$24982 \\ 25010$		32 31
	18224 98		19937			97630			25038		30
$\frac{30}{31}$	$\frac{18252}{18252}$		$\overline{19965}$			$\frac{97623}{}$			$\overline{25066}$		$\frac{3}{29}$
32		315	19994	97981	21701	97617	1	$97\tilde{2}23$	25094		28
33	18309 98	310		97975			23429	97217	25122	96793	27
	18338 98										
	$\begin{array}{c c} 18367   98 \\ 18395   98 \end{array}$		$\begin{array}{c} 20079 \\ 20108 \end{array}$		21786	97598	23486 23514		$\begin{vmatrix} 25179 \\ 25207 \end{vmatrix}$		$\begin{array}{c} 25 \\ 24 \end{array}$
	18424 98		20136		21843		23542		25235		23
	18452 98		20165	97946	21871	97579	23571	97182	25263	96756	22
~ ~	18481 98	11	20193		21899		23599		25291		21
	18509 98		$\begin{bmatrix} 20222 \\ 20250 \end{bmatrix}$			97566		97169	25320		20
	$\begin{array}{c c} 18538 & 98 \\ 18567 & 98 \end{array}$		$20230 \\ 20279$		$\begin{vmatrix} 21956 \\ 21985 \end{vmatrix}$	97553	23656 23684	$\frac{97162}{97155}$	25376	$96734 \\ 96727$	19 18
	18595 98		20307	97916	22013			97148	25404		17
44	18624 98	250	20336	97910	22041	97541	23740	97141	25432	96712	16
	18652 98		$\frac{20364}{2000000000000000000000000000000000000$		$\boxed{22070}$		23769		$\frac{25460}{}$	<del></del> i	$\frac{15}{2}$
		240	20393			97528		97127	25488		14
47	$18710   98 \\ 18738   98$		$\begin{bmatrix} 20421 \\ 20450 \end{bmatrix}$		$\begin{vmatrix} 22126 \\ 22155 \end{vmatrix}$			97120	$\begin{vmatrix} 25516 \\ 25545 \end{vmatrix}$		13 12
	$18738   98 \\ 18767   98$		$20450 \\ 20478$		$\frac{22155}{22183}$			$\frac{97113}{97106}$	25573		11
		3218	20507		22212		23910		25601	96667	10
51	18824 98	212	20535	97869	22240	97496	23938	97093	25629	96660	9
			20563		22268		23966		25657		8
	$18881   98 \\ 18910   98$		$\begin{vmatrix} 20592 \\ 20620 \end{vmatrix}$		22297 $22325$		$\begin{vmatrix} 23995 \\ 24023 \end{vmatrix}$		25685 $25713$		7
	18938 98		20649		22353		24023		25741		5
56	18967 98	3185	20677	97839	22382	97463	24079	97058	25769	96623	4
57	18995 98	3179			22410	97457	24108	97051	25798		3
	19024 98		20734		22438		24136		25826		2
$\frac{59}{M}$	$\frac{19052 98}{N. \text{ CS.}} \frac{1}{N}$		$\frac{20763}{\text{N. CS.}}$	97821 N. S.	$\frac{22457}{\text{N. CS.}}$	97444	$\frac{24164}{\text{N. CS.}}$		$\frac{25854}{\text{N. CS.}}$	$\frac{96600}{N}$	$\frac{1}{M}$
17/1	79 Deg		78 I		$\frac{N. \text{ CS.}}{77 \text{ I}}$		76 I				147
	ta neg	3.	10 1	reg. 1	111	Jeg.	101	reg.	15	Deg.	<u>_</u>

· ·	15 1	ler 1	16 L	lar I	17 1	lev.	181	eg.	19 1	)eg.	
M	N. S.	N. CS.	N. S. 1	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	N CS	M
0	$\frac{25882}{25882}$			$\frac{1000}{96126}$	$\frac{100}{29237}$	$\frac{1000}{95630}$	30902	$\frac{1000}{95106}$	$\frac{32557}{32557}$		
ĺ	25910					95622				94542	
$\frac{1}{2}$	25938			96110		95613					
3	25966	96570	27648	96102	29321	95605	30985	95079	32639		
4			27676			95596			32667	94514	
5 6			27704		-		31040		32694	94504	
7	$26050 \\ 26079$		$\begin{vmatrix} 27731 \\ 27759 \end{vmatrix}$	96078	$29404 \\ 29432$	$95579 \\ 95571$	31008	95052 95043	32749	$\frac{94495}{94485}$	
8		96532		96062	29460		31123		32777	94476	
9	26135			96054	29487	95554		95024	32804	94466	
10	26163			96046		95545			32832	94457	
11	26191			96037		95536			32859	94447	
13	$\begin{vmatrix} 26219 \\ 26247 \end{vmatrix}$		$ 27899  \\  27927 $	96029	29571 $29599$	95528	31233		32887	94438	
	26275		27927				31289	94988 94979		$94428 \\ 94418$	
15			27983			95502				94409	
3		$\frac{96471}{96471}$		$\frac{-}{95997}$	$\frac{29682}{29682}$		$\frac{31344}{31344}$		$\frac{32997}{32997}$	94399	
17			28039				31372		33024	94390	
18	26387	96456	28067	95981	29737	95476	31399	94943	33051	94380	42
19	26415		28095		29765		31427			94370	
20			28123		1		31454			94361	
	$\begin{vmatrix} 26471 \\ 26500 \end{vmatrix}$		28150 28178		29821 29849		31482 31510		$\begin{array}{c} 33134 \\ 33161 \end{array}$	$94351 \\ 94342$	
23	26528	96417	28206			95433				94332	
	26556		28234				31565			94322	
25	26584	96402	28262	95923	29932	95415	31593	94878	33244	94313	35
	26612			95915		95407		94869	33271	94303	
	26640					95398				94293	400 m
29	26668 26696		28346 $28374$	95898		95389 95380	31675	$94851 \\ 94842$	33326	$ 94284 \\ 94274$	
130		96363	28402			95372		94832	33381	94264	30
31	26752		$\frac{28429}{28429}$			$\frac{\overline{95363}}{95363}$	l		1		-
32			28457			95354				94245	
33	26808	96340	28485			95345					
34	26836	96332	28513	95849	30182	95337	31841	94795	33490	94225	26
35		96324	28541	95841		95328			33518		
$\begin{bmatrix} 36 \\ 37 \end{bmatrix}$	110000	$ 96316  \\  96308 $		$95832 \\ 95824$		$\begin{vmatrix} 95319 \\ 95310 \end{vmatrix}$		$94777 \\ 94768$		$94206 \\ 94196$	
	26948			95816			$31923 \\ 31951$	94758		94190 $94186$	
39		96293		95807		95293					
		96285	28680	95799	30348	95284	32006	94740	33655	94167	20
41		96277		95791		95275				94157	
		96269		95782		95266				94147	
44		96261 $96253$		95766		95257 95248				$\begin{vmatrix} 94137 \\ 94127 \end{vmatrix}$	
		96246		95757		95240	32110 $32144$	$94702 \\ 94693$			
$\frac{1}{46}$				$\frac{\overline{95749}}{95749}$	1	$\frac{35231}{95231}$	$\frac{32144}{32171}$	$\frac{34633}{94684}$	11	$\frac{94118}{94108}$	1
47		96230		95740		95231				94108 $94098$	
48	27228	96222	28903	95732	30570	95213	32227	94665		94088	
49		96214	28931	95724	30597	95204	32254	94656	33901	94078	11
		96205		95715		95195				94068	
51 52	1100 27	$2 96198 \\ 0 96190$			30690	95186	32309	94637		$ 94058 \\94049$	
53		96180				95177 $95168$				94049 $94039$	
54	27396	96174				95159				94029	
55	5 27424	96166	29098	95673	30763	95150	32419	94599	34065	94019	5
56		96158		95664	30791	95142	32447	94590		94009	
57 58		96150		95656		95133				93999	
59		$8 96142 \\ 96134$		95647 $ 95639$		95124		94571		( 93989   <sub> </sub> 93979	
M	- 10.000	N. S.	1	$\frac{30039}{\overline{N}}$ S.	11	$\frac{93113}{\text{N. S.}}$	$\frac{52529}{\text{N.CS.}}$	$\frac{94561}{\text{N. s.}}$	11	N. S.	M
	111 013	$\frac{1}{\mathrm{Deg.}}$									- ATA
1_	1 14	Deg.	11 13.	Deg.	11 12	Deg.	11 71.	Deg.	11 70 1	Deg.	

1-	20 Deg.	21 Deg.	11 (10) 1)	r ()0 7)		-
M			22 Deg. N. S. IN. CS.	23 Deg.	24 Deg.	1
1 -0	.		1 -11 -11 -11	-		
li			8  37488  92707	$\begin{vmatrix} 39073 & 92050 \\ 39100 & 92039 \end{vmatrix}$		
2	34257 9394	9 35891 93337	37515 92697		4070091343 $4072791331$	58
3	1	9  35918 93327	7  37542  92686	39153 92016	40753 91319	
4				39180  92005	40780 91307	56
5 6					40806  91295	55
7		$egin{array}{c c} 36000 & 93295 \ 36027 & 93285 \end{array}$	$\begin{bmatrix} 37622 & 92653 \\ 37649 & 92642 \end{bmatrix}$		40833 91283	
8			37676 92631		$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
9	34448 93879	36081 93264	37703 92620	39314 91948		51
10	34475 93869	9  36108  93253	37730 92609	39341 91936	40939 91236	
$\frac{11}{12}$	$\begin{vmatrix} 34503 & 93859 \\ 34530 & 93849 \end{vmatrix}$			39367 91925		49
13	34557 93839		$  37784  92587 \\   37811  92576$	39394 91914		48
14	34584 93829		37838 92565	$\begin{vmatrix} 39421 & 91902 \\ 39448 & 91891 \end{vmatrix}$	$\begin{vmatrix} 41019 & 91200 \\ 41045 & 91188 \end{vmatrix}$	$\begin{vmatrix} 47 \\ 46 \end{vmatrix}$
15	34612 93819		37865 92554	39474 91879		
$\overline{16}$	34639 93809			39501 91868	$\frac{11098}{41098} \frac{31170}{91164}$	$\frac{10}{44}$
17	34666 93799	36298 93180	37919 92532	39528 91856	$\begin{vmatrix} 41098 & 91164 \\ 41125 & 91152 \end{vmatrix}$	44 43
18	34694 93789	36325 93169	37946 92521	39555 91845	41151 91140	42
$\begin{array}{c} 19 \\ 20 \end{array}$	34721 93779	36352 93159	37973  92510	39581 91833	41178 91128	41
$\frac{20}{21}$	34748 93769	$\begin{vmatrix} 36379 & 93148 \\ 36406 & 93137 \end{vmatrix}$		39608 91822		
	34803 93748	$\frac{136434}{136434}$ $\frac{93137}{93127}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{vmatrix} 39635 & 91810 \\ 39661 & 91799 \end{vmatrix}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
23	34830 93738	36461 93116	38080 92466	39688 91787	41284 91092	37
24	34857 93728	36488 93106	38107  92455	39715 91775		
25	34884 93718	36515 93095		39741 91764	41337 91056	35
20	34912 93708	36542 93084	38161 92432	39768 91752		
28	34966 93688	36569 93074 36596 93063	$38188   92421 \\ 38215   92410  $	$\begin{vmatrix} 39795 & 91741 \\ 39822 & 91729 \end{vmatrix}$	41390 91032	33
	34993 93677		38241 92399	39848 91718	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
	35021 93667			39875 91706	41469 90996	
$\overline{31}$	35048 93657		38295 92377	3990291694	$\frac{21100}{41496} \frac{90984}{90984}$	$\frac{30}{29}$
	35075 93647	36704 93020	38322 92366	39928 91683		28
	35102 93637		38349 92355	39955 91671	41549 90960	27
34 35	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	35758 92999	38376 92343	39982 91660	41575 90948	26
	35183 93606	36785 92988 36812 92978	38403 92332 38430 92321	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	41602 90936	
	35211 93596	36839 92967	38456 92310	40062 91625	$\begin{vmatrix} 41628 & 90924 \\ 41655 & 90911 \end{vmatrix}$	23
38	35239 93585	36867 92956		40088 91613	41681 90899	22
	35266 93575	36894 92945	38510 92287	40115 91601	41707 90887	21
	$   \begin{array}{c c}     35293 & 93565 \\     35320 & 93555   \end{array} $		38537 92276	40141 91590		
	35347 93544		$\begin{vmatrix} 38564 & 92265 \\ 38591 & 92254 \end{vmatrix}$		41760 90863 41787 90851	
43	35375 93534	37002 92902	38617 92243	40195 91565 40221 91555	41787 90851 41813 90839	18
44	35402 93524	37029 92892	38644 92231	40248 91543	41840 90826	_ 5
	$\frac{35429}{93514}$	37056 92884	38671 92220	40275 91531	41866 90814	15
	35456 93503	37083 92870	38698   92209	$40301   \overline{91519}  $	41892 90802	14
	35484 93493		38725 92198	40328 91508	41919 90790	13
	$35511 \mid 93483 \\ 35538 \mid 93472 \mid$		38752 92186		41945 90778	
50	35565   93462	37191 92827	$\begin{vmatrix} 38778 & 92175 \\ 38805 & 92164 \end{vmatrix}$		41972 90766	
51	35592   93452	37218 92816	38832 92152		$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10
52	35619 93441	37245 92805	38859 92141		42051 90729	8
53	35647   93431	37272 92794	38886 92130	40488 91437	42077 90717	7
	$35674   93420   \\ 35701   93410  $		38912 92119	40514 91425		6
	$35701 93410 \\ 35728 93400$	$\begin{array}{c c} 37326 & 92773 \\ 37353 & 92762 \end{array}$	$\begin{vmatrix} 38939 & 92107 \\ 38966 & 92096 \end{vmatrix}$	40541 91414	42130 90692	5
	35755 93389		38993 92085	$     \begin{array}{r}       40567   91402 \\       40594   91390     \end{array} $	$\frac{42156}{690680}$	4 3
58	35782   93379	37407 92740	39020 92073		42209 90655	2
	35810 93368	37434 92729	39046 92062	40647 91366	42235 90643	ĩ
M	N. CS.   N. S.	N. CS. N. S.	N. CS. N. S.	N. CS. N. S.	N. CS. N. S.	M
	69 Deg.	68 Deg.	67 Deg.	66 Deg.	65 Deg.	
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	25 Deg.	26 Deg.	27 Deg.	28 Deg.	29 Deg.
M	N. S. N. US.	N. S. N. CS.	N. S. N. CS.	N. S. N. CS. 88295	N. S. N. CS. M
0	$oxed{42262} oxed{90631} \ oxed{42288} oxed{90618}$	$egin{array}{c c} 43837 & 89879 \ 43863 & 89867 \ \hline \end{array}$	45399 89101 45425 89087	46947 88295  $ 46973 88281 $	$oxed{48481} egin{array}{c c} 87462 & 60 \\ 48506 & 87448 & 59 \\ \hline \end{array}$
2		43889 89854		46999 88267	48532 87434 58
3		43916 89841	45477 89061	47024 88254	48557 87420 57
4	42367 90582	43942 89828		47050 88240	48583 87406 56
5 6	$oxed{42394}90569\ 42420\ 90557$	43968 89816		47076 88226  $ 47101 88213 $	48608 87391 55
7	42426 90537 42446 90545	$ 43994 89803  \\ 44020 89790 $	45554 89021 45580 89008	47101 88213  $ 47127 88199 $	$oxed{48634} 87377 54 \ 48659 87363 53$
8	42473 90532	44046 89777	45606 88995		48684 87349 52
	42499 90520	44072 89764	45632 88981	47178 88172	48710 87335 51
E .	42525 90507	44098 89752	45658 88968		48735 87321 50
11	$oxed{42552} oxed{90495} \ oxed{42578} oxed{90483}$	$\begin{vmatrix} 44124 & 89739 \\ 44151 & 89726 \end{vmatrix}$		47229 88144 47255 88130	$oxed{48761}8730649 \ 487868729248$
£1 .	42604 90470		45736 88928		48811 87278 47
14	42631 90458	44203 89700	,		48837 87264 46
A	42657 90446	44229 89687	45787 88902	47332 88089	48862 87250 45
	42683 90433	44255 89674		47358 88075	48888 87235 44
		44281 89662	45839 88875	47383 88062  $ 47409 88048 $	48913 87221 43
	$\frac{42736}{42762} \frac{90408}{90396}$	$oxed{44307 39649}\ 44333 89635$	45865 88862   45891 88848	47409 88048 47434 88034	$egin{array}{ c c c c c c c c c c c c c c c c c c c$
- Fi	42788 90383	44359 89623			48989 87178 40
21	42815 90371	44385 89610	45942 88822	47486 88006	49014 87164 39
		44411 89597		47511 87993	49040 87150 38
	$egin{array}{c c} 42867 & 90346 \ 42894 & 90334 \ \hline \end{array}$	$ 44437 89584  \\  44464 89571 $	$\begin{vmatrix} 45994 & 88795 \\ 46020 & 88782 \end{vmatrix}$	47537 87979 47562 87965	$oxed{49065} ar{87136} ar{37} \ 49090 ar{87121} ar{36}$
25		44490 89558	46046 88768	47588 87951	49116 87107 35
	42946 90309	44516 89545	46072 88755	47614 87937	49141 87093 34
27	42972 90296	44542 89532	46097 88741	47639 87923	49166 87079 33
	$\begin{vmatrix} 42999 & 90284 \\ 43025 & 90271 \end{vmatrix}$	44568 89519	46123 88728		$\begin{vmatrix} 49192 & 87064 & 32 \\ 49217 & 87050 & 31 \end{vmatrix}$
29 20	$\begin{vmatrix} 43025 & 90271 \\ 43051 & 90259 \end{vmatrix}$	$ 44594 89506  \\  44620 89493 $	$\begin{vmatrix} 46149 & 88715 \\ 46175 & 88701 \end{vmatrix}$	47690 87896 47716 87882	$oxed{ 49217 87050 31} \ oxed{ 49242 87036 30}$
$\frac{30}{31}$	$\frac{13077}{43077} \frac{90246}{90246}$	44646 39480	46201 88688		$ \frac{19212}{49268} \frac{57021}{87021} \frac{29}{29} $
14			46226 88674		49293 87007 28
\$ 33	43130 90221	44698 89454	46252 88661	47793 87840	49318 86993 27
34	43156 90203	44724 39441	46278 88647	47818 87826	49344 86978 261
					$ 49369 86964 25  \  49394 86949 24$
	$\begin{vmatrix} 43205 & 30103 \\ 43235 & 90171 \end{vmatrix}$		46355 88607		
		44828 89389		47920 87770	49445 86921 22
			46407 88580		49470 86906 21
			46433 88566		49495 86892 20
			46458 88553  $ 46484 88539 $		$\begin{vmatrix} 49521   86878   19 \\ 49546   86863   18 \end{vmatrix}$
			46519 88526		49571 86849 17
444	43418 90082	44984 89211	46536 88512	48073 87687	49596 86834 16
-			46561 88499		49622 86820 15
			46587 88485		49647 86805 14
			46613 88472 46639 88458		$ 49672 86791 13  \\  49697 86777 12 $
			46664 88445		49723 86762 11
50	43575 90007	45140 89232	46690 88431	48226 87603	49748 86748 10
	43602 89994				49773 86733 9
			46742 88404 46767 88390		49798 86719 8 49824 86704 7
			46793 88377		49849:86690 6
55	43706 89943	45269 89167	46819 88363	48354 87532	49874 86675 5
56	43733 89930	45295 89153	46844  88349	48379 87518	49899 86661 4
	43759 89918		46870 88336		
	43785 89905  $ 43811 89892 $	$\begin{vmatrix} 45347 & 89127 \\ 45373 & 89114 \end{vmatrix}$	46921 88308	48456 87476	49950   86632   2   49975   86617   1
$\frac{1}{M}$	N. CS. N. S.	N. CS. N. S.	N. CS. N. S.	N. CS. N. S.	N. CS. N. S. M
1	64 Deg.	63 Deg.	62 Deg.	61 Deg.	1000000000000000000000000000000000000
1	04 Deg.	i os Deg.	1 02 Deg.	ll of Deg.	il oo Deg.

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1	30 Deg.	31 Deg.	32 Deg.	33 Deg.	34 Deg.	
	N. S. N. CS 0 50000 8660	-	-	_		. M
1	1 50025 8658			-		
	2 50050 8657	3 51554 8568	7 53041 8477		$\begin{vmatrix} 55943 & 8288' \\ 55968 & 8287 \end{vmatrix}$	
( ) ( ) ( ) ( ) ( ) ( )	3 50076 8655		2 53066 8475	54537 83819	55992  82858	
	$rac{4 50101 8654}{5 50126 8653}$			3  54561  83804	56016 82839	56
2 4	6 50151 8651			$\begin{bmatrix} 54586 & 83788 \\ 54610 & 83772 \end{bmatrix}$		2 55
	7 50176 8650	1 51678 8561	2 53164 84697	7 54635 83756		5   54   53
	8 50201 8648		1 0 0 100 1	54659 83740	56112 8277:	3 52
1	$9   50227   8647 \\ 0   50252   8645 $					
1	1			$  54708  83708  \\   54732  83692 $		
15			6  53288 84619	54756 82676	56208 82708	
13			_	54781  83660	56232  82692	47
15				11	56256 82675	
16			_		56280 82659	-
17	50428 86354	1 51927 8546	1 53411 84542	54878 83597	$\begin{vmatrix} 56305 & 82643 \\ 56329 & 82626 \end{vmatrix}$	
18			5 53435 84526	54902 83581	56353 82610	
19			$1  53460 84511 \\ 6  53484 84495$	54927 83565	56377 82593	41
21		5 52026 8540	0   53484   84495 1   53509   84480	54951 83549 54975 83533	56401 82577 $ 56425 82561$	التالاناة
22	50553 86281	52051  8538	5   53534   84464	54999 83517	$\begin{vmatrix} 56425 & 82561 \\ 56449 & 82544 \end{vmatrix}$	$\begin{vmatrix} 39 \\ 38 \end{vmatrix}$
23		6  52076 8537(	0  53558 84448	55024 83501	56473 82528	37
24 25					56497 82511	36
26			11		56521  82495  56545  82478	
27			53656 84386	55121 83437	56569 82462	33
28			11 10 TO 10	55145 83421	56593 82446	
29 30				55169 83405 55194 83389	56617 82429	31
$\frac{31}{31}$	50779 86148		11		56641 82413	
32	50804 86133	52299 85234	53779 84308		56665 82396 56689 82380	29 28
33	50829 86119	52324 85218	53804 84292	55266 83340	56713 82363	27
34	50854 86104  50879 86089	52349 85203	53828 84277 53853 84261	55291 83324	56736 82347	26
36	50904 86074	52399 85173	53877 84245	55315-83308 55339-83292	56784 82330	25 24
37	50929 86059	52423  85157	33902 84230		56808 82297	23
	50954 86045	52448   85142   52473   85127		55388  83260	56832 82281	22
40	51004 86015		53951 84198 53975 84182	55412 83244 55436 83228		21
41	51029 86000	52522 85096	54000 84167		$\begin{vmatrix} 56880 & 82248 \\ 56904 & 82231 \end{vmatrix}$	20   19
42		52547 85081	34024 84151	55484 83195	56928 82214	18
	$ 51079 85970 \  51104 85956$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	54049 84135 54073 84120	55509 83179	56952   82198	17
45		52621 85035	54097 84120	55533 83163 55557 83147	56976 82181 57000 82165	16 15
$\overline{46}$		$  \overline{52646}  \overline{85020} $	54122 84088		$\frac{57000}{57024} \frac{82103}{82148}$	$\frac{10}{14}$
47	51179 85911	52671 85005	54140 84072		57047 82132	13
48 49	$51204   85896 \\ 51229   85881$		54171 84057	55630 83098	57071 82115	12
	$\begin{vmatrix} 51229 & 85881 \\ 51254 & 85866 \end{vmatrix}$	52745 84974	54195 84041 54220 84025	55654   83082	57095 82098	11
51	51279 85851	52770 84943	54244 84009	55702 83050	$57119 82082 \\ 57143 82065$	10
	51304 85836	52794 84928	54269 83994	55726 83034	57167  82048	8
		$\begin{vmatrix} 52819 & 84913 \\ 52844 & 84897 \end{vmatrix}$	$\begin{bmatrix} 54293 & 83978 \\ 54317 & 83962 \end{bmatrix}$		57191 82032	7
	51379 85792	52869 84882	54342 83946		$57215 82015 \ 57238 81999$	6
56	51404 85777	52893 84866	54366 83930	55823 82969	57262 81982	4
	51429 85762 51454 85747	52918 84851	54391 83915	55847 82953	57286 81965	3
	51479 85732	52967 84830	54415 83899 54440 83883		57310 81949	2
M	N. CS. N. S.	$\overline{N. \text{ Cs.}}$ $\overline{N. \text{ S.}}$	N. CS. N. S.		$\frac{57334}{N. \text{ CS.}} \left  \frac{81932}{N. \text{ S.}} \right $	$\frac{1}{M}$
	59 Deg.	58 Deg.	57 Deg.	56 Deg.		141
	5	1 30 17 35	, o. Dog.	30 Deg.	55 Deg.	

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7.4		Jeg.	36 D		N. S.	Jeg.		Deg.	!	Jeg.	7.4
M	N. S.	N. CS.	N.S.	N. CS.		N. CS.	N. S.	N. CS.	N. S.	N. CS.	$\frac{M}{20}$
0	57358 57381		58779 58802	80902	60182 60205	79864 79846	61566	78801 78783	$\begin{vmatrix} 62932 \\ 62955 \end{vmatrix}$	77715	60 59
2		81882	58826		60228	79829	61612	78765	62977		58
$\tilde{3}$	57429			80850	60251	79811	61635	78747	63000	77660	
4	57453		58873		1 -	79793	61658		63022		56
5	57.177			80816	60298	79776	61681	78711	63045	77623	55
6	57501	81815		80799	60321	79758	61704	78694	63068		54
7 8	57524 57548		58943	80782   80765	60344	79741 79723	$61726 \\ 61749$	$\begin{array}{c} 78676 \\ 78658 \end{array}$	$ 63090  \\  63113 $		53
	57572	3	58990		60390	79706	61772	78640	63135	77550	52 51
10	-,			30730	60414	79688	61795	78622	63158	77531	50
11				30713	60437	79671	61818	78604	63180	77513	
12		81714		30696	60460	79653	61841	7858€	63203		
13	57667		59084		69483		61864	78568	63225	77475	
14	57691 57715		591088591318		$60506 \\ 60529$		61887 61909	78550 78532	$\begin{vmatrix} 63248 \\ 63271 \end{vmatrix}$	77458 77439	
¥											
16	57738 57762		59154 8 59178 8		60553 60576	79583 79565	$61932 \\ 61955$	78514 78496	$\begin{vmatrix} 63293 \\ 63316 \end{vmatrix}$	77421 77402	44
	57786			80593	60599	79547	61938	78478	63338	77384	
<b>u</b> :				80576	60622	79530	62001	78460	63361	77366	
20	57833	81580	59248	80558	60645	79512	62024	78442	63383	77347	40
21	57857		59272		60668		62046		63406	77329	
		81546	59295		60691		62069	78405		77310	
a 1	57904 57928		59318 8 $ 59342 8$				$\begin{array}{c} 62092 \\ 62115 \end{array}$	78387 78369	$63451 \\ 63473$	77292 77273	
4	57952		59365		60761		62138	78351		77255	
21 a 1	57976		59389	- 1 }	60784		62160	78333		77236	
.27	57999	81462	594128	11	60807	79388	62183	78315	63540		33
	58023		59436 8		60830	79371	62206	78297		77199	_
		\$1428		30403	60853	79353	62229	78279		1	$\frac{31}{20}$
1	58070		1	30386	60876	79235	$\frac{62251}{22274}$	78261	63668		$\frac{30}{20}$
$\begin{array}{c} 31 \\ 32 \end{array}$		81395		30368	60899	79318	$\begin{vmatrix} 62274 \\ 62297 \end{vmatrix}$	78243		77144   77125	29
33	58118 58141	81378	59529 8 59552 8		60922			78225 78206			27
9 1			59576		1	1	1 1	1	0-0		4
	58189		59599		60991	79247	62365	78170	63720	77070	
	58212		59622					78152		77051	
	58236		59646							77033	
	58260 58283		59669 8 59693 8				62433  $ 62456 $			77014	
	58307		59716				62479		2	76977	- 4
			59739				62502			76959	
42	58354	81208	59763 8	80178	61153	79122	62524	78043	63877	76940	18
	58378		59786							76921	
	58401		59809						63922		
	$\frac{58425}{59440}$		59832					77988		76884	$\frac{15}{14}$
46 47	58449		59856				62615	$77970 \\ 77952$		76866	14 13
	58472 58496		59879  $ 59902 $				62660			76828	13 12
	58519		59926				62683			76810	_
	58543		59949						64056		10
51	58567	81055	59972	80021	61360	78962	62728	77879	64078		9
	58590		59995						64100		8
	58614 58637		$\begin{vmatrix} 60019 \\ 60042 \end{vmatrix}$				62774	77843	$64123 \\ 64145$	76735	7 6
	58661		60065		61451		62819			76698	5
	58684		60089							76679	4
57	58708	80953	60112	79916	61497	78855	62864	77769	64212	76661	3
58	58731	80936					62887			76642	2
$\frac{59}{5}$	58755		60158							76623	
Ni	N. CS.		N. CS.		-	N. S.	<u> </u>	N.S.		N.S.	M
	54 I	Deg.	53 D	eg.	52	Deg.	51 I	Deg.	50 ]	Deg.	
-		1.1		THE RESERVE	-		-	-			-

-	40 De	e.o.	. 41	Deg.	11 40	Llor	0 40	\	11 4 ( 3		-
M		<u>اچ.</u> ۱. CS.	N. S.	N. CS.	N. S.	Deg.	43 1			Deg.	
$\frac{1}{0}$		6604	65606	75471		N. CS.	N. S.	N. CS.	N.S.	N.CS.	M
ĺ			65628		$  66913 \\   66935$		$68200 \\ 68221$	73135	69466	71934	60
$\frac{1}{2}$	64323 7		65650	75433			68242	73116 73096	69487 69508		59  58
3		6548	65672	75414	66978	74256	68264	73076	69529		57
4		6530	65694		66999		68285	73056	69549	71853	
6		$6511 \\ 6492$	65716	75375	67021	74217	68306	73036	69570	71833	55
7		6473	65759	75356 75337	67064	74198 74178	$68327 \\ 68349$	73016	69591	71813	54
8	64457 76	6455	65781	75318	67086	74159		72996 72976	$69612 \\ 69633$	71792 $71772$	53 52
9		6436	65803	75299	67107	74139		72957	69654	71752	51
-		6417		75280	67129	74120	68412	72937	69675	71732	50
11	64524 76 64546 76	6398	65847	75261	67151	74100		72917	69696	71711	4.9
	64568 76		$ 65869  \\  65891 $	75222	67172 67194	74080 74061		72897	69717	71691	48
	64590 76		I I	75203		74041		72877 $72857$	$69737 \\ 69758$	71671   71650	47
15	64612 76			75184	67237	74022		72837			45
		304	65956	75165	$\overline{67258}$	$\overline{74002}$	1	$\frac{1}{72817}$	69800		$\frac{10}{44}$
		5286	65978	75146	67280	73983	68561	72797		71590	
	64679 76			75126	67301	73963	68582	72777	69842	71569	42
		$\begin{bmatrix} 248 \\ 229 \end{bmatrix}$		75107 $75088$	$\begin{array}{c} 67323 \\ 67344 \end{array}$	73944		72757			41
			66066	75069		73924   73904		$72737 \\ 72717$			40
					67387			72697			39 38
		173	66109	75030	67409	73865	68688				37
				75011			68709	72657	69966	71447	36
		135	66153 66175						المناسبين المناسب		35
			1					$72617 \ 72597$			34
	6490176	878	66218	74934				72577		71386 $71366$	
		059	66240	74915				2557			31
					67559	73728	68835	$72537 \parallel$			30
			66284	74876				72517			$\overline{29}$
		$\begin{vmatrix} 003 \\ 984 \end{vmatrix}$	66306 66327					72497			28
			nna int.		67623 67645	73669		72477 $72457$	70153  70174		27
					67666			72437		71243	26 25
		927	66393  <sup>,</sup>	74780	67688			72417		71203	
	65099 75		66414		67709			$72397 \parallel$		71182	23
1	65122 75 $65144 75$		66436 66458		67730			72377	1		22
			66480		67752 67773			$72357 \  72337 \ $			21
41	65188 75				67795			- 1			$\frac{20}{19}$
		813	66523	74664	67816	73491	69088				18
			66545		67837		69109	72277	70360	71059	17
4	$65254 75 \ 65276 75$	756	66566 66588	11			69130 1 69151 1				16
-	$\frac{65298}{65298} \frac{75}{75}$			[		j)		72236			15
	65320 75		66632			$\begin{array}{c} 73412 \\ 73393 \end{array}$	69172		70422		14
48	65342 75	6699	66653						70443		13
	$65364 \boxed{75}$	680	€6675	74528	67965	73353	69235		704841		11
	65386 75		66697	1	67987	733331	69256	$72136 \ $	70505	70916	10
	$65408   75 \\ 65430   75$		66718 66740					72116	70525		9
	65452 75		66762	74451	$ 68029  \\  68051 $		69298	$72095 \parallel 72075 \parallel$	70546 70567		8
54	65474 75	5585	66783	74431			69340	72055	70587		6
	65496 75		66805	74412	68093	73234	69361	72035	70608		5
	65518 75		66827		68115	73215	69382	$72015 \ $	70628	70793	4
	$65540   75 \\ 65562   75$		$66848 \\ 66870$	74373	68136	73195	69403	71995	70649		3
	65584 75			74333	68170	731 75	69424	71974	70670		2
	65606 75			74314	68200	73135	69466	71934	700901		$\begin{bmatrix} 1 \\ 0 \end{bmatrix}$
M	N. CS. N	N. S.	N. CS.	N.S.	$\overline{N. CS.}$		N. CS.		$\overline{N. CS.}$		M
	49 Des	g.	48 I		47 I		46 D		45 I		
	· · · · · · · · · · · · · · · · · · ·	7		- C	1	7	10 1	2	10 1.	S.	

1		0 De	grees.	1 D	egree.	1 9 De	grees.	1 3 Da	egrees.	
ı	M	N. Tan.	N. Cot.	N. Tan.	N. Cot.	N. Tan	N. Cot.	N. Tan	N. Cot.	M
		00000	0000 • 00	01746	57.2900	03492	28 • 6363	$\frac{10.141}{05241}$	19.0811	60
Į.	1	00029	$3437 \cdot 75$	01775	$56 \cdot 3506$	03521	28.3994	05270	18.9755	59
44.	2	00058	1718.87	01804	55.4415	03550	28 • 1664	05299	18.8711	<b>5</b> 8
1	3 4	00087	$1145 \cdot 92 \\ 859 \cdot 436$	01833	54.5613 $53.7086$	03579	27.9372	05328	18.7678	
48.44	5	00116 00145	687.549	01862 01891	53.7086 $52.8821$	03609	$27 \cdot 7117$ $27 \cdot 4899$	05387	18.6656 18.5645	
1	6	00175	572.957	01920	52.0807	03667	27 · 27 15	05416	18.4645	54
į	7	00204	491.106	01949	$51 \cdot 3032$		27.0566	05445	18.3655	
ľ	8	00233	429.718 $381.971$	01978	50.5485 $49.8157$	$\begin{vmatrix} 03725 \\ 03754 \end{vmatrix}$	26.8450 $26.6367$	05474	18 · 2677 18 · 1708	
100	10	00202	343.774	02007	49.0137 $49.1039$	03783	26.0307 $26.4316$	05533	18.1708 $18.0750$	
Part ( )	11	00320	312.521	02066	48 • 4121	03812	$26 \cdot 2296$	05562	17.9801	49
	12	00349	286 · 478	02095	47.7395	03842	26.0307	05591	17.8863	
	13 14	00378	$264 \cdot 441$ $245 \cdot 552$	$02124 \\ 02153$	$47 \cdot 0853$ $46 \cdot 4489$	03871 03900	25.8348 $25.6418$	05620	17.7934 $17.7015$	
I Jayan	15	00436	$249 \cdot 332$ $229 \cdot 182$	$02133 \\ 02182$	45.8294	03929	25.0418 $25.4517$	05678	17.7013 $17.6106$	
S. Carrie	16	00465	214.858	02211	45.2261	03958	25.2644	05708	$\frac{17 \cdot 5205}{17 \cdot 5205}$	
de galant	17	00495	$202 \cdot 219$	02240	44.6386	03987	$25 \cdot 0798$	05737	17.4314	
Y SARCA	18	00524	190.984	02269	$44 \cdot 0661$	04016	$24 \cdot 8978$	05766	17.3432	
New Street	19	00553 $00582$	180.932 $171.885$	02298	43.5081 $42.9641$	04046	24.7185	05795	17.2558	
Chapter	20 21	$\begin{array}{c} 00582 \\ 00611 \end{array}$	171.885 $163.700$	$02328 \ 02357$	42.9641 $42.4335$	$\begin{vmatrix} 04075 \\ 04104 \end{vmatrix}$	24.5418 $24.3675$	$05824 \\ 05854$	$17 \cdot 1693$ $17 \cdot 0837$	
Sec.	22	00640	$156 \cdot 259$	02386	41.9158	04133	$24 \cdot 1957$	05883	16.9990	
Section of the last	23	00669	$149 \cdot 465$	02415	$41 \cdot 4106$	04162	$24 \cdot 0263$	05912	16.9150	
1	24	00698	143 237	02444	40.9174	04191	23.8593	05941	16.8319	
wygg a'r	25 26	00727	$137 \cdot 507$ $132 \cdot 219$	$02473 \\ 02502$	40.4358 $39.9655$	$\begin{bmatrix} 04220 \\ 04250 \end{bmatrix}$	$23 \cdot 6945$ $23 \cdot 5321$	05970	16.7496 $16.6681$	
	27	00785	$127 \cdot 321$	02531	39.5059		$23 \cdot 3718$	06029	16.5874	
200	28	00814	122.774		$39 \cdot 0568$	04308	$23 \cdot 2137$	06058	16.5075	
100	29	00844	118 · 540	02589	38.6177	04337	23.0577	06087	16.4283	,
1	30	00873	$\frac{114 \cdot 589}{114 \cdot 333}$	02619	38 · 1885	04366	22.9037	06116	$\frac{16 \cdot 3499}{1}$	
200	31 32	$00902 \\ 00931$	110.892 $107.426$	$02648 \ 02677$	$37 \cdot 7686 \\ 37 \cdot 3579$	$\begin{vmatrix} 04395 \\ 04424 \end{vmatrix}$	22.7518 $22.6020$	$\begin{vmatrix} 06145 \\ 06175 \end{vmatrix}$	$16 \cdot 2722$ $16 \cdot 1952$	
	33	00960	$104 \cdot 171$	02706	36.9560		22.4541	06204	16.1352	
100	34	00989	101 · 107	02735	$36 \cdot 5627$		22.3081	06233	16.0435	26
100	35	01018	98.2179	02764	36.1776	04512	22.1640	06262	15.9687	
l l	36 37	$01047 \\ 01076$	$95 \cdot 4895$ $92 \cdot 9085$	$02793 \\ 02822$	35.8006 $35.4313$		22.0217 $21.8813$	$06291 \\ 06321$	15.8945 $15.8211$	
4 4 4 4 4 4	38	01105	90.4633	02851	35.0695	1	21.7426	06350	15.7483	
1000	39	01135	88 • 1436	02881	34.7151	04628	$21 \cdot 6056$	06379	15.6762	21
7. AP.	40	01164	85.9398	02910	34.3678		$21 \cdot 4704$	06408	15.6048	
A.	41 42	$01193 \\ 01222$	83.8435 81.8470	02939	34.0273 $33.6935$	_	21.3369 $21.2049$	$\begin{vmatrix} 06437 \\ 06467 \end{vmatrix}$	15.5340 $15.4638$	
1	43	01251	$79 \cdot 9434$	02997	$33 \cdot 3662$		$21 \cdot 0747$	06496	15.3943	
37.50	44	01280	$78 \cdot 1263$	03026	$33 \cdot 0452$		$20 \cdot 9460$	06525	$15 \cdot 3254$	
1	45	01309	76.3900	03055	$\frac{32 \cdot 7303}{}$	04803	20.8188	06554	$\underline{15 \cdot 2571}$	
1	46	01338	74.7292	03084	32.4213	04832	20.6932	06584		
	47 48	01367 01396	$73 \cdot 1390$ $71 \cdot 6151$	$03114 \\ 03143$	$32 \cdot 1181$ $31 \cdot 8205$	$04862 \ 04891$	20.5691 $20.4465$	$06613 \\ 06642$	$15 \cdot 1222$ $15 \cdot 0557$	
	49	01396	70.1533	03172	31.5284	$04091 \\ 04920$	20.4405 $20.3253$	06671	13.0337 $14.9898$	11
1. 1.	50	01455	$68 \cdot 7501$	03201	$31 \cdot 2416$	04949	$20 \cdot 2056$	06700	$14 \cdot 9244$	10
-	51	01484	67.4019	03230	30.9599	04978	20.0872	06730	14.8596	9
1	52 53	$01513 \\ 01542$	$66 \cdot 1055 \\ 64 \cdot 8580$	03259 $03288$	30.6833 $30.4116$	$\begin{bmatrix} 05007 \\ 05037 \end{bmatrix}$	$19 \cdot 9702$ $19 \cdot 8546$	$\begin{vmatrix} 06759 \\ 06788 \end{vmatrix}$	14.7954 $14.7317$	8
	54	01542	63.6567	03200	30.1446	05066	19.7403	06817	14.6685	6
100	55	01600	$62 \cdot 4992$	03346	29.8823	05095	19.6273	06847	14.6059	5
	56	01629	$61 \cdot 3829$	03376	29.6245	05124	19.5156	06876	14.5438	3
	57 58	01658 01687	$60 \cdot 3058$ $59 \cdot 2659$	$03405 \\ 03434$	$29 \cdot 3711$ $29 \cdot 1220$	$ \begin{array}{c} 05153 \\ 05182 \\  \end{array}$	$19 \cdot 4051$ $19 \cdot 2959$	$06905 \\ 06934$	$14 \cdot 4823$ $14 \cdot 4212$	2
	59	01716	58.2612	03463	28 · 8771	05212	19.1879	06963	14.3607	1 *
	60	01746	57 • 2900	03492	28 • 6363	05241	19.0811	06993	14.3007	0
1	M N. Cot. N. Tan.			/i		N. Cot N. Tan.		N. Cot. N. Tan.		M
,		89 D	egrees.	88 De	egrees.	87 De	egrees.	86 Degrees.		
-	Maria Company		The state of the s	COPPARA SOL	- Charles and the same		A CONTRACTOR OF THE PARTY OF TH	THE PERSON NAMED IN	NAME OF TAXABLE PARTY.	-

TENEST .		~			SECTION OF	······································			Sea. L
		egrees.		egrees.		grees.		grees.	
M	N. Tan.	N. Cot.	N. Tan.		N. Tan.	N. Cot.	N. Tan.	N. Cot.	M
$0 \\ 1$	06993	$14 \cdot 3007$ $14 \cdot 2411$	08749 08778	11.4301 $11.3919$	10510 10540	9.51436 $9.48781$	12278 12308	$8 \cdot 14435$ $8 \cdot 12481$	60 59
2	07051	14.1821	08807	11.3540	10569	9.46141	12338	8.10536	
3	07080	14.1235	08837	11.3163	10599	$9 \cdot 43515$	12367	8.08600	
4 5	07110 07139	14.0655 $14.0079$	08866 08895	$11 \cdot 2789$ $11 \cdot 2417$	10628 10657	$9 \cdot 40904$ $9 \cdot 38307$	$\begin{array}{ c c c c c }\hline 12397 \\ 12426 \\ \hline \end{array}$	8.06674 8.04756	
6	07168	13.9507	08925	11.2048		9.35724	12456	8.02848	
7	07197	13.8940	08954	11.1681	10716	9.33154	12485	8.00948	
8 9	07227 $07256$	13.8378 $13.7821$	08983	$11 \cdot 1316$ $11 \cdot 0954$	10746	$9 \cdot 30599$ $9 \cdot 28058$	$\begin{array}{ c c c c }\hline 12515 \\ 12544 \\ \end{array}$	7·99058 7·97176	
10	07285	13.7821 $13.7267$	09042	11.0594	10805	9.25530	12574	7.97170	
11	07314	13.6719	09071	11.0237	10834	9 • 23016	12603	7.93438	49
12 13	07344 07373	13.6174 $13.5634$	09101 09130	10.9881 $10.9528$	10863 10893	$9 \cdot 20566$ $9 \cdot 18028$	$\begin{array}{ c c c c }\hline 12633 \\ 12662 \\ \end{array}$	7.91582 $7.89734$	
14	07373	13.5034 $13.5098$	09159	10.9178	10933	9.15020	12692	7.87895	
15	07431	$13 \cdot 4566$	09189	10.8829	10952	9.13093	12722	7.86064	
16	07461	13.4039	09218	10.8483	10981	9 · 10646	12751	7.84242	5
17 18	07490 07519	$13 \cdot 3515$ $13 \cdot 2996$	09247	10.8139 $10.7797$	$\begin{vmatrix} 11011 \\ 11040 \end{vmatrix}$	9.08211	12781	7.82428	
19	07519	13.2990 $13.2480$	09306	10.7797 $10.7457$	11040	9.05789 9.03379	12810 12840	7·80622 7·78825	
20	07578	$13 \cdot 1969$	09335	10.7119	11099	9.00983	12869	7.77035	
21	07607	13.1461	09365	10.6783	11128	8.98598	12899	7.75254	
22 23	07636 07665	13·0958 13·0458	09394 09423	10.6450 $10.6118$	11158	8.96227 $8.93867$	$\begin{array}{ c c c }\hline 12929 \\ 12958 \\ \end{array}$	$7 \cdot 73480$ $7 \cdot 71715$	
24	07695	$12 \cdot 9962$	09453	10:5789	11217	8.91520	12988	7.69957	
25	07724	12.9469	09482	10.5462	11246	8.89185	13017	7.68208	
26 27	$07753 \\ 07782$	12.8981 $12.8496$	09511 09541	10.5136 $10.4813$	11276 11305	8.86862 $8.84551$	$\begin{vmatrix} 13047 \\ 13076 \end{vmatrix}$	7·66466 7·64732	
28	07812	12.8014	09570	10.4491	11335	8.82252	13106	7.63005	
29	07841	$12 \cdot 7536$	09600	10.4172	11364	8.79964	13136	$7 \cdot 61287$	31
30	97870	$\frac{12 \cdot 7062}{}$	09629	10.3854	11394	8.77689	13165	$\frac{7 \cdot 59575}{$	
31 32	07899 07929	12.6591 $12.6124$	09658 09688	10.3538 $10.3224$	11423 11452	8.75425 $8.73172$	13195 13224	7.57872	
33	07929	12.0124 $12.5660$	09000	10.3224 $10.2913$	11432	8.70931	13254	7.56176 $7.54487$	
34	07987	12.5199	09746	10.2602	11511	8 • 68701	13284	7.52806	26
35	08017 08046	12.4742 $12.4288$	09776	$10 \cdot 2294$ $10 \cdot 1988$	11541   11570	8 66482	13313	7.51132	
36 37	08075	12.4288	09834	10.1988 $10.1683$	11600	$8 \cdot 64275 \\ 8 \cdot 62078$	13343 13372	7·49465 7·47806	
38	08104	$12 \cdot 3390$	09864	10.1381	11629	8.59893	13402	7.46154	
39	08134	12.2946	09893	10.1080 $10.0780$	11659	8.57718	13432	7.44509	
40	08163 08192	$12 \cdot 2505 \\ 12 \cdot 2067$	09923	10.0780	11688	8.55555 $8.53402$	13461 13491	$7 \cdot 42871$ $7 \cdot 41240$	
42	08221	$-12 \cdot 1632$	09981	10.0187	11747	8.51259	13521	7.39616	18
43	08251	12.1201	10011	9.98930	11777	8.49128	13550		17
44 45	08280 08309	12.0772 $12.0346$	10040   10069	9.96007 9.93101	11806 11836	8.47007 $8.44896$	13580 13609	$7 \cdot 36389$ $7 \cdot 34786$	
46	08339	$\frac{12 \cdot 0910}{11 \cdot 9923}$	10099	9.90211	11865	8 · 42795	13639	$7 \cdot 3190$	
47	08368	$11 \cdot 9504$	10128	9,87338	11895	8.40705	13669	7.31600	
48	08397	11.9087	10158	9.84482	11924	8.38625	13698	7.30018	
49 50	08427 08456	11.8673 $11.8262$	10187 $10216$	9.81641 9.78817	11954 11983	$8 \cdot 36555$ $8 \cdot 34496$	13728 13758	$7 \cdot 28442$ $7 \cdot 26873$	
51	08485	11.7853	10246	9.76009	12013	8.32446	13787	7.25310	9
52	08514	11.7448	10275	9.73217	12042	8.30406	13817	7.23754	8
53 54	08544 68573	11.7045 $11.6645$	10305 $10334$	9.70441 9.67680	12072 12101	$8 \cdot 28376$ $8 \cdot 26355$	13846 13876	$7 \cdot 22204$ $7 \cdot 20661$	7
55	08602	11.6248	10363	9.64935	12131	8.24345	13906	$7 \cdot 20001$	5
56	68632	11.5853	10393	9.62205	12160	8 • 22344	13935	$7 \cdot 17594$	4
57 58	08661	11.5461 $11.5072$	10422 10452	9.59490 9.56791	$\begin{array}{ c c c c }\hline 12190 \\ 12219 \\ \hline \end{array}$	$8 \cdot 20352$ $8 \cdot 18370$	13965 13995	7.16071	3
59	08720	11.3072	10452	9.56791 $9.54106$	12219	8.16398	14024	$7 \cdot 14553$ $7 \cdot 13042$	2
60	08749	11.4301	10510	9 · 51436	12278	8.14435	14054	7.11537	Ô
M	N. Cot.	N. Tan.	N. Cot.	N. Tan.	N. Cot.	N. Tan.	N. Cot.	N. Tan.	M
9	85 D	egrees.	84 D	egrees.	83 D	egrees.	82 D	egrees.	

	8 De	grees.	$9 D\epsilon$	egrees.	10 D	egrees.	11 D	11 Degrees.		
M	N. Tan.		N. Tan	N. Cot.	N. Tan.	N. Cot.	N. Tan.		M	
0	14054	$7 \cdot 11537$	15838	6.31375	17633	5.67128	19438	5.14455	60	
1	14084	7.10038	15868	6.30189		5.66165	19468	5 · 13658		
2	14113	7.08546	15898	6.29007	17693	5.65205	19498	5.12862		
3 4	14143 14173	$7 \cdot 07059$ $7 \cdot 05579$	15928 15958	$6 \cdot 27829$ $6 \cdot 26655$	17723 17753	$5 \cdot 64248$ $5 \cdot 63295$	19529 19559	$5 \cdot 12069$ $5 \cdot 11279$		
	14202	7.04105	15988	$6 \cdot 25486$	17783	5.62344	19589	5.10490		
5 6	14232	7.02637	16017	$6 \cdot 24321$	17813	5.61397	19619	5.09704	54	
7	14262	7.01174	16047	6.23160	( )	5 • 60452	19649	5.08921		
8 9	$\begin{array}{c c} 14291 \\ 14321 \end{array}$	6.99718 6.98268	$\begin{vmatrix} 16077 \\ 16107 \end{vmatrix}$	$6 \cdot 22003$ $6 \cdot 20851$	17873 17903	5.59511 5.58573	19680 19710	5.08139 5.07360		
10	14351	6.96823	16137	6.19703	17903	5.57638	19740	5.07500 $5.06584$		
11	14381	6 • 95385	16167	6 • 18559	17963	$5 \cdot 56706$	19770	5.05809		
12	14410	6.93952	16196	6 • 17419	17993	5.55777	19801	5.05037		
13 14	$14440 \\ 14470$	6 • 92525	16226	6·16283 6·15151	18023	5.54851	19831	5.04267		
15	14470	6.91104 6.89688	16256 $16286$	6.13131 $6.14023$	18053 18083	$5 \cdot 53927$ $5 \cdot 53007$	19861 19891	5.03499 5.02734		
16	14529	6.88278	16316	$\frac{6 \cdot 12899}{6 \cdot 12899}$	18113	$\frac{-5.52090}{5.52090}$	19921	$\frac{5 \cdot 01971}{5 \cdot 01971}$		
17	14559	6.86874	16346	6.12399	18143	5.52090 $5.51176$	19952	5.01971 $5.01210$		
18	14588	6.85475	16376	$6 \cdot 10664$	18173	$5 \cdot 50264$	19982	5.00451	42	
19	14618	6.84082	16405	6.09552	11	5 • 49356	20012			
20 21	14648 $14678$	6.82694 $6.81312$	16435 16465	$6 \cdot 08444$ $6 \cdot 07340$		5 · 48451 5 · 47548	20042	4.98940 4.98188	39	
22	14707	6.79936	16495	6.07340 $6.06240$	18293	5.47548 $5.46648$	20103	4.97438	_	
23	14737	6.78564	16525	6.05143	18323	$5 \cdot 45751$	20133	4.96690	37	
24	14767	6.77199	16555	$6 \cdot 04051$	18353	$5 \cdot 44857$	20164	4.95945	36	
25	14796 $14826$	6.75838	16585	6.02962	18383	5 43966	20194	4.95201	35	
26 27	14856	$6 \cdot 74483$ $6 \cdot 73133$	$16615 \\ 16645$	6.01978 6.00797	18414 18444	$5 \cdot 43077$ $5 \cdot 42192$	20224 20254	$4 \cdot 94460$ $4 \cdot 93721$	34 33	
28	14886	6.71789	16674	5.99720	18474	5.41309	20285	4.92984		
29	14915	6.70450	16704	$5 \cdot 98646$	18504	$5 \cdot 40429$	20315	4.92249	31	
30	14945	6.69116	16734	$\frac{5 \cdot 97576}{}$	18534	$5 \cdot 39552$	$\frac{20345}{}$	$4 \cdot 91516$	30	
31	14975	6.67787	16764	$5 \cdot 96510$	18564	5.38677	20376	4.90785	29	
32 33	$15005 \\ 15034$	6.66463	16794	5.95448	18594	5.37805	20406	4.90056		
34	15064	$6 \cdot 65144 \\ 6 \cdot 63831$	16824   16854	$5 \cdot 94390$ $5 \cdot 93335$	18624 18654	5·36936 5·36070	20436	4.89330 $4.88605$		
35	15094	$6 \cdot 62523$	16884	$5 \cdot 92283$	18684	$5 \cdot 35206$	20497	4.87882	_	
36	15124	$6 \cdot 61219$	16914	$5 \cdot 91235$	18714	$5 \cdot 34345$	20527	4.87162	24	
37	15153 15183	6.59921	16944	5.90191	18745	5.33487	20557	4.86444	23	
38 39	15213	6.58627 $6.57339$	16974 $17004$	5.89151 $5.88114$	18775 18805	$5 \cdot 32631$ $5 \cdot 31778$	20588	4.85727 $4.85013$		
40	15243	6.56055	17033	5.87080	18835	$5 \cdot 30928$	20648	4.84300		
41	15272	6.54777	17063	5.86051	18865	$5 \cdot 30080$	20679	4.83590		
42	15302	6.53503	17093	5.85024	18895	5 29235	20709	4.82882		
43 44	$\frac{15332}{15362}$	6.52234 $6.50970$	17123 17153	5.84001 $5.82982$	18925 18955	$5 \cdot 28393$ $5 \cdot 27553$	20739 20770	4.82175 $4.81471$		
45	15391	$6 \cdot 49710$	17183	5.81966	18986	5.26715	20800	4.80769	15	
$\frac{-}{46}$	15421	${6 \cdot 48456}$	17213	5.80953	19016	5.25880	20830	4.80068	$\overline{14}$	
47	15451	$6 \cdot 47206$	17243	5.79944	19046	$5 \cdot 25048$	20861	4.79370	13	
48	15481	6 • 45961	17273	5.78938	19076	5.24218	20891	4.78673	12	
49	$\frac{15511}{15540}$	6.42484	17303	5.77936	19106	$5 \cdot 23391$ $5 \cdot 22566$	20921	4.77978	11 10	
50 51	$\begin{array}{c} 15540 \\ 15570 \end{array}$	$6 \cdot 43484 \\ 6 \cdot 42253$	17333 17363	5.76937 $5.75941$	19136 19166	5.22566 $5.21744$		4.77286 $4.76595$	9	
52	15600	$6 \cdot 41026$	17393	5.74949	19197	$5 \cdot 20925$	21013	4.75906	8	
53	15630	$6 \cdot 39804$	17423	5.73960	19227	5.20107	21043	4.75219	7	
54	15660	6.38587	17453	5.72974	19257	5.19293	21073	4.74534	6 5	
55 56	15689 15719	$6 \cdot 37374 \\ 6 \cdot 36165$	17483 17513	5.71992 $5.71013$	19287 19317	$5 \cdot 18480 \\ 5 \cdot 17671$	21104 $21134$	4.73851 $4.73170$	4	
57	15749	6.34961	17543	5.71013 $5.70037$	19347	5.16863	21164	4.73170 $4.72490$	3	
58	15779	6.33761	17573	$5 \cdot 69064$	19378	$5 \cdot 16058$	21195	4.71813	2	
59	15809	6.32566	17603	5.68094	19408	5 15256	21225	4.71137	$\frac{1}{0}$	
60	15838	6·31375	17633	5·67128	19438	5·14455	_		$\frac{\sigma}{M}$	
M	N. Cot.	N. Tan.	N. Cot.	N Tan.	N. Cot	N. Tan.				
	81 De	egrees.	80 De	egrees.	79 De	egrees. \	78 De	egrees.		

	1 12 De	egrees.	13 D	egrees.	14 De	egrees.	15 De	egrees.	
M	N. Tan.	N. Tan.	N. Tan.	N. Cot.	N. Tan.	N. Cot.	N. Tan.	N. Cot.	M
${0}$	21256	4.70463	23087	4.33148	24933	4.01078	26795	3.73205	60
1	21286	4.69791	23117	4.32573	24964	4.00582	26826	3.72771	59
2	21316	4.69121	23148	4.32001	24995	4.00086	26857	3.72338	58
3	21347	4.68452	23179	4.31430	25026	3.99592	26888	3.71907	57
5	21377 21408	4.67786 4.67121	23209	4.30860	25056	3.99099	26920		56
6	21408	4.67121 $4.66458$	23240	$4 \cdot 30291 \ 4 \cdot 29724$	25087 25118	3.98607 $3.98117$	26951 26982	3.71046 3.70616	
7	21469	4.65797	23301	4.29159	25149	3.97627	27013	3.70018	
8	21499	4.65138	23332	4.28595	25180	3.97139	27044		52
9	21529	$4 \cdot 64480$	23363	4.28032	25211	3.96651	27076	3.69335	51
10	21560	4.63825	23393	4.27471	25242	3.96165	27107		50
11 12	21590 $21621$	$4 \cdot 63171$ $4 \cdot 62518$	23424 23455	$4 \cdot 26911 \\ 4 \cdot 26352$	25273 25304	3.95680 3.95196	27138 27169	3.68485 3.68061	49
13	21651	4.61868	23484	4.25795	25335	3.94713	27109		48
14	21682	4.61219	23516	$4 \cdot 25239$	25366	3.94232		3.67217	46
15	21712	$4 \cdot 60572$	23547	4.24685	25397	3.93751	27263	3.66796	
16	21743	4.59927	23578	4.24132	25428	3.93271	27294	3.66376	44
17	21773	4.59283	23608	4.23580	25459	3.92793	27326	3.65957	43
18	21804	4.58641	23639	4.23030	25490	3.92316	27357	3.65538	
19	21834	4.58001	23670	4.22481	25521	3.91839	27388	3.65121	
20 21	21864 21895	4.57363 $4.56726$	23700 $23731$	$4 \cdot 21933$ $4 \cdot 21387$	25552 25583	3.91364 $3.90890$	27419 27451		
22	21095	4.56720 $4.56091$	23762	4.21337 $4.20842$	25614	3.90417	27481	3.64289 3.63874	
23	21956	4.55458	23793	$4 \cdot 20298$	25645	3.89945	27513		37
24	21986	4.54826	23823	$4 \cdot 19756$	25576	3.89474		3.63048	36
25	22017	4.54196	23854	$4 \cdot 19215$	25707	3.89004	27576		
26	22047	4.53568	23885	4.18675	25738	3.88536	27607	3.62224	
27 28	22078 22108	4.52941 $4.52316$	23916 23946	4·18137 4·17600	25769 25800	3.88068 3.87601	27638	3.61814 3.61405	
29	22139	4.52510 $4.51693$	1	4.17064	25831	3.87136	27701	3.60996	
30	22169	4.51071	24008	$4 \cdot 16530$	25862	3.86671	27732	3.60588	
31	22200	4.50451	24039	4.15997	25893	3.86208	27764	3.60181	
32	22231	4.49832	24069	$4 \cdot 15465$	25924	3.85745	27795	3.59775	
33	22261	$4 \cdot 49215$		$4 \cdot 14934$	25955	3.85284		3.59370	
34	22292	4.48600		4.14405		3.84824	1	3.58966	
35	22322 22353	$4 \cdot 47986$ $4 \cdot 47374$	24162 24193	$4 \cdot 13877$ $4 \cdot 13350$		3.84364 3.83904		3.58562 3.58160	
37	22383	4.46764	24223	$4 \cdot 13330$ $4 \cdot 12825$	26048 26079	3.83449		3.57758	
38	22414	4.46155		4.12301	26110	3.82992		3.57357	
39	22444	$4 \cdot 45548$		$4 \cdot 11778$	26141	3.82537	28015	3.56957	
40	22475	4.44942	7	$4 \cdot 11256$	26172	3.82083	28046	3.56557	
41	22505	4 44338	24347	4.10736	26203	3.81630	28077	3.56159	
42 43	22536 22567	$4 \cdot 43735$ $4 \cdot 43134$	24377 24408	$4 \cdot 10216$ $4 \cdot 09699$	26235 26266	3.81177 3.80726	28109 28140	3.55761 3.55364	
44	22597	4.42534	24439	4.09033 $4.09182$		3.80726	28172	3.54968	
45	22628	4.41936	24470	4.08666	26328	3.79827	28203	3.54573	
46	22658	4.41340	24501	4.08152	-26359	3.79378	28234	3.54179	-
47	22689	4.40745		4.07639	26390		28266	3.53785	
48	22719	$4 \cdot 40152$	24562	4.07127	26421	3.78485	28297	3.53393	12
49	22750	4.39560	1)	4.06616	26452	3.78040	28329	3.53001	
50 51	22781	4.38969	11	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	26483	3.77595	28360	3.52609	
52	22811 22842	$4 \cdot 38381$ $4 \cdot 37793$	24655 24686	4.05599 $4.05092$	26515 26546	3.77152 3.76709		3.52219 3.51829	
53	22872	4.37207		4.04586	26577	3.76268		3.51623 3.51441	
54	22903	4.36623	24747	4.04081	26608	3.75828	28486	3.51053	
55				4.03578		3.75388	28517	3.50666	5
56	1			4.03075				3.50279	
57 58	22995			4.02574 $4.02074$	14		11	3.49894	_
59	23026 23056				$\begin{vmatrix} 26733 \\ 26764 \end{vmatrix}$		28612 28643	$\begin{vmatrix} 3 \cdot 49509 \\ 3 \cdot 49125 \end{vmatrix}$	
60				4.01078	26795		28675	3.48741	
M	N. Cot.			N. Tan.	N. Cot.		N. Cot.	N. Tan.	M
		egrees.		egrees.		egrees.		egrees.	
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16 Degrees	I		1.C.D	000000	1 1 7 T	0.000	1 10 T)	00000	10 D		
Texas	I	M			-						75/8
1   28706   3-48569   30606   3-26746   32524   3-07464   34465   2-90147   59     2   28738   3-479776   30669   3-26067   32588   3-06867   34530   2-89600   57     4   28800   3-47216   30700   3-25729   32621   3-06654   34530   2-89605   57     5   28893   3-46837   30732   3-25302   32633   3-06265   34596   2-89056   55     6   28864   3-46468   30764   3-25055   3-2655   3-06500   34698   2-88783   54     7   28895   3-46080   30706   3-24719   3-2717   3-05649   34661   2-88511   53     8   28927   3-45703   30828   3-24383   32749   3-05349   34663   2-88511   53     8   28927   3-45703   30828   3-24383   32749   3-05349   34663   2-88511   53     8   28927   3-45703   30828   3-24383   32749   3-05349   34663   2-88790   51     10   28990   3-44951   30891   3-23714   32814   3-0479   34756   2-87700   50     11   29021   3-44576   30821   3-2348   32838   3-04152   34824   2-87161   48     12   29053   3-4202   3-955   3-23048   32878   3-04152   34824   2-87161   48     13   29041   3-43683   31019   3-22353   32975   3-03600   34922   2-85356   45     15   29147   3-43438   31105   3-21392   3004   3-02667   34937   2-85824   42     16   29179   3-42713   31147   3-21053   32975   3-03600   34922   2-85356   45     17   29210   3-42343   31147   3-21053   33072   3-02372   35019   2-85555   42     19   29274   3-41604   31178   3-20734   33104   3-02077   35062   2-85289   41     19   29274   3-41604   31178   3-20734   33104   3-02077   35062   2-85289   41     29305   3-41236   31240   3-2009   31360   3-01499   3-2588   2-85023   40     29305   3-33042   31242   3-2009   31363   3-04053   35182   2-85289   41     29305   3-33042   31494   3-1456   3-1540   3-2077   3-1540   3-2077   3-1540   3-2077   3-1540   3-2077   3-1540   3-2077   3-1540   3-2077   3-1540   3-2077   3-1540   3-2077   3-1540   3-2077   3-1540   3-2077   3-1540   3-2077   3-1540   3-2077   3-1540   3-2077   3-1540   3-2077   3-1540   3-2077   3-1540   3-2077   3-1540   3-2077   3-1540   3-2077   3-1540   3-2077   3-1540		-					'				
2   28733   3.47977   30687   3.26406   32556   3.06857   3.4508   2.89807   56     3   28769   3.47598   30669   3.26507   32588   3.06857   3.4503   2.89807   56     5   28832   3.46837   30762   3.25302   3.2653   3.06654   3.4563   2.89805   56     6   28864   3.46465   30764   3.25055   32653   3.06654   3.4661   2.88511   53     7   28895   3.46080   30764   3.25055   32653   3.06950   3.4628   2.88783   54     8   289927   3.45703   30898   3.24363   3.2717   3.06649   34661   2.88511   53     9   28958   3.456327   30860   3.24049   3.2782   3.05049   34752   2.87700   50     11   29021   3.444576   30923   8.23818   3.3846   3.04490   3.4782   2.87700   50     12   29053   3.44202   3.9555   3.23048   3.2878   3.04150   3.4782   2.87701   50     13   29014   3.43845   3.1019   3.22384   3.2933   3.03556   3.4859   2.86624   46     15   29117   3.43084   3.1019   3.22384   3.2933   3.03556   3.4859   2.86624   46     15   29127   3.424713   3.1083   3.21722   3.3007   3.02963   3.4954   2.86089   41     15   29247   3.41604   3.1178   3.20734   3.3104   3.02077   3.3019   2.55556   42     19   29274   3.41604   3.1178   3.20734   3.3104   3.02077   3.3059   2.55556   42     2   2   23335   3.3466   3.1449   3.1178   3.20734   3.119   3.0260   3.0149   3.117   2.84785   30     2   2   2   2   3.2394   3.1146   3.1179   3.328   3.00310   3.0260   3.565   3.4859   2.86034   44     2   2   2   2   2   3   3   3   3   3	Į.										
A	ı								34498	2.89873	58
Separate   Separate	ı						1 1				
Column   C	I										
Record   Section   Secti					4						
98958   3.46327   30860   3.24049   32782   3.05049   34726   2.87270   51     10	1						1 1		34661		
10   28990	ı								1		
11   29021   3.44576   30923   8.23381   32846   3.04450   34791   2.877430   49   12   29084   3.44502   30987   3.22715   32911   3.03854   34854   2.876161   48   15   29147   3.44306   31051   3.22034   32943   3.03556   34884   2.86624   46   15   29147   3.44308   31051   3.22034   32943   3.03556   34889   2.86624   46   17   29210   3.42343   31115   3.22033   33040   3.02667   34987   2.85582   43   17   29210   3.42343   31115   3.21392   33040   3.02667   34987   2.85582   43   18   29242   3.41973   31147   3.21063   33072   3.02372   35012   2.85582   43   19   29274   3.41604   31178   3.20734   33104   3.02077   35052   2.85582   43   19   29305   3.41236   31210   3.20406   3.3169   3.01489   35117   2.84758   39   22   29368   3.40502   31274   3.19752   33201   3.01196   35150   2.84544   38   32   29483   3.39406   3.1363   3.19456   3.3233   3.00903   35183   2.84229   29483   3.39406   3.1370   3.18775   33298   3.00319   35248   2.83702   35   22   29588   3.38679   31434   3.18177   33283   3.00319   35248   2.83702   35   22   29588   3.38679   31434   3.18187   33330   3.00028   35242   2.83370   35   29590   3.37955   31498   3.17481   33327   2.99158   3.3946   3.3946   3.1876   3.18451   33330   2.99478   3.36378   2.84239   34   2.83702   35   2.85888   3.3817   3.18451   3.3339   2.9947   3.3466   2.82941   3.3442   3.2922   3.29958   3.38679   31438   3.18169   3.3452   2.98588   3.3817   3.4848   3.18187   3.3638   2.99478   3.36586   3.83877   3.18451   3.3339   3.29947   3.3546   3.29478   3.36586   3.83877   3.1846   3.18575   3.3589   2.97717   3.5543   2.88231   3.29488   3.36586   3.38877   3.18488   3.18189   3.36578   3.39716   3.39586   3.34873   3.18578   3.3849   3.38580   3.34684   3.29575   3.35809   3.18481   3.18488   3.3492   3.85850   3.3444   3.28792   3.18586   3.3617   3.18576   3.3589   2.97717   3.5543   2.883314   2.883314   3.29438   3.30331   3.3386   3.39468   3.38377   3.18566   3.16189   3.3589   2.97717   3.5543   2.883314   3.2933   3.30340   3.386		_					1				
13   29084   3.43829   30987   3.22154   32911   3.03854   34856   2.86632   47     14   29116   3.43456   31019   3.22384   32943   3.03556   34889   2.86634   45     15   29147   3.43084   31651   3.22033   32975   3.03260   34922   2.86536   45     16   29179   3.42713   31083   3.21722   33007   3.02963   34924   2.86639   44     17   20210   3.42343   31115   3.21392   33040   3.02667   34987   2.85855   42     19   29274   3.41604   31178   3.20734   33104   3.02077   35052   2.85855   42     19   29274   3.41604   31178   3.20734   33104   3.02077   35052   2.85855   42     19   29336   3.40869   31242   3.20069   3.0163   3.0173   3.5085   2.85029   41     29337   3.40869   31242   3.20079   33169   3.01489   3.5117   2.84758   39     22   29386   3.40502   31274   3.19762   33201   3.01196   35150   2.84494   38     23   29400   3.40136   31306   3.19426   33233   3.00039   35132   2.84229   3.25264							1		1		
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17   29210   3-42843   31145   3-21392   33040   3-02667   34987   2-85525   42   19   29274   3-41604   31178   3-20734   33104   3-02077   35052   2-85289   41   29237   3-40869   31242   3-20079   33169   3-01489   35117   2-85525   42   29337   3-40869   31242   3-20079   33169   3-01489   35117   2-84758   39   22   29368   3-40502   31274   3-19762   33201   3-01196   35150   2-84494   38   3-24940   3-24	1										
18	-				1		33040				
20	I	18	29242					3.02372	35019	2.85555	42
21	ı								1		
22   23368   3.40502   31274   3.19752   33201   3.01196   35150   2.84494   38   24   29432   3.39771   31338   3.19100   33266   3.00611   35216   2.83965   36   25   29463   3.39406   31370   3.18775   33298   3.00319   35248   2.83702   35   27   29526   3.38679   31443   3.18127   33363   2.99738   35314   2.83303   2.99738   35314   2.83303   2.99738   35314   2.83303   2.99738   35314   2.83303   2.99738   35314   2.83303   2.99738   3.00019   3.5248   2.83702   35   3.00019   3.5248   2.83702   35   3.00019   3.5248   2.83702   35   3.00019   3.5248   2.83702   35   3.00019   3.5248   2.83702   35   3.00019   3.5248   2.83403   3.00019   3.5248   2.83702   35   3.00019   3.0001									,		
24	2		29368	$3 \cdot 40502$	31274	3.19752	33201	3.01196	35150	2.84494	38
25	1										
26	No.						1	1			
27					1		1				
29   29590   3.37595   31498   3.17481   33427   2.99158   35379   2.82653   31   30   29621   3.37594   31530   3.17159   33460   2.98868   35412   2.82391   30   31   29653   3.37594   31530   3.17159   33460   2.98868   35412   2.82391   30   31   29653   3.36575   31594   3.16517   33524   2.98290   35475   2.81870   28   32   29716   3.36516   31626   3.16197   33557   2.98004   35570   2.81610   27   34   29748   3.36158   31658   3.15877   33589   2.97717   3.5543   2.81350   26   35   29780   3.35800   31690   3.15558   33621   2.97490   3.5576   2.81091   25   36   29811   3.35443   32722   3.15240   33654   2.97144   35608   2.80833   24   2.98292   32477   3.2843   3.35087   31754   3.14922   33686   2.96573   3.5644   2.80574   23   38   2.9875   3.34732   31786   3.14605   33718   2.96573   3.5644   2.80574   23   32   2.98004   3.34023   31850   3.13972   33783   2.96004   3.5740   2.80059   21   2.9970   3.33670   31882   3.13656   33816   2.95720   3.5770   2.79802   20   20   20   20   20   20   20	b	27	29526	3.38679	31434	3.18127	33363	2.99738	35314	2.83176	33
30	l	_									
31   29653   3.37234   31562   3.16338   33492   2.98580   35445   2.81310   29   32   29685   3.36875   31594   3.16517   33524   2.98292   35477   2.81870   28   32   29748   3.36516   31626   3.16197   33557   2.98004   35510   2.81610   27   34   29748   3.36518   31658   3.15877   33589   2.97777   35543   2.81350   26   35   29780   3.35800   31690   3.15558   33621   2.97420   35576   2.81091   25   36   29811   3.35443   32722   3.15240   33654   2.97144   35608   2.80833   24   37   29843   3.35087   31754   3.14922   33686   2.96858   35641   2.80574   23   23   23   23   23   23   23   2											_
32   29685   3.36875   31594   3.16517   33524   2.98292   35477   2.81870   28   33   29716   3.36516   31626   3.16197   33557   2.98004   35510   2.81610   27   34   29780   3.36580   31658   3.15877   33589   2.97717   3.543   2.81350   26   28111   3.35443   32722   3.15240   33654   2.97144   35608   2.80833   24   37   29843   3.35087   31754   3.14922   33686   2.96858   35641   2.80574   23   38   29875   3.34732   31786   3.14605   33718   2.96573   35674   2.80316   22   39   29906   3.34377   31818   3.14288   33751   2.96288   35707   2.80059   21   40   29938   3.34023   31850   3.13972   33783   2.96004   35740   2.79802   20   41   29970   3.33670   31882   3.13656   33816   2.95720   35772   2.79545   19   42   30001   3.33317   31914   3.13341   33848   2.95437   35805   2.79289   18   43   30033   3.32965   31946   3.13027   33881   2.95155   35833   2.79033   17   44   30065   3.32614   31978   3.1213   33913   2.94872   35904   2.78528   14   3097   3.3264   32010   3.12400   33945   2.94590   35904   2.78528   14   30097   3.3264   32010   3.12400   33945   2.94590   35904   2.78528   14   30024   3.30868   32139   3.11153   34075   2.93468   36002   2.77761   12   49   30224   3.30868   32139   3.11153   34075   2.93468   36035   2.77254   10   30287   3.30174   32203   3.10532   34140   2.92910   36101   2.77002   9   330351   3.29483   32267   3.09914   34205   2.92354   36167   2.76498   7   30478   3.28169   32235   3.00293   34173   2.92632   36134   2.76590   5   30541   3.27426   32460   3.08073   34400   2.90696   36364   2.74997   5   30541   3.27426   32460   3.08073   34400   2.90696   36364   2.74997   5   30541   3.27426   32460   3.08073   34400   2.90696   36364   2.74997   5   30541   3.27426   32460   3.08073   34400   2.90696   36364   2.74997   5   30541   3.27426   32460   3.08073   34400   2.90696   36364   2.74997   36331   2.75246   3   3   3   3   3   3   3   3   3	ľ										
33	100										
35		33	29716	3.36516	31626	3.16197		2.98004	35510	2.81610	27
36	į										
37   29843   3.35087   31754   3.14922   33686   2.96858   35641   2.80574   23   28   29875   3.34732   31786   3.14605   33718   2.96573   35674   2.80316   22   28   29906   3.34377   31818   3.14288   33751   2.96288   35707   2.80059   21   40   29938   3.34023   31850   3.13972   33783   2.96004   35740   2.79802   20   41   29970   3.33670   31882   3.13656   33816   2.95720   35772   2.79545   19   42   30001   3.33317   31914   3.13341   33848   2.95437   35805   2.79289   18   43   30033   3.32965   31946   3.13027   33881   2.95155   35838   2.79033   17   44   30065   3.32614   31978   3.12713   33913   2.94872   35871   2.78778   16   45   30097   3.32264   32010   3.12400   33945   2.94590   35904   2.78523   15   46   30128   3.31914   32042   3.12087   33978   2.94309   35937   2.78269   14   47   30160   3.31565   32074   3.11775   34010   2.94028   35969   2.78014   13   48   30192   3.31216   32106   3.11464   34043   2.93748   36002   2.77761   12   49   30224   3.30868   32139   3.11153   34075   2.93468   36035   2.77507   11   49   30287   3.30174   32203   3.10532   34140   2.92910   36101   2.77002   9   52   30319   3.29829   32235   3.10223   34173   2.92632   36134   2.76750   8   7   30478   3.29433   32267   3.09914   34205   2.92354   36167   2.764498   7   54   30382   3.29139   3.29299   3.99060   34238   2.92076   36199   2.76247   6   55   30444   3.28795   32331   3.09298   34270   2.91799   36232   2.75996   5   56   30446   3.28452   32363   3.08991   34303   2.91523   36265   2.75746   4   57   30478   3.28109   32396   3.08685   34335   2.91246   36298   2.75496   5   59   30541   3.27426   32460   3.08073   34400   2.90696   36364   2.744997   5   59   30541   3.27426   32460   3.08073   34400   2.90696   36364   2.744997   5   50   30573   3.27085   32492   3.07768   34433   2.90421   36397   2.74748   0   M   N. Cot.   N. Tan.   N. Cot.   N. Tan.   N. Cot.   N. Tan.   M	k										
39   29906   3.34377   31818   3.14288   33751   2.96288   35707   2.80059   21	ı										
40       29938       3.34023       31850       3.13972       33783       2.96004       35740       2.79802       20         41       29970       3.33670       31882       3.13656       33816       2.95720       35772       2.79545       19         42       30001       3.33317       31914       3.13341       33848       2.95437       35805       2.79289       18         43       30033       3.32965       31946       3.13027       33881       2.95155       35833       2.79033       17         44       30065       3.32614       31978       3.1213       33913       2.94590       35904       2.78523       15         46       30128       3.31914       32042       3.12087       33978       2.94590       35904       2.78523       15         46       30128       3.31914       32042       3.12087       33978       2.94590       35937       2.78269       14         47       30160       3.31565       32074       3.11753       34010       2.94028       35969       2.78014       13         48       30192       3.5116       32106       3.11464       34043       2.93748       36002 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td>1</td><td>,</td><td></td><td></td><td></td></t<>							1	,			
41       29970       3.33670       31882       3.13656       33816       2.95720       35772       2.79545       19         42       30001       3.33317       31914       3.13341       33848       2.95437       35805       2.79289       18         43       30033       3.32965       31946       3.13027       33881       2.95155       35838       2.79033       17         44       30065       3.32614       31978       3.12713       33913       2.94872       35871       2.78778       16         45       30097       3.32264       32010       3.12400       33945       2.94309       35904       2.78523       15         46       30128       3.31914       32042       3.12087       33978       2.94309       35904       2.78523       15         47       30160       3.31565       32074       3.11775       34010       2.94028       35969       2.78014       13         48       30192       3.51216       32106       3.11464       34043       2.93748       36002       2.77761       12         49       30287       3.3051       3.29483       32171       3.10842       34108       2.93189	1							1			
42   30001   3.33317   31914   3.13341   33848   2.95437   35805   2.79289   18   43   30033   3.32965   31946   3.13027   33881   2.95155   35838   2.79033   17   44   30065   3.32614   31978   3.12713   33913   2.94872   35871   2.78778   16   45   30097   3.32264   32010   3.12400   33945   2.94590   35904   2.78523   15   46   30128   3.31914   32042   3.12087   33978   2.94590   35937   2.78269   14   47   30160   3.31565   32074   3.11775   34010   2.94028   35969   2.78014   13   48   30192   3.31216   32106   3.11464   34043   2.93748   36002   2.77761   12   49   30224   3.30868   32139   3.11153   34075   2.93468   36035   2.77507   11   49   30287   3.30521   32171   3.10842   34108   2.93189   36068   2.77254   10   50   30255   3.30521   32171   3.10842   34108   2.92910   36101   2.77002   9   52   30319   3.29829   32235   3.10223   34140   2.92910   36101   2.77002   9   53   30351   3.29483   32267   3.09914   34205   2.92354   36167   2.76498   7   54   30382   3.29139   32299   3.99606   34238   2.92076   36199   2.76247   6   55   30414   3.28795   32331   3.09298   34270   2.91799   36232   2.75996   5   56   30446   3.28452   32363   3.08891   34303   2.91523   36265   2.75746   4   57   30478   3.28109   32396   3.08685   34335   2.91246   36298   2.75496   3   58   30509   3.27767   32428   3.08879   34368   2.90971   36331   2.75246   2   59   30541   3.27426   32460   3.08073   34400   2.90696   36364   2.74997   3   60   30573   3.27085   32492   3.07768   34433   2.90421   36397   2.74748   M   M   N. Cot.   N. Tan.   N. Cot.   N. Tan.   M.   M   M   M   M   N. Cot.   N. Tan.   M. Cot.   N. Tan.   M   M   M   M   M   M   M   M   M	-										
44         30065         3.32614         31978         3.12713         33913         2.94872         35871         2.78778         16           45         30097         3.32264         32010         3.12400         33945         2.94590         35904         2.78523         15           46         30128         3.31914         32042         3.12087         33978         2.94309         35904         2.78269         14           47         30160         3.31565         32074         3.11775         34010         2.94028         35969         2.78014         13           48         30192         3.31216         32106         3.11464         34043         2.93748         36002         2.77761         12           49         30224         3.30868         32139         3.11153         34075         2.93468         36035         2.77254         10           50         30255         3.30521         32171         3.10842         34140         2.92910         36101         2.77002         9           52         30319         3.29829         32235         3.10223         34173         2.92632         36134         2.76498         7           54         <		42	30001	3.33317	31914	$3 \cdot 13341$	33848	2.95437	35805	2.79289	18
45   30097   3.32264   32010   3.12400   33945   2.94590   35904   2.78523   15   14   15   15   15   15   15   15	2000										
14											
47   30160   3.31565   32074   3.11775   34010   2.94028   35969   2.78014   13   1464   34043   2.93748   36002   2.77761   12   14   30224   3.30868   32139   3.11153   34075   2.93468   36035   2.77507   11   11   11   11   11   11   11	Ch de	_									
49       30224       3.30868       32139       3.11153       34075       2.93468       36035       2.77507       11         50       30255       3.30521       32171       3.10842       34108       2.93189       36068       2.77254       10         51       30287       3.30174       32203       3.10532       34140       2.92910       36101       2.77002       9         52       30319       3.29829       32235       3.10223       34173       2.92632       36134       2.76750       8         53       30351       3.29483       32267       3.09914       34205       2.92354       36167       2.76498       7         54       30382       3.29139       32999       3.99606       34238       2.92076       36199       2.76247       6         55       30414       3.28795       32331       3.09298       34270       2.91799       36232       2.75996       5         56       30446       3.28452       32363       3.08685       34335       2.91246       36298       2.75496       3         57       30478       3.27085       32428       3.08379       34368       2.90971       36331       2.	1		30160		32074	3.11775	34010	2.94028	35969	2.78014	13
50         30255         3·30521         32171         3·10842         34108         2·93189         36068         2·77254         10           51         30287         3·30174         32203         3·10532         34140         2·92910         36101         2·77002         9           52         30319         3·29829         32235         3·10223         34173         2·92632         36134         2·76750         8           53         30351         3·29483         32267         3·09914         34205         2·92354         36167         2·76498         7           54         30382         3·29139         32299         3·99606         34238         2·92076         36199         2·76247         6           55         30414         3·28795         32331         3·09298         34270         2·91799         36232         2·75746         4           57         30478         3·28109         32396         3·08685         34335         2·91246         36298         2·75496         3           58         30509         3·27767         32428         3·08073         34400         2·90696         36364         2·74997         1           59         30		48									
51         30287         3·30174         32203         3·10532         34140         2·92910         36101         2·77002         9           52         30319         3·29829         32235         3·10223         34173         2·92632         36134         2·76750         8           53         30351         3·29483         32267         3·09914         34205         2·92354         36167         2·76498         7           54         30382         3·29139         32299         3·99606         34238         2·92076         36199         2·76247         6           55         30414         3·28795         32331         3·09298         34270         2·91799         36232         2·75996         5           56         30446         3·28452         32363         3·08991         34303         2·91523         36265         2·75466         4           57         30478         3·28109         32396         3·08685         34335         2·91246         36298         2·75496         3           58         30509         3·27767         32428         3·08073         34400         2·90696         36364         2·74997         1           59         305	4		_					1			4.0
52         30319         3.29829         32235         3.10223         34173         2.92632         36134         2.76750         8           53         30351         3.29483         32267         3.09914         34205         2.92354         36167         2.76498         7           54         30382         3.29139         32299         3.99606         34238         2.92076         36199         2.76247         6           55         30414         3.28795         32331         3.09298         34270         2.91799         36232         2.75996         5           56         30446         3.28452         32363         3.08991         34303         2.91523         36265         2.75746         4           57         30478         3.28109         32396         3.08685         34335         2.91246         36298         2.75496         3           58         30509         3.27767         32428         3.08379         34368         2.90971         36331         2.75246         2           59         30541         3.27085         32492         3.07768         34433         2.90421         36397         2.74748         0           M         N. C	1										9
54         30382         3.29139         32299         3.99606         34238         2.92076         36199         2.76247         6           55         30414         3.28795         32331         3.09298         34270         2.91799         36232         2.75996         5           56         30446         3.28452         32363         3.08991         34303         2.91523         36265         2.75746         4           57         30478         3.28109         32396         3.08685         34335         2.91246         36298         2.75496         3           58         30509         3.27767         32428         3.08379         34368         2.90971         36331         2.75246         2           59         30541         3.27426         32460         3.08073         34400         2.90696         36364         2.74997         1           60         30573         3.27085         32492         3.07768         34433         2.90421         36397         2.74748         0           M         N. Cot.         N. Tan.         N. Cot.         N. Tan.         N. Cot.         N. Tan.         M. Cot.         N. Tan.         M. Cot.         N. Tan. <td></td> <td>52</td> <td>30319</td> <td>3.29829</td> <td>32235</td> <td>3 • 10223</td> <td>34173</td> <td>2.92632</td> <td>36134</td> <td>2.76750</td> <td>_</td>		52	30319	3.29829	32235	3 • 10223	34173	2.92632	36134	2.76750	_
55         30414         3.28795         32331         3.09298         34270         2.91799         36232         2.75996         5           56         30446         3.28452         32363         3.08991         34303         2.91523         36265         2.75746         4           57         30478         3.28109         32396         3.08685         34335         2.91246         36298         2.75496         3           58         30509         3.27767         32428         3.08379         34368         2.90971         36331         2.75246         2           59         30541         3.27426         32460         3.08073         34400         2.90696         36364         2.74997         1           60         30573         3.27085         32492         3.07768         34433         2.90421         36397         2.74748         0           M         N. Cot.         N. Tan.         N. Cot.         N. Tan.         N. Cot.         N. Tan.         M. Tan.		_			•						_
56         30446         3.28452         32363         3.08991         34303         2.91523         36265         2.75746         4           57         30478         3.28109         32396         3.08685         34335         2.91246         36298         2.75496         3           58         30509         3.27767         32428         3.08379         34368         2.90971         36331         2.75246         2           59         30541         3.27426         32460         3.08073         34400         2.90696         36364         2.74997         1           60         30573         3.27085         32492         3.07768         34433         2.90421         36397         2.74748         0           M         N. Cot.         N. Tan.         N. Cot.         N. Tan.         N. Cot.         N. Tan.         M. Tan.	1	_	5								
57         30478         3.28109         32396         3.08685         34335         2.91246         36298         2.75496         3           58         30509         3.27767         32428         3.08379         34368         2.90971         36331         2.75246         2           59         30541         3.27426         32460         3.08073         34400         2.90696         36364         2.74997         1           60         30573         3.27085         32492         3.07768         34433         2.90421         36397         2.74748         0           M         N. Cot.         N. Tan.         N. Cot.         N. Tan.         N. Cot.         N. Tan.         M	I				,	3.08991	34303			2.75746	4
59       30541       3.27426       32460       3.08073       34400       2.90696       36364       2.74997       0         M       N. Cot.       N. Tan.       M	1	57		3.28109							
		_				,			1		
M N. Cot. N. Tan. N. Cot. N. Tan. N. Cot. N. Tan. M. Cot. N. Tan.	1	_									
73 Degrees. 72 Degrees. 71 Degrees. 70 Degrees.									N. Cot.	N. Tan.	M
	İ		73 D	egrees.	72 D	egrees.	71 De	egrees.	70 De	egrees.	

	20 De	egrees.	21 D	egrees.	22 D	egrees.	23 D	egrees.	
M	N. Tan.	N. Cot.	N. Tan.	N. Cot.	N. Tan.	N. Cot.	N. Tan.	N. Cot.	M
J	36397	2.74748	38386	2.60509	40403	2.47509	42447	2.35585	60
1	36430	2.74499	38420	2.60283	40436	2.47302		2.35395	
2 3	36463 36496	2·74251 2·74004	38453 38487	$2 \cdot 60057$ $2 \cdot 59831$	40470 40504	2·47095 2·46888		2.35205	
4	36529	2.74004 $2.73756$	38520	2.59606	40538	2.46682		2·35015 2·34825	
5	36562	2.73509	38553	2.59381	40572	2.46476	_	2.34636	
6	36595	2.73263	38587	2.59156	40606	2.46270	42654	2.34447	54
7 8	36628	2.73017	38620	2·58932 2·58708	40640	2.46065	42688	2.34258	
. 9	36661 36694	2.72771 $2.72526$	38654 38687	2.58708	40674	2·45860 2·45655	42722 42757	2·34069 2·33881	52 51
10	36727	2.72281	38721	2.58261	40741	2.45451	42791	2.33693	
11	36760	2.72036	38754	2.58038	40775	2.45246	42826	2.33505	
12	36793	2.71792	38787	2.57815	40809	2.45043	42860	2.33317	48
13 14	36826 36859	2.71548 $2.71305$	38821 38854	2.57593 $2.57371$	40843	2·44839 2·44636	42894 42929	2·33130 2·32943	
15	36892	2.71303 $2.71062$	38888	2.57371	40911	2.44433	42929	3.32756	
16	36925	2.70819	38921	2.56928	40945	2.44230	42998	$2 \cdot 32570$	44
17	36958	2.70513	38955	2.56707	40979	2.44027	43032	2.32383	
18	36991	2.70335	38988	2.56487	41013	2 • 43825	43067	2.32197	42
19	37024	2.70094	39022	2.56266	41047	2.43623	43101	2.32012	
20 21	37057 37090	2.69853 2.69612	39055 39089	2.56046 $2.55827$	41081	2·43422 2·43220	43136	2·31826 2·31641	40 39
22	37123	2.69371	39122	2.55608	41119	2.43220	43170	2.31641 $2.31456$	_
23	37157	2.69131	39156	2.55389	41183	2 • 42819	43239		37
24	37190	2.68892	39190	2.55170	41217	2.42618	43274		
25 26	37223 37256	2.68653	39223 39257	2.54952 $2.54734$	41251	2·42418 2·42218	43308	2·30902 2·30718	_
27	37289	2.68414 2.68175	39290	2.54734 $2.54516$	41319	2.42210	43378	2.30718 2.30534	
28	37322	2.67937	39324	2.54299	41353	2.41819	43412	2.30351	32
29	37355	2.67700	39357	2.54082	41387	2.41620	43447	2.30167	31
30	37388	2 · 67462	39391	2.53865	41421	2.41421	43481	$\frac{2 \cdot 29984}{}$	30
31	37422	2.67225	39425	2.53648	41455	2.41223	43516	2.29801	29
32	37455	2.66989 2.66752	39458 39492	2.53432 $2.53217$	41490	$2 \cdot 41025$ $2 \cdot 40827$	43550 43585	2·29619 2·29437	
34	37521	2.66516	39526	2.53001	41558	2.40629	43620		_
35	37554	2.66281	39559	2.52786	41592	2.40432	43654		
36	37588	2.66046	39593	2.52571	41626	2.40235	43689	2.28891	
37	37621 37654	2.65811 2.65576	39626 39660	2.52357 $2.52142$	41660	2·40038 2·39841	43724 43758	2·28710 2·28528	
39	37687	2.65370 $2.65342$	39694	2.5112	41728	2.39645			
40	37720	2.65109	39727	2.51715	41763			2.28167	
41	37754	2.64875	39761	2.51502	41797	2.39253	43862		
42 43	37787 37820	2.64642	39795 39829	2.51289 $2.51076$	41831	2·39058 2·38862	43897	2·27806 2·27626	
43	37853	2.64410 $2.64177$	39862	2.51076	41865		43932	$2 \cdot 27626$ $2 \cdot 27447$	
45	37887	2.63945	39896	2.50652	41933	2.38473	44001	2.27267	_
46	37920	2.63714	39930	2.50440	41968	2.38279	44036	2.27088	14
47	37953	2.63483	39963	2.50229	42002	2.38084	44071	2.26909	13
48	37986	2.63252	39997	2.50018	42036	2.37891	44105	2.26730	
49 50	38020 38053	$2 \cdot 63021$ $2 \cdot 62791$	40031	2·49807 2·49597			44140	$2 \cdot 26552$ $2 \cdot 26374$	
51	38086	2.62791	40003	2.49386	42103	1	44210		
52	38120	2.62332	40132	2.49177	42173	2.37118	44244	2.26018	8
53		2.62103		2.48967	42207				
54 55		2.61874 2.61646			42242 42276			2.25663 2.25486	_
56	38253	2.61418		2.48340			<b>FI</b>		4
57	1	2.61190	1	2.48132	42345	2.36158	44418	2.25132	3
58		2.60963		2.47924	42379			1	2
59		2.60736	40369	2.47716 $2.47509$	42413 42447		44488		$\begin{vmatrix} 1 \\ 0 \end{vmatrix}$
60	1		11		11	1		1	
M N. Cot. N. Tan. N. Cot. N. Tan.		N. Cot.		N. Cot.		M			
2	69 Degrees. 68 Degrees			egrees.	1 67 D	egrees.	11 66 D	egrees.	

	94 D	egrees.	95 D	egrees.	1 96 D	egrees.	1 .07 D	egrees.	
M	N. Tan.	N. Cot.	N. Tan.	N. Cot.	N. Tan. 1	N. Cot.	N. Tan.	N. Cot.	7.5
0	44523	2.24604	46631	2 · 1445	48773	2.05030	50953	1.96261	M
1	44558	2.24428	46666	2.14288	48809	2.04879	50989	1.96120	60
2	44593	2.24252	46702	2.14125	48845	2.04728	51026	1.95979	58
3	44627	2.24077	46737	2.13963	48881	2.04577	51063	1.95838	57
4 5	44662	2·23902 2·23727	46772	2·13801 2·13639	48917 48953	$2 \cdot 04426$ $2 \cdot 04276$	51099 51136	1.95698 1.95557	56
6	44732	2.23553	46843	$2 \cdot 13033$	48989	2.04270 $2.04125$	51173	1.95417	55 54
7	44767	2.23378	46879	2.13316	49026	2.03975	51209	1.95277	53
8	44802	2.23204	46914	2.13154		2.03825	51246	1.95137	52
9 10	44837	2·23030 2·22857	46950	2.12993		2.03675	51283	1.94997	51
11	44907	2.22683	46985	$2 \cdot 12832$ $2 \cdot 12671$	49134 49170	2·03526 2·03376	51319 51356	1.94858 1.94718	50 49
12	44942	2.22510	47056	$2 \cdot 12511$	49206	2.03227	51393	1.94579	48
13	44977	2.22337	47092	2 • 12350	1	2.03078	51430		47
14	45012	2.22164	47128	2.12190	49278	2.02929	51467	1.94301	46
15	45047	$\frac{2 \cdot 21992}{}$	47163	2.12030		2.02780	51503	1.94162	
16 17	45082 45117	2·21819 2·21647	47199	2.11871	49351	2.02631	51540	1.94023	44
18	45152	2.21647 $2.21475$	47234	$2 \cdot 11711$ $2 \cdot 11552$	49387 49423	$2 \cdot 02483$ $2 \cdot 02335$	51577 51614	1.93885 1.93746	43
19	45187	2.21304	47305	2.11392	49459	2.02187	61651	1.93608	42
20	45222	2.21132	47341	2.11233	49495	2.02039	51688	1.93470	40
21	45257	2.20961	47377	2.11075	49532	2.01891	51724		39
22 23	45292 45327	$2 \cdot 20790$ $2 \cdot 20619$	47412	2·10916 2·10758	49568 49604	2.01743 $2.01596$	51761 51798	1.93197 1.93057	38
24	45362	2.20449	47483	$2 \cdot 10730$	49640	2.01330	51835	1.93037 $1.92920$	37 36
25	45397	2.20278	47519	2.10441	49677	2.01302	51872	1.92782	35
26	45432	2.20108	47555	2.10284		2.01155	51909	1.92645	34
27 28	45467 45502	2·19938 2·19769	47590 47626	2.00126 2.09969		2.01008 $2.00862$	51946	1.92508	
29	45537	$2 \cdot 19709$	47662	2.09909	49786 49822	2.00002	51983 52020	1.92371 $1.92335$	32 31
30	45573	2.19430	47698		1	2.00569	52057	1.92098	30
31	45608	2.19261	47733	2.09498	49894	2.00423	52094	1.91962	29
32		2.19092		2.09341	49931	2.00277	52131	1.91825	
33	45678 45713	2.18923	-	2.09184		2.00131	52168	1.91690	27
34 35	45748	2·18755 2·18587	47840 47876	2·09028 2·08872		1.99986 $1.99841$	52205 52242	1.91554 1.91418	26 25
36	45784	2.18419		2.08716	50076	1.99695	52279		24
37	45819	2 · 18251	47948	2.08560		1.99550	52316	1.91148	23
38	45854 45889	2.18084		2.08405	50149	1.99406	52353	1.91017	
39 40	45924	$2 \cdot 17916$ $2 \cdot 17749$	48019	2.08250 $2.08094$		1.99261 $1.99116$	52390 52427	1.90876 1.90741	
41	45960	2.17582	48091	2.07939		1.98972	52464	1.90607	
42	45995	2.17416	48127	2.07785	50295	1.98828	52501	1.90472	18
43	46030	2.17249	48163	2.07630	50331	1.98684	52538	1.90337	
44 45	46065 46101	$2 \cdot 17083$ $2 \cdot 16917$	48198 48234	2.07476 $2.07321$	50368	1.98540 1.98396	52575	1.90203 1.90069	
	45136	$\frac{2 \cdot 16317}{2 \cdot 16751}$					52613		
46 47	46171	2.16751	48270 48306	2.07167 $2.07014$	50441	1.98253 $1.98110$	52650 52687	1.89935 1.89801	14 13
48	46206	2.16420	43342	2.06860	50514	1.97966	52724	1.89667	
49	46242	2.16255	48378	2.06706	50550	1.97823	52761	1.89533	11
50	46277	2.16090	48414	2.06553	50587	1.97680	52798	1.89400	10
51 52	46312 46348	$2 \cdot 15925$ $2 \cdot 15760$	48450 48486	2.06400 $2.06247$	50623 50660	1.97538 1.97395	52836 52873	1.89266 $1.89133$	9 8
53	46383	2.15596	48521	2.06094	50696	1.97393 $1.97253$	52910	1.89000	7
54	46418	2.15432	48557	2.05942	50733	1.97111	52947	1.88867	6
55	46454	2.15268	48593	2.05789	50769	1.96969	52984	1.88734	5
56 57	46489	$2 \cdot 15104$ $2 \cdot 14940$	48629 48665	2.05637 $2.05485$	50806	1.96827 1.96685	53024	1.88602 $1.88469$	3
58	46560	2.14940	48701	2.05485		1.96544	53059 53096	1.88337	2
59	46595	2.14614	48737	2.05182		1.96402	53134	1.88205	1
60	46631	2.14451	48773	2.05030	50953	1.96261	53171	1.88073	0
M	-	N. Tan.	N. Cot.	N. Tan.	N. Cot	N. Tan.	N. Cot.	N. Tan.	M
. 4	65 D	egr es.	64 D	egrees.	63 De	egrees.	62 De	egrees.	1

_	4 00 D		00 D	croos II	20 Da	egrees.	31 De	grees.	
		grees.		egrees.  N. Cot.	N. Tan.	N. Cot.	N. Tan	N. Cot.	DIE
M	N. Tan.	N. Cot.	N. Tan.						$\frac{\mathbf{M}}{\mathbf{G}}$
0	53171 53208	1.88073 1.87941	55431 55469	1.80405 $1.80281$	57735 57774	1.73205 $1.73089$	60086	1.66428 1.66318	60 f
$\frac{1}{2}$	53246	1.87809	55507	1.80158	57813	1.77973	60165	1.66209	58
3	53283	1.87677	55545	1.80034	57851	1.72857	60205	1.66099	57
4	53320	1.87546	55583	1.79911	57890	1.72741	60245	1.65990	56
5	53358	1.87415	55621 55659	1.79788 $1.79665$	57929 57968	1.72625 $1.72509$	$60284 \\ 60324$	1.65881 $1.65772$	55 54
6 7	53395	1.87283 $1.87152$	55697	1.79665 $1.79542$	58007	1.72309 $1.72393$	60364	1.65663	
8	53470	1.87021	55736	1.79419	58046	1.72278	60403	1.65554	
9	53507	1.86891	55774	1.79296	58085	1.72163	60443	1.65445	51
10	53545	1.86760	55812	1.79174	58124	1.72047	60483	1.95337 $1.65228$	50
11 12	53582 53620	1.86630 $1.86499$	55850 55888	1.79051 $1.78929$	58162 58201	1.71932 $1.71817$	60522 60562	1.65220 $1.65120$	49 48
13	53657	1.86369	55926	1.78807	58240	1.71702	60602	1.65011	47
14	53694	1.86239	56964	1.78685	58279	1.71588	60642	1.64903	
15	53732	1.86109	56003	1.78563	58318	1.71473	60681	1.64795	45
16	53769	1.85979	56041	1.78441	58357	1.71358	60721	1.64687	44
17	53807	1.85850	56079	1.78319	58396	1.71244	60761	1.64579	43
18	53844	1.85720	56117 56156	1.78198 $1.78077$	58435 58474	1.71129 $1.71015$	60801 60841	1.64471 $1.64363$	
19 20	53882	1.75591 $1.85462$	56194	1.77955	58513	1.70901	60881	1.64256	
21	53957	1.85333	56232	1.77834	58552	1.70787		1.64148	39
22	53995	1.85204	56270	1.77713	58591	1.70673	60960	1.64041	
23	54032	1.85075	56309	1.77592	58631	1.70560	61000	1.63933 1.63826	
24 25	54070 54107	1.84946 1.84818	56347 56385	1.77471 $1.77351$	58670 58709	1.70446 $1.70332$	61040 61080	1.63719	
26	54107	1.84689	56424	1.77230	58748	1.70219	61120	1.63612	
27	54183	1.84561	56462	1.77110	58787	1.70106	61160	1.63505	33
28	54220	1.84433	56500	1.76990	58826	1.79992	61200	1.63398	
29	54258	1.84305	56539 56577	1.76869 $1.76749$	58865 58904	1.69879 $1.69766$	$\begin{array}{ c c c c } \hline 61240 \\ 61280 \\ \hline \end{array}$	1.63292 $1.63185$	
$\frac{30}{21}$	54296	1.84177		$\frac{1.76749}{1.76629}$	58944	1.69653	61320	$\frac{1.63079}{1.63079}$	
31 32	54333	1.84049 $1.83922$	56616 56654	1.76529 $1.76510$	58983	1.69541	61360	1.62972	
33	54409	1.83794	56693	1.76390	59022	1.69428	61400	1.62866	27
34	54446	1.83667	56731	1.76271	59061	1.69315	61440	1.62760	
35	54484	1.83540	56769	1.76151	59101	1.69203	14	$1 \cdot 62654$ $1 \cdot 62548$	
36	54522	1.83413 $1.83286$	56808 56846	1.76032 $1.75913$	59140 59179	1.69091 $1.68979$	61520 61561	1.62442	
38		1.83250 $1.83159$	56885	1.75794	59218			1.62336	
39		1.83033	56923	1.75675	59258	1.68754	41	1.62230	21
40		1.82906	57962	1.75556	59297			1.62125	
41		1.82780	57000	1.75437	59336	1.68531 $1.68419$	11	1.62019 $1.61914$	
42 43		1.82654 $1.82528$	57039 57078	1.75319 $1.75200$	59376 59415		11	1.61808	
44	1 1	1.82402	1	1.75082	59454	20	61842	1.61703	16
45		1.82276	57155	1.74964	59494	1.68085	61882	1.61598	15
46	54900	1.82150	57193	1.74846	59533		41		
47	54938	1.82025	57232	1.74728	59573	1	15		
48		1.81899	57271	1.74610 $1.74492$	59,612		11	1	1
49		1.81774 1.81649			59651 59691	•			_
51		1.81524	11	1.74257			14	1	
52	55127	1.81399	57425		59770	1.67309	62164	1.60865	
53		1		1	11			1	.1
54 54	1		11	1.73905 $1.73788$		•	11		_
56					12		11		
5			15	1.73555	59967	1.66757	62366	1.60348	3
58	1		11	1		4	51		_
5			11		60046		12	A	1
6		[		N. Tan.	1]	N. Tan.	N. Cot.		$\frac{1}{M}$
M			-		· · · · · · · · · · · · · · · · · · ·				- 111
22	1 61 L	egrees.	W 60 T	egrees.	11 59 L	egrees.	" 58 T	egrees.	1

	32 Degrees.    33 Degrees.		egrees.	34 Degrees.		35 Degrees.		1	
M	-	N. Cot.	N. Tan.	N. Cot.	N. Tan.   N. Cot.		N. Tan. N. Cot.		M
(	62487	1.60033	64941	1.53986	67451	1.48256	70021	1.42815	
1			11			1.48163	70064	1.42726	59
2 3			1.1	1	67536	1.48070	11		
4						1.47977 $1.47885$		1.42550 $1.42462$	
1						1.47792			
6					67705	1.47699	70281	1.42286	
8		1.59311 1.59208							53
9		1.59208				1.47514 1.47422			52 51
10		1.59002	65355			1.47330			
11		1.58900	1		67917	1.47238	70499	1.41847	49
12		1.58797 $1.58695$			1	1.47146			1
14		1.58595 $1.58593$			68002 68045	1.47053 $1.46962$	70586 70629		
15		1.58490		1		1.46902 $1.46870$	13	•	
16	63136	1.58388	65604	1.52429	68130	1.46778	70717	1.41409	I
17		1.58286	11	1	68173	1.46686	70760	1.41322	43
18		1.58184	65688	1.52235	1.4	1.46595			
19 20	1	1.58083 1.57981	65729 65771	1.52139 $1.52043$	68258 68301	1.46503 1.46411	70848 70891	1.41148	41 40.
21		1.57879	65813	1.52045 $1.51946$	68343	1.46320	70391		39
22		1.57778	65854	1.51850	68386	1.46229	70979	1.40887	38
23		1.57676	65896	1.51754		1.46137	71023	1.40800	
24 25		1.57575 $1.57474$		1.51658 1.51562	68471 68514	1.46046 $1.45955$	71066	1.40714	
26		1.57372	66021	1.51362 $1.51466$	68557	1.45955 $1.45864$	71110 71154	1.40627 $1.40540$	35 34
27	63584	1.57271	66063	1.51370	68600	1.45773	71198	1.40454	
28	63625	1.57170	66105	1.51275	68642	1.45682	71242	1.40368	32
29 30		1.57069 $1.56969$	66147	1.51179 $1.51084$	68685	1.45592	71285	1.40281	31
$\frac{30}{31}$	63748				68728	$\frac{1.45501}{45410}$	71329		30
32		1.56868 $1.56767$	66230	1.50988 1.50893	68771 68814	1.45410 $1.45320$	71373	1.40109 1.40022	29 28
33	63830	1.56667	66314	1.50797	68857	1.45320 $1.45220$	71461		27
34	63871	$1 \cdot 56566$	66356	1.50702	68900	1.45139	71505	1.39850	26
35	63912	1.56466	66398	1.50607	68942	1.45048	71549		25
36	63953 63994	1.56366 $1.56265$	66440	1.50512 $1.50417$	68985 69028	1.44958 $1.44868$	71593	1.39679 $1.39593$	
38	64035	1.56165	66524	1.50322	69071	1.44778	71681	1.39507	
39	64076	1.56065	66566	1.50228	69114	1.44688	71725	1.39421	
40	64117	1.55966	66608	1.50133	69157	1.44598	71769	1.39336	
41 42	64158 64199	1.55866 $1.55766$	66650	1.50038 $1.49944$	69200 69243	1·44508 1·44418	71813	1.39250 $1.39165$	
43	64240	1.55666	66734	1.49849	69286	1.44329	71901	1.39103 $1.39079$	18 17
44	64281	1.55567	66776	1.49755	69329	1.44239	71946	1.38994	16
45	64322	$\frac{1\cdot 55467}{}$	66818	1.49661	69372	1.44149	71990	1.38909	15
46	64363	1.55368	66860	1.49566	69416	1.44060	72034	1.38824	14
47 48	64404	1.55269 $1.55170$	66902 66944	1.49472 $1.49378$		1.43970 $1.43881$	72078 72122	1.38738 $1.38653$	
49	64487	1.55170 $1.55071$	66986	1.49378	69502 69545	1.43881 $1.43792$	72122	1.38553 $1.38568$	
50	64528	1.54972	67028	1.49190	69588	1.43703	72211	1.38484	10
51	64569	1.54873	67071	1.49097	69631	1.43614	72255	1.38399	9
52 53	64610 64652	1.54774 $1.54675$	67113 67155	1.49003 $1.48909$	69675	1.43525	72299	1.38314	8
54	64693	1.54576	67197	1.48909	69718 69761	$1 \cdot 43436 \\ 1 \cdot 43347$	72344 72388	1.38229 $1.38145$	7
55	64734	1.54478	67239	1.48722	69804	1.43258	72432	1.38060	5
56	64775	1.54379	67282	1.48629	69847	1.43169	72477	1.37976	4
57. 58	64817	1.54281 $1.54183$	67324	1.48536	69891	1.43080	72521	1.37891	3
59	64899	1.54183 $1.54085$	67366 67409	1.48442 $1.48349$	69934 69977	1.42992 $1.42903$	72565 72610	1.37807 $1.37722$	2 1
60	64941	1.53986	67451	1.48256	70021	1.42815	72654	1.37638	0
M	N. Cot.	N. Tan.	N. Cot.		N. Cot	N. Tan.	N. Cot.		M
	57 Degrees.		56 De	grees.			54 Degrees.		1
			4.400		55 Degrees. 54 Degrees.				

N. Tan.   N. Cot.   N. T		1 20 Dagwaga II and D							-	
Table   Tabl				37 Degrees.		38 Degrees.		39 Degrees.		
1   72699		<del></del>								
Page							1			
5									_	
F   72877	3									
6   72921   1.37134   75629   1.32244   78457   1.27458   81316   1.22950   54   77296   1.3666   75675   7.32144   78457   1.27452   81316   1.22977   52   73055   73056   75675   7.31984   78551   1.27306   31441   1.22768   50   11   73104   1.36683   75967   1.31904   7589   1.27330   31461   1.22768   50   11   73144   1.36716   75858   1.31826   76845   1.27153   31510   1.22656   49   73274   73274   73276   73656   75956   7.31745   78692   1.27077   31558   1.22612   48   73273   73234   1.36549   75950   1.31666   78739   1.27001   81606   1.22539   47   73273   1.36836   75964   7.31507   78354   1.26649   73233   1.66833   76042   1.31507   78334   1.26649   73474   73413   1.36217   76134   1.31345   78928   1.22674   48   73457   1.36133   76180   1.31269   7875   1.26698   81800   1.22349   43   73457   1.36133   76180   1.31269   7875   1.26622   81849   1.22164   42   73502   1.36661   76226   1.31190   79022   1.26546   81898   1.22104   41   73592   1.35685   76348   1.30031   79117   1.26395   81899   1.21950   39   22   73637   1.35637   76364   1.30952   79164   1.26319   82044   1.21868   38   37361   1.35719   76410   1.30873   79212   1.26649   81995   1.21950   39   73956   1.35637   76640   1.30873   79212   1.26649   82238   1.21593   39   37   3966   1.35307   76640   1.30830   79494   1.25867   82381   1.21673   82   73816   1.35507   76640   1.30830   79494   1.25697   82385   1.21593   30   73996   1.35637   76640   7.30087   79496   1.25792   32355   1.21833   37   41411   1.34896   76673   1.30087   79496   1.25693   82190   1.21673   83   74086   1.34668   77057   1.30987   79496   1.25693   82381   1.21673   83   74086   1.34846   77057   1.29937   7944   1.25697   82385   1.21383   31   74041   1.34866   77057   1.29937   79496   1.25698   82581   1.21638   83   74407   1.34465   77070   1.29853   79894   1.25516   82855   1.21383   77447   1.34668   77478   1.29937   79586   1.24499   82385   1.21039   74402   1.34495   77458   1.29937   77458   1.29937   77458   1.29337										
7, 72966										
S   73010								1		
10				75721				81364	1.22904	52
11   73144   1.86716   75858   1.31825   78645   1.27163   81510   1.22658   49   12   73189   1.36633   75904   1.31745   78692   1.270071   81505   1.22612   48   1.37323   1.36646   75996   1.31566   78733   1.27001   81605   1.22627   46   15   73323   1.36363   76042   1.31507   78834   1.26694   81703   1.22324   47   17   73413   1.36217   76134   1.31348   78928   1.26698   81800   1.22249   43   18   73457   1.36133   76180   1.31269   78975   1.26622   81849   1.22164   12   12   12   12   12   12   12   1										_
12   73189										
13   73234   1.36549   75950   1.31666   78739   1.22001   81606   1.22539   47   1573233   1.36366   75996   1.31586   78884   1.26849   81703   1.22324   45   1673233   1.36383   76042   1.31507   78834   1.26849   81703   1.22324   45   17   73413   1.36217   76134   1.31345   78928   1.26692   81800   1.22249   42   19   73502   1.36051   76226   1.31190   79022   1.26546   81894   1.22174   42   12   73547   1.35568   76272   1.31110   79070   1.26471   81946   1.22031   40   1.2233   43   43   43   43   43   43   43										
15	13		1.36549	75950	1.31666	78739	1.27001	81606	$1 \cdot 22539$	47
16										
17   73413   1-36217   76134   1-31348   78928   1-266622   81890   1-22476   42   19   73502   1-36051   76226   1-31190   79022   1-26546   81898   1-22176   42   12   12   12   12   12   12   12										
18								1		
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27	25	73771	1.35554	76502	1.30716	79306	1.26093	82190	1.21670	35
28										
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32				,						
33	31	74041	1.35060	76779	1.30244	79591	1.25642	82483	1.21238	29
34	32	i i	1.34978		1.30166			82531		
35										
36										
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39						1 1				
40       74447       1·34323       77196       1·29541       80020       1·24969       82923       1·20593       20         41       74492       1·34242       77242       1·29463       80067       1·24895       82972       1·20522       19         42       74538       1·34160       77289       1·29385       80115       1·24820       83022       1·20451       18         43       74583       1·34079       77335       1·29307       80163       1·24746       83071       1·20379       17         44       74628       1·33998       77382       1·29229       80211       1·24672       83120       1·20308       16         45       74674       1·33916       77428       1·29152       80258       1·24597       83169       1·20237       15         46       74719       1·33835       77475       1·29074       80306       1·24523       83218       1·20166       14         47       74764       1·33754       77568       1·28919       80402       1·24375       83317       1·20024       12         49       74855       1·33592       77615       1·28842       80450       1·24301       8366       <										
41       74492       1 · 34242       77242       1 · 29463       80067       1 · 24895       82972       1 · 20522       19         42       74538       1 · 34160       77289       1 · 29385       80115       1 · 24820       83022       1 · 20451       18         43       74583       1 · 34079       77335       1 · 29307       80163       1 · 24746       83071       1 · 20379       17         44       74628       1 · 33916       77428       1 · 29152       80258       1 · 24597       83169       1 · 20379       15         46       74719       1 · 33835       77475       1 · 29074       80306       1 · 24523       83218       1 · 20166       14         47       74764       1 · 33754       77521       1 · 28997       80354       1 · 24449       83268       1 · 20024       12         48       74810       1 · 33673       77568       1 · 28919       80402       1 · 24375       83317       1 · 20024       12         49       74855       1 · 33592       77615       1 · 28764       80498       1 · 2427       83415       1 · 19882       10         51       74946       1 · 33430       77708       1 · 28687										
42       74538       1·34160       77289       1·29385       80115       1·24820       83022       1·20451       18         43       74583       1·34079       77335       1·29307       80163       1·24746       83071       1·20379       17         44       74628       1·33998       77382       1·29229       80211       1·24672       83120       1·20308       16         45       74674       1·33916       77475       1·29074       80306       1·24523       83169       1·20237       15         46       74719       1·33835       77475       1·29074       80306       1·24523       83218       1·20166       14         47       74764       1·33754       77568       1·28919       80402       1·24375       83317       1·20024       12         49       74855       1·33592       77615       1·28842       80492       1·24375       83317       1·20024       12         50       74900       1·33511       77661       1·28764       80498       1·24227       83415       1·19882       10         51       74946       1·33349       77754       1·28610       80594       1·24079       83514						1				
44       74628       1 · 33998       77382       1 · 29229       80211       1 · 24672       83120       1 · 20308       16         45       74674       1 · 33916       77428       1 · 29152       80258       1 · 24523       83169       1 · 20237       15         46       74719       1 · 33835       77475       1 · 29074       80306       1 · 24523       83218       1 · 20166       14         47       74764       1 · 33754       77568       1 · 28919       80402       1 · 24375       83317       1 · 20024       12         49       74855       1 · 33592       77615       1 · 28842       80450       1 · 24301       83366       1 · 19953       11         50       74900       1 · 33511       77661       1 · 28764       80498       1 · 24227       83415       1 · 19882       10         51       74946       1 · 33430       77708       1 · 28687       80546       1 · 24153       83465       1 · 19811       9         52       74991       1 · 33349       77754       1 · 28610       80594       1 · 24079       83514       1 · 19740       8         53       75037       1 · 33268       77801       1 · 28329	42	74538	1.34160	77289		80115	1.24820	83022	1.20451	18
45         74674         1·33916         77428         1·29152         80258         1·24597         83169         1·20237         15           46         74719         1·33835         77475         1·29074         80306         1·24523         83218         1·20166         14           47         74764         1·33754         77521         1·28997         80354         1·24449         83268         1·20095         13           48         74810         1·33673         77568         1·28919         80402         1·24375         83317         1·20024         12           49         74855         1·33592         77615         1·28842         80450         1·24301         83366         1·19953         11           50         74900         1·33511         77661         1·28764         80498         1·24227         83415         1·19882         10           51         74946         1·33349         77754         1·28610         80594         1·24079         83514         1·19740         8           53         75037         1·33268         77801         1·28533         80642         1·24079         83514         1·19740         8           54         <										
46         74719         1 · 33835         77475         1 · 29074         80306         1 · 24523         83218         1 · 20166         14           47         74764         1 · 33754         77521         1 · 28997         80354         1 · 24449         83268         1 · 20095         13           48         74810         1 · 33673         77568         1 · 28919         80402         1 · 24375         83317         1 · 20024         12           49         74855         1 · 33592         77615         1 · 28764         80498         1 · 24301         83366         1 · 19953         11           50         74900         1 · 33511         77661         1 · 28764         80498         1 · 24227         83415         1 · 19882         10           51         74946         1 · 33430         77708         1 · 28687         80546         1 · 24153         83465         1 · 19811         9           52         74991         1 · 33268         77801         1 · 28533         80642         1 · 24079         83514         1 · 19740         8           53         75082         1 · 33107         77895         1 · 28379         80738         1 · 23931         83613         1 · 19599	_	1								
47         74764         1·33754         77521         1·28997         80354         1·24449         83268         1·20095         13           48         74810         1·33673         77568         1·28919         80402         1·24375         83317         1·20024         12           49         74855         1·33592         77615         1·28842         80450         1·24301         83366         1·19953         11           50         74900         1·33511         77661         1·28764         80498         1·24227         83415         1·19882         10           51         74946         1·33430         77708         1·28687         80546         1·24153         83465         1·19811         9           52         74991         1·33349         77754         1·28610         80594         1·24079         83514         1·19740         8           53         75037         1·33268         77801         1·28533         80642         1·24005         83564         1·19669         7           54         75082         1·33187         77895         1·28379         80738         1·23931         83613         1·19599         6           55 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>										
48       74810       1 · 33673       77568       1 · 28919       80402       1 · 24375       83317       1 · 20024       12         49       74855       1 · 33592       77615       1 · 28842       80450       1 · 24301       83366       1 · 19953       11         50       74900       1 · 33511       77661       1 · 28764       80498       1 · 24227       83415       1 · 19882       10         51       74946       1 · 33430       77708       1 · 28670       80546       1 · 24153       83465       1 · 19811       9         52       74991       1 · 33349       77754       1 · 28610       80594       1 · 24079       83514       1 · 19740       8         53       75037       1 · 33268       77801       1 · 28533       80642       1 · 24005       83564       1 · 19740       8         54       75082       1 · 33187       77848       1 · 28379       80690       1 · 23931       83613       1 · 19599       6         55       75128       1 · 33026       77941       1 · 28302       80786       1 · 23784       83712       1 · 19457       4         57       75219       1 · 32865       77035       1 · 28148 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>,</td></t<>										,
50         74900         1·33511         77661         1·28764         80498         1·24227         83415         1·19882         10           51         74946         1·33430         77708         1·28687         80546         1·24153         83465         1·19811         9           52         74991         1·33349         77754         1·28610         80594         1·24079         83514         1·19740         8           53         75037         1·33268         77801         1·28533         80642         1·24005         83564         1·19669         7           54         75082         1·33187         77848         1·28456         80690         1·23931         83613         1·19599         6           55         75128         1·33107         77895         1·28379         80738         1·23858         83662         1·19528         5           56         75174         1·32946         77988         1·28225         80834         1·23710         83761         1·19387         3           58         75264         1·32865         77035         1·28148         80882         1·23637         83811         1·19316         2           59         75	48	74810	1.33673		1.28919	80402	1.24375	83317	1.20024	12
51       74946       1 · 33430       77708       1 · 28687       80546       1 · 24153       83465       1 · 19811       9         52       74991       1 · 33349       77754       1 · 28610       80594       1 · 24079       83514       1 · 19740       8         53       75037       1 · 33268       77801       1 · 28533       80642       1 · 24005       83564       1 · 19669       7         54       75082       1 · 33187       77848       1 · 28379       80690       1 · 23931       83613       1 · 19599       6         55       75128       1 · 33107       77895       1 · 28379       80738       1 · 23858       83662       1 · 19528       5         56       75174       1 · 33026       77941       1 · 28302       80786       1 · 23784       83712       1 · 19457       4         57       75219       1 · 32946       77988       1 · 28225       80834       1 · 23710       63761       1 · 19387       3         58       75264       1 · 32865       77035       1 · 28148       80882       1 · 23637       83811       1 · 19316       2         59       75310       1 · 32785       77082       1 · 28071       8										
52         74991         1.33349         77754         1.28610         80594         1.24079         83514         1.19740         8           53         75037         1.33268         77801         1.28533         80642         1.24005         83564         1.19669         7           54         75082         1.33187         77848         1.28456         80690         1.23931         83613         1.19599         6           55         75128         1.33107         77895         1.28379         80738         1.23858         83662         1.19528         5           56         75174         1.33026         77941         1.28302         80786         1.23784         83712         1.19457         4           57         75219         1.32946         77988         1.28225         80834         1.23710         63761         1.19387         3           58         75264         1.32865         77035         1.28148         80882         1.23637         83811         1.19316         2           59         75310         1.32785         77082         1.28071         80930         1.23563         83860         1.19246         1           60         753										
53         75037         1 · 33268         77801         1 · 28533         80642         1 · 24005         83564         1 · 19669         7           54         75082         1 · 33187         77848         1 · 28456         80690         1 · 23931         83613         1 · 19599         6           55         75128         1 · 33107         77895         1 · 28379         80738         1 · 23858         83662         1 · 19528         5           56         75174         1 · 33026         77941         1 · 28302         80786         1 · 23784         83712         1 · 19457         4           57         75219         1 · 32946         77988         1 · 28225         80834         1 · 23710         83761         1 · 19387         3           58         75264         1 · 32865         77035         1 · 28148         80882         1 · 23637         83811         1 · 19316         2           59         75310         1 · 32785         77082         1 · 28071         80930         1 · 23563         83860         1 · 19175         0           M         N. Cot.         N. Tan.         N. Cot.         N. Tan.         N. Cot.         N. Tan.         N. Cot.         N. Tan. <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>										
54         75082         1·33187         77848         1·28456         80690         1·23931         83613         1·19599         6           55         75128         1·33107         77895         1·28379         80738         1·23858         83662         1·19528         5           56         75174         1·33026         77941         1·28302         80786         1·23784         83712         1·19457         4           57         75219         1·32946         77988         1·28225         80834         1·23710         63761         1·19387         3           58         75264         1·32865         77035         1·28148         80882         1·23637         83811         1·19316         2           59         75310         1·32785         77082         1·28071         80930         1·23563         83860         1·19246         1           60         75355         1·32704         77129         1·27994         80978         1·23490         83910         1·19175         0           M         N. Cot.         N. Tan.         N. C		75037	1.33268		1.28533				1.19669	7
56         75174         1 · 33026         77941         1 · 28302         80786         1 · 23784         83712         1 · 19457         4           57         75219         1 · 32946         77988         1 · 28225         80834         1 · 23710         63761         1 · 19387         3           58         75264         1 · 32865         77035         1 · 28148         80882         1 · 23637         83811         1 · 19316         2           59         75310         1 · 32785         77082         1 · 28071         80930         1 · 23563         83860         1 · 19246         1           60         75355         1 · 32704         77129         1 · 27994         80978         1 · 23490         83910         1 · 19175         0           M         N. Cot.         N. Tan.         N. Cot.         N. Tan.         N. Cot.         N. Tan.         N. Cot.         N. Tan.         N. Tan.								83613		
57       75219       1 · 32946       77988       1 · 28225       80834       1 · 23710       63761       1 · 19387       3         58       75264       1 · 32865       77035       1 · 28148       80882       1 · 23637       83811       1 · 19316       2         59       75310       1 · 32785       77082       1 · 28071       80930       1 · 23563       83860       1 · 19246       1         60       75355       1 · 32704       77129       1 · 27994       80978       1 · 23490       83910       1 · 19175       0         M       N. Cot.       N. Tan.       N. Cot.       N. Tan.       N. Cot.       N. Tan.       N. Cot.       N. Tan.       M					1					
58     75264     1 · 32865     77035     1 · 28148     80882     1 · 23637     83811     1 · 19316     2       59     75310     1 · 32785     77082     1 · 28071     80930     1 · 23563     83860     1 · 19246     1       60     75355     1 · 32704     77129     1 · 27994     80978     1 · 23490     83910     1 · 19175     0       M     N. Cot.     N. Tan.     N. Cot.     N. Tan.     N. Cot.     N. Tan.     N. Cot.     N. Tan.						1				
59       75310       1 · 32785       77082       1 · 28071       80930       1 · 23563       83860       1 · 19246       1         M       N. Cot.       N. Tan.       N. Tan.       N. Tan.       N. Cot.       N. Tan.       N. Tan.       N. Cot.       N. Tan.	_	75264	1.32865	11		1				2
M N. Cot. N. Tan. N. Cot. N. Tan. N. Cot. N. Tan. M. Cot. N. Tan. M.	59	75310	1.32785	77082	1.28071	80930	1.23563	83860	1.19246	1
		-	(4)	11				11		0
53 Degrees.   52 Degrees.   51 Degrees.   50 Degrees.										M
	7	1 53 D	egrees.	1 52 D	egrees.	51 D	egrees.	50 D	egrees.	

2	Amon National Control of the 18th									
ı		40 D	egrees.	41 D	egrees.	42 Degrees.		43 Degrees.		
1	M	N. Tan.	N. Cot.	N. Tan.	N. Cot.	N. Tan.	N. Cot	N. Tan.	N. Cot.	M
I	0	83910	1.19175	86929	1.15037	90040	1.11061	93252	1.07237	60
Ī	1	83960 84009	$1 \cdot 19105$ $1 \cdot 19035$	86980 87031	1.14969 $1.14902$	90093	$1 \cdot 10996$ $1 \cdot 10931$	93306	1.07174	
i	2 3	84059	1.19035 $1.18964$	87082	1.14902 $1.14834$		1.10931 $1.10867$	93360	1.07112 $1.07049$	
a a	1 4	84108		87133	1.14767	90251	1.10802	93469	1.06987	
1	5	84158	1.18824	87184	1.14699	90304	1.10737	93524	1.06925	
	6	84208	1.18754	87236	1.14632		1.10672	93578	1.06862	
1	7 8	84258 84307	1·18684 1·18614	87287 87338	1.14565 $1.14498$	90410	1.10607 $1.10543$	93633 93688	1.06800	
H	9	84357	1.18544	87389	1.14430	90465	1.10343	93742	1.06738 $1.06676$	
1	10	84407	1.18474	87441	1.14363	90569	1.10414	93797	1.06613	
1	11	84457	1.18404	87492	1.14296	90621	1.10349	93852	1.06551	49
S of	12	84507	1.18334	87543	1.14229	90674	1.10285	93906	1.06489	
ALC: N	13 14	84556 84606	1.18264 1.18194	87595	1.14162 $1.14095$	90727	$1 \cdot 10220$ $1 \cdot 10156$	93961 94016	1.06427 $1.06365$	
H	15	84656	1.18134 $1.18125$	87698	1.14038	90834	1.10130	94071	1.06303	
-	16	84706	1.18055	87749	1.13961	90887	$\frac{1.10027}{1.10027}$	94125	1.06241	
1	17	84756	1.17986	87801	1.13501 $1.13894$	90940	1.10027 $1.09963$	94125	1.06241	
1	18	84806	1.17916	87852	1.13828	90993	1.09899	94235	1.06117	2 1
-	19	84856	1.17846	.87904	1 · 13761	91046	1.09834	\$ F (	1.06056	41
ı	20	84906	1.17777	87955	1.13694	91099	1.09770	94345	1.05994	
	21 22	84956 85006	1.17708 1.17638	88007	1.13627 $1.13561$	91153 91206	1.09706 $1.09642$	94400	1.05932 $1.05870$	
1	23	85057	1.17569	88110	1.13494	91259	1.09578	94510	1.05870	
1	24	85107	1.17500	88162	1.13428	91313	1.09514	94565	1.05747	36
i d	25	85157	$1 \cdot 17430$	88214	1.13361	91366	1.09450	94620	1.05685	
ă 1	26	85207	1.17361	88265	1.13295	91419	1.09386	94676	1.05624	
4	27 28	85257 85307	$1 \cdot 17292$ $1 \cdot 17223$	88317 88369	$1 \cdot 13228$ $1 \cdot 13162$	91473 91526	1.09322 $1.09258$	94731	1.05562 $1.05501$	33 32
1.5	29	85358	1.17154	88421	1.13096	91580	1.09195	94841	1.05439	
Total Section	30	85408	1.17085	88473	1.13029	91633	1.09131	94896	1.05378	
4	31	85458	1.17016	88524	1.12963	91687	1.09067	94952	1.05317	29
1	32	85509	1.16947	88576	1.12897	91740	1.09003		1.05255	28
ŧ	33	85559	1.16878		1.12831	91794	1.08940	95062	1.05194	
i.	34 35	85609 85660	1.16809 $1.16741$	88680 88732	$1 \cdot 12765$ $1 \cdot 12699$	91847 91901	1.08876 $1.08813$	95118 95173	1.05133 $1.05072$	2
i.	36	85710	1.16741 $1.16672$	88784	$1 \cdot 12633$		1.08749	95229	1.05072 $1.05010$	
2	37	85761	1.16603	88836	1.12567	92008	1.08686	95284	1.04949	
	38	85811	1.16535	88888	1.12501	92062	1.08622	95340	1.04888	
1	39	85862	1.16466	88940	1.12435	92116	1.08559	95395	1.04827	
Ì	40 41	85912 85963	$1 \cdot 16398$ $1 \cdot 16329$	88992 89045	$1 \cdot 12369$ $1 \cdot 12303$	92170	1.08496 1.08432	95451 95506	1.04766 $1.04705$	
ı	42	86014	$1 \cdot 16261$	89097	1.12238	92277	1.08369	95562	1.04644	
100	43	86064	1.16192	89149	1.12172	92331	1.08306	95618	1.04583	17
	44	86115	1.16124	89201	1.12106	92385	1.08243	95673	1.04522	
-	45	86166	1.16056	89253	1.12041	92439	1.08179	95729	1.04461	15
	46	86216	1.15987	89306	1.11975	92493	1.08116	95785	1.04401	
	47	86267 86318	1.15919 $1.15851$	89358 89410	1.11909	92547	1.08053 $1.07990$	95841	1.04340 $1.04279$	
4	49	86368	1.15051				1.07990 $1.07927$	96952	1.04279 $1.04218$	
1	50	86419	1.15715	89515	1.11713	92709	,1.07864	96008	1.04158	
	51	86470	1.15647	3			1.07801	96064	1.04097	9
	52	86521	1.15579	89620	1·11582 1·11517	1 - 1	1.07738 1.07676	96120	1.04036 $1.03976$	8 7
1	53 54	86572 86623	1·15511 1·15443	89672 89725			1.07678	96176 96232	1.03976 $1.03915$	6
į	55	86674		89777		92980	1.07550	96288	1.03315 $1.03855$	5
	56	86725	1.15308	89830	1.11321	93034	1.07487	96344	1.03794	4
1	57	86776		89883	1.11256		1.07425	96400	1.03734	
1	<b>58 59</b>	86827	1·15172 1·15104	89935 89988	$1 \cdot 11191$ $1 \cdot 11126$	93143	1.07362 $1.07299$	96457 96513	1.03674 $1.03613$	2
I	60	86929	1.15104	90040	1.11061	93197	1.07299	96569	1.03553	0
Į	M	N. Cot.		N. Cot.	N. Tan.		N. Tan.	N. Cot.		M
	49 Degrees.				egrees.		egrees.		egrees.	
		. 10 1)	081000.	10 10	5 60 6 4 6 4 6 4 6 4 6 4 6 4 6 4 6 4 6 4		25 - 200.	- PACE - 1	S. C. C. C.	'

	44 D	egrees.					
M	N. Tan.	N. Cot.	M	M	N. Tan.	N. Cot.	M
0	96569	1.03553	60	31	98327	1.01702	29
1	96625	1.03493	59	32	98384	1.01642	28
2	96681	1.03433	58	33	98441	1.01583	27
3	96738	1.03372	57	34	98499	1.01524	26
4	96794	1.03312	56	35	98556	1.01465	25
5	96850	1.03252	55	36	98613	1.01406	24
6	96907	1.03192	$54 \cdot$	37	98671	1.01347	23
7	96963	1.03132	53	38	98728	1.01288	22
8	97020	1.03072	52	39	98786	1.01229	21
9	97076		51	40	98843	1.01170	20
10	97133	1.02952	50	41	98901	1.01112	19
11	97189	1.02892	49	42	98958	1.01053	18
12	97246	1.02832	48	43	99016	1.00994	17
13	97302	1.02772	47	44	99073	1.00935	16
14	97359	1.02713	46	45	99131	1.00876	15
15	97416	1.02653	45	46	99189	1.00818	14
16	97472	1.02593	44	47	99247	1.00759	13
17	97529	1.02533	43	48	99304	1.00701	12
18	97586	1.02474	42	49	99362	1.00642	11
19	97643	1.02414	41	50	99420	1.00583	10
20	97700	1.02355	40	51	99478	1.00525	9
21	97756	1.02295	39	52	99536	1.00467	8
22	97813	1.02236	38	53	99594	1.00408	7
<b>2</b> 3	97870	1.02176	37	54	99652	1.00350	6
24	97927	1.02117	36	55	99710	1.00291	5
25	97984	1.02057	35	56	99768	1.00233	4
26	98041	1.01998	34	57	99826	1.00175	3
27	98098	1.01939	33	58	99884	1.00116	2
<b>2</b> 8	98155	1.01879	32	59	99942	1.00058	1
29	98213	1.01820	31	60	10000	1.00000	0
30	98270	1.01761	30				1
M	N. Cot.	N. Tan.	M	M	N. Cot.	N. Tan.	M
	45 D	egrees.			45 D	egrees.	



